



1982 OFFSHORE GEOTECHNICAL
SITE INVESTIGATION
KUGDJUK SITE
BEAUFORT SEA

Report to
GULF CANADA
RESOURCES INC.

Calgary, Alberta

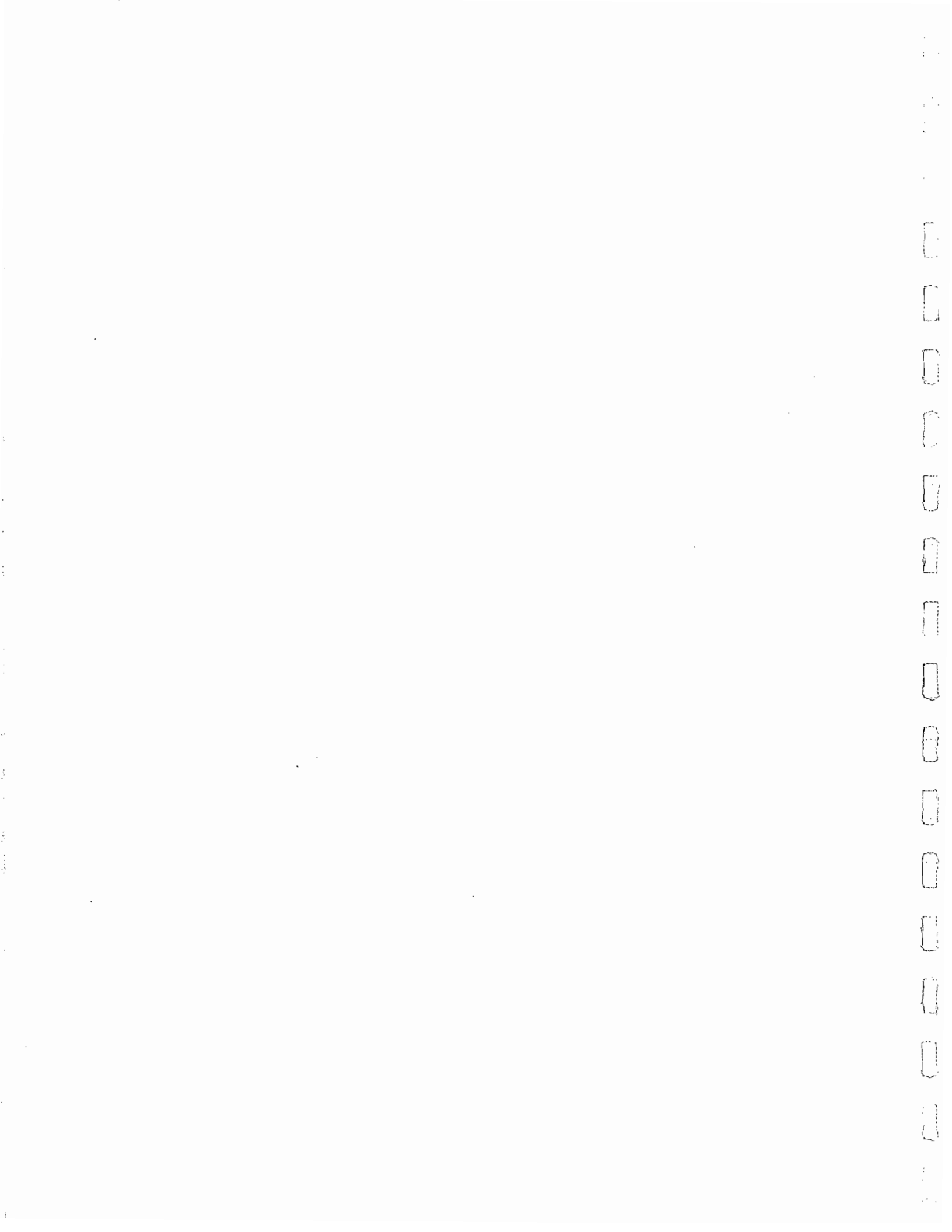
by

EBA Engineering Consultants Ltd.



and

 **McClelland engineers, inc.**



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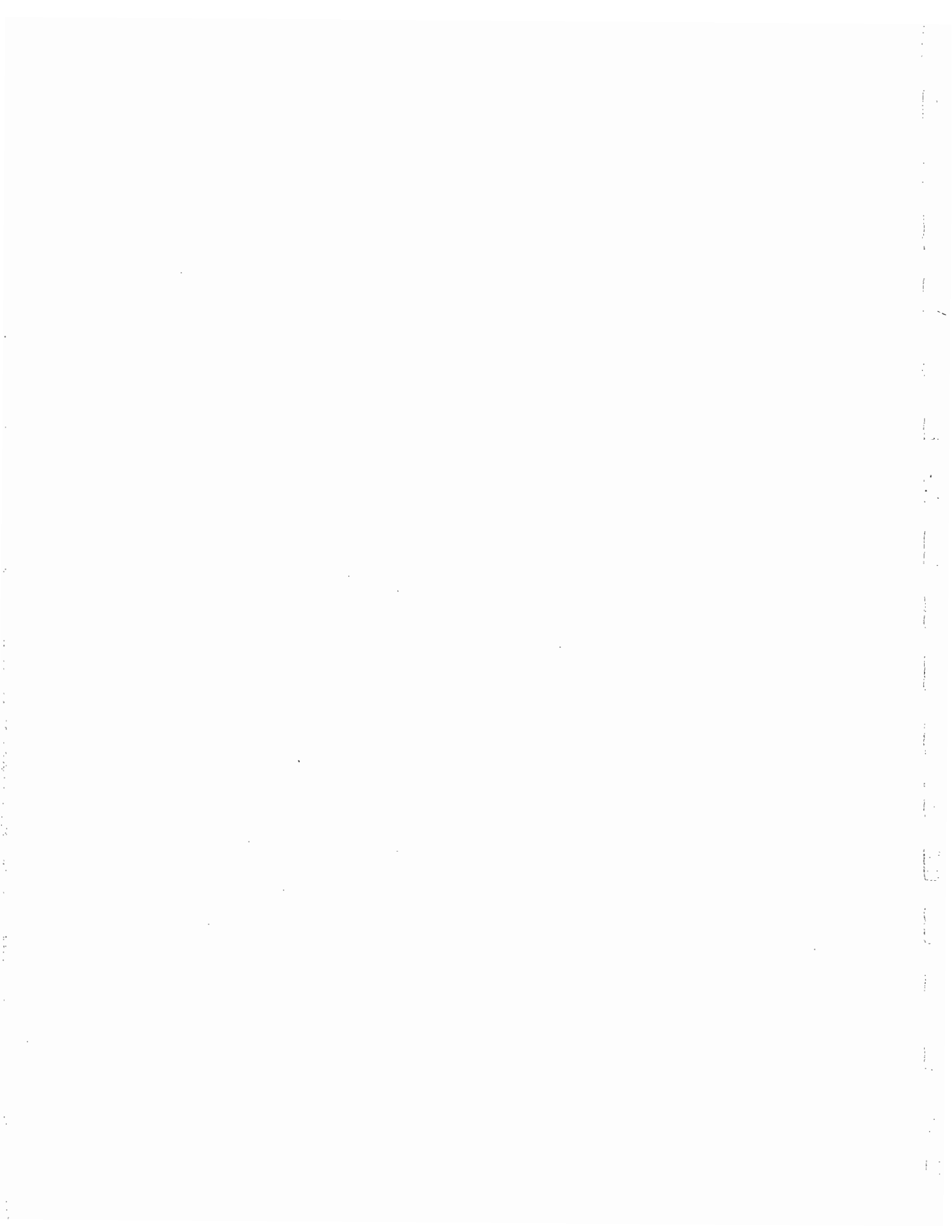
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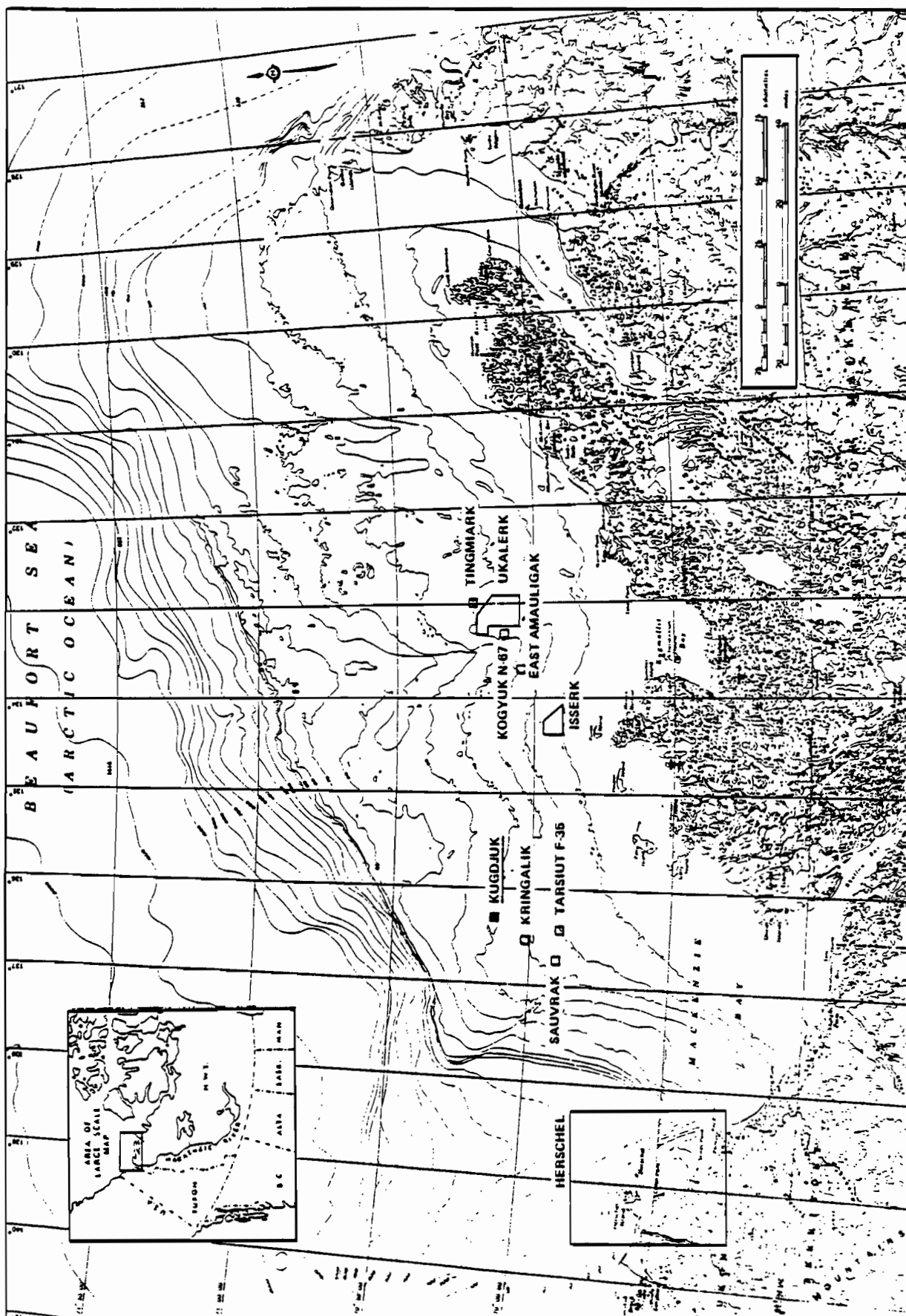
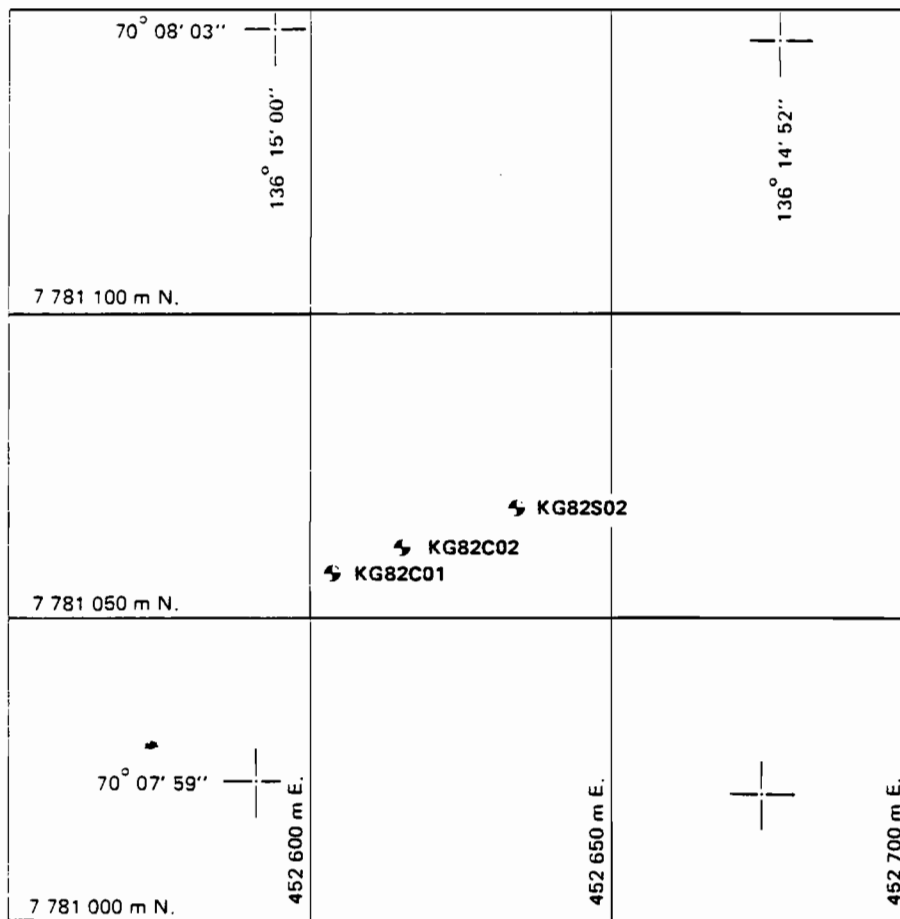


FIGURE 1 GENERAL LOCATION MAP



*Note: Locations provided by
Canadian Engineering Surveys Co. Ltd.*

FIGURE 2 BOREHOLE LOCATION MAP
KUGDJUK AREA

TABLE 1 SUMMARY OF TEST LOCATIONS

TEST	NO.	LOCATION			GEO	DEPTH OF PENETRATION (m)	DATE
		UTM	m.E	LAT.			
		m.N (UTM ZONE 8)		°N	°W		(yy-mm-dd)
Cone Test	KG82C01	7 781 060	452 605	70°08'	136°15'	34.0	82-08-06
Cone Test	KG82C02	7 781 060	452 615	70°08'	136°15'	13.0	82-08-06
Sampled Borehole with supplementary Remote Vane tests	KG82S02	7 781 070	452 635	70°08'	136°15'	52.8	82-08-07

Note: 1. All positions supplied by CES Ltd.

2. KG82 denotes a borehole/probehole at the Kudgdjuk site drilled/tested in 1982. "S" refers to "sampled", "R" refers to "Remote Vane", "C" refer to "static cone", and "P" refers to "pressurimeter". The number following the letter designation is the borehole/probehole number.



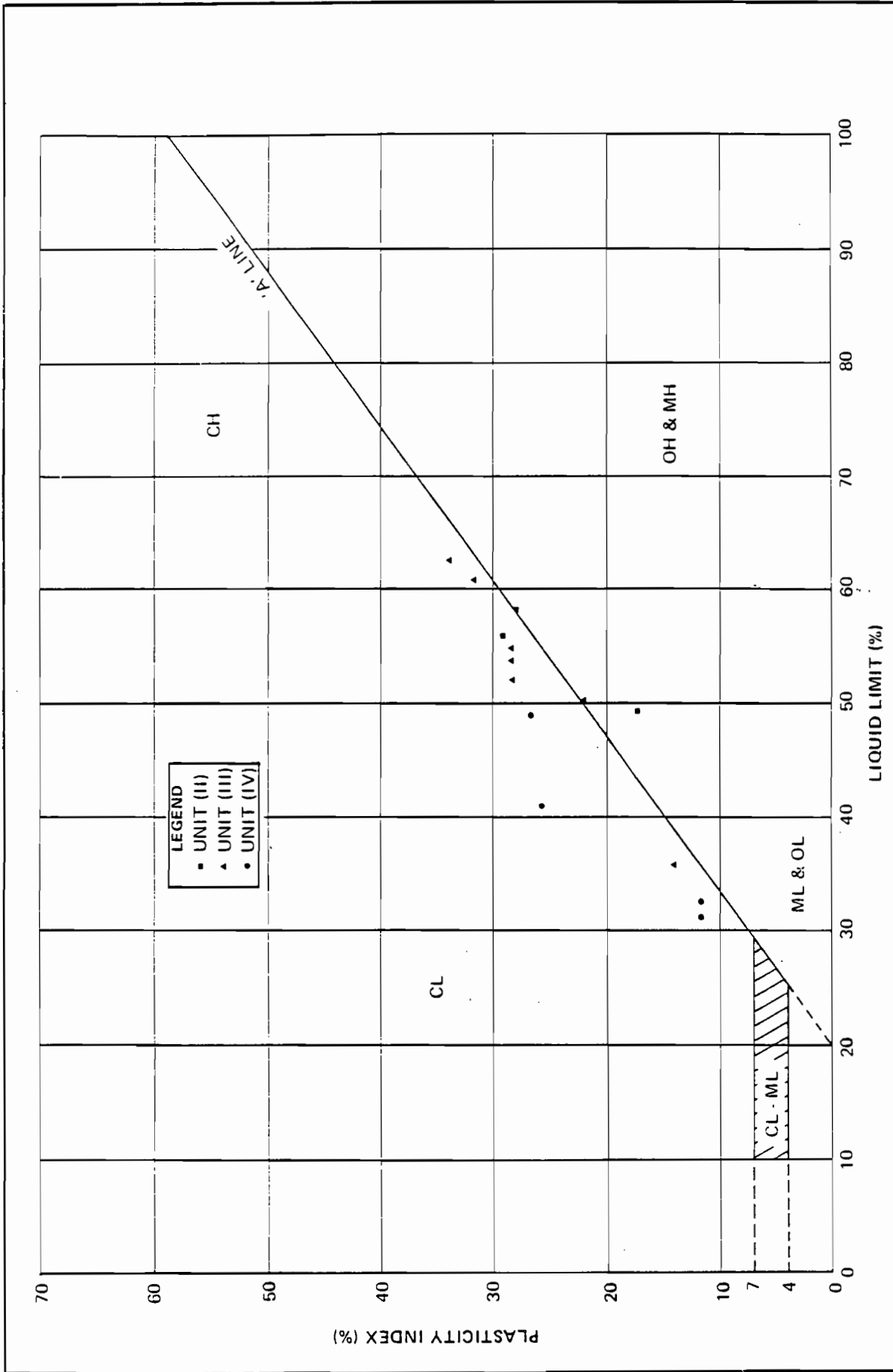


FIGURE 3 PLASTICITY CHART

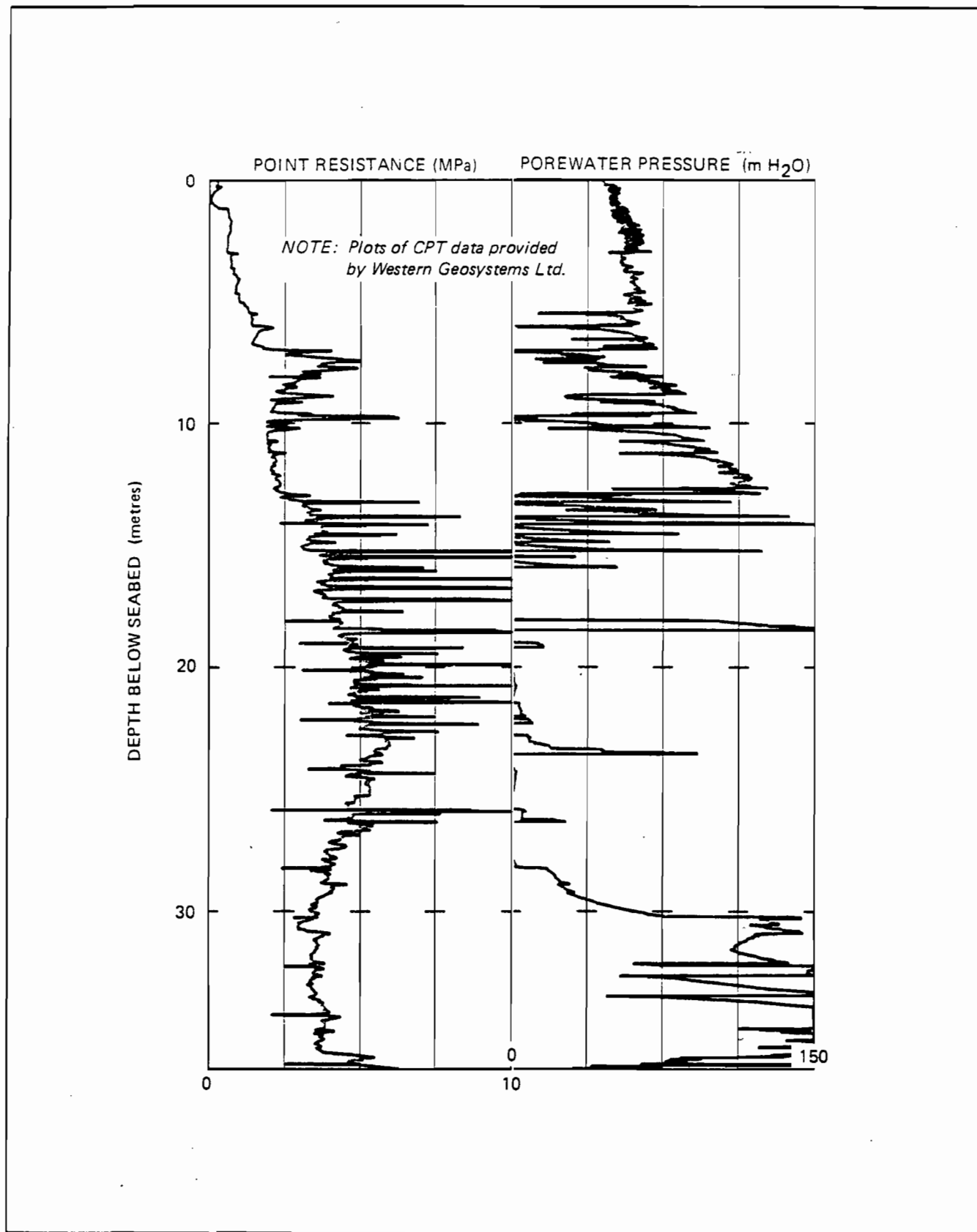


FIGURE 4 CONE PENETRATION TEST PROFILE
TEST KG82C01 - KUGDJUK

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APPENDIX A

Borehole Logs

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SYSTEM INTERNATIONAL UNITS

QUANTITY	NAME	SYMBOL	EXPRESSED IN TERMS OF OTHER SI UNITS	EXPRESSED IN TERMS OF BASE AND SUPPLEMENTARY UNITS
SI UNITS				
length	metre	m		
mass	kilogram	kg		
time	second	s		
electric current	ampere	A		
thermodynamic temperature	kelvin	K		
amount of substance	mole	mol		
luminous intensity	candela	cd		
SI SUPPLEMENTARY UNITS				
plane angle	radian	rad		
solid angle	steradian	sr		
EXAMPLES OF SI DERIVED UNITS WITH SPECIAL NAMES				
frequency	hertz	Hz	1/s	s ⁻¹
force	newton	N	m · kg/s ²	m · kg · s ⁻²
pressure, stress	pascal	Pa	N/m ²	m ⁻¹ · kg · s ⁻²
energy, work, quantity of heat	joule	J	N · m	m ² · kg · s ⁻²
power, radiant flux	watt	W	J/s	m ² · kg · s ⁻³
EXAMPLES OF SI DERIVED UNITS WITHOUT SPECIAL NAMES				
velocity - linear	metre per second		m/s	m · s ⁻¹
- angular	(radian per second)		rad/s	rad · s ⁻¹
acceleration - linear	(metre per second) per second		m/s ²	m · s ⁻²
- angular	(radian per second) per second		rad/s ²	rad · s ⁻²
concentration (of amount of substance)	mole per cubic metre		mol/m ³	mol · m ⁻³
dynamic viscosity	pascal second		Pa · s	m ⁻¹ · kg · s ⁻¹
moment of force	newton metre		N · m	m ² · kg · s ⁻²
surface tension	newton per metre		N/m	kg · s ⁻²
heat flux density, irradiance	watt per square metre		W/m ²	kg · s ⁻³
heat capacity, entropy	joule per kelvin		J/K	m ² · s ⁻² · K ⁻¹
specific heat capacity, specific entropy	joule per kilogram kelvin		J/(kg · K)	m ² · s ⁻² · K ⁻¹
specific energy	joule per kilogram		J/kg	m ² · s ⁻²
thermal conductivity	watt per metre kelvin		W/(m · K)	m · kg · s ⁻³ · K ⁻¹

OTHER UNITS PERMITTED FOR USE WITH SI

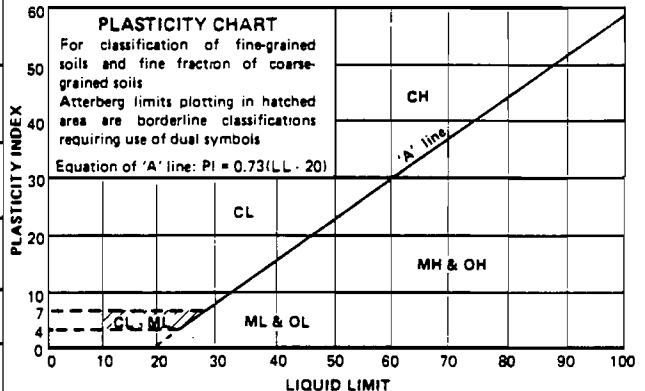
QUANTITY	NAME	SYMBOL	DEFINITION
time	minute	min	1 min = 60 s
	hour	h	1 h = 3,600 s
	day	d	1 d = 86,400 s
	year	a	
plane angle	degree	°	1° = (π/180) rad
	minute	'	1' = (π/10,800) rad
	second	"	1" = (π/648,000) rad
area	hectare	ha	1 ha = 10,000 m ²
volume	litre	L	1,000 L = 1 m ³
temperature	degree Celsius	°C	0° C = 273.15° K temperature interval 1 C° = 1 K°
mass	tonne	t	1 t = 1,000 kg = 1 Mg

MULTIPLYING FACTOR	PREFIX	SYMBOL	MULTIPLYING FACTOR	PREFIX	SYMBOL
1,000,000,000,000,000,000 = 10 ¹⁸	exa	E	0.1 = 10 ⁻¹	deci*	d
1,000,000,000,000,000 = 10 ¹⁵	peta	P	0.01 = 10 ⁻²	centi*	c
1,000,000,000,000 = 10 ¹²	tetra	T	0.001 = 10 ⁻³	milli	m
1,000,000,000 = 10 ⁹	giga	G	0.000,001 = 10 ⁻⁶	micro	μ
1,000,000 = 10 ⁶	mega	M	0.000,000,001 = 10 ⁻⁹	nano	n
1,000 = 10 ³	kilo	k	0.000,000,000,001 = 10 ⁻¹²	pico	p
100 = 10 ²	hecto*	h	0.000,000,000,000,001 = 10 ⁻¹⁵	femto	f
10 = 10 ¹	deca*	da	0.000,000,000,000,000,001 = 10 ⁻¹⁸	atto	a

* to be avoided where possible

UNIFIED SOIL CLASSIFICATION†

MAJOR DIVISIONS		GROUP SYMBOLS	TYPICAL NAMES	CLASSIFICATION CRITERIA		
COARSE-GRAINED SOILS <small>More than 50% retained on No. 200 sieve*</small>	GRAVELS <small>50% or more of coarse fraction retained on No. 4 sieve</small>	CLEAN GRAVELS	GW Well-graded gravels and gravel-sand mixtures, little or no fines	$C_u = \frac{D_{60}}{D_{10}}$ Greater than 4 $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Between 1 and 3 Not meeting both criteria for GW Atterberg limits plot below 'A' line or plasticity index less than 4 Atterberg limits plot above 'A' line and plasticity index greater than 7 Atterberg limits plotting in hatched area are borderline classifications requiring use of dual symbols		
		GRAVELS WITH FINES	GP Poorly-graded gravels and gravel-sand mixtures, little or no fines			
		GRAVELS WITH FINES	GM Silty gravels, gravel-sand-silt mixtures			
		GRAVELS WITH FINES	GC Clayey gravels, gravel-sand clay mixtures			
	SANDS <small>More than 50% of coarse fraction passes No. 4 sieve</small>	CLEAN SANDS	SW Well-graded sands and gravelly sands, little or no fines	Classification on basis of percentage of fines Less than 5% pass No. 200 sieve More than 12% pass No. 200 sieve 5% to 12% pass No. 200 sieve GW, GP, SW, SP GM, GC, SM, SC Borderline classification requiring use of dual symbols		
			CLEAN SANDS		SP Poorly-graded sands and gravelly sands, little or no fines	
		SANDS WITH FINES	SM Silty sands, sand-silt mixtures		$C_u = \frac{D_{60}}{D_{10}}$ Greater than 6 $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}}$ Between 1 and 3 Not meeting both criteria for SW Atterberg limits plot below 'A' line or plasticity index less than 4 Atterberg limits plotting in hatched area are borderline classifications requiring use of dual symbols	
			SC Clayey sands, sand-clay mixtures			
		FINE-GRAINED SOILS <small>50% or more passes No. 200 sieve*</small>	SILTS AND CLAYS <small>Liquid limit 50% or less</small>		ML Inorganic silts, very fine sands, rock flour, silty or clayey fine sands	PLASTICITY CHART For classification of fine-grained soils and fine fraction of coarse-grained soils Atterberg limits plotting in hatched area are borderline classifications requiring use of dual symbols Equation of 'A' line: $PI = 0.73(LL - 20)$
					CL Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays	
OL Organic silts and organic silty clays of low plasticity						
SILTS AND CLAYS <small>Liquid limit greater than 50%</small>	MH Inorganic silts, micaceous or diatomaceous fine sands or silts, elastic silts		*Based on the material passing the 3 in. (75 mm) sieve †ASTM Designation D 2487, for identification procedure see D 2488			
	CH Inorganic silts of high plasticity, fat clays					
	OH Organic clays of medium to high plasticity					
	PT Peat, muck and other highly organic soils					



GROUND ICE DESCRIPTION

ICE NOT VISIBLE				VISIBLE ICE LESS THAN 50% BY VOLUME			
GROUP SYMBOLS	SYMBOLS	SUBGROUP DESCRIPTION		GROUP SYMBOLS	SYMBOLS	SUBGROUP DESCRIPTION	
N	Nf	Poorly-bonded or friable		V	Vx	Individual ice crystals or inclusions	
	Nbn	No excess ice, well-bonded			Vc	Ice coatings on particles	
	Nbe	Excess ice, well-bonded			Vr	Random or irregularly oriented ice formations	
					Vs	Stratified or distinctly oriented ice formations	
				VISIBLE ICE GREATER THAN 50% BY VOLUME			
ICE	ICE + Soil Type	Ice with soil inclusions					
	ICE	Ice without soil inclusions (greater than 25 mm (1 in.) thick)					

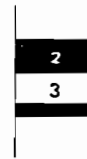
- NOTE:**
- Dual symbols are used to indicate borderline or mixed ice classifications
 - Visual estimates of ice contents indicated on borehole logs \pm 5%
 - This system of ground ice description has been modified from NRC Technical Memo 79, Guide to the Field Description of Permafrost for Engineering Purposes

LEGEND
 Soil Ice

SYMBOLS AND ABBREVIATIONS USED ON BOREHOLE LOGS

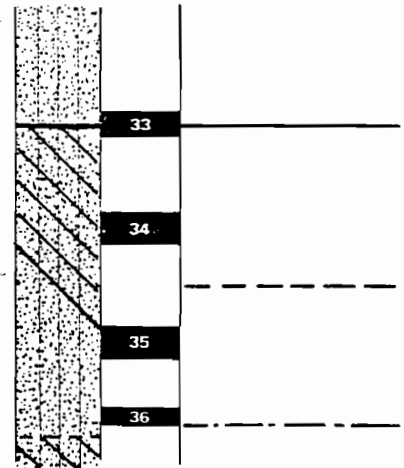
SOIL SAMPLE

- represented by sample identification number which increase sequentially from the top of the hole; thickness of block is equivalent to sample recovery



SOIL BOUNDARIES

- have been indicated using the following system
- stratum boundary observed within sample
- stratum boundary assumed to occur within $\pm 0.5\text{m}$ of the marked level and is probably gradational between the two samples
- stratum boundary assumed to occur within $\pm 1.0\text{m}$ of the marked level
- stratum boundary notation for both depth below seabed (41.5 metres) and elevation below sealevel (uncorrected for tides) (-64.6 metres El.)



41.5 (-64.6 El.)

SOIL DESCRIPTION

UNIFIED SOIL CLASSIFICATION

- determined in accordance with chart on following page

USC

TEXTURAL DESCRIPTION

- determined in accordance with attached sheet and used to augment Unified Soil Classification

Special terms used include:

- e.g. - "becoming trace of/with some CLAY"
indicating an overall change in a feature of the stratum not sufficient to change the total description
- "trace of/with some CLAY"
indicating small feature displayed in that sample only

MUNSELL COLOUR DESIGNATION

- describing wet grey soil, e.g.
- describing dry grey soil, e.g.

(5Y 4/2)

(10YR 6/1)

GROUND ICE DESCRIPTION

- determined in accordance with chart on following page; extra effort has been made to better describe the degree and extent of soil bonding and also a value of core temperature ($^{\circ}\text{C}$) at that level

- see also definition of terms in text

e.g. FROZEN - 2.3
- Nf - Nbn
- poorly to slightly bonded
SAND: Nbn - 2.8
CLAY: not frozen

TEST RESULTS

- see legend at bottom of borehole log

CONSISTENCY

Fine-Grained Soils

Major portion passing No. 200 Sieve. Includes (1) inorganic and organic silts and clays, (2) gravelly, sandy, or silty clays, and (3) clayey silt. Consistency is rated according to shear strength, as indicated by penetrometer readings or vane shear readings.

Descriptive Term	Unconfined Compressive Strength kPa	Equivalent Blows per Foot (N)
Very Soft	less than 25	0 - 2
Soft	25 to 50	2 - 4
Firm	50 to 100	4 - 8
Stiff	100 to 200	8 - 16
Very Stiff	200 to 400	15 - 50
Hard	400 and higher	>50

Coarse-Grained Soils

Major portion retained in No. 200 Sieve. Includes (1) clean gravels and sands, and (2) silty or clayey gravels and sands. Condition is rated according to relative density, as determined by laboratory tests.

Descriptive Term	Relative Density	Equivalent Blows per foot (N)
Very Loose	0 - 20%	0 - 4
Loose	20 - 40%	4 - 10
Compact or Medium	40 - 75%	10 - 30
Dense	75 - 90%	30 - 50
Very Dense	90 - 100%	50 +

The number of blows (N) on a 2" O.D. split spoon sampler by a 140 lbs. weight falling 30" required to drive the sample a distance of 1' (in accordance with ASTM D1586).

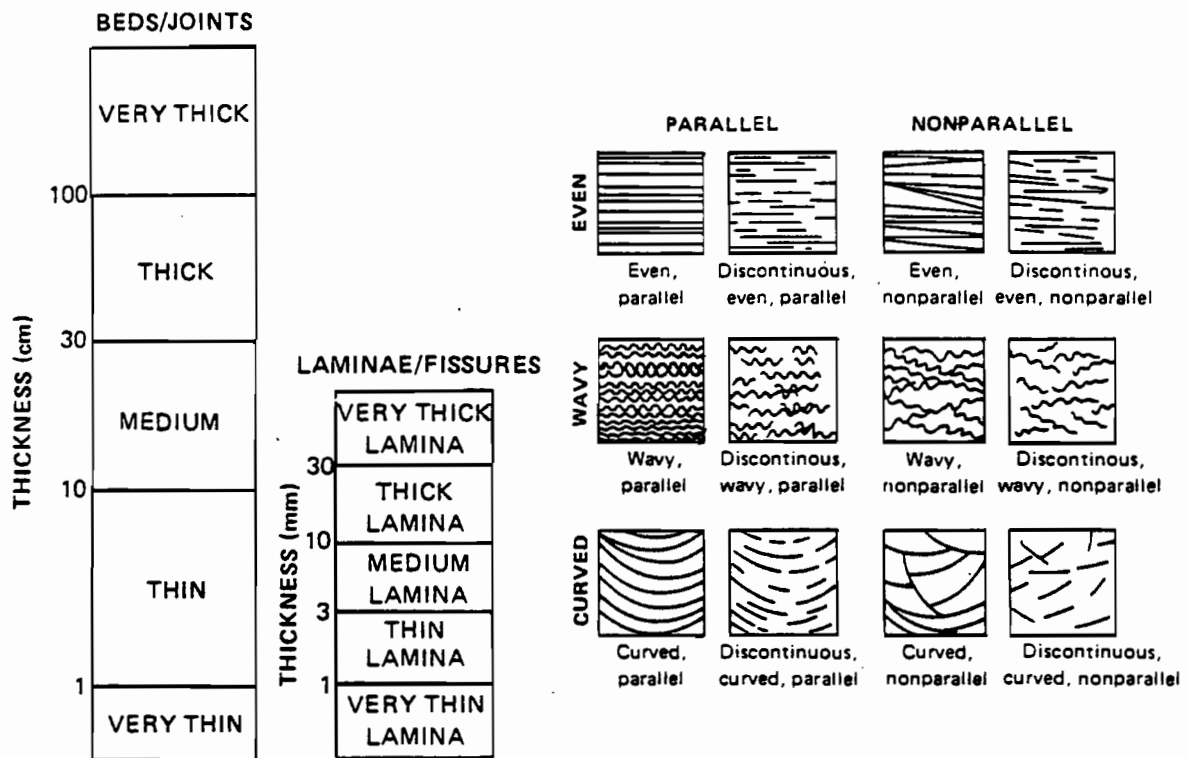
PLASTICITY

Low - Liquid limit less than 50
High - Liquid limit greater than 50

DESCRIPTION OF SEDIMENTARY STRUCTURES

BEDS SEDIMENTATION UNITS DEPOSITED UNDER ESSENTIALLY CONSTANT PHYSICAL CONDITIONS, SEPARATED BY BEDDING PLANES WHICH ARE RECOGNIZABLE BY TEXTURAL OR COMPOSITIONAL CHANGES RESULTING FROM PERIODS OF NON-DEPOSITION OR EROSION, OR ABRUPT CHANGES IN DEPOSITIONAL CONDITIONS. BEDS MAY BE INTERNALLY HOMOGENEOUS, OR COMPOSED OF SMALLER UNITS- LAMINAE

LAMINAE THE SMALLEST MEGASCOPIC LAYERS IN A SEDIMENTARY SEQUENCE, REPRESENTING MINOR FLUCTUATIONS IN PHYSICAL CONDITIONS DURING THE DEPOSITION OF BEDS. LAMINAE ARE RELATIVELY UNIFORM IN TEXTURE AND COMPOSITION AND GENERALLY LACK MEGASCOPIC INTERNAL LAYERING.

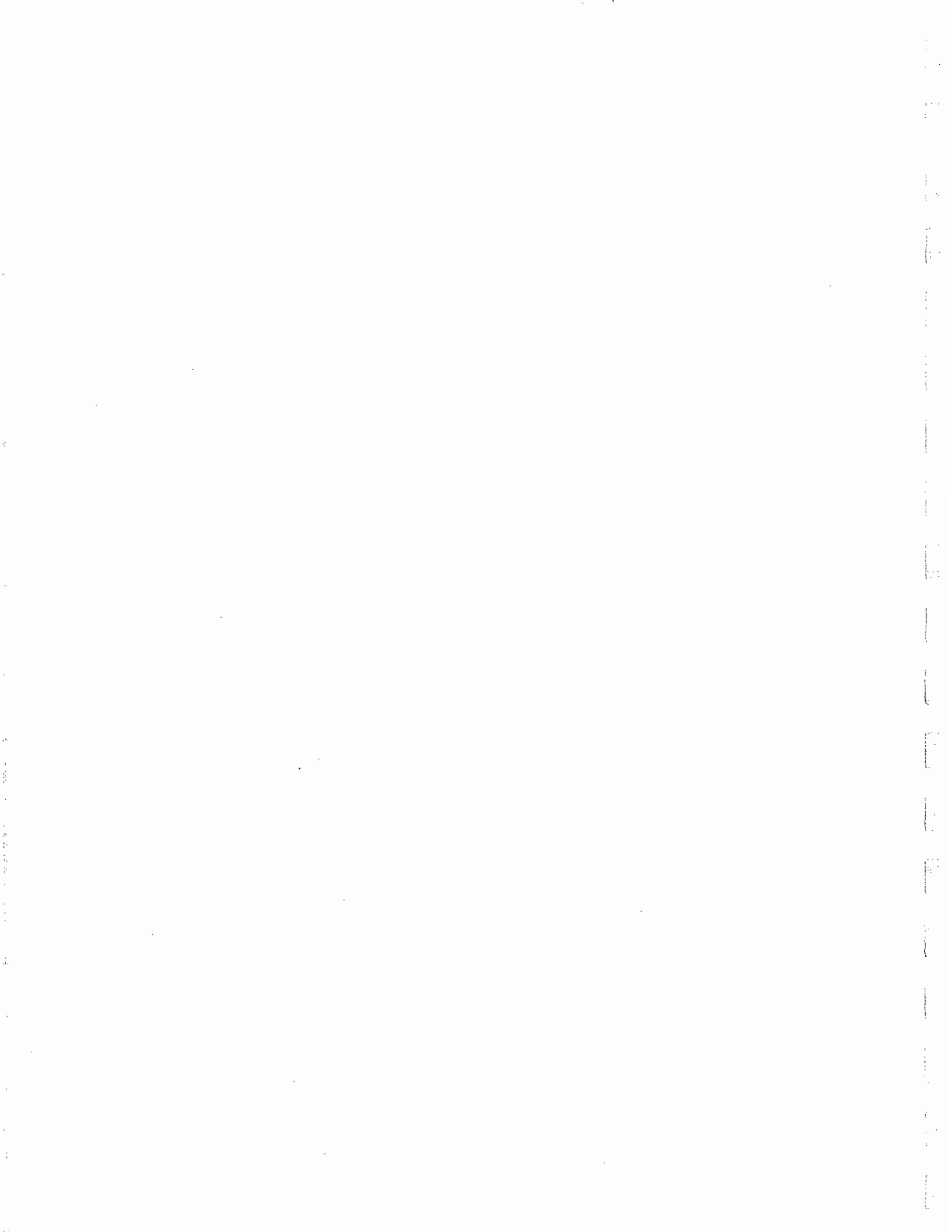


e.g. Thick bed
Thickly spaced joint

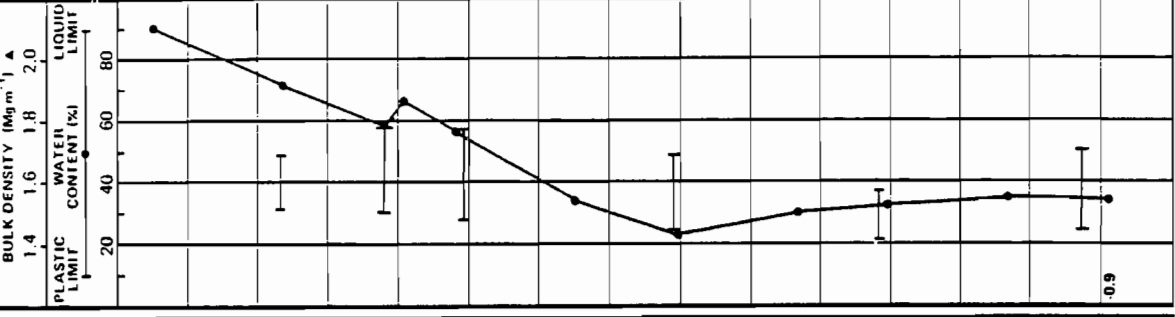
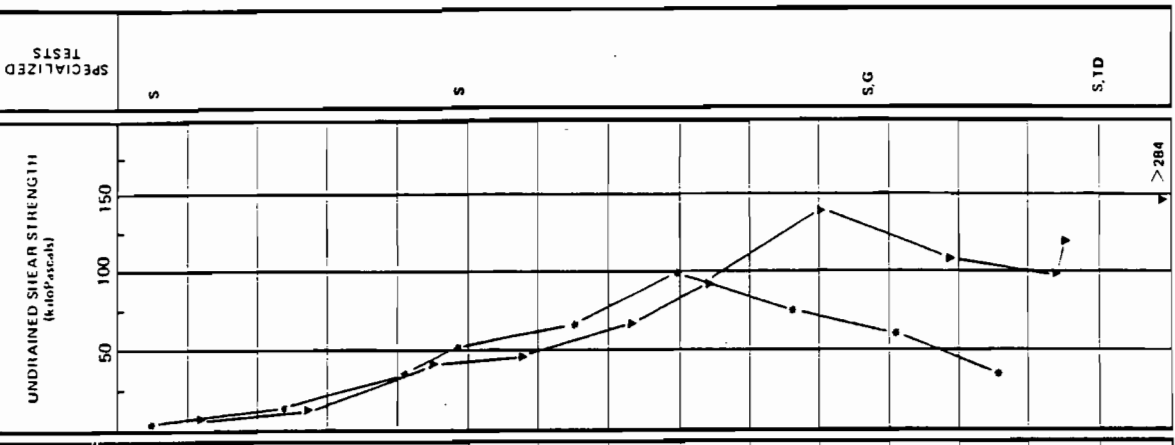
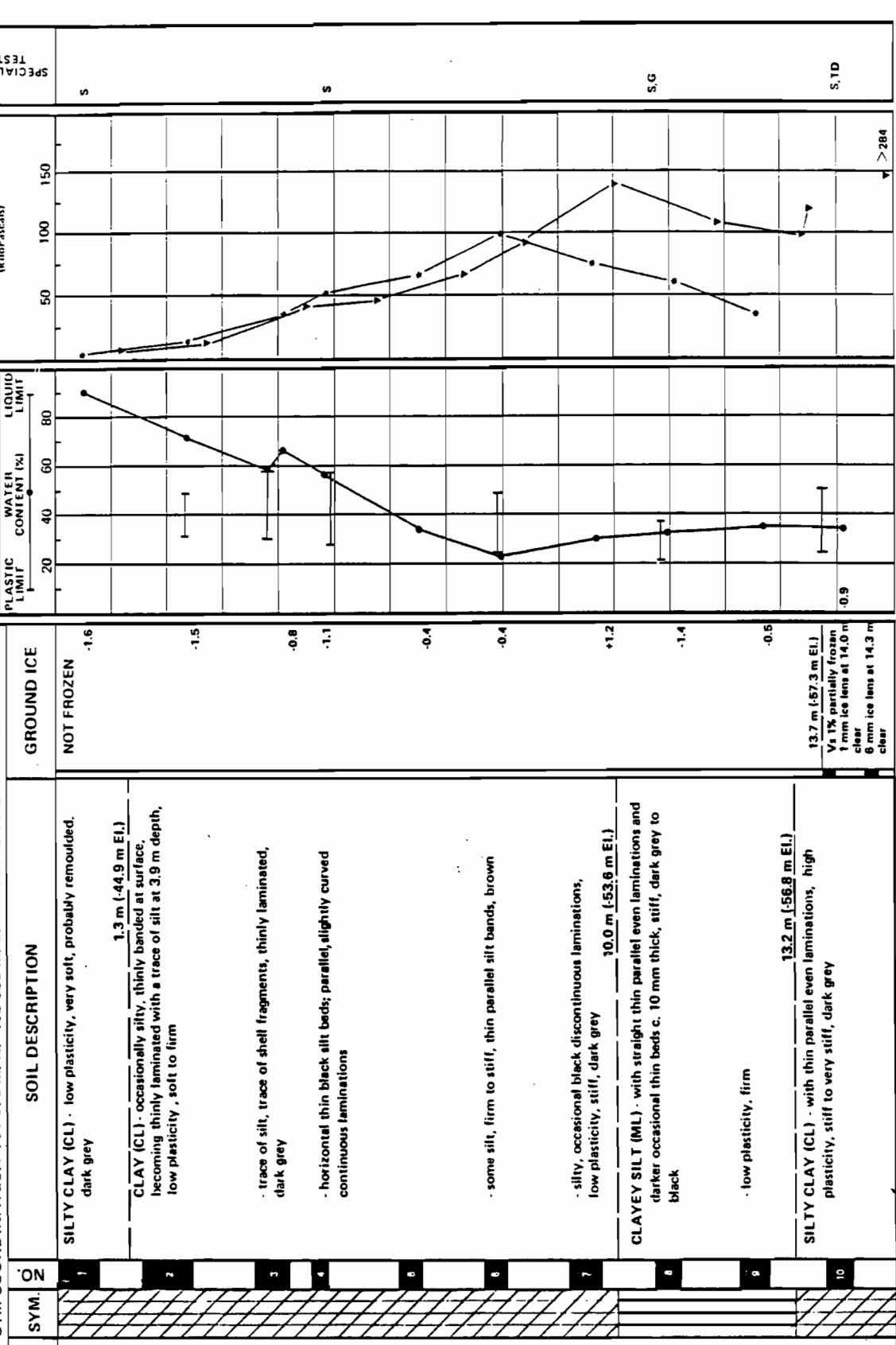
e.g. Thin lamina
Thinly spaced fissures

(After Campbell, 1967)

(Modified after Ingram, 1954
and Campbell, 1967)



LOCATION: KUGDJUK
 UTM COORDINATES: 7 781 070 m. N. 452 635 m. E. WATER DEPTH: 43.6 m



DEPTH BELOW SEABED (metres)	SYMBOL	SOIL DESCRIPTION	GROUND ICE	TEST IDENTIFICATION	SPECIALIZED TESTS
0	1	SILTY CLAY (CL) - low plasticity, very soft, probably remoulded. dark grey	NOT FROZEN		S
1.3	2	CLAY (CL) - occasionally silty, thinly banded at surface, becoming thinly laminated with a trace of silt at 3.9 m depth, low plasticity - soft to firm			S
3.9	3	- trace of silt, trace of shell fragments, thinly laminated, dark grey			S
4.4	4	- horizontal thin black silt beds; parallel, slightly curved continuous laminations			S
5.3	5	- some silt, firm to stiff, thin parallel silt bands, brown			S
6.0	6	- silty, occasional black discontinuous laminations, low plasticity, stiff, dark grey			S
7.0	7	CLAYEY SILT (ML) - with straight thin parallel even laminations and darker occasional thin beds c. 10 mm thick, stiff, dark grey to black			S, G
10.0	8				S, TD
13.2	9	SILTY CLAY (CL) - with thin parallel even laminations, high plasticity, stiff to very stiff, dark grey			S, TD
13.7	10	13.7 m (-57.3 m EI.) Vs 1% partially frozen 1 mm ice lens at 14.0 m 6 mm ice lens at 14.3 m clear			S, TD

BOREHOLE NUMBER
 KG 82 S02
 PAGE 2 OF 2

TEST IDENTIFICATION
 C - Consolidation
 DS - Direct Shear
 TD - TDR
 Ca - Calorimetry
 I - Triaxial Shear
 S - P.W. Salinity
 G - Gas Analysis

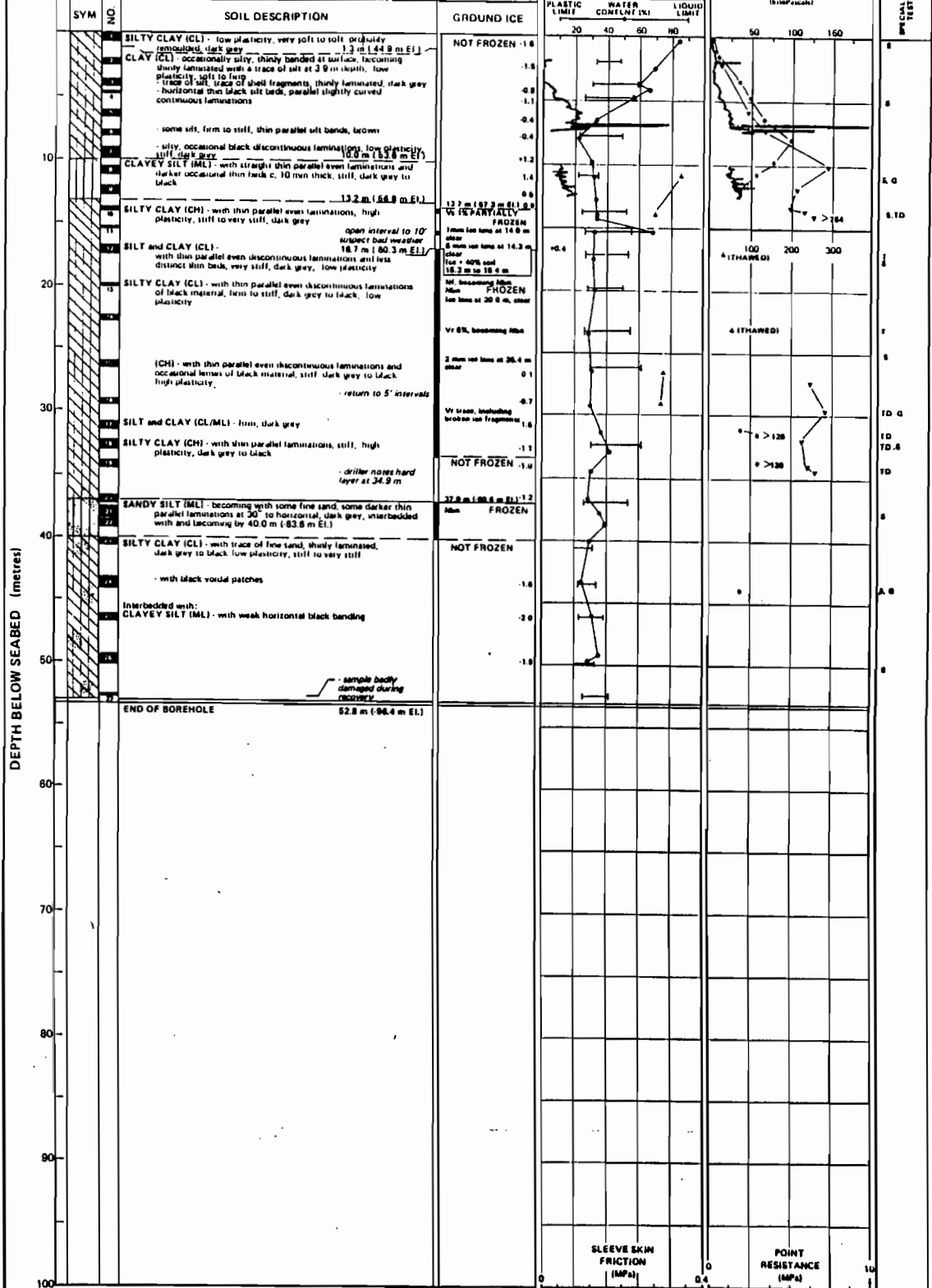
LEGEND
 SOIL SYMBOLS
 SAND (stippled), SILT (horizontal lines), CLAY (diagonal lines)
 SHEAR STRENGTH
 Torvane (circle), Fall Cone (square), UU Triaxial (triangle), CU Triaxial (diamond), Picon Vane (circle with cross), Remote Institu Vane (inverted triangle)

JOB No.: 101 - 3657
 DRILLING COMPLETED: 82/08/09
 BOREHOLE DEPTH: 52.8 (-96.4 m EI.)
 DRILLING RIG: S5000/MV BRODERICK
 LOG COMPILED BY: JPR



BOREHOLE LOG AND LABORATORY TEST RESULTS

LOCATION: KUGDUK
 UTM COORDINATES: 7 781 070 m. N. 462 636 m. E. WATER DEPTH: 43.6 m



DEPTH BELOW SEABED (metres)



JOB No.: 101-3657
 DRILLING COMPLETED: 82/08/09
 BOREHOLE DEPTH: 52.8 m (-96.4 m EI.)
 DRILLING RIG: S5600/MV BRODERICK
 LOG COMPILED BY: JPR

SOIL SYMBOLS		
SAND	SILT	CLAY

LEGEND	
SHEAR STRENGTH	
Terrace	Full Core
Min. Vane	Un. Triaxial
Plastic Vane	CU Triaxial
Modified Vane	Remolded Plastic Vane

TEST IDENTIFICATION	
C	Compressibility
DS	Direct Shear
TD	TD
TO	TO
G	Gas Analysis
Cc	Calorimetry
I	Triaxial Shear
S	P-W. Seismicity

BOREHOLE NUMBER
 KG 82 502
 PAGE 1 OF 2

BOREHOLE LOG AND LABORATORY TEST RESULTS
 CONE PENETRATION TEST DATA

PENETRATION TEST
 KG8202

APPENDIX B

Diagnostic Profiles

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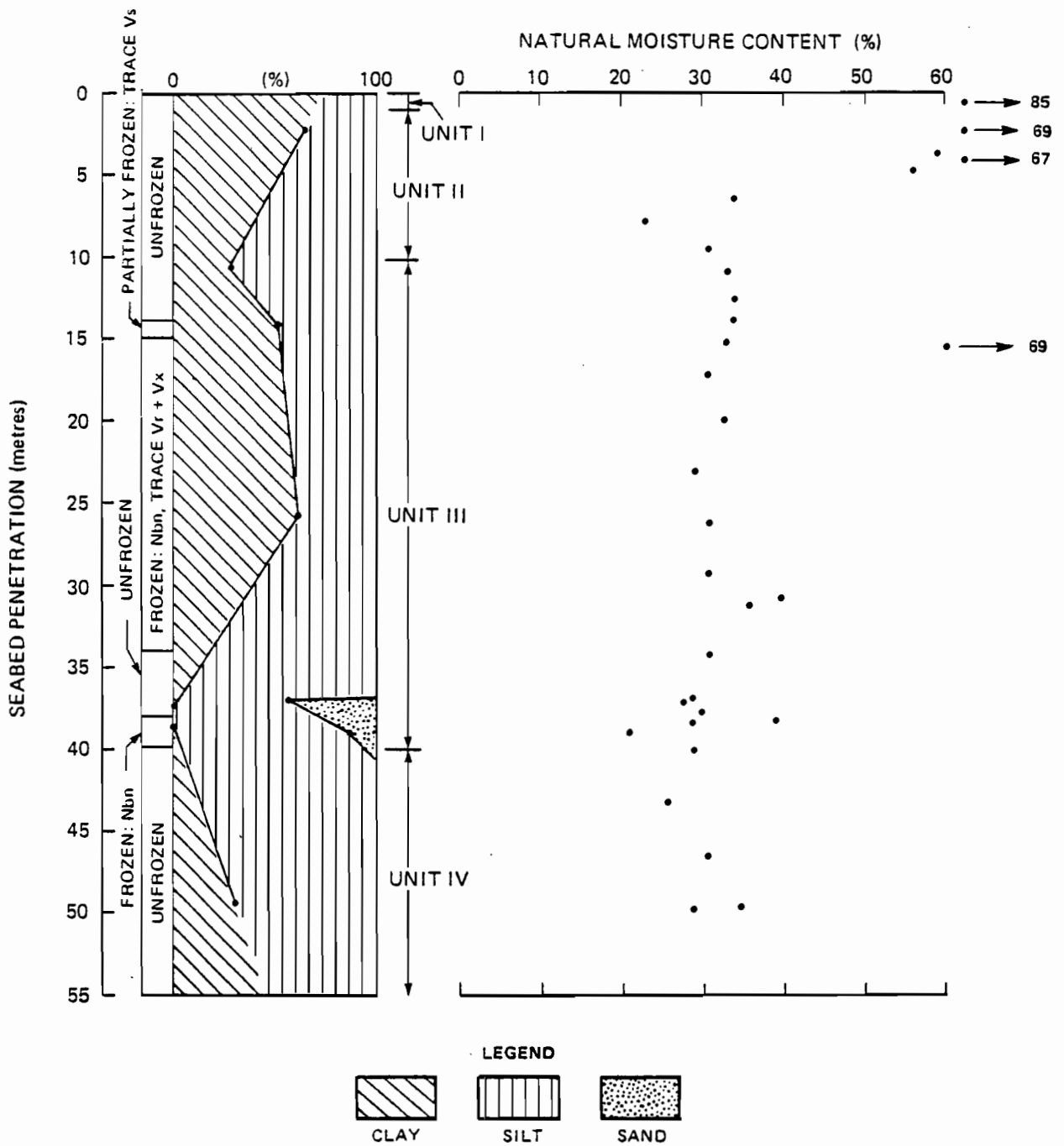


FIGURE B.1 NATURAL MOISTURE CONTENT PROFILE, KUGDJUK AREA

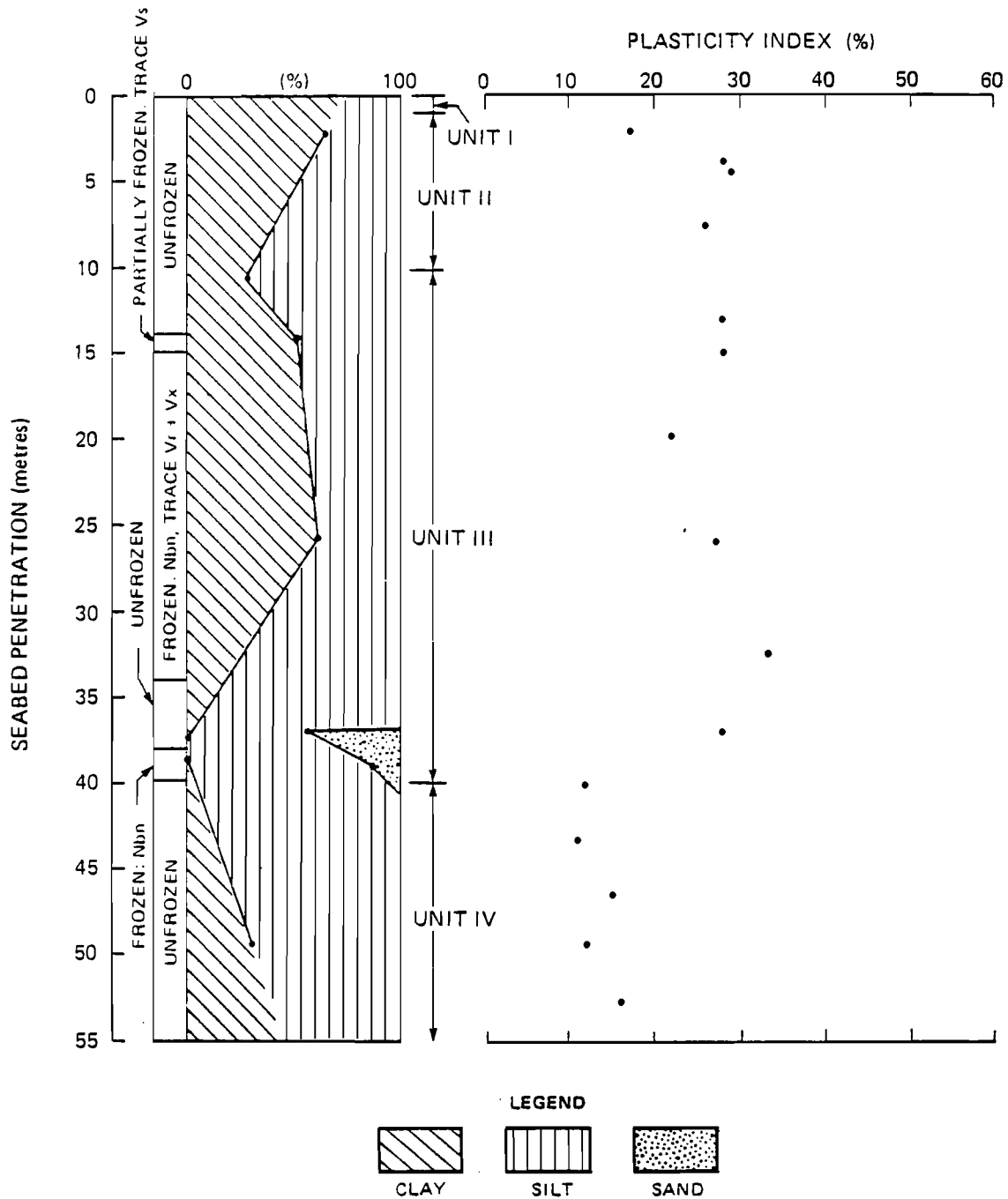


FIGURE B.2 PLASTICITY INDEX PROFILE, KUGDJUK AREA

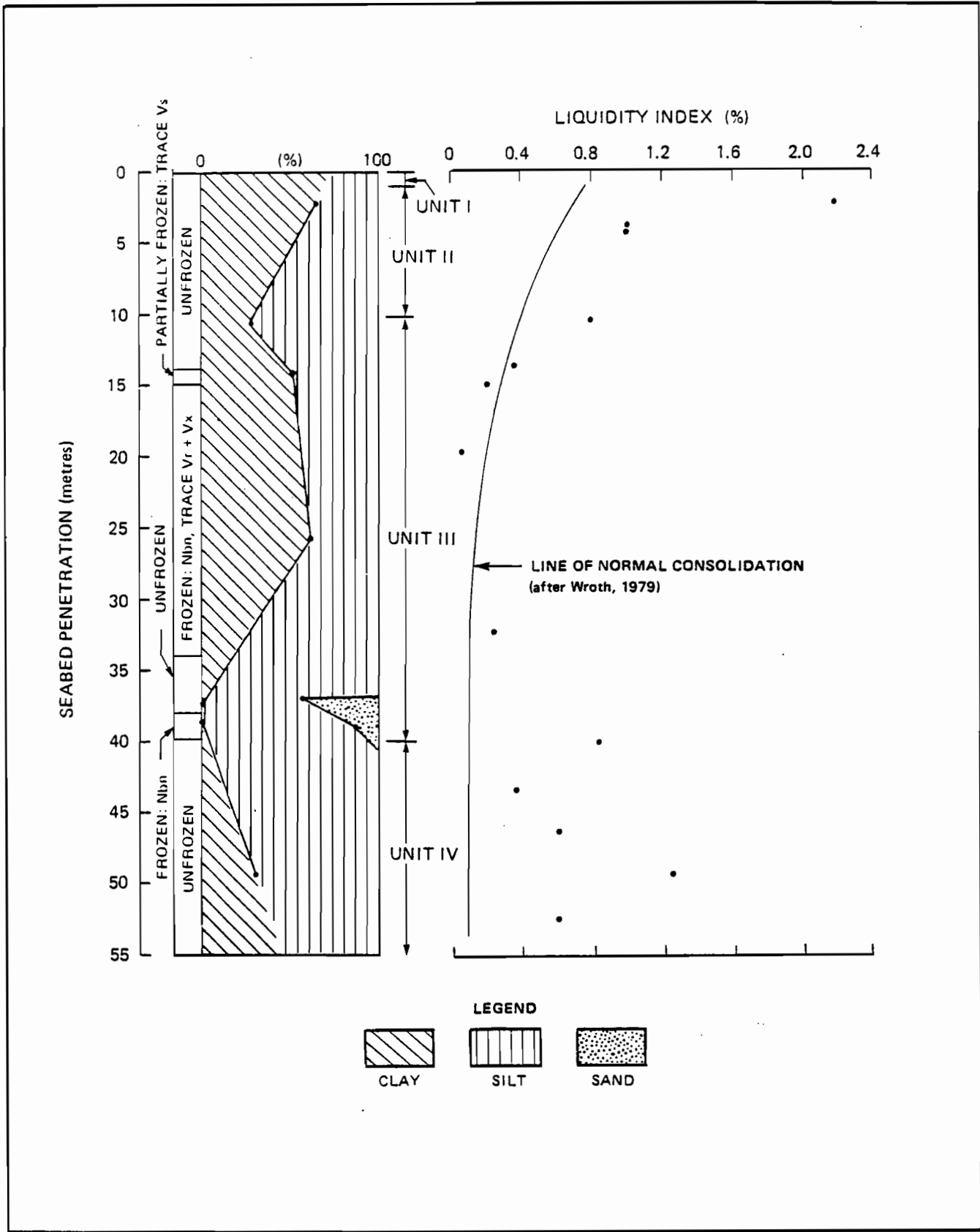


FIGURE B.3 LIQUIDITY INDEX PROFILE, KUGDJUK AREA

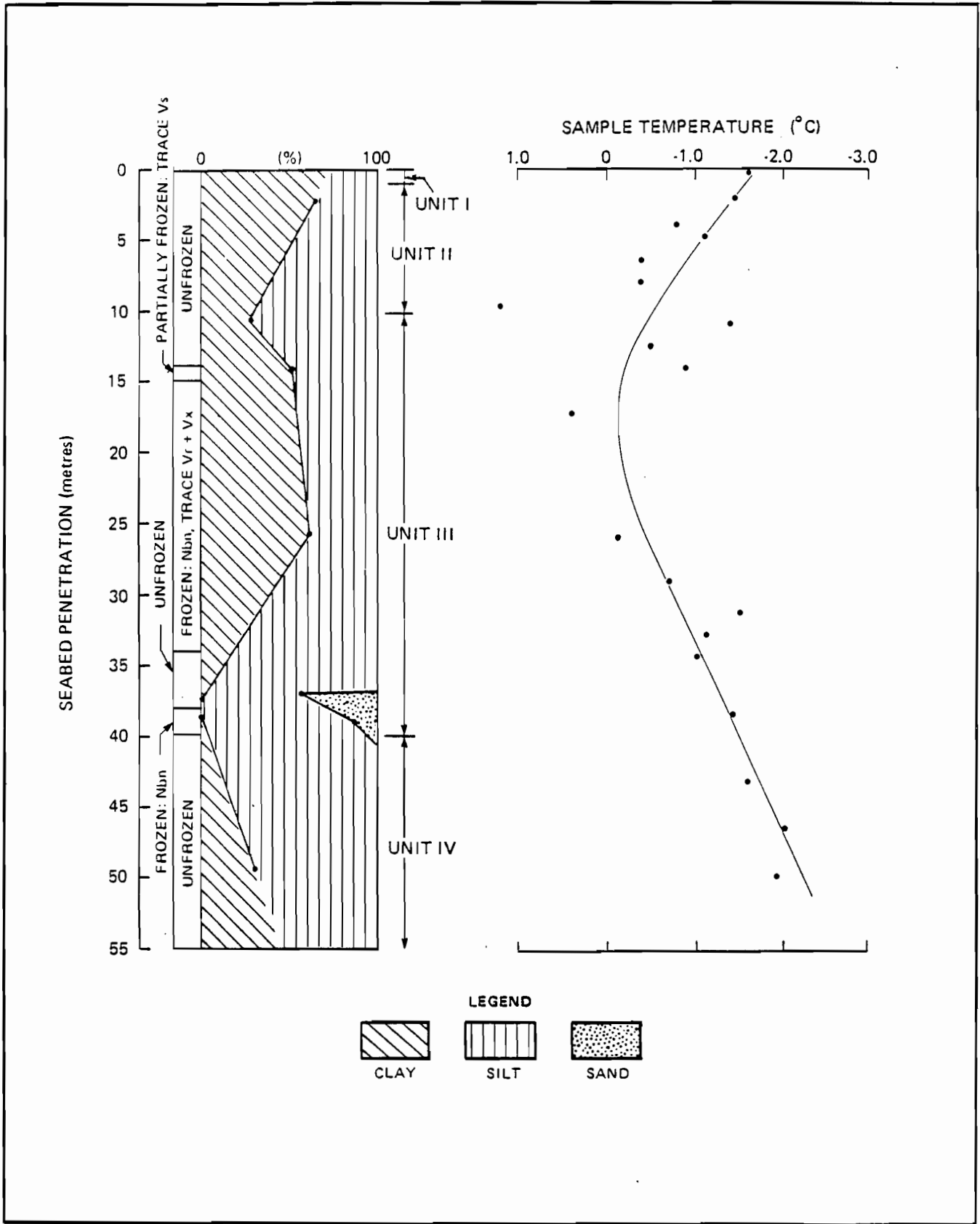


FIGURE B.4 SAMPLE TEMPERATURE PROFILE, KUGDJUK AREA

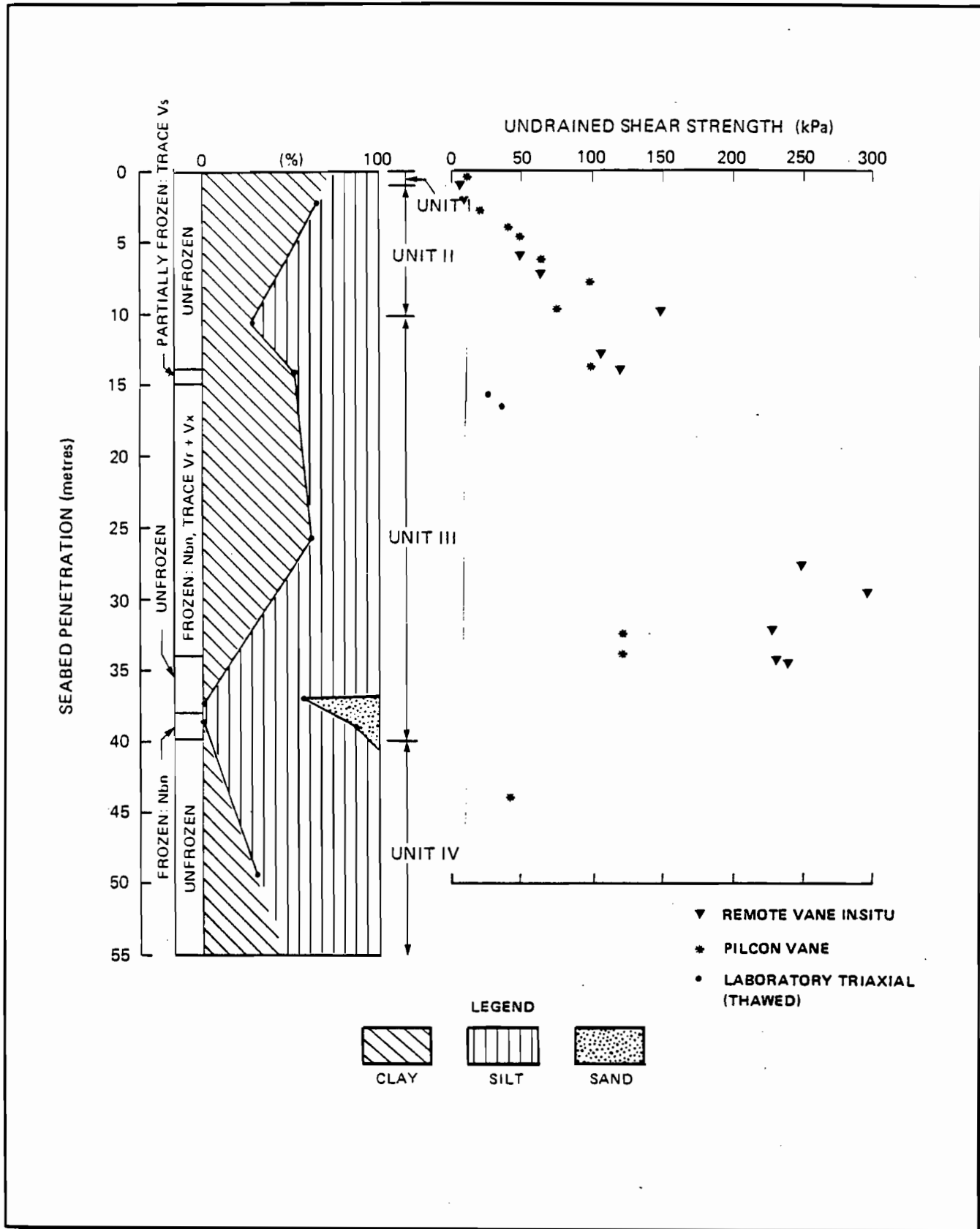


FIGURE B.5 UNDRAINED SHEAR STRENGTH PROFILE, KUGDJUK AREA

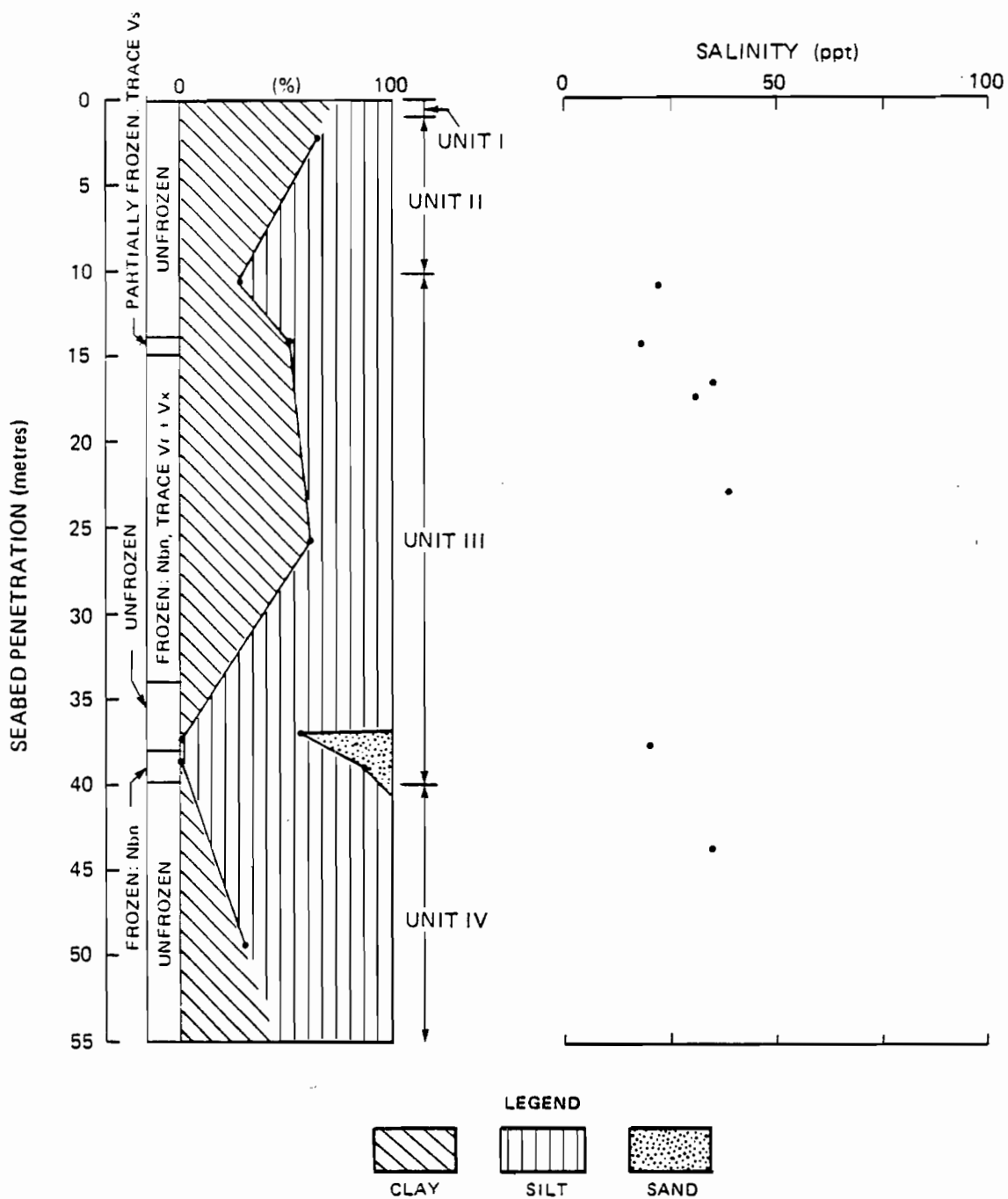


FIGURE B.6 SALINITY PROFILE, KUGDJUK AREA

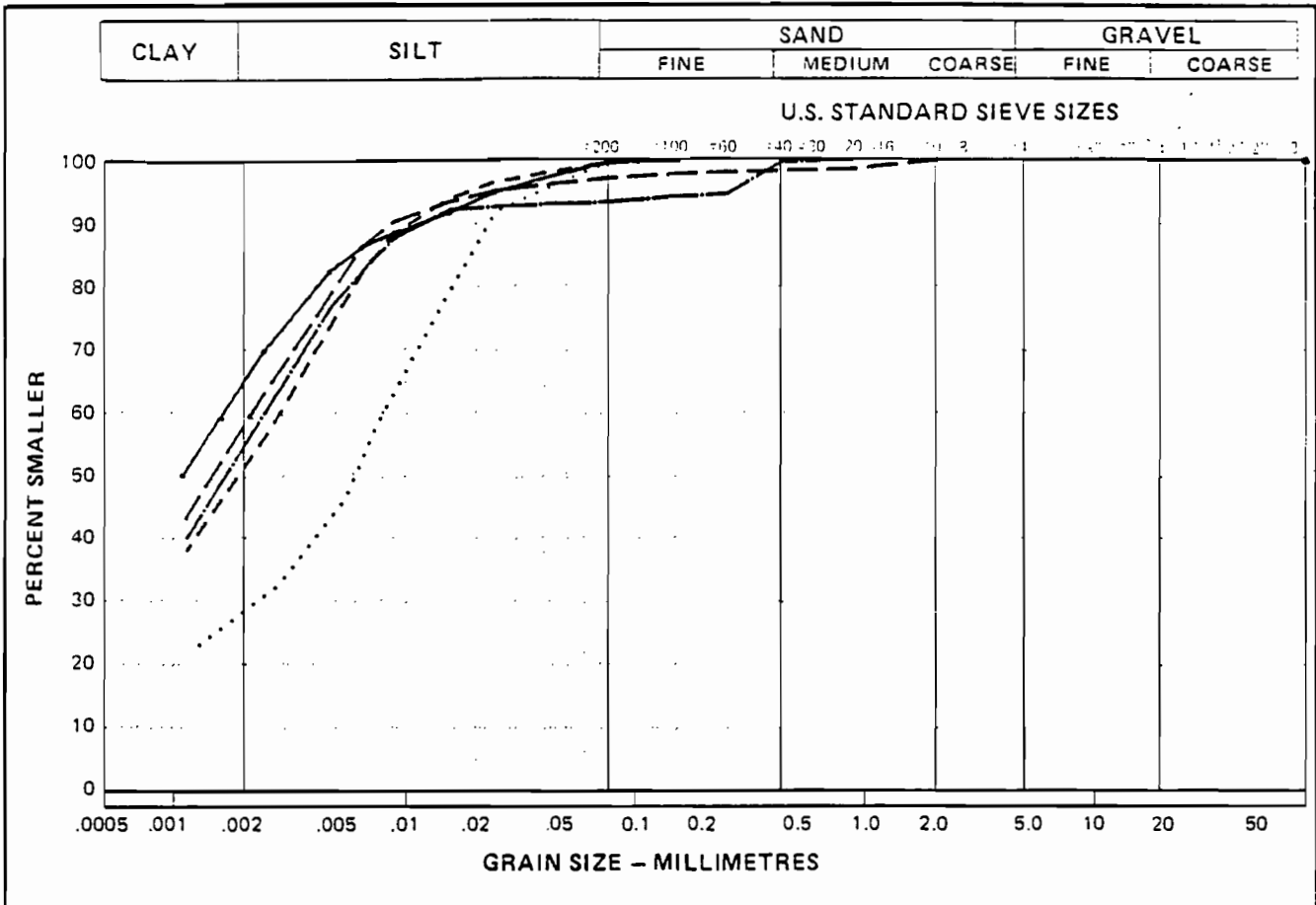
APPENDIX C

Classification and Index Test Results



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PARTICLE - SIZE ANALYSIS OF SOILS

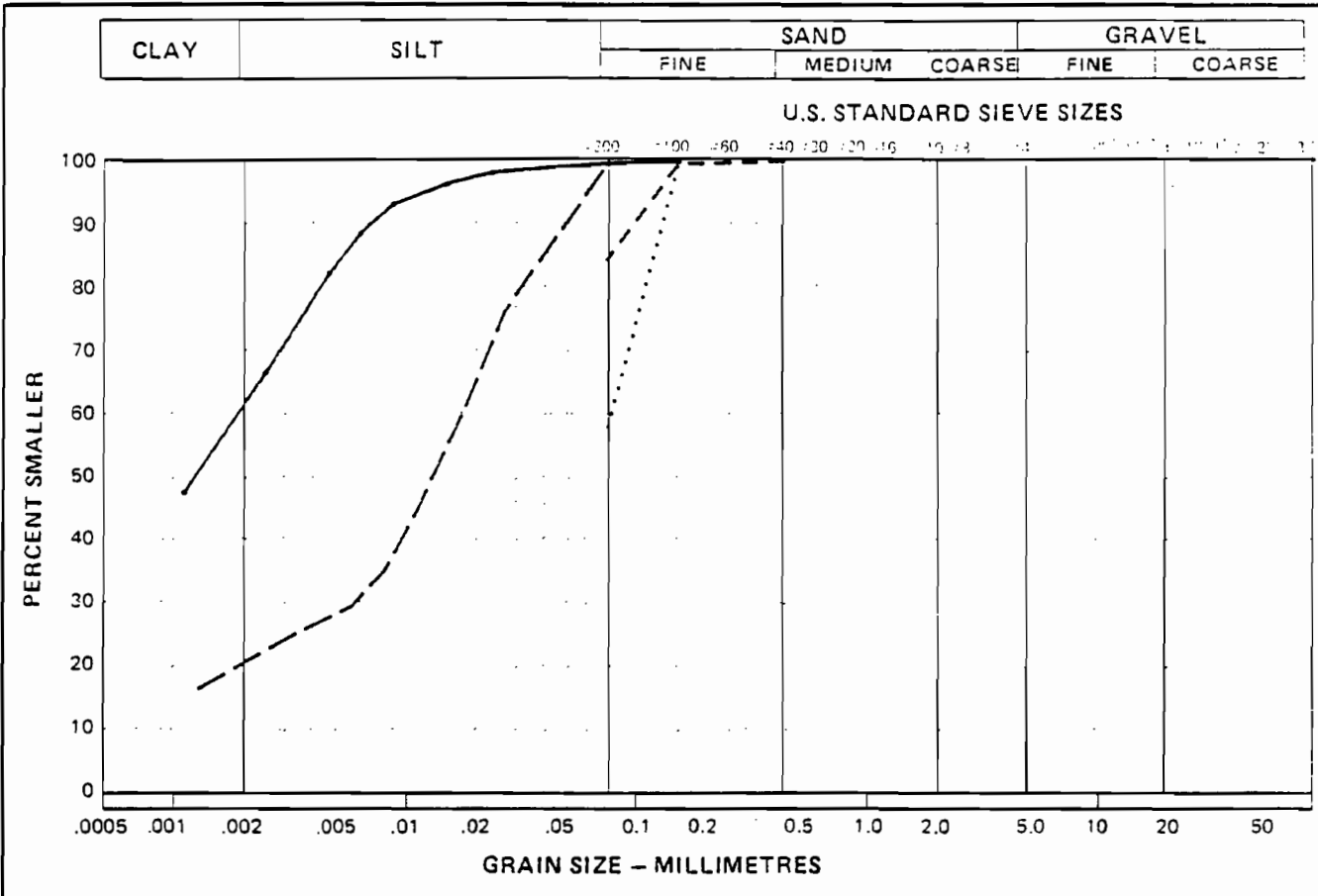


SYMBOL	BOREHOLE NUMBER	DEPTH (m)	DESCRIPTION				Cu	Cc	U.S.C.
			CLAY (%)	SILT (%)	SAND (%)	GRAVEL (%)			
_____	KG82S02	2.17 - 2.34	65.1	34.8	.1	0.0	-	-	
.....	KG82S02	10.67 - 10.83	28.1	71.8	.1	0.0	-	-	
-----	KG82S02	13.72 - 13.93	51.3	48.6	.1	0.0	-	-	
_____	KG82S02	16.75 - 17.24	57.9	39.5	2.6	0.0	-	-	
_____	KG82S02	22.86 - 23.22	54.6	39.0	6.4	0.0	-	-	

JOB NO. 101 -3657

DATE 82-09-29

PARTICLE - SIZE ANALYSIS OF SOILS



SYMBOL	BOREHOLE NUMBER	DEPTH (m)	DESCRIPTION				Cu	Cc	U.S.C.
			CLAY (%)	SILT (%)	SAND (%)	GRAVEL (%)			
_____	KG82S02	25.91 - 26.10	61.8	38.1	.1	0.0	-	-	
.....	KG82S02	37.01 - 37.10	-	57.5	42.5	0.0	-	-	
-----	KG82S02	37.85 - 37.92	-	84.6	15.4	0.0	-	-	
_____	KG82S02	49.38 - 49.66	20.3	79.6	.1	0.0	-	-	

JOB NO. 101 -3657

DATE 82-10-01

APPENDIX D

Shear Strength Test Results

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APPENDIX D

GLOSSARY OF TERMS RELATED TO SHEAR STRENGTH

- Axial Stress : Vertical stress applied to a sample (Force/X-Sectional Area)
- B : The ratio of pore pressure response to a change in isotropic pressure. Indicative of the degree of saturation.
- Back Pressure : An increase in pore pressure applied to a sample for the purpose of increasing saturation.
- c' : Effective value of cohesion.
- Cell Pressure : Isotropic confining pressure to which a sample is subjected during triaxial testing.
- Consolidation : Volumetric change in soil with time resulting from loading under drained condition.
- Deviator Stress : The net applied axial stress during triaxial testing. Mathematically, the difference between the major and minor principal stresses ($\sigma_1' - \sigma_3'$).
- Effective Stress : The net stress present in a saturated soil after the pore pressure has been subtracted. The stress difference between the total and measured pore pressure.
- Epore : Computer output heading for excess pore pressure
- Excess Pore Pressure : The pore pressure generated or developed during shear.
- Jacketed : A sample is enclosed in a thin, impermeable, latex membrane.
- K_0 : The ratio of the effective horizontal stress to the effective vertical stress. σ_3' / σ_1'
- ParA : Computer output heading for Skempton's pore pressure parameter A. A is the ratio of change in excess pore pressure to change in deviator stress.
- Peak Strength : The maximum deviator stress that can be applied to a sample.

GLOSSARY (continued)

- ϕ' : Internal angle of friction under effective stress conditions.
- Pore Pressure Response: A change in pore pressure resulting from a change in stress condition.
- Reshaped Strength : Analogous to remoulded strength. Shear strength measured after soil structure completely removed.
- Strain : Ratio of deformation over a fixed reference length to the initial reference length. Expressed as a percent.
- s1 : Computer output heading for the effective major principal stress, σ_1' . In triaxial testing this represents the total vertical stress.
- s3 : Computer output heading for the effective minor principal stress, σ_3' . In triaxial testing, this represents the cell pressure.
- Tpore : Computer output heading for total pore pressure.
- VolCh : Computer output heading for the volume changes a sample undergoes during loading.
- Wet Density : Mass of the soil particles and water in a unit volume of soil.
- Dry Density : Mass of the dry soil particles in a unit volume of soil.



Project No. 1
 Test No. KC02502
 Test Hole No. 1-1R
 Depth of Sample m. 22.86 (75.32)
 Confining Pressure kPa. 484.0
 Water Content %. 30.32
 Wet Density Mg/m³. 1.97
 Peak Stress kPa. 109.6

Project Address
 Job No. 101-4857
 Date Tested 8/21/05
 Client
 Attention

Test No. 2
 Test Hole No. 1-1R
 Depth of Sample m. 19.75 (64.78)
 Confining Pressure kPa. 484.0
 Water Content %. 35.74
 Wet Density Mg/m³. 1.85
 Peak Stress kPa. 62.4

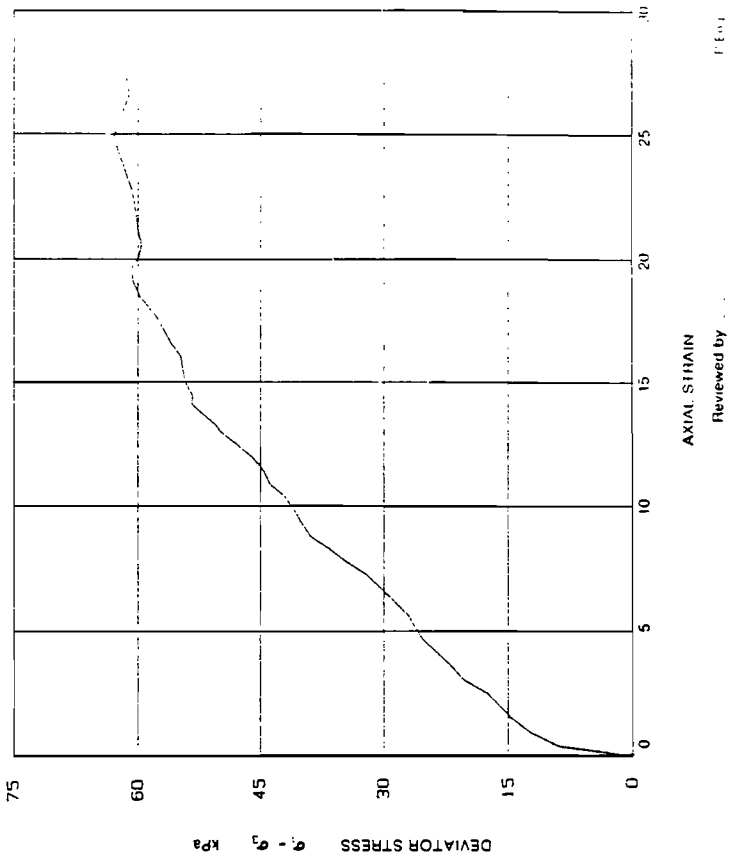
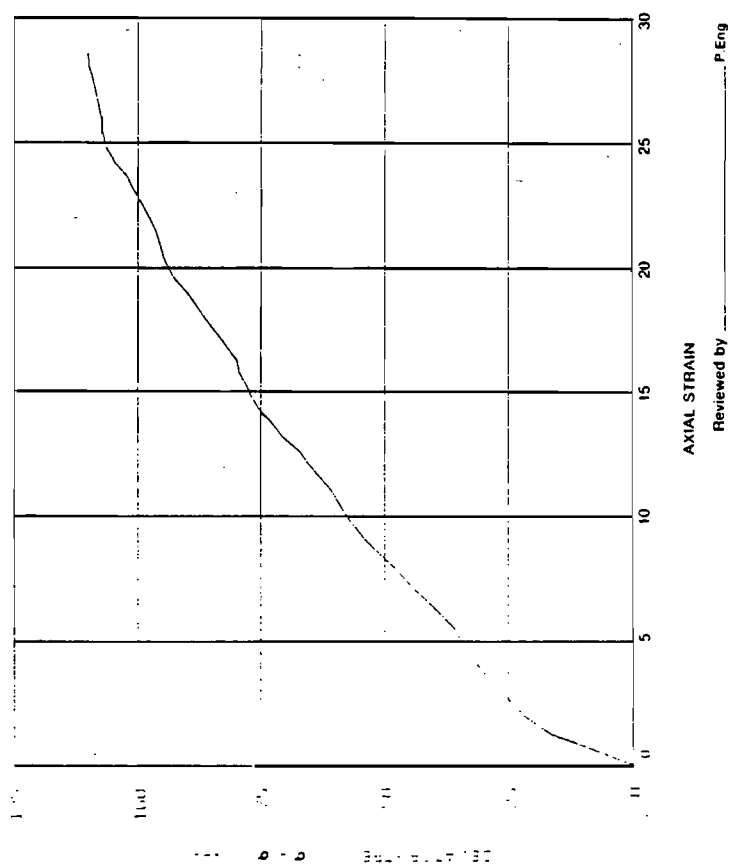


FIGURE D.1 UNCONSOLIDATED - UNDRAINED TRIAXIAL TEST
 KUGDJUK SITE

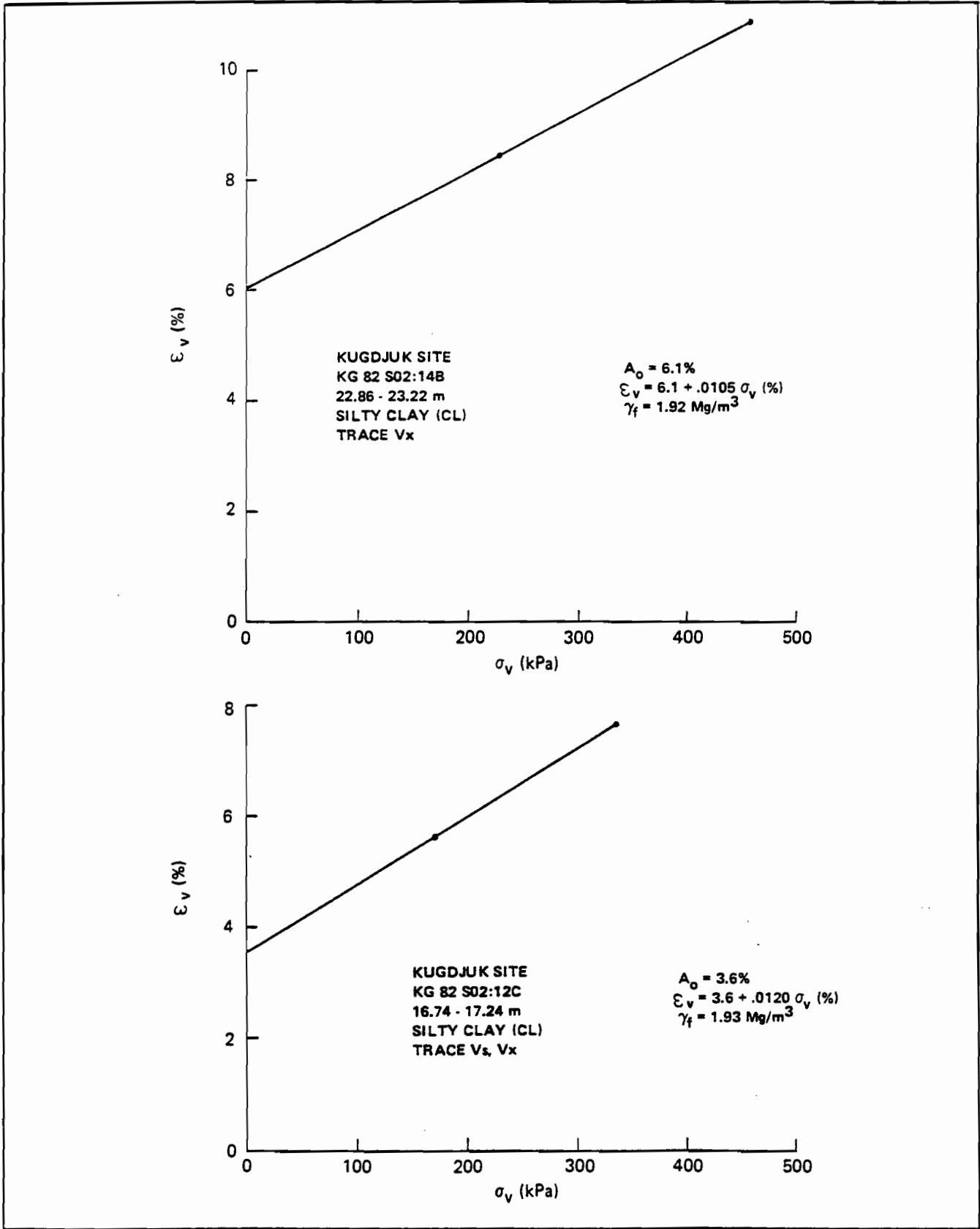


FIGURE D.2 THAW STRAIN TEST RESULTS
KUGDJUK SITE



APPENDIX E

Consolidation Test Results

THE UNIVERSITY OF CHICAGO

APPENDIX F

Subconsultants Results

THE UNIVERSITY OF CHICAGO

REPORT ON
HYDROCARBON GAS ANALYSES
BOREHOLE KG82502 - Kugdjuk

JOB 101-3657.3

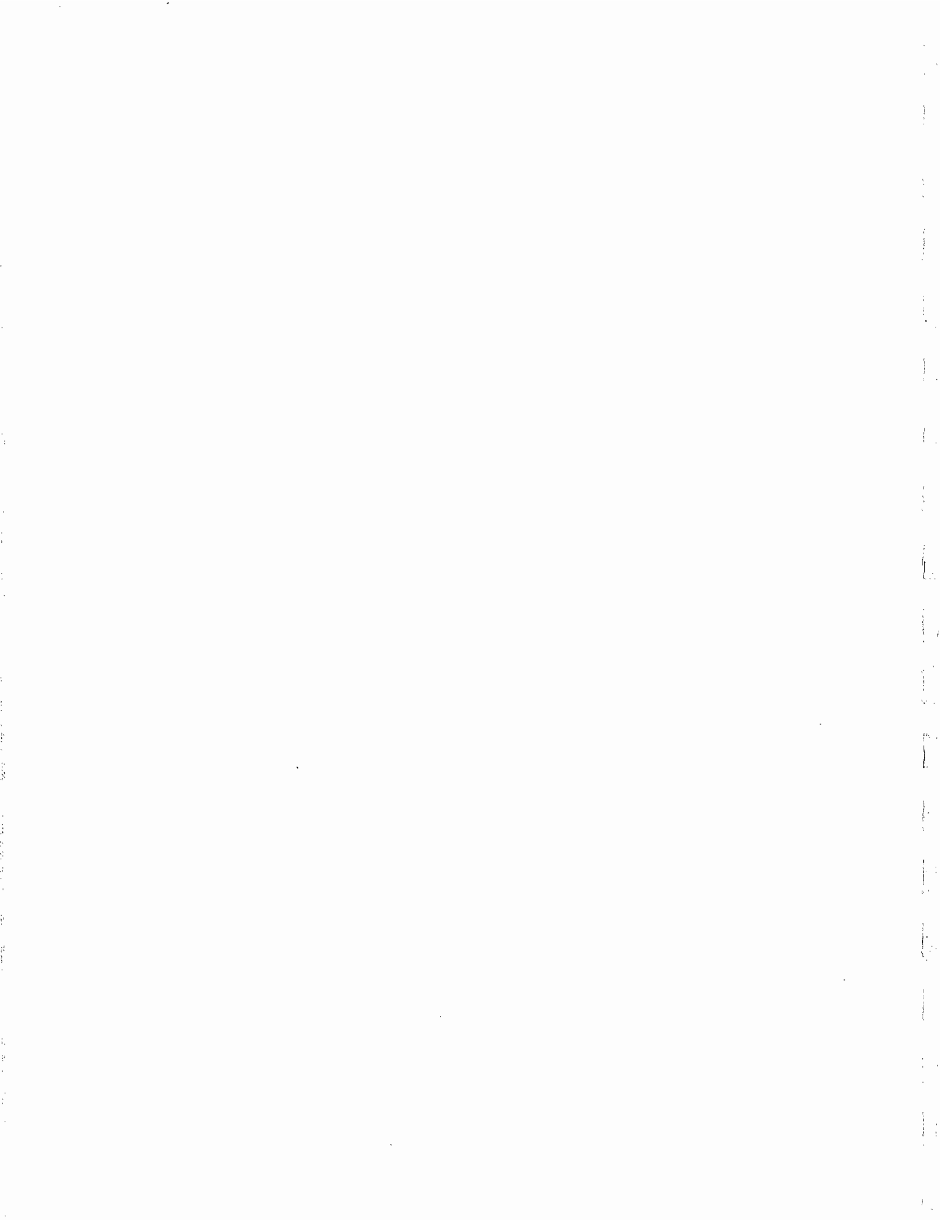
FOR

EBA ENGINEERING CONSULTANTS LTD.
J.P. RUFFELL

PREPARED BY

Dr. J.F. BARKER
DEPARTMENT OF EARTH SCIENCES
UNIVERSITY OF WATERLOO

DECEMBER 2, 1982



METHODS

At the drill site, fresh core material is placed in cans with water so as to eliminate any head space. In the laboratory, 100 cm³ of helium is added and 100 cm³ of water withdrawn via gas-tight septa. The sediment/water/helium mixture is vigorously shaken so that hydrocarbon gases will be taken into the helium gas phase. A few microlitres of the gas phase is analyzed by gas chromatography for methane, ethane, ethylene, propane, and propylene. A commercial, analyzed gas mixture is used as standards. The concentration of each component is reported in parts per million (ppm) on a volume basis (v/v). That is, 10⁴ ppm, v/v indicates that there is 1 cm³ of that gas per 100 cm³ of wet sediment. It is assumed that 100 cm³ (100 ml) of wet sediment has been canned at the drill site. In addition, the sediment was dried and weighed so that the amount of gas per dry weight of sediment can be reported if the client wishes.

RESULTS

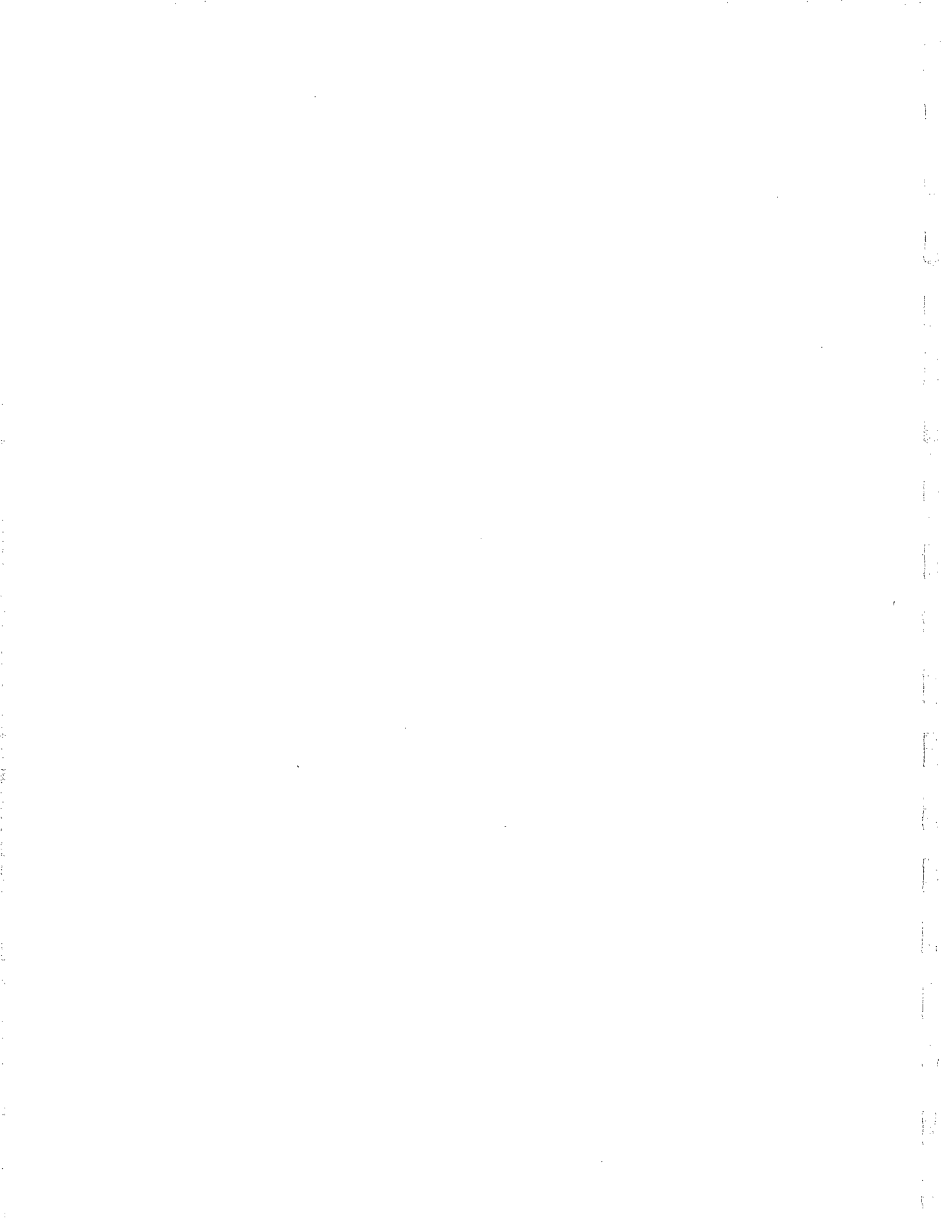
Results of the hydrocarbon gas analysis for the three core samples are as follows:

SAMPLE	DEPTH (m)	GAS CONTENT (ppm, v/v)		
		Methane	Ethylene	Ethane
8B	10.9	3.4 x 10 ²	—	1
10C	29.0	4.7 x 10 ²	<1	4
24A	43.7	2.5 x 10 ²	—	3

Dashes indicate the component was not detected. Propane and propylene also were not detected. The lack of significant petrogenic components (ethane and propane) and the trace of ethylene, a biogenic gas, suggest that the hydrocarbon gases are dominantly biogenic. Methane is the dominant gas and little variation in methane concentration with depth is noted. These concentrations of methane do not exceed the solubility of methane in porewaters and so the biogenic methane produced at this stage is dissolved in the porewaters (or ice) and does not contribute significantly to pore pressures.

APPENDIX G

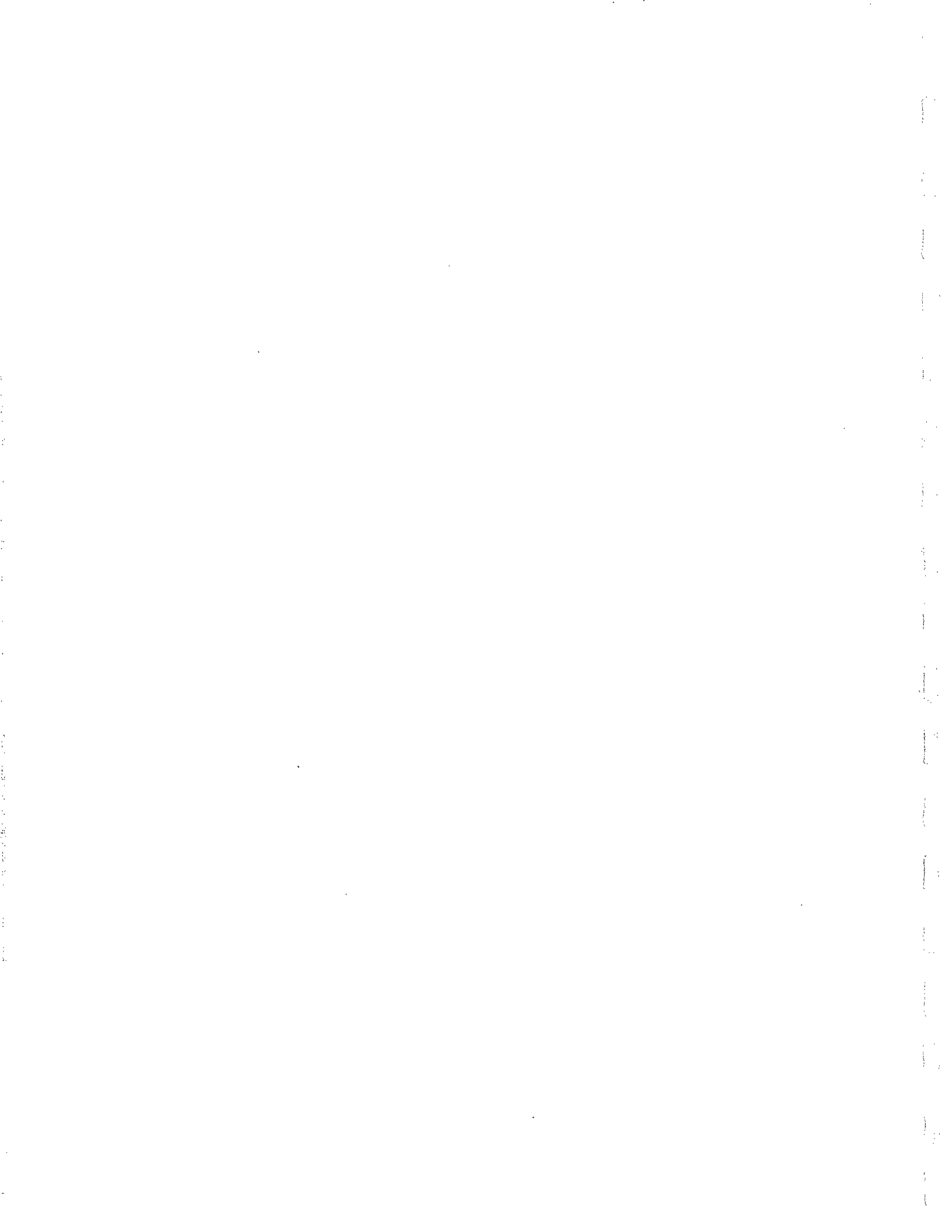
Laboratory Test Procedures



LABORATORY TEST PROCEDURES

Procedures Specified

1. Classification and Index Tests
2. Triaxial Shear Tests
3. Direct Shear Tests
4. Laboratory Miniature Vane
5. Swedish Fall Cone Shear Strength Determination
6. Consolidation Tests
7. Porewater Salinity Tests
8. Organic Content Determination
9. Radiography



LABORATORY TEST PROCEDURES

1. CLASSIFICATION AND INDEX TESTS

These tests are quite routine and the standard ASTM procedures employed are listed below:

<u>TEST</u>	<u>ASTM DESIGNATION</u>
Moisture Content	D 2216
Liquid Limit (1)	D 423
Plastic Limit and Plasticity Index	D 424
Grain Size	D 421 & 422
Specific Gravity	D 854
Relative Density	D 2049
Unified Soil Classification	D 2487

NOTE: 1. All liquid limits reported were obtained from 3 point determinations.

2. SHEAR STRENGTH TESTS

Procedure #1 - Unconfined Compression

Procedure #2 - Unconsolidated Undrained Triaxial
With and without pore pressure measurement

Test specimen is mounted in triaxial cell and jacketed. Cell pressure equivalent to estimated in situ total horizontal stress ($K_0 = 0.7$) is applied without sample drainage. A pore pressure response test is carried out prior to shear. If $B < 0.95$, sample is loaded to failure at rate of 1%/min with no pore pressure measurement. If $B > 0.95$ specimen loaded to failure at rate of 0.02%/min with pore pressures monitored continuously. Frozen samples are permitted to thaw (undrained condition) prior to measurement of B value.

For quick UU tests, data is presented in the form of stress-strain curves. Where pore pressure is monitored, the following curves are obtained:

1. Stress-strain
2. Effective stress ratio-strain
3. Excess pore pressure-strain
4. P/Q stress path

CONSOLIDATED-UNDRAINED TRIAXIAL TESTS

Procedure 1 - Sample is mounted in triaxial cell and jacketed. A pore pressure response test is carried out prior to shearing. If further saturation is required, back pressure can be applied to the sample. Frozen samples are placed in a pre-chilled triaxial cell, then permitted to thaw before commencing consolidation. Cell pressure equivalent to estimated total horizontal stress is applied with drainage allowed. Once consolidation is complete, drainage is shut off. Samples are sheared by increasing axial stress at controlled rate of strain based on the consolidation characteristics of the material determined during the consolidation phase of the test. Stress-strain curve and other diagnostic plots are produced.

CONSOLIDATED-DRAINED TRIAXIAL TESTS

Procedure 1 - Sample is mounted in triaxial cell and jacketed, then thawed under a nominal pressure of 35 kPa. A pore pressure response test is carried out prior to shearing. If further saturation is required, back pressure can be applied to the sample. Sample is consolidated to cell pressure equivalent to estimated mean horizontal in situ effective stress. With drainage open, sample is sheared by increasing the axial stress at a controlled rate of strain. The rate of strain is selected on the basis of consolidation properties of the soil determined during the consolidation phase of the test. Stress-strain curve and other diagnostic plots are produced.

Procedure 2 - Lack of undisturbed samples of sand from certain strata necessitate reconstituting disturbed samples for strength testing. Relative density test is conducted on the sand and reconstituted samples are then prepared to approximately 70% relative density. A pore pressure response test is carried out prior to shearing. If saturation is required, back pressure is applied to the sample. Sample is consolidated to cell pressure equivalent to the estimated in situ mean horizontal effective stress. With the drainage open, the sample is sheared by increasing the axial stress at a controlled rate of strain as detailed in Procedure 1. Stress-strain curve and other diagnostic plots are produced.

- NOTES:
1. Standard UU triaxial procedure ASTM D2850.
 2. Standard CU and CD triaxial procedures taken from Bishop & Henkel (1969).
 3. Samples reconstituted according to procedures outlined in Bjerrum, Kringstad, and Kummeneje (1961).

3. DIRECT SHEAR TESTS

Procedure 1 - Standard direct shear procedure. Frozen samples are permitted to thaw and consolidate under applied normal pressure before commencing shear. Resheared strength is measured on plane cut after peak strength has been determined. Generally, a minimum of 3 tests are performed on each material type to define effective stress parameters c' and ϕ' . Shear stress - deformation curve and other diagnostic plots produced.

Procedure 2 - If no undisturbed sample is available, an appropriate sample may be reconstituted for testing following the same general procedure indicated above.

- NOTES:
1. Standard direct shear procedure ASTM D 3080.
 2. Samples reconstituted according to procedures outlined in Bjerrum, Kringstad, and Kummeneje (1961).

4. LABORATORY MINIATURE VANE

Procedure 1 - Sample is either retained in sampling tube or extruded into split ring. Vane is lowered into sample ensuring total submergence of the vane. Vane is rotated at 10 degrees/min. Test is run until steady post-peak value is reached. Stress-strain curves, peak and post-peak shear strengths are produced.

5. FALL-CONE SHEAR STRENGTH DETERMINATION

Procedure 1 - Small portion of sample is extruded into testing cup. Cone is selected with reference to expected shear strength of soil. Cone is lowered to contact the surface of the sample and is then released. Depth of penetration of cone is measured. Shear strength is interpreted from cone strength correlation charts.

6. STANDARD OEDOMETER/CONSOLIDATION TESTS

Procedure 1 - Sample is set up in oedometer with dry stones. Standard incremental loading is applied done to a specified vertical effective stress that exceeds the in situ effective overburden pressure. The oedometer is then flooded with a saline solution similar to that of the soil, unloaded and permitted to rebound. After rebound, the specimen is reloaded in increments of 50% increase until a specified vertical effective stress, is reached. Thereafter, the standard doubling of pressures is resumed to test completion. All load increments are left on for a time interval determined by the root time method. e -log- p' curve, c_v , k , m_v , and P_c' data produced.

Procedure 2 - Sample is set up frozen in oedometer, then moved from cold room to standard apparatus. Stress is applied to seat load cap and sample is then thawed under nominal pressure. Procedure continues as for Procedure 1. e -log- p' curve, c_v , k , m_v , and P_c' data produced.

NOTE: 1. Modifications made to standard procedure (ASTM D 2435) are taken from Andresen et al. (1979) and Broms (1980), as recommended for overconsolidated soils. Procedure is appropriate in view of large reduction in total stress that typically occurs upon sampling.

In addition to the specific procedures described above, all samples programmed for testing may have other basic tests performed as follows:

1. Moisture content
2. Bulk density
3. Core photography (where practical)
4. Detailed description of sedimentological features, and
5. Identification and preservation of discrete organic matter when present.

7. POREWATER SALINITY TESTS

Procedure 1 - Sample is trimmed to remove disturbed material. Porewater is extruded from thawed sample and chloride titration is performed to establish equivalent salinity (NaCl).

NOTES: 1. A silver nitrate titration is performed to determine the chloride ion content (ASTM D 512 Method B).

2. Chloride ion content was converted to an equivalent salinity using the following empirical relationship.

$$\text{Salinity (o/oo)} = 0.03 + (1.805 \times \text{Chlorinity (o/oo)})$$

8. ORGANIC CONTENT DETERMINATION

Procedure 1 - Small portion of sample is weighed then oven dried. Dried sample is mixed with hydrogen peroxide solution (H₂O₂) and boiled. After reaction ceases sample is oven dried and reweighed. Loss in weight is inferred as organic content.

9. RADIOGRAPHY

Procedure 1 - Samples are transported to be radiographed on subcontractors premises. Samples are returned with processed film negatives.

Procedure 2 - Samples are radiographed at EBA. Samples are removed from storage area and returned immediately. Film is processed on site and results reviewed.

NOTE: 1. For report presentation, radiography subcontractor can prepare high quality B/W prints from film negatives.

APPENDIX H

CONE PENETRATION TEST DATA

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Beaufort Sea - Cone Penetration Test Data

1982 Saurak
Kugdjuk
Kringalik

1983 Stokes Point

Frontier Development Division
March 1983

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Sauvrak
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10A
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13A
14

Kugdjuk
01
02

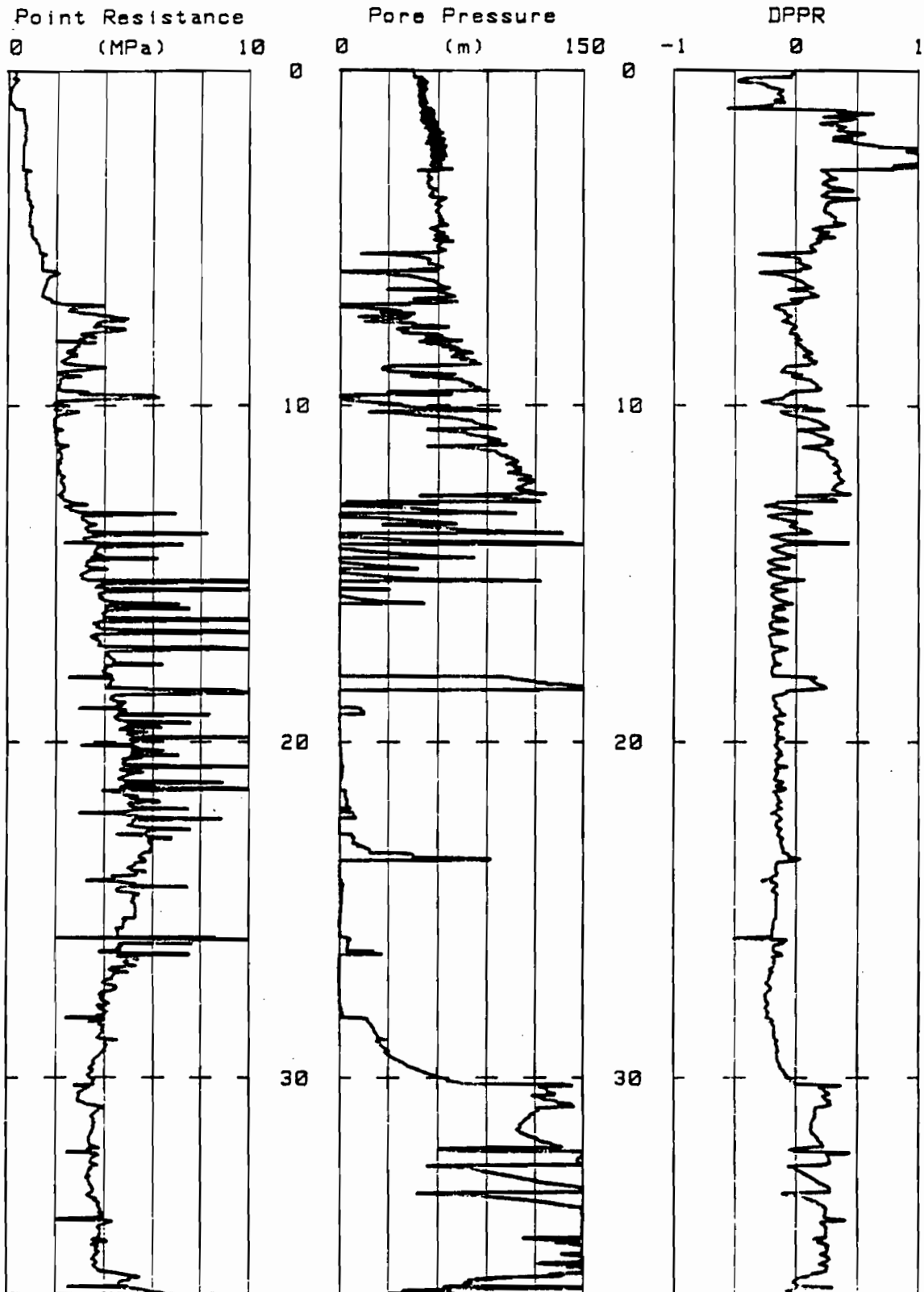
Kringalik
01 (0 - 40 m)
01 (40 - 71.5 m)
03
05
06

Stokes Point
10A
15
16
17
19A
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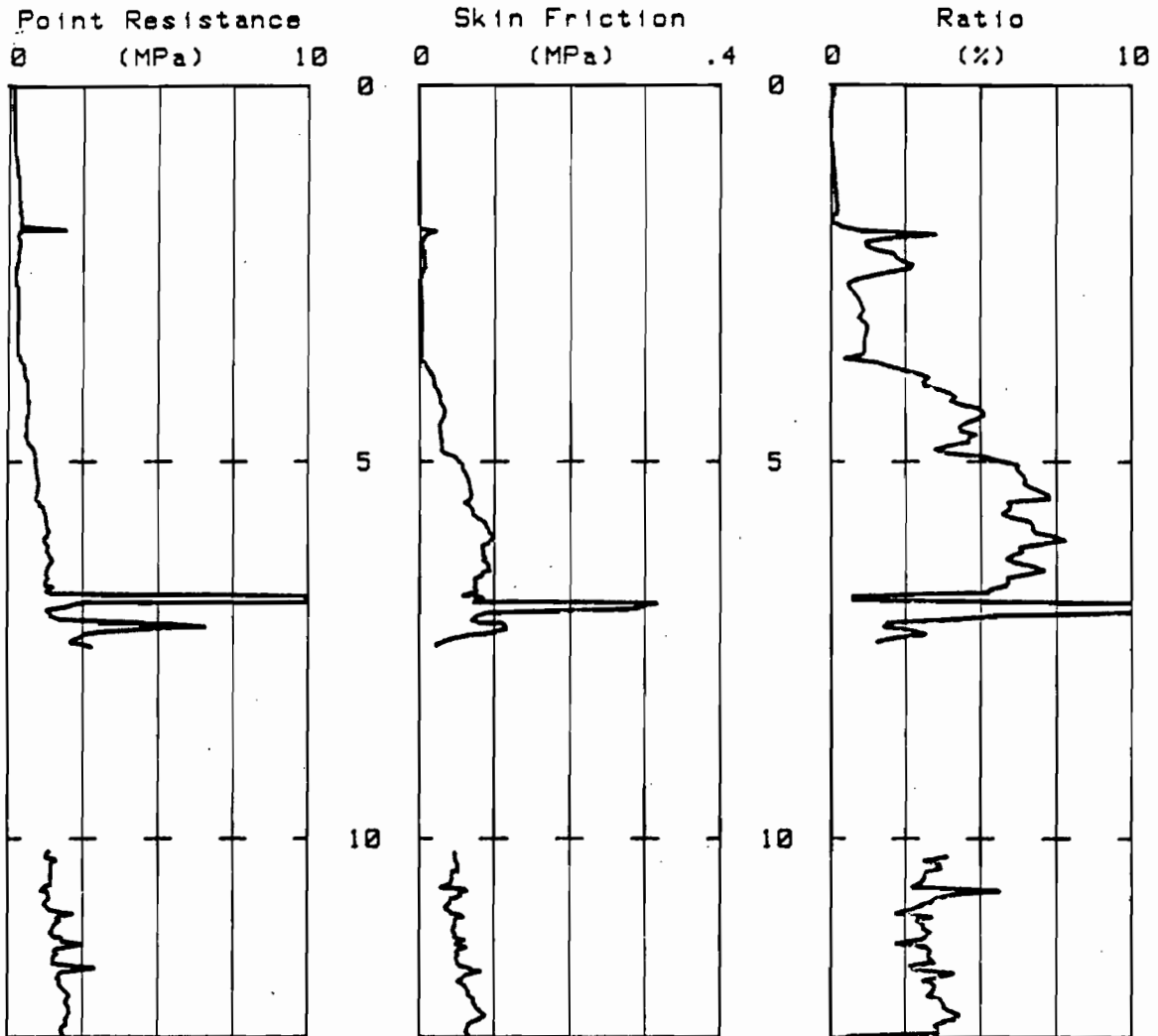
Location: Kugdjuk
Test No. 01
Code: KGB2C01

Date: 82 08 08
Operator: Geosystems
Soil Penetration (m): 36.45
Water depth (m): 45.0



Location: Kugdjuk
Test No. 02
Code: KGB2C02

Date: 82 08 08
Operator: Geosystems
Soil Penetration (m): 12.64
Water depth (m):



Location: Stokes Point

Date: 83 02 09

Test No. 10A

Operator: B. Morris

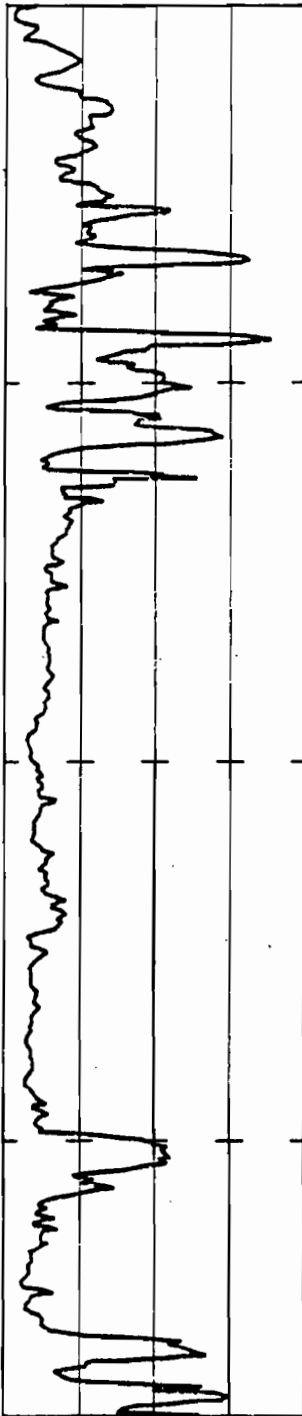
Code: 83SP10A

Soil Penetration (m): 18.64

Water depth (m): 1.7

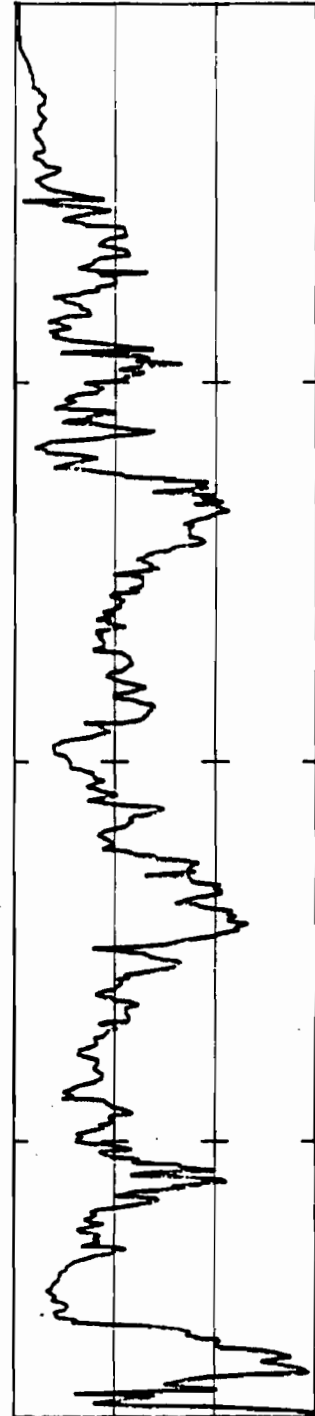
Point Resistance

0 (MPa) 20



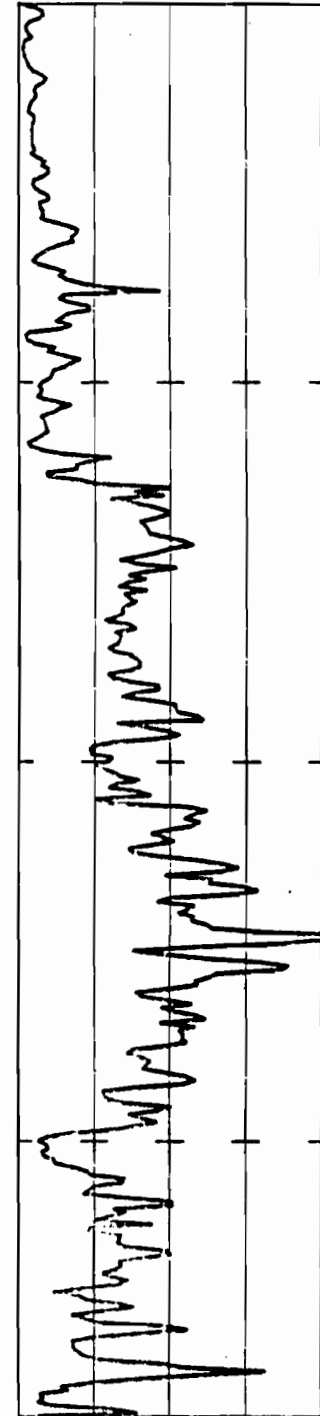
Skin Friction

0 (MPa) .3



Ratio

0 (%) 10



Location: Stokes Point

Date: 83 02 08

Test No. 15

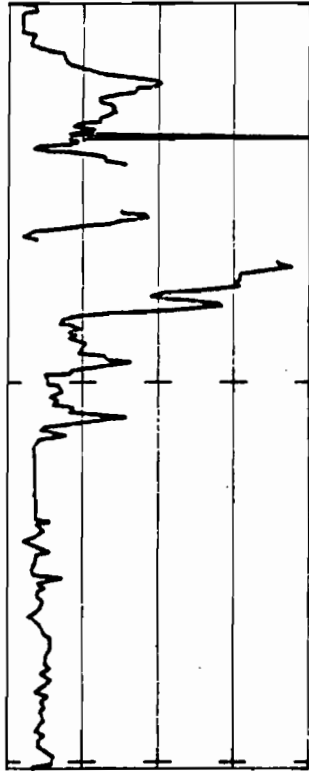
Operator: B. Morris

Code: 83SP15

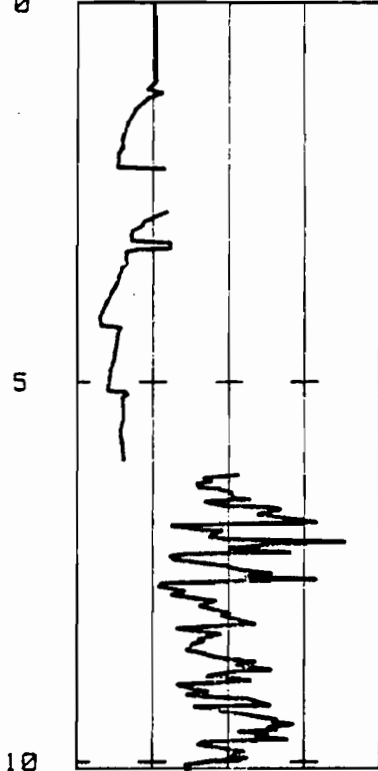
Soil Penetration (m): 10.09

Water depth (m): 1.7

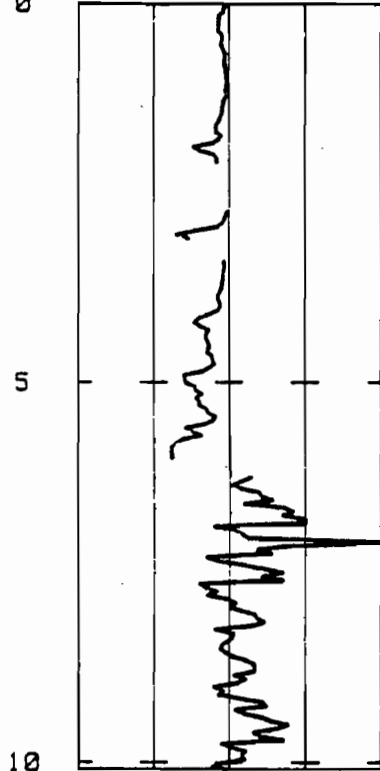
Point Resistance
0 (MPa) 20



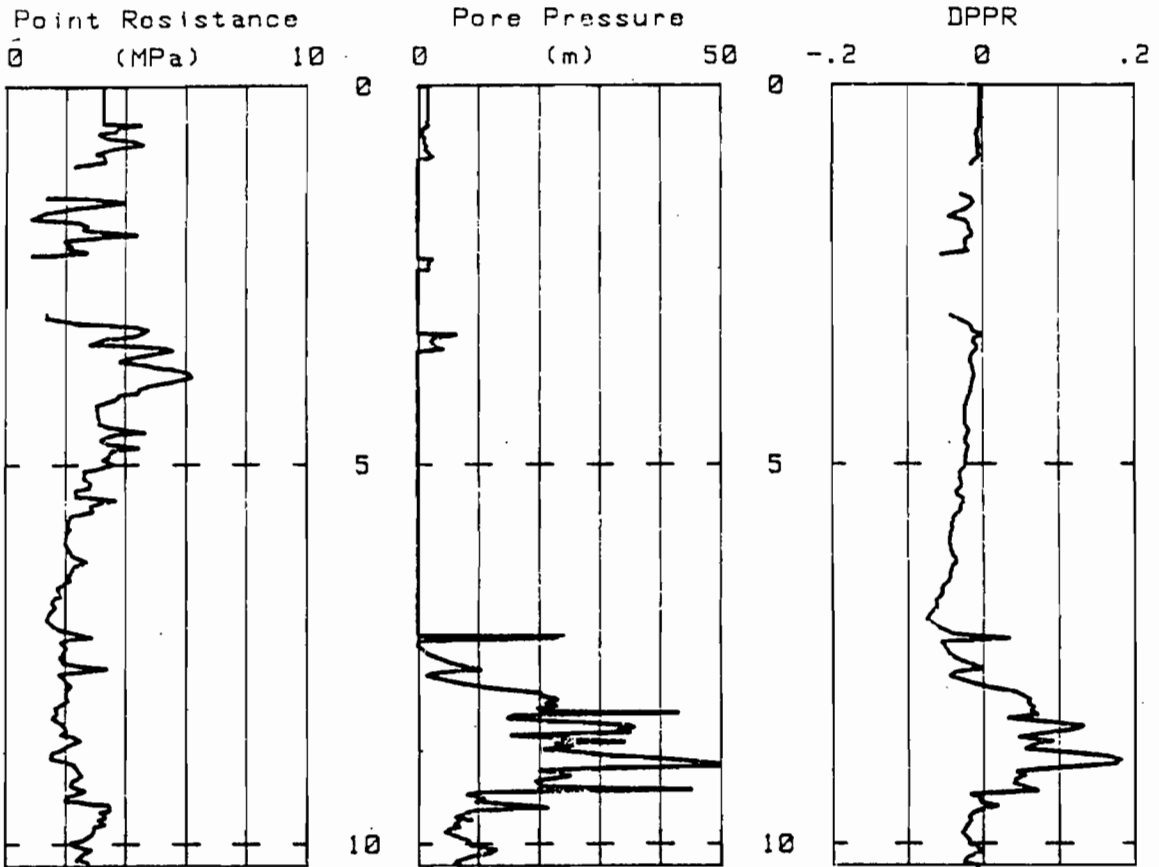
Pore Pressure
-15 0 (m) 45



DPPR
-0.2 0 .2



Location: Stokes Point Date: 83 02 08
Test No. 16 Operator: B.Morris
Code: 83SP16 Soil Penetration (m): 10.29
Water depth (m): 2.4



Location: Stokes Point

Date: 83 02 08

Test No. 17

Operator: B. Morris

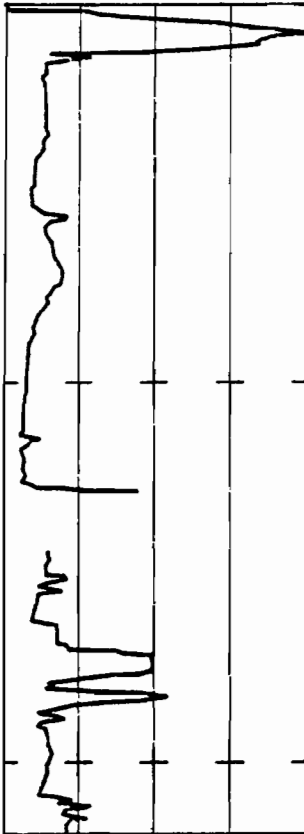
Code: 83SP17

Soil Penetration (m): 10.94

Water depth (m): 5.2

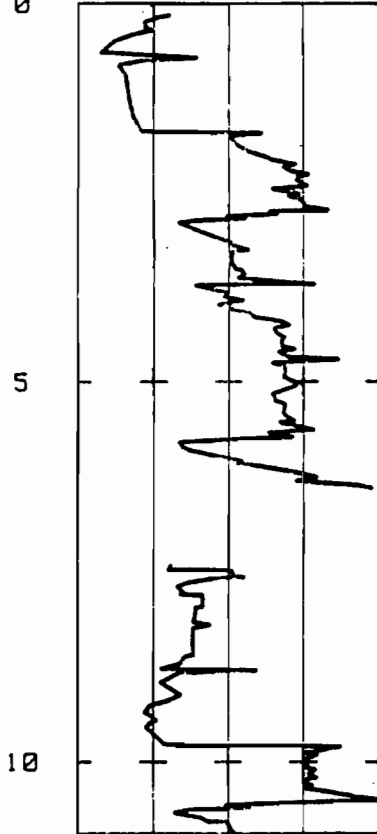
Point Resistance

0 (MPa) 10



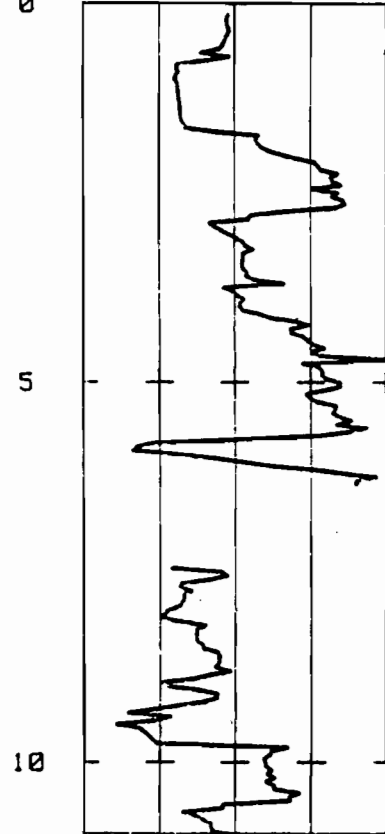
Pore Pressure

-10 0 (m) 30

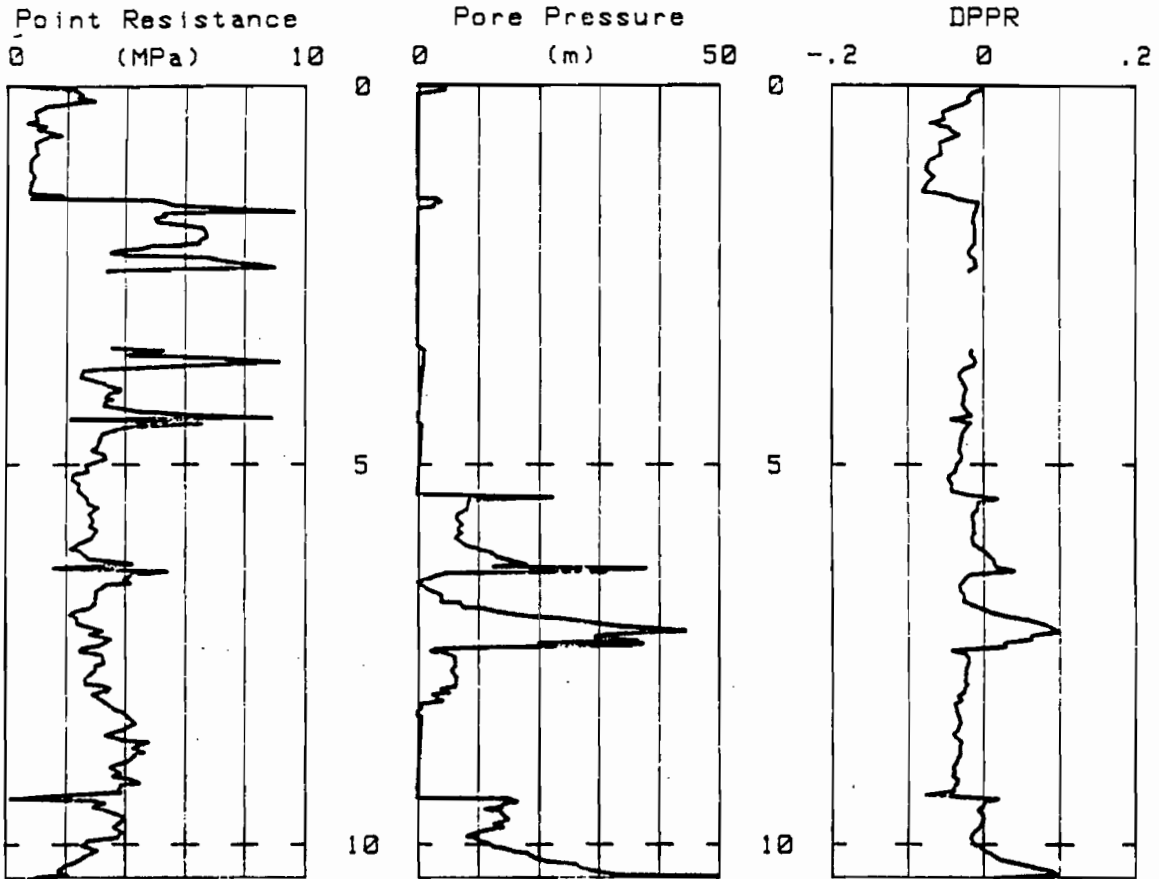


DPPR

-0.2 0 .2

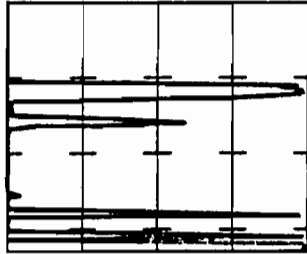


Location: Stokes Point Date: 83 02 07
Test No. 19A Operator: B. Morris
Code: 83SP19A Soil Penetration (m): 10.44
Water depth (m): 4.6

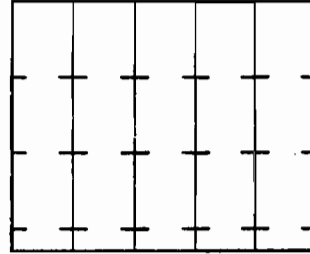


Location: Stokes Point Date: 83 02 02
Test No. 21 Operator: B.Morris
Code: 83SP21 Soil Penetration (m): 3.29
Water depth (m): 1.8

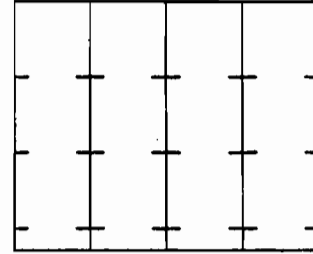
Point Resistance
0 (MPa) 20



Pore Pressure
0 (m) 50



DPPR
-1 0 1



Location: Stokes Point

Date: 83 01 30

Test No. 22

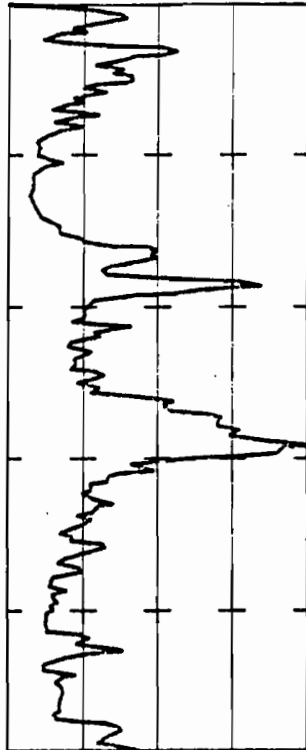
Operator: B.Morris

Code: 83SP22

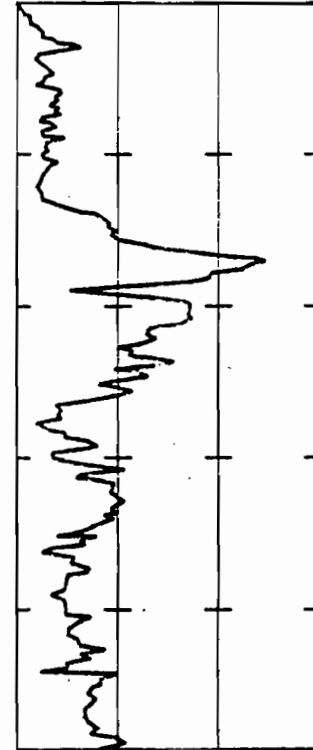
Soil Penetration (m): 9.84

Water depth (m): 5.1

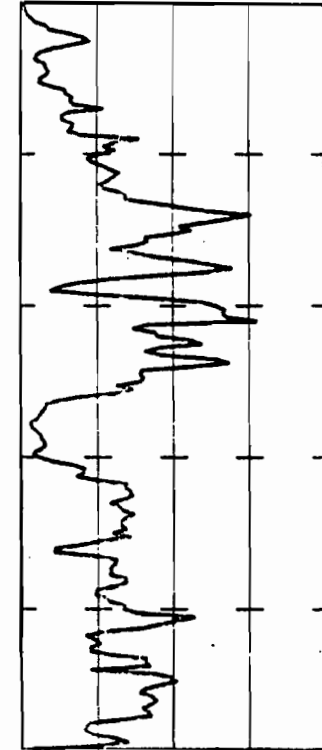
Point Resistance
0 (MPa) 10



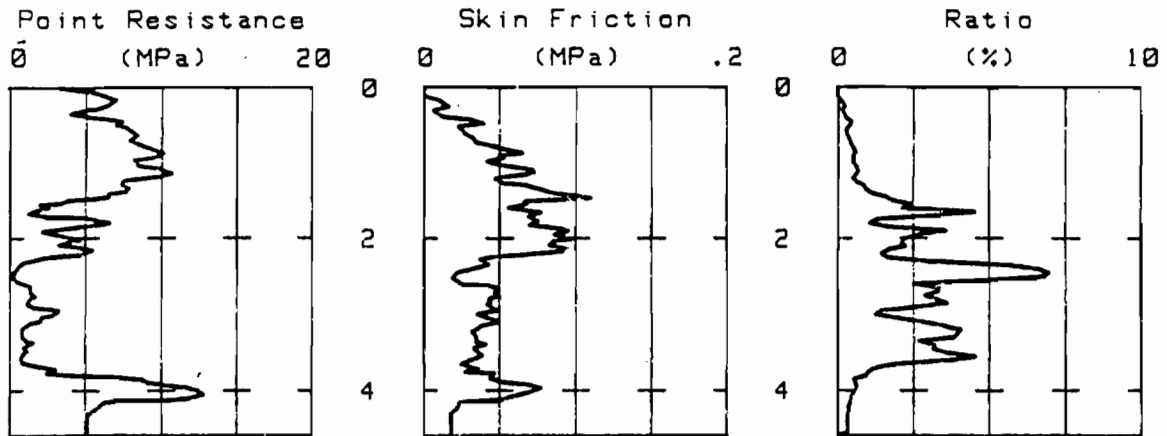
Skin Friction
0 (MPa) .3



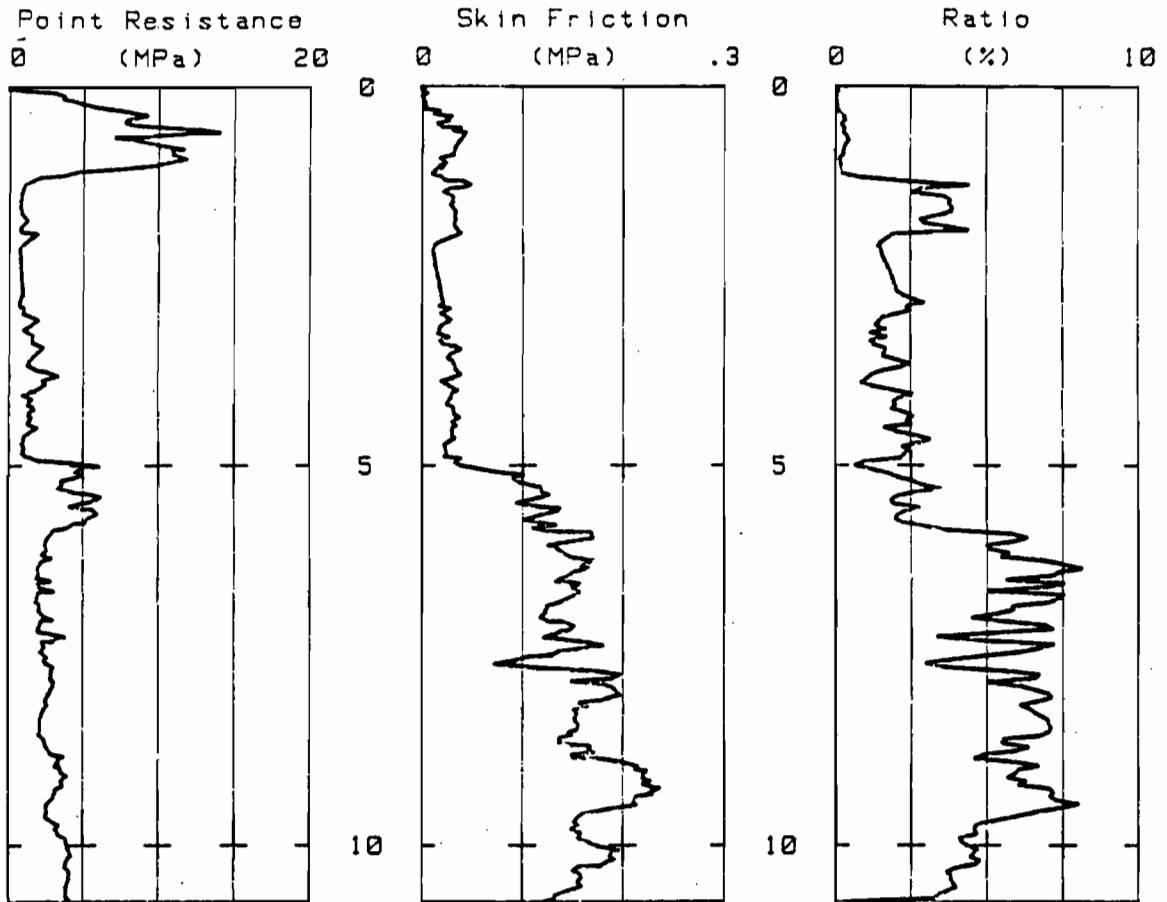
Ratio
0 (%) 10



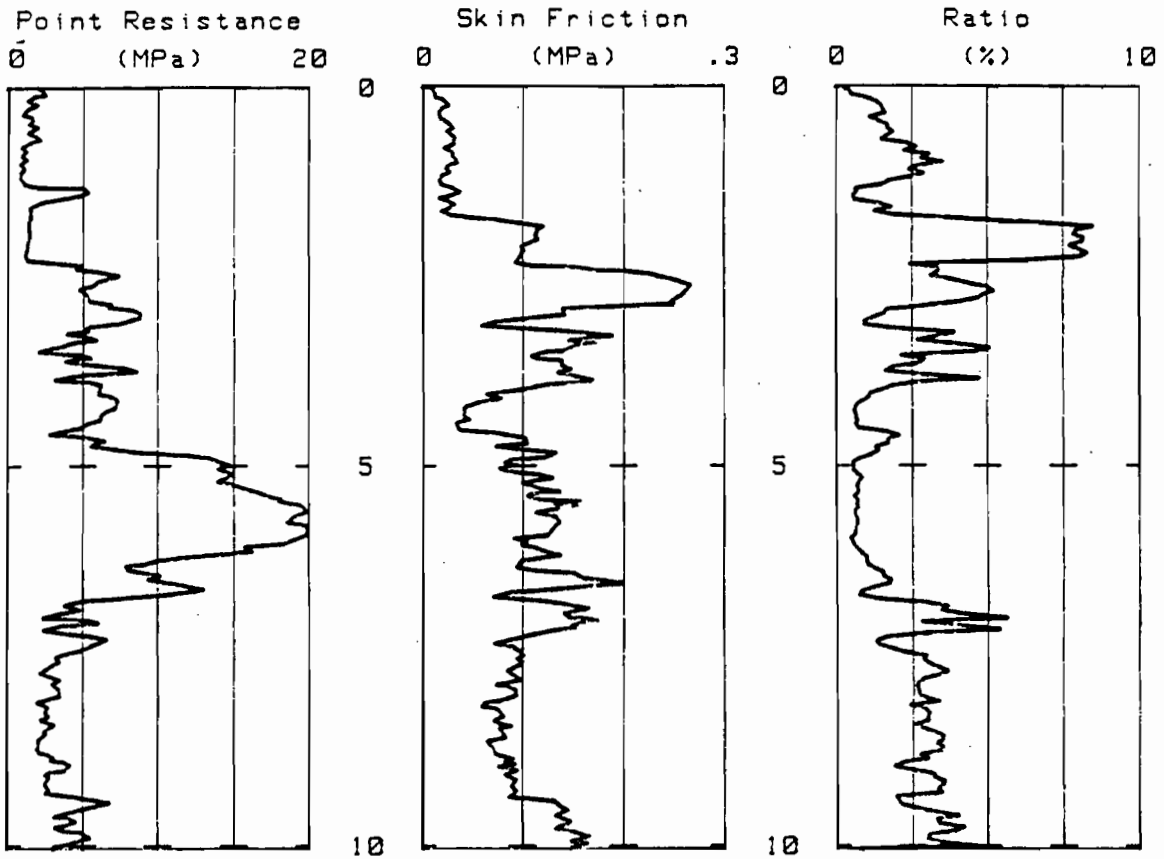
Location: Stokes Point Date: 83 01 30
Test No. 23 Operator: B.Morris
Code: 83SP23 Soil Penetration (m): 4.59
Water depth (m): 7.1



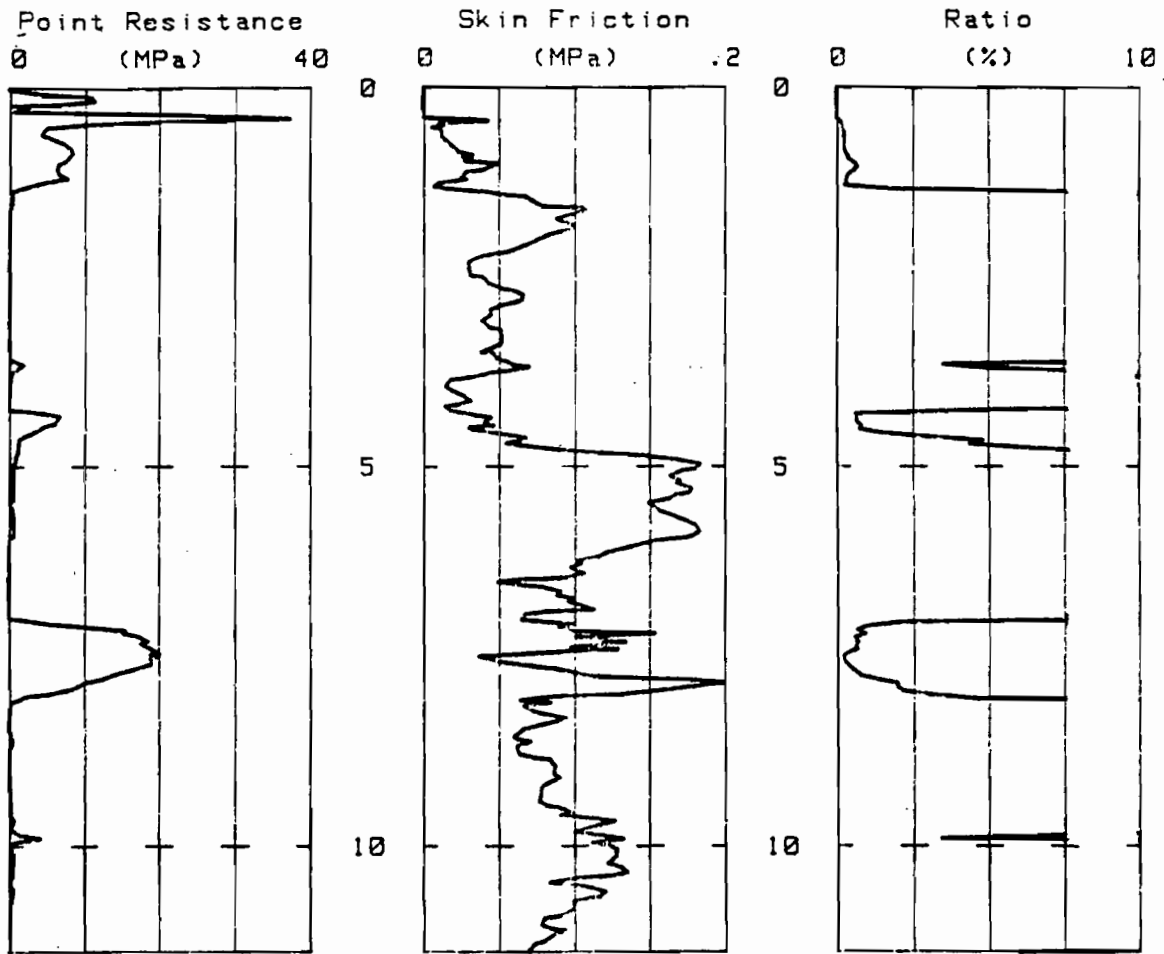
Location: Stokes Point Date: 83 01 28
Test No. 25 Operator: B.Morris
Code: B3SP25 Soil Penetration (m): 10.74
Water depth (m): 1.75



Location: Stokes Point Date: 83 01 28
Test No. 26 Operator: B.Morris
Code: 83SP26 Soil Penetration (m): 10.04
Water depth (m): 6.7



Location: Stokes Point Date: 83 01 25
Test No. 31 Operator: B. Morris
Code: 83SP31 Soil Penetration (m): 11.39
Water depth (m): 1.5



Location: Stokes Point

Date: 83 01 26

Test No. 32

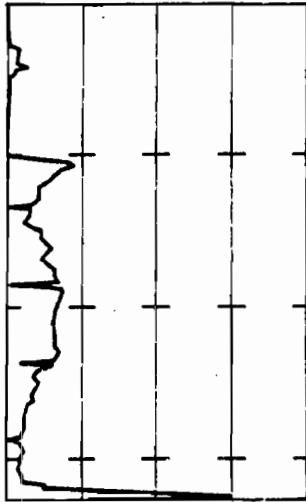
Operator: B. Morris

Code: 83SP32

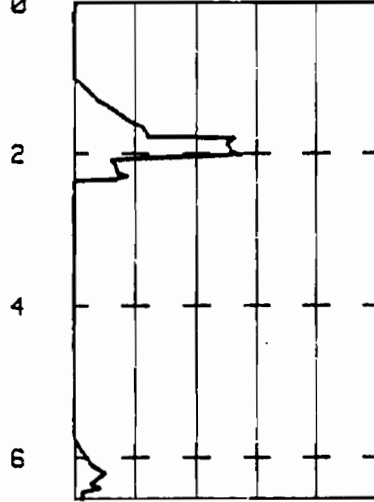
Soil Penetration (m): 6.54

Water depth (m): 7.0

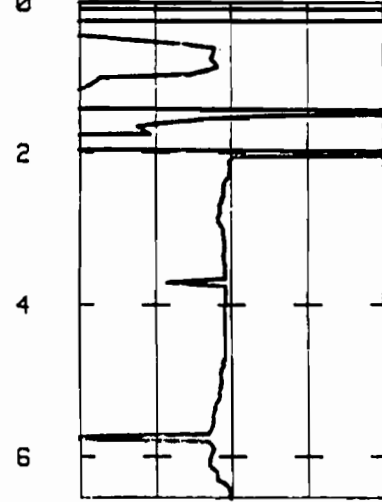
Point Resistance
0 (MPa) 20



Pore Pressure
0 (m) 50



DPPR
-1 0 1



Location: Stokes Point
Test No. 33
Code: 83SP33

Date: 83 02 03
Operator: B.Morris
Soil Penetration (m): 30.44
Water depth (m): 2.9

