VOLUME II

1975 PIPELINE BORROW INVESTIGATIONS RICHARDS ISLAND TO FORT GOOD HOPE, N.W.T.

Northern Engineering Services Company Limited

Engineering Services

Arctic Gas



VOLUME II

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1975 PIPELINE BORROW INVESTIGATIONS -

RICHARDS ISLAND TO FORT GOOD HOPE, N.W.T.

Prepared For

Canadian Arctic Gas Study Limited

Bу

Northern Engineering Services Company Limited

Calgary, Alberta

November, 1976

Project 13011

635 - 6TH AVENUE S.W., CALGARY, ALBERTA T2P 0T5 - TELEPHONE (403) 265-8500-TELEX 038-24868-TWX 821-2283

17 December, 1976

Canadian Arctic Gas Study Limited 1270 Calgary House 550 - 6 Avenue S.W. Calgary, Alberta T2P 0S2

Attention: A.W. Wirth Vice President Engineering & Construction

Reference: Volume II; 1975 Pipeline Borrow Investigations - Richards Island to Fort Good Hope

Dear Sirs,

We are pleased to submit this report which contains information on 48 borrow deposits along the Mackenzie Valley from Richards Island to Fort Good Hope in the Northwest Territories.

This work was undertaken as part of budget item 13011.

Yours truly,

NORTHERN ENGINEERING SERVICES COMPANY LIMITED

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P.H. Dau, P.Eng., President

JKW:gj

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1. SUMMARY

Granular materials in the order of 260,000,000 cubic yards have been identified and investigated along the proposed Canadian Arctic Gas Cross Delta and prime pipeline routes in the Richards Island to Fort Good Hope portion of the borrow investigation. A total of 48 deposits were investigated during the summer of 1975 by Northern Engineering Services Company Limited between Richards Island and Fort Good Hope, N.W.T. of which 35 were investigated in detail by geophysics, test pitting and drilling. The remaining 13 were investigated by geological field reconnaissance only. Geological and biological reconnaissance was used to obtain information on the location and extent, quantity, quality, biological factors, and development parameters for each of the 48 borrow deposits. Archaeology, land use, land availability and socio-economic factors were not included in the scope of the study.

This report contains descriptions of the field and laboratory results that pertain to each borrow deposit that was investigated. The detailed site specific information for each borrow deposit is presented as a complete package in the respective "Individual Site Report" under Section 11. Separate sections describing the regional geological and biological setting of the Richards Island to Fort Good Hope area, the geophysical methods used to investigate the borrow deposits, and the logistics of this portion of the borrow investigation are included in this report. As a result of this study, eight new granular material borrow deposits were located. These deposits, not documented in the Granular Materials Inventory, the Mackenzie Highway investigations or oil company borrow studies, represent approximately 16 of the 260 million cubic yards of available granular material between Richards Island and Fort Good Hope. -Northern Engineering Services -

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2. INTRODUCTION

During the summer of 1975 a borrow exploration program was undertaken by Northern Engineering Services Company Limited (NESCL) for Canadian Arctic Gas Study Limited (CAGSL) along the proposed gas pipeline route north of latitude 60° N in Canada.

Territory covered by the program included the Yukon coastal plain portion of the Coastal Route, the Cross Delta Route and the Prime Route with the East of Fort Simpson realignment.

The program obtained preliminary site specific information on potential granular borrow deposits along the pipeline (for location of individual deposits see Appendix B). Emphasis was placed on investigating sources that were outside areas covered by the DIAND Granular Materials Inventory and on gathering further information on granular deposits in previously documented areas where shortages of good quality borrow have been identified. In addition, field visits were made to borrow sources which appear in the pipeline application and further information was gathered on surface and subsurface aspects of the terrain along the pipeline.

Prior to this borrow field study, airphotos, published surficial geology maps, and DIAND Granular Materials Inventory reports were assessed to obtain information on potential borrow sources that could be used in pipeline construction. Preliminary choices of borrow sources for the pipeline and its facilities are shown in the pipeline application and in two NESCL reports entitled: "Pipeline Related Borrow Studies" (July, 1974); and "Pipeline Related Borrow Studies Cross Delta Alternative Route and East of Fort Simpson Realignment" (November, 1975).

The borrow investigation obtained preliminary information on the location of potential borrow deposits provided information concerning the nature of the deposit and provided a rough estimate of the insitu quantities of each deposit. For final design and contractual purposes this program will have to be followed by further detailed investigations. Data obtained during the 1975 field investigation are contained in this report which is preliminary and not intended for final design or contractual purposes.

The borrow field program consisted of a geological and biological reconnaissance of granular material sources followed by ground geophysical investigation, test pitting and drilling of promising deposits selected during the reconnaissance. Archaeology, land use, land availability and socio-economic factors were not included in the scope of the study. The borrow investigation from Richards Island to latitude 60° N was carried out concurrently with the 1975 wharf investigation to optimize the use of helicopters, tugboats, and fuel barges.

Organization, management, and supervision for this project were provided by NESCL. Engineering field support, field geophysical activities, and the geological reconnaissance from Fort Good Hope to latitude 60° N were carried out by NESCL personnel. The geological reconnaissance along the Yukon coastal plain and from Richards Island to Fort Good Hope was done by Dr. V. N. Rampton, P. Eng., of Terrain Analysis and Mapping Services Limited, Ottawa, Ontario. Biological reconnaissance was conducted by Mr. D. R. Wooley, Wildlife Biologist, of Renewable Resources Consulting Services Limited, Edmonton, Alberta. Samples collected in the field were tested by R. M. Hardy and Associates Limited, Calgary, Alberta. Drilling crews and equipment were supplied by Kenting

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Big Indian Drilling, Calgary, Alberta, helicopter support in the Mackenzie Delta area by Kenting Aviation Limited, Calgary, Alberta, and barge facilities by Northern Transportation Company Limited (NTCL), Hay River, N.W.T. Other groups that provided support for the borrow field program are listed in the Equipment and Personnel section of this report.

The field investigation for the borrow study started at the Alaska/Yukon border July 12, 1975, and continued to the Fort Simpson, N.W.T. area, where it was completed September 21, 1975. The report on this program has been divided into the following three volumes:

Volume I:	1975 Pipeline Borrow Investigations - Yukon
	Coastal Plain. (Published May, 1976).
Volume II:	1975 Pipeline Borrow Investigations -
	Richards Island to Fort Good Hope, N.W.T.
Volume III:	1975 Pipeline Borrow Investigations -
	Fort Good Hope, N.W.T. to Latitude 60° N.

Volume II describes the borrow investigation in the Mackenzie Delta and northern Mackenzie River valley portion of the pipeline route. The majority of this area had been previously investigated during the DIAND Granular Materials Inventory. This inventory indicated that shortages of good quality borrow material exist in portions of this region. Areas where shortages had been identified were investigated in greater detail in order to identify additional borrow sources, to obtain further information on previously explored deposits, or to locate alternative bedrock quarry sites. A total of 48 deposits were investigated during this phase of the borrow study. Thirty-five deposits were drilled and test pitted, and 13 were investigated on a reconnaissance basis. – Northern Engineering Services -

3. EQUIPMENT AND PERSONNEL

3.1 Equipment

3.1.1 Drills and Ancillary Equipment

The Kenting Big Indian Heli-Drill was used to drill test holes in the selected borrow sites. The Heli-Drill is a helicoptertransportable Mayhew 200 drilling rig mounted on a detachable base which can be levelled by means of three hydraulic jacks. The power units for the drill and air compressor consist of two Wisconsin VH4D 30-horsepower air-cooled gasoline engines which operate independently of each other. The Heli-Drill is usually transported as two packages. The first package consists of the drill frame, rotary table, draw works, mast assembly, and one power unit, and the second package consists of the drill base upon which the air compressor and the second power unit are mounted. Each of these two components weighs approximately 3400 pounds and is equipped with custom slinging cables to ensure a properly balanced load for transportation by helicopter.

All ancillary drilling equipment and tools such as drill rods, drilling bits, hand tools, and spare parts were carried in a steel mesh tool basket weighing approximately 3500 pounds. A mud pump complete with power unit was also taken into the field to provide wet drilling capabilities for the Heli-Drill. The air compressor and mud pump units are easily interchangeable.

The Kenting Big Indian Heli-Drill was selected for this borrow investigation because it can be used either with the compressed air or water circulation modes for drilling. In addition, the Heli-Drill has more versatility for handling a greater number and variety of downhole sampling tools and drill bits. The Kelly and Sand line cables were modified by double lining to provide greater pulling capabilities in the event that either the drill bit or sampling tools became lodged during removal.

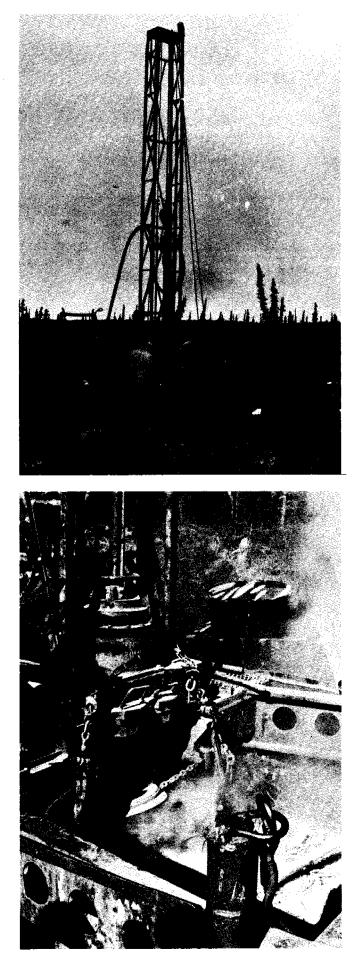


Photo 3.1.1

View of Kenting Big Indian Heli-Drill at deposit N75-107B-B15 drilling by means of airflush to prove out depth of granular material.

Photo 3.1.2

Close up view of drilling action while rig rotates on boulder.

3.1.2 <u>Test Pitting</u> Equipment

Two 150 cfm gas-powered Ingersol-Rand air compressors were used to facilitate the test pit excavations. Each air compressor was equipped with two 60-pound air hammers, 200 feet of steel reinforced rubber air hose, and an assortment of 3-inch wide clay spades and 2-inch wide asphalt spades. The air compressors and associated equipment were supplied by Modern Industrial Rentals Ltd., Calgary, Alberta and were equipped with an upper hook for slinging by helicopter. The air compressor with its complete complement of tools weighed approximately 3000 pounds.

Each test pitting crew of four men was provided with long handled spades and picks.

3.1.3 Geophysical Equipment

A complete description of the geophysical equipment used in this portion of the borrow source investigation is presented in Section 6 of this report entitled: "Geophysical Investigations of Granular Deposits".

3.1.4 Helicopters

A Bell 206B Jet Ranger helicopter, supplied by Kenting Aviation Ltd. from its Inuvik, N.W.T. base, was used for the geological reconnaissance crew. This helicopter is turbine-powered and has a capacity to carry four passengers, or sling up to 1100 pounds of cargo. In addition to ferrying the geological reconnaissance party, on occasion, the Bell 206B Jet Ranger helicopter was used to position the geophysical crew and equipment.

A Sikorsky S58E gasoline-powered helicopter provided by Kenting Aviation Ltd., with a maximum rated sling load lifting capacity of 4000 pounds, was selected to transport the Heli-Drill components,



Photo 3.1.3

Kenting Aviation Ltd. Sikorsky S58E helicopter hooking up to transport the Heli-Drill.

air compressors, bulky gravel samples, and the crews for the geophysical, test pitting, and drilling activities. The Sikorsky S58E helicopter has a very large cabin configuration which provides a very convenient, efficient and economical mode for transporting passengers, small equipment, and samples in a single air lifting operation.

3.1.5 Sampling Equipment

Test pitting was the principal method used to obtain representative granular material samples. Drilling was carried out to establish or confirm the depths of granular material at selected deposits and as a result sophisticated sampling and coring tools were not required. The air return cuttings and observation of the drilling action were used to assess the downhole conditions and evaluate the quality of material being drilled.

3.1.6 Radio Communications Equipment

The number of separate crews working concurrently at scattered locations away from the base camp necessitated a good communications network for both emergency purposes and efficient coordination of crew movements. Motorola Model PT300 lunch bucket type FM radios powered by rechargeable nickel-cadmium batteries were issued to the geological reconnaissance party, the geophysical party, the drilling crew, two test pitting crews, the Sikorsky S58E helicopter, and the base camp.

The S58E helicopter was used, almost entirely, to move the crews and their related equipment. As a result, the Motorola radio connected into the helicopter's intercom system became the field control centre for maintaining and coordinating the daily field program logistics. These portable radios proved to be invaluable for maintaining efficient operations during the course of the field program.

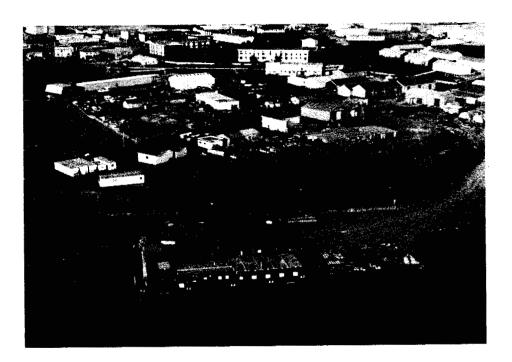
In addition, the base camp was equipped with "Very High Frequency" (VHF) and "High Single Side Band" (HSSB) radios to provide communications to the outside and southern population centres.

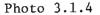
3.1.7 Accommodation and Support Facilities

The 24-man barge camp, 150-ton supply barge, Mark II Jetboat and casual tugboat charter were provided by Northern Transportation Company Limited (NTCL). The 24-man camp was specifically built and equipped to be mounted on a 300-ton river barge and contained sleeping quarters, kitchen, dinette, recreation area, radio room, washroom, laundry facilities, power plant, and general shop.

Support facilities from the Mackenzie Delta to south of Little Chicago consisted of Cessna 185 for light fixed-wing charters

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NTCL Barge Camp along with the fuel barge at Inuvik N.W.T.

and fixed-wing Twin Otter charters for larger crew changes and bulkier supply transportation. These aircraft were provided by Corridor Air Limited and Kenn Borek Airways Limited of Inuvik, N.W.T., respectively. In the region between Little Chicago and Fort Good Hope, the fixed-wing support facilities were provided by Corridor Air Limited and Nahanni Air Limited of Norman Wells, N.W.T. in their respective Cessna 185 and Beaver aircraft.

3.2 Personnel

The following personnel were involved during the borrow source investigation from Richards Island to Fort Good Hope:

Personnel 1 Project Manager 1 Project Engineer 1 Project Geologist

Affiliation

NESCL

NESCL

Terrain Analysis & Mapping Services Ltd.

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Personnel	Affiliation
l Wildlife Biologist	Renewable Resources Consulting Services Ltd.
1 Junior Geologist	NESCL
1 Geophysicist	NESCL
2 Junior Geophysicists	NESCL
2 Geotechnical Engineers	NESCL
6 Test Pitting Northern Labourers	NESCL
1 Driller	Kenting Big Indian Drilling
l Driller's Helper	Kenting Big Indian Drilling
2 Helicopter Pilots	Kenting Big Indian Drilling
2 Helicopter Engineers	Kenting Big Indian Drilling
l Cook	NTCL
l Cook's Helper	NTCL
1 Camp Attendant	NTCL
l Camp Mechanic/Radioman	NTCL
1 Tugboat Captain	Keen Industries Limited
3 Tugboat Deckhands	Keen Industries Limited

The entire field party, with the exception of the tugboat crew, was billeted on the NTCL Camp Barge for the duration of the field program. The tugboat crew had their own quarters on their tugboat. Northern Engineering Services -

4. LOGISTICS AND METHODOLOGY OF FIELD OPERATIONS

4.1 Logistics

The detailed criteria regarding the logistics for the Richards Island to Fort Good Hope portion of the borrow investigation have been documented separately in a report entitled: "1975 Summer Wharf and Borrow Investigation Logistics Summary". The field operations for the borrow study were completely integrated with the 1975 wharf investigation on the Richards Island side of the Mackenzie Delta. The results of the 1975 wharf investigation have been recorded in a report entitled: "1975 Field Investigation - Wharf Report".

Although the detailed chronological documentation of the logistics for the borrow study has been compiled separately in the above captioned report, a brief description of the logistical planning and execution of the borrow source investigation for the Richards Island to Fort Good Hope portion of the study is listed as follows:

- (a) Following the completion of the field program for the borrow study along the Yukon coastal plain on August 7, 1975 (Ref. Volume I - 1975 Pipeline Borrow Investigation -Yukon Coastal Plain), the Richards Island to Fort Good Hope portion of the borrow study was commenced on August 8, 1975.
- (b) During the night of August 7, 1975, the Barge Camp 702 was moved from its mooring at Tiktalek Channel on the west side of Shallow Bay to a new mooring on Neklek Channel immediately south of Tununuk Point. The operational logistics of the borrow field program were fully integrated with the wharf site drilling operations which had been operating from this location using Barge Camp 21 as their base.

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- (c) The field drilling, test pitting, and geophysics commenced on site N75-107C-B1 at 1.00 p.m., August 8, 1975. The borrow source field program for prospective sites on Richards Island and east to Parsons Lake was carried out from the Neklek Channel base camp.
- (d) During the night of August 11, 1975, Camps 702 and 21 were moved by the tugboat, Delta Eagle, from the Neklek Channel. Camp 702 was moored at its new location near Reindeer Station at 4.30 a.m., August 12, 1975 and the "Delta Eagle" continued to the Inuvik wharf site with Camp 21. The field program for the borrow study was carried out from Reindeer Station until the evening of August 12, 1975.
- (e) The "Delta Eagle" returned to Reindeer Station on August 12, 1975 and moved Camp 702 to the NTCL docks in Inuvik during the night of August 12, 1975 and arrived in Inuvik at 6.00 a.m., August 13, 1975. The borrow study was carried out from Inuvik until the evening of August 16, 1975.
- (f) The Camp 702 borrow field operations were moved from Inuvik on the night of August 16, 1975 and arrived at the Thunder River location on the evening of August 18, 1975. Inclement weather, which grounded the helicopters, curtailed any field operations during this two day move.
- (g) Borrow source field operations continued from the Thunder River location until August 26, 1975.
- (h) Camp 702 was moved from Thunder River to Wharf site 15, near the Loon River confluence north of Fort Good Hope, during August 26 and 27, 1975. The borrow source field operations were maintained during this two-day move.
- (i) The remaining field work on the selected borrow sites north of Fort Good Hope was carried out, using Camp 702 at Wharf Site 15 as a base of operations.

(j) The field work on the Richards Island to Fort Good Hope portion of the borrow study was completed on August 29, 1975.

4.2 <u>Methodology</u>

4.2.1 Literature Review and Office Study

Pertinent geological information from various studies such as the Geological Survey of Canada maps and reports, the DIAND Granular Materials Inventory, pipeline alignment sheets, private industry reports, and previous NESCL project reports were compiled and assessed for the Richards Island to Fort Good Hope portion of the study area. These served as background for airphoto mapping of prospective granular material deposits. Deposits were selected for further investigation according to their position relative to the proposed pipeline right of way, their position relative to major stream valleys, the amount of overburden covering the granular material, and the anticipated quality of the insitu granular material. Special efforts were made to prove out granular deposits in areas previously identified as having shortages of granular materials.

4.2.2 Geological Field Reconnaissance

The airphoto interpretation and office studies served as a basis for planning and conducting the preliminary geological field reconnaissance. A senior geologist and a geological technician carried out the site by site ground check of each potential borrow source which had been selected by airphoto interpretation. The outlines of the prospective borrow sites were delineated on the corresponding airphoto along with any additional salient features of the deposit. The exact location of the test pits, drill holes, and transects for ground geophysics was specified and designated during this reconnaissance for each borrow site selected for additional investigation.

A project biologist accompanied the geological reconnaissance group to provide a biological assessment. A biological overview of the region is provided under Section 7.

4.2.3 Field Investigation

On the basis of the geological reconnaissance and the time period available to complete the detailed field investigation for the Richards Island to Fort Good Hope study area, a total of 35 borrow deposits were selected for test pitting, drilling and geophysics. This schedule was based on the completion of two borrow deposits each work day. An additional 13 borrow deposits were ground checked during the geological reconnaissance.

Generally, two to three test pits per borrow deposit were completed by the two test pitting crews consisting of three northern labourers for each crew. The supervision of the two test pitting crews, sampling and logging was carried out by a junior geotechnical engineer. The test pits excavated were generally 4 by 6 feet in area, and extended from 4 to 10 feet in depth. The 60-pound hammers, powered by compressed air, were used to extend these test pits beneath the permafrost table. In general, the test pits were selected in areas where the active layer was thought to be the deepest to minimize the need for compressors. All organic peat and/or vegetation material on the surface of the test pit location was carefully removed and replaced after the test pit had been backfilled.

When the test pit had been excavated to the desired depth, a representative sample of granular material was taken from the exposed vertical wall of the test pit. These samples generally I

weighed 400 to 500 pounds and were contained in six to ten sample bags. The material was retained in heavy plastic bags in order to minimize the loss of moisture content and fines. In addition to the samples, a photographic record of one vertical face of the test pit was taken in a series of frames from the surface to the bottom of the pit. These photos are on file at NESCL.



Photo 4.2.1

Typical view of a test pit excavation at deposit N75-106P-B3.

The depth of selected borrow deposits were checked by drilling in areas that were representation of the deposit. A helicopterportable "Heli-Drill", which is described in detail in Section 3 of this report, was used. In general, the drill holes were located where the active layer was shallowest in order to minimize

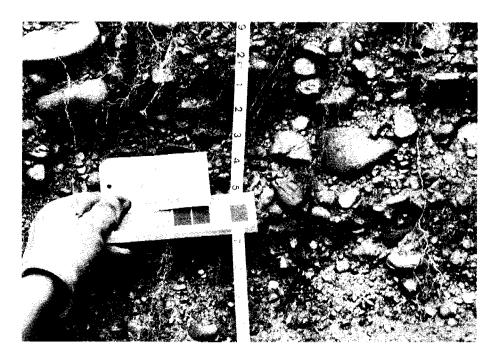


Photo 4.2.2

Typical view of a test pit side wall at deposit N75-107C-B2.

caving and "blow out" problems during the drilling operations. An open-hole air circulation technique was used primarily, although a wet circulation capability was available on this drilling rig. The subsurface logging was conducted by observing the air flushed cuttings and the downhole drill action.

The ground geophysics conducted at each borrow deposit were carried out by a three-man crew. The details and the results of the geophysical investigation are included in Section 6 and Appendix "C" of this report.

4.2.4 Laboratory Testing

The entire series of test pit samples obtained for this portion of the borrow study were forwarded to R.M. Hardy and Associates Limited, Calgary, Alberta. The following laboratory tests were carried out:

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-Northern Engineering Services

(a)	Mechanical Grain Size Analysis	ASTM C	136 - 71
(b)	Moisture Content	ASTM C	566 - 67
(c)	Petrographic Analysis	ASTM C	295 - 65
(d)	Los Angeles Abrasion Test	ASTM C	131 - 69
(e)	Sulphate Soundness Test	ASTM C	88 - 73
(f)	Organic Content	ASTM C	40 - 73

The schedule of samples to be tested, and the types of tests to be conducted on each sample, were provided to R.M. Hardy and Associates Limited by NESCL. The results of the laboratory tests are included in the individual site reports.

It should be noted that none of the drill hole logs were verified by laboratory testing.

4.2.5 <u>Report Format</u>

The site specific information for each potential borrow deposit is incorporated in the "Individual Site Reports", which is outlined in Section 11 of this report.

5. REGIONAL GEOLOGY AND GEOMORPHOLOGY OF THE RICHARDS ISLAND TO FORT GOOD HOPE AREA

5.1. General

The study area includes parts of the Arctic Coastal Plain and Anderson Plain. That part of the Arctic Coastal Plain covered by this study consists of three parts:

- (a) the Pleistocene Coastlands, an extensive lake dotted lowland 50 to 200 feet above sea level, which is underlain by thick Pleistocene deposits;
- (b) the Caribou Hills, a rolling upland, much of which is over 500 feet above sea level and which is underlain by relatively soft rock formations; and
- (c) the Mackenzie Delta, a flat, deltaic plain covered by a maze of lakes and channels, which is developed on postglacial fine-grained unconsolidated sediments.

The Anderson Plain north of 68° latitude is a gently undulating to flat upland, which rises from 200 feet at its northern edge to 800 feet plus near North Caribou Lake. The northern section, called the Campbell Lake Hills, is interrupted by a broad trench incised into bedrock and occupied by Campbell Lake. South of 68° latitude to near Yeltea Lake, the Anderson Plain is still broadly undulating, but is commonly above 1000 feet elevation. Bedrock is exposed along the edges of numerous broad valleys. The Anderson Plain is lower and flatter between Yeltea Lake and Fort Good Hope, generally between 200 and 700 feet elevation, and has fewer incised valleys. The southwest edge of the Anderson Plain is defined by the Mackenzie River trench, which is occupied by the river and adjacent low flat benches.

5.2 Bedrock

Tertiary strata lies well over a hundred feet below the ground surface in the Pleistocene Coastlands, but rises to near the surface under the northern part of the Caribou Hills, where interbedded, poorly consolidated Tertiary conglomerates, sandstones, and mudstones are exposed along most escarpments. The southern end of the Caribou Hills is underlain by Cretaceous shales.

The Campbell Lake Hills north of Campbell Lake are erosion resistant Precambrian quartzites and argillites and Paleozoic carbonates. South of Campbell Lake, the terrain is primarily underlain by Cretaceous and Devonian shales and sandstones with more competent sandstones often capping plateaus. East of Thunder River bedrock is middle Devonian limestones and shales, frequently capped by Cretaceous shales and sandstones. The Devonian limestones and more resistant Cretaceous sandstones are frequently cliff formers.

5.3 Surficial Deposits

The Mackenzie Delta is formed primarily of organic silts and sands. The surface of the Delta is marked by not only delta channels, but numerous thermokarst lakes and shallow depressions.

Most of the Pleistocene Coastlands and Campbell Hills are blanketed by either morainal or glaciofluvial deposits, or thermally modified versions of these materials as they were glaciated in early Wisconsin time. Outwash deposits are concentrated near Ya-Ya Lake, the East Channel of the Mackenzie River, the northern edge of the Caribou Hills, east of Parsons Lake, and adjacent to the Eskimo Lakes. Most of the remaining area is covered by 5 to 20 feet of till, or lacustrine deposits of thermokarst origin. During deglaciation of the Caribou Hills, drainage was often blocked and a thin blanket of glaciolacustrine silt and clay covers earlier glacial deposits in lower areas. Materials of variable texture are generally capped by 5 to 10 feet of ice-rich silt and peat in depressions and on flat areas.

Throughout the western part of the Pleistocene Coastlands and in the broad depressions within the Caribou Hills, the previously described glacial and postglacial sediments are underlain by a thick sequence of interbedded fluvial and deltaic sands and marine clays. The marine clays of this sequence are found mainly on the northwest part of Richards Island.

The hummocky topography of the Pleistocene Coastlands and parts of the Caribou Hills results from the variable ice content of surface sediments. Most hills are underlain by sediments

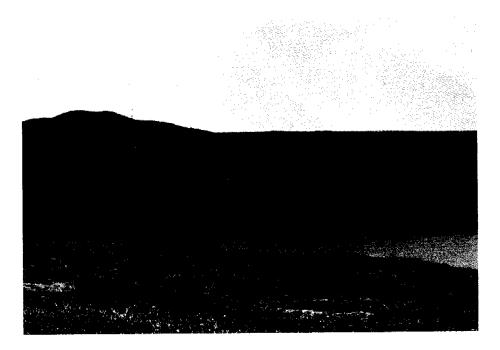


Photo 5.3.1

Potential borrow deposit located in the tundra area near Parsons Lake N.W.T.

containing very icy sediments or massive ice layers, whereas sediments underlying depressions contain less ice. The ice layers underlying the hills were melted by thermokarst processes during the formation of the depressions.

The Campbell Lake - Stitidgi Lake lowlands contains glaciolacustrine clays capped by a blanket of peat. The southeastern flank consists of fluted bedrock and drumlinized till with a few eskers paralleling the northeast trending drumlins and flutes. A peat layer blankets the drift over much of this area.

Moraine ridges, kame complexes, and outwash deposits define the irregular margin of a former glacier ("classical Wisconsin" limit) from southeast of Sitidgi Lake east past Travaillant Lake to southeast of Tutsieta Lake. This glacial limit was largely controlled by bedrock relief. The outwash is generally in the form of valley trains that occupy broad valleys incised in bedrock and leading ultimately to the Kugulak and Anderson Rivers.

The terrain between Campbell Lake and Fish Trap Lake is rolling to hummocky moraine with patches of organic material. Southeast of Fish Trap Lake to near Yeltea Lake, till and colluvium varying in depth from 5 feet to greater than 50 feet cover a highly dissected bedrock surface. Surficial deposits are thickest in the broad incised valleys and depressions. Glaciolacustrine deposits are scattered throughout the lowlands and depressions. Peat is confined to poorly drained depressions and broad flat areas.

The hummocky to rolling nature of some glacial deposits between Campbell Lake and Yeltea Lake is most often due to the presence of icy sediments and massive ice under hills, and relatively low in content of sediments underlying intervening thermokarst depressions.

South of Yeltea Lake, most of the Anderson Plain is covered by till, 3 to 40 feet thick, in the form of a morainal plain. In

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major valleys, such as those occupied by the Loon and Hare Indian Rivers, till overlies thick preglacial sands and gravels. Discontinuous glaciolacustrine sediments and glaciofluvial sands overlie the till in both these valleys and peat is common in poorly draied depressions. A major esker-kame complex parallels the lower Hare Indian River.



Photo 5.3.2

Potential borrow deposit located in the forested area north of Fort Good Hope.

Benches along the Mackenzie River trench are covered by up to 150 feet of glaciolacustrine silt and clay and are frequently capped by sand. On higher benches, hummocky moraine is present and only the lower areas of the benches are veneered by lacustrine deposits. Peat is common in poorly drained broad depressions. The previously mentioned glacial deposits often overlie preglacial sands and gravels. Alluvial fan deposits and kame terraces are often present adjacent to the base of the escarpment bordering the Mackenzie River trench.

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5.4 Permafrost and Ground Ice

The study area lies within the zone of continuous permafrost north of Thunder River. Taliks exist under most water bodies. The active layer is generally one and two feet thick under areas with thick turf or peat cover. Under exposed gravels on south facing slopes it increases to about 6 feet thick just north of Inuvik, but is again shallower in the treed area just south of Inuvik. However, thaw depths in well drained gravels near Travaillant Lake often exceed 10 feet.

South of Thunder River widespread discontinuous permafrost is present. Active layers are shallow, 1 to 3 feet deep, in areas covered by thick turf or peat but are in excess of 12 feet under well drained gravel deposits. Some ridges and well drained slopes may be free of permafrost near Fort Good Hope. Imperfectly drained sand or gravel with a thin peat or organic cover have active layer depths of 3 to 10 feet.

Ground ice in the form of tabular bodies of massive ice is common under many hills and ridges in the area north of Inuvik. Although ice is most common at the contact between till or finegrained deposits and the underlying sand or gravel, it is not restricted to this horizon and may occur within any unconsolidated material at variable depths to at least 200 feet. Many glaciofluvial deposits are known to contain or overlie massive ice of this type. Ice lenses, are common in tills and finetextured materials in this area; commonly these deposits contain about 20 percent excess ice with somewhat higher ice contents near the base of the active layer. Sandy outwash also frequently contains thin ice lenses. Ice wedges occur in all materials.

Tabular bodies of massive ice, ice lenses, and reticulate ice are plentiful in lacustrine deposits as far south as Fort Good Hope. Till generally contains a concentration of ice lenses in the upper 5 feet that can form as much as 25 percent of the total

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sediment volume. However, tabular bodies of massive ice in till seems to be confined to areas north of Thunder River. In this same area, irregular bodies of massive ice may also be present in sandy and silty fluvial and glaciofluvial material. Ice wedges are still present in materials having shallow active layers, but are absent or negligible in gravels having active layers of 8 feet or more.

5.5. Regional and Local Drainage

The Hare Indian and Loon Rivers are the only rivers of any significant size that drain into the Mackenzie River in the Richards Island to Fort Good Hope section. Other streams are minor as most of the drainage is north to the Anderson, Kugaluk, and Miner River systems. The Mackenzie River, itself, forms a maze of distributaries throughout the Mackenzie Delta, although major discharge is confined to larger channels. The East Channel of the Mackenzie River leaves the Delta at Tununuk separating Richards Island from the mainland.

On the Pleistocene Coastlands and flatter parts of the Caribou Hills, small beaded creeks flow between lakes and many areas seem to be drained through seepage along icewedge trenches. These trenches are characteristic of polygonal ground common to depressions and swales. On areas with gentle regional slopes such as higher portions of the Caribou Hills and much of the Anderson Plain, local drainage appears to be through seepage along fen-filled valley bottoms or shallow drainageways which lack a definite stream channel. In valleys where a clearly defined stream channel is present, low terraces are often not integrated into the stream drainage and are characterized by standing water on their surfaces. On outwash plains, old channels are also poorly drained and covered by fens and wet meadows.

5.6 Granular Materials

Granular materials in the study area are concentrated in the following environments:

- The Ya-Ya esker and associated outwash deposits on Richards Island.
- (2) Kame terraces and complexes along the northern edge of the Caribou Hills.
- (3) Exhumed Tertiary gravels throughout the Caribou Hills.
- (4) Kame complexes between Parson's Lake and the Eskimo Lakes.
- (5) Eskers and kame terraces along the southeastern edge of the trench occupied by Campbell Lake.
- (6) Numerous kame complexes, kame deltas, and outwash plains that are associated with a glacier limit that can be traced from southeast of Sitidgi Lake past Travaillant Lake to southeast of Tutsieta Lake.
- (7) Kame terraces along the edge of the Mackenzie River trench.
- (8) Loon River fluvial terraces.
- (9) An esker-kame complex northeast of Fort Good Hope.

Northern Engineering Services

6.

GEOPHYSICAL INVESTIGATIONS OF GRANULAR DEPOSITS

6.1 General

Gravel deposits can often be delineated from surrounding soils by measuring the electrical resistivity of the ground. Figure 6.4.1 shows the resistivity ranges of the soil types of the Unified Soil Classification System. Clean gravels (GP) have a resistivity in excess of 1000 ohm-m, gravels with fines (GC) have lower resistivities. It is often difficult to differentiate sands from gravels by resistivity measurements.

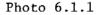
The relatively simple situation, shown in Figure 6.4.1, becomes considerably more complex in permafrost regions. Figure 6.4.2 shows the variation in resistivity with temperature for several soil types; when the ground freezes the resistivity increases; and for gravels, this increase is sudden. The trend of a resistivity increase, in going from clay to silt to gravel, is maintained when the ground is in the frozen state. However, in addition to temperature the ice content of the ground influences resistivity, as is illustrated in Figure 6.4.3. High resistivity (> 5000 ohm-m) in permafrost regions can, therefore, be due to low ground temperatures, high ice content and frozen gravel.

Thus, the resistivity of gravel deposits depends, in addition to soil type, on temperature and ice content. The value of resistivity over a frozen deposit can, therefore, not be used as a criteria for soil type without correlation to borehole data.

Often the best use of geophysics in borrow inventory programs is in delineating the extent of granular deposits and extrapolating subsurface information between boreholes. This requires that many geophysical soundings are made, so that a clear indication is obtained of the relative values of resistivity on and around granular deposits. During this investigation only a few (1 to 3) measurements were made near or on a deposit, and the results of geophysical surveys were, therefore, often inconclusive.

Resistivity surveys, particularly in the Arctic, require electromagnetic rather than electrical methods. In electrical methods, the contact resistance of probes inserted in the ground has to be kept low. Establishing low contact resistance is difficult on permafrost. Also very small lateral variation in depth of active layer can have very large effects on electrical resistivity measurements. Electromagnetic methods have significant advantages over electrical methods in resistivity surveying in the Arctic. Electromagnetic methods for shallow exploration (\sim 30 ft) were still under development at the time of the borrow program. Non-contact electromagnetic methods for shallow exploration became available shortly after the conclusion of the borrow investigation.





Geophysical resistivity instruments set up at a potential borrow deposit in the Noell Lake area just north of Inuvik N.W.T.

6.2 Resistivity Results

During the borrow investigation, two geophysical measurements were made:

- (a) vertical soundings with four probes (galvanic) in a Schlumberger array,
- (b) VLF radiohm resistivity measurements.

Because vertical soundings with probes is a relatively slow process, there was only time for a few soundings. From these data it has been difficult to draw a reliable interpretation about soil types at granular deposit sites.

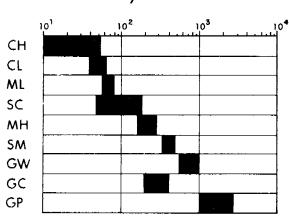
The VLF radiation has a depth of penetration that is too deep for shallow exploration. VLF radiation in the area investigated in this volume mainly reflected depth of frozen ground or depth to bedrock.

Because the geophysical measurements, employed at the time of the survey, were of limited value to this program, and were not used in either determining the extent or depth of the deposits, the data are not included in this volume.

Shortly after the field program for the borrow investigation was completed, electromagnetic equipment designed for shallow exploration became available. The equipment was tested, for its ability to delineate granular deposits in five existing deposits in the Calgary area. The results of these tests are given in Appendix C. The equipment described and tested in Appendix C has the following advantages over the conventional methods used in the borrow investigation:

(a) productivity of surveying increased by at least a factor 10, so that a deposit can be quickly scanned.

- (b) depth of exploration limited to depth of interest (20-30 ft),
- (c) local resolution of ground conditions (10-15 ft), so that changes in subsurface conditions are mapped with a resolution of 10-15 ft.



/ (ohm-m)

FIGURE 6.4.1

THE RANGES IN RESISTIVITY ASSOCIATED WITH THE SOIL TYPES OF UNIFIED ENGINEERING CLASSIFICATION SYSTEM. (CH-FAT CLAY; ML-SILTY CLAY; SC-SANDY CLAY; MH-SILT; S-SAND; GW-WELL SORTED GRAVEL; GC-GRAVEL WITH CLAY; GP-POORLY SORTED GRAVEL).



CANADIAN ARCTIC GAS STUDY LIMITED

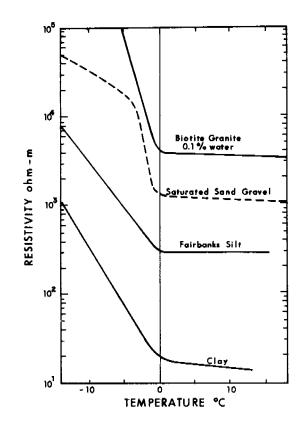


FIGURE 6.4.2. THE RESISTIVITY OF SEVERAL SOILS AND ONE ROCK TYPE AS A FUNCTION OF TEMPERATURE (HOEKSTRA ET AL., 1975)²



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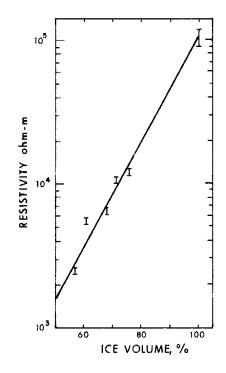


FIGURE 6.4.3. RESISTIVITY OF FROZEN SILT AS A FUNCTION OF ICE CONTENT (HOEKSTRA ET AL., 1975)²



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7. BIOLOGICAL OVERVIEW - RICHARDS ISLAND TO FORT GOOD HOPE

7.1 Vegetation

The vegetation along the proposed route is transitional between treeless tundra on the Mackenzie Delta and coniferous boreal forest on the Anderson Plain, consisting mainly of open stands of low spruce with an extensive ground cover of lichen. A more detailed description of the vegetation of the Mackenzie Delta is found in Corns (1974), while Rowe (1972) and Zoltai and Pettapiece (1973) provided descriptions of the vegetation of the Anderson Plain.

The tundra vegetation of Richards Island and the Caribou Hills consists mainly of a low shrub-heath type on drier sites, with sedge-cottongrass-heath and raised centre polygon types in wetter depressional areas. Common species found here include dwarf birch, willow, alder, Labrador tea, lingonberry, crowberry, sedge, cottongrass, lichen, and moss.

The forest-tundra transition extends south on the Anderson Plain from the Caribou Hills to the Thunder River. The vegetation consists of a mosaic of stunted forest usually along the shores of lakes, streams, and rivers, separated by patches of tundra vegetation including polygon areas. The primary species are black and white spruce and tamarack, accompanied by alder and willow shrubs. The pattern shows a gradual change from north to south as forest expands and tundra shrinks.

South from the Thunder River to Yeltea Lake an open subarctic woodland predominates. Areas of bog and fen are intermixed with open stands of dwarfed trees. Characteristic of the park-like coniferious stands on upland sites is a ground cover of lightcoloured lichens. The most abundant species on all sites is

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black spruce and associated with it on well drained soils are white spruce and white birch, while tamarack is usually found on poorly drained soils.

A closed coniferous forest is characteristic from Yeltea Lake to Fort Good Hope. On some well drained soils, especially beside the Tieda, Loon, and Hare Indian rivers, white spruce attains sawlog size, but in general, stunted white and black spruce with willow and alder prevail over large areas of poorly drained soils. White birch is commonly found on well drained upland soils. Non-forested land is made up of bogs, fens, and recently burned areas.

7.2 Mammals

The distribution of mammals in this area varies along the tundraforest gradient. In the north, on Richards Island and in the northern portion of the Caribou Hills, grizzly bear, Arctic fox, reindeer and Arctic ground squirrel are found whereas moose, beaver, caribou and marten are found in the forested areas.

Richards Island is an important denning area for grizzly bears. Protection of denning habitat is important because of the low productivity and restricted range of the grizzly bear. Black bear dens have been identified in the Thunder River valley and along the banks of the Mackenzie River (Slaney 1974).

Muskrats are found in most lakes, but prefer lakes with high banks as found in upland portions of Richards Island and in the Parsons Lake area (Slaney 1974).

White foxes are common on the coast of Richards Island and red foxes are abundant inland. All dens found by Slaney (1974) on Richards Island were considered to be red fox dens. Of 45 dens located in 1972-73, 29 were found in sandy soil, 12 in sandy/loam soils and 4 in gravel.

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Sparse beaver populations are found throughout the study area. Habitat near the proposed pipeline in the area north of treeline was designated by Dennington *et al.* (1973c) as Class IV (insignificant) with the exception of Holmes Creek. South of treeline wetland complexes such as the Campbell-Sitidgi Lakes lowland are Class III (poor quality) habitat. Class III beaver habitat is associated with wetland complexes which are more numerous south of Travaillant Lake. One such area north of Payne Creek is Class II (intermediate quality).

The best moose habitat in this region occurs on islands in the Mackenzie River which are Class I (good) moose wintering range (Prescott *et al.* 1973). Apart from these areas, moose habitat is generally of low quality along the proposed pipeline route north of Fort Good Hope. The Hare Indian River and a small wetlands complex immediately northwest of the Hare Indian River are Class III (poor) moose wintering habitat. The only other Class III moose habitat along the pipeline route between Fort Good Hope and Richards Island is found in the Campbell-Sitidgi Lake lowlands and in the Holmes Creek area. The balance of the area is Class IV (insignificant or nil) moose wintering range. Moose range throughout the area north of Holmes Creek during the summer period.

Three subspecies of caribou are found in this region. Woodland caribou are scattered throughout the forested portion of the region. A population of 1000-2000 caribou of undetermined subspecies has been estimated for the Travaillant-Husky lake area (Canadian Wildlife Service 1973). Part of the Bluenose herd winter in the Travaillant Lake area. Evidence presented in the Berger Inquiry (1975) relating to ongoing studies by the Canadian Wildlife Service, indicates an estimated population of 94,000 animals to be extending their winter range westward. Semidomesticated reindeer are herded north of Inuvik and moved from summer range on the Tuktoyaktuk Peninsula to winter range near tree line in the Parsons Lake area. Other species such as the marten, mink, and red squirrel are found primarily south of tree line.

7.3 Birds

The diverse vegetation types found in the area provide a variety of habitat for birds, with a pronounced north-south gradient in species diversity influenced by the transition from tundra to forest vegetation. Richards Island is a staging and migration area for waterfowl and is considered Class 2b (good) to Class 2a (very good) waterfowl habitat. Habitat quality declines southwards and is replaced by Class 3a (poor), 4a (marginal), and 4b (insignificant to nil). South of the Campbell and Sitidgi lakes, the quality of waterfowl habitat declines to Class 3a to 4b with small areas of better habitat becoming more scattered.

Land birds increase in species diversity from north to south, (Salter and Davis 1974) in response to increased diversity of terrestrial habitats. Although the diversity of land birds increases, the density does not increase.

Snow geese utilize the outer Mackenzie Delta as far as the western edge of Richards Island for staging (Tull 1975). The only breeding area for geese (predominantly white-fronted geese) recorded along the pipeline route outside of the Mackenzie Delta is the section from Richards Island to Noel Lake. Breeding whistling swans utilize portions of Richards Island. Densities of 1.2 swans per square mile were recorded in 1975 (Tull 1975).

Ducks are found in relatively high densities along the proposed route south of the Mackenzie Delta, south of Travaillant Lake and east of Travaillant Lake. Most common species include oldsquaw, goldeneye, greater and lesser scaup, widgeon (in forested areas), and pintail. Loons, particularly the Arctic loon, are common along the route south of Richards Island and south of Travaillant Lake (Tull 1975). Numerous loons were observed during this field survey on lakes adjacent to potential borrow sources.

The only known peregrine falcon nests within two and one-half miles of the route or potential borrow sources are in the Campbell Lake Hills. There are no known gyrfalcon nests within two and one-half miles of the route (Tull 1975).

7.4 Fish

All major streams and rivers crossed by the route and in the vicinity of potential borrow sources support fish populations. Some rivers have potential for overwintering fish populations, including the East Channel of the Mackenzie River, Loon River, Thunder River and Hare Indian River. Other important fish habitat in the area is associated with large deep lakes, such as Noell Lake and Travaillant Lake where grayling, lake trout, whitefish, and cisco occur. Available fisheries information is provided in the individual site reports.

8. DATA PRESENTATION

8.1 Individual Site Reports

8.1.1 General

The data has been presented so that all information related to a given borrow deposit is available as an individual package. The information includes:

- (1) Airphoto and Summary
- (2) Site Report
- (3) Test Pit and Test Hole Logs
- (4) Laboratory Test Data

8.1.2 Airphoto and Summary

An airphoto and synoptic page introduces each individual site report. The physical outline of the borrow deposit, location of test pits and/or test holes, and the proposed pipeline route are noted on the airphoto. A brief summary outlining the Physical Setting, Material, Volume, and Assessment for each individual deposit is denoted on the airphoto page.

8.1.3 Site Report

All pertinent data and assessments which have been compiled for the potential borrow deposits investigated from Richards Island to Fort Good Hope are discussed and presented on a site specific basis under the following headings:

 (a) <u>Physical Setting</u> - location of deposit in relation to the pipeline right of way and the geological setting. Drainage is given (ref. Appendix A) as well as geomorphology, ice contents and organic soil cover.

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- (b) <u>Biological Setting</u> A general description of vegetation, observed and recorded mammal and bird use of the area, and fisheries potential of adjacent waterbodies are given for each site. These data were used to make an initial biological assessment of development of the site and will be used to identify sites requiring further investigation.
- (c) <u>Materials</u> description of soils in the deposit according to the test hole logs which are classified according to the Terms and Symbols Section in Appendix A. In the Materials and the Development and Rehabilitation sections the materials are indicated as being sources of excellent, good, fair and poor quality granular material. These terms are based upon the definitions as found in "Appendix A" pp A-16 and A-17.
- (d) <u>Volume</u> estimated total volume of granular material as calculated by planimetering the outline of the deposit and using a conservative depth of the deposit according to test hole logs and airphoto interpretation.
- (e) <u>Development and Rehabilitation</u> the sections on Physical Setting, Biological Setting, Materials, and Volumes were used to describe the potential development of the deposit. A brief general plan for development of the deposit was formulated with the understanding that additional environmental concerns may alter final design.

8.1.4 Test Pit and Test Hole Logs

An individual test pit or test hole log has been prepared on the standard NESCL form and in accordance with the standardized "Terms and Symbols" section which is included in Appendix A. The test pit and/or test hole log data are presented within the respective individual site reports.

8.1.5 Laboratory Test Data

The grain size information for each sample tested is presented on the "Grain Size Distribution Curve", plotted and produced by R.M. Hardy and Associates Ltd. The remaining laboratory tests such as Los Angeles abrasion, sulphate soundness, organic content and petrographic analyses are summarized and tabulated on the form entitled: "Summary of Laboratory Tests to Determine Aggregate Suitability in Concrete". In those cases where the fine aggregate was also tested the results are similarily tabulated and crossreferenced to the coarse aggregate results. Each individual site report includes all test results which are pertinent to that specific borrow source.

8.2 <u>Strip Maps</u>

In addition to the site specific airphotos, the location and shape of each potential borrow source which has been investigated from Richards Island to Fort Good Hope have been plotted on the Project Strip Maps at a scale of 1:250,000. These project strip maps were produced using the National Topographic Surveys map series and are presented in Appendix B.

9. CONCLUSIONS

The 1975 CAGSL-NESCL borrow field program and previously documented studies have shown that adequate construction materials are present along the pipeline route between Richards Island and Fort Good Hope. Granular deposits and shallow bedrock are not evenly distributed and careful consideration in allocation and development of these resources will be needed to ensure that requirements by northern communities, highways, and industry can be met.

Forty-eight deposits were investigated in this area of the Mackenzie Valley during the summer of 1975. Seventeen of these deposits had not been documented in the detailed site investigations for the DIAND Granular Materials Inventory. Eight of the above 17 new deposits are recommended for potential development based on granular material quality. A total of approximately 260 million cubic yards of fair to excellent quality borrow material were found in the deposits investigated in 1975 (see Table I, page 51).

The DIAND Granular Materials Inventory has covered the area from Richards Island to Fort Good Hope. Additional field work has been done by the oil and gas producers (see Bibliography, page 601) on the Ya-Ya esker and by DIAND on several deposits in the Mackenzie Delta area between Richards Island and Parsons Lake. The CAGSL-NESCL study has provided further detail as required on certain deposits described in the DIAND Granular Materials Inventory and has added site specific information on seventeen sites which were not included in the detailed borrow site reports done for the DIAND inventory by Ripley, Klohn, Leonoff International Limited, EBA Engineering Consultants Limited, and Pemcan Services "72". Granular deposits from Richards Island to Fort Good Hope are concentrated in outwash deposits (including eskers, kame terraces, kame deltas and kame complexes), exhumed Tertiary gravels, and fluvial terraces.

Granular deposits were investigated by airphoto analysis, field reconnaissance, geophysics, test pitting and drilling. The results of the airphoto analysis, field reconnaissance, test pitting and drilling appear in the individual site reports which make up Section 11 of this volume.

Geophysical investigations were done to supplement information obtained from airphoto analysis, field reconnaissance, and subsurface exploration of the individual borrow deposits. Electrical resistivity measurements were made at most borrow deposits investigated. The resistivity of the ground was determined by vertical soundings with probes in a Schlumberger array and with VLF radiohm. Both methods were of little value in helping to delineate the extent of the deposit or arriving at the depth of the deposit.

Shortly after completion of the field portion of the borrow investigation specially designed electromagnetic equipment for shallow exploration became available. This equipment was tested on 5 existing borrow pits in the Calgary area; the results show this equipment to perform well for delineating unfrozen granular deposits.

Following the field reconnaissance of borrow sources and a review of other available information, no biological factors were identified which would preclude development of the deposits recommended in this report. Development of the deposits will have localized impacts on the environment. Implementation of environmental design guidelines in the final location of borrow deposits and ancillary facilities, together with scheduling of activities, should maintain acceptable levels of impact.

TABLE T SUMMARY TABLE OF DEPOSITS INVESTIGATED RICHARDS ISLAND TO FORT GOOD HOPE

DEPOSIT NO. (R) - denotes	DIAND DEPOSIT	GRANULAR MATERIAL (NESCL Volume)	NON-GRANU	LAR MATERIAL	SITES NOT RECOMMENDED		
reconnaissance site only	NUMBER	x 10 ⁶ cu. yd.	Till	Bedrock	(Major reasons)		
1070 B1	222	14.0					
107C-B1	226	1.0					
107C-B2		7.9		1			
107C-B3(R)	225						
107B-B1	320	3.0 5.4					
107B-B2	319						
107B-B3	309	6.0					
107B-B4	315	10.0					
107B-B5	-	0.3					
107B-B6	-	-	Х		till; thick over-		
				i i	burden.		
107B-B7	-	-			too silty; thick		
					overburden.		
107B-B8		1.0			too silty, thick		
					overburden; massive		
					ice.		
107B-B9	452	5.8					
107B-B10	-	9.4					
107B-B11	-	0.8					
107B-B12	-	0.5			1		
107B-B13	1153a	4.6					
107B-B14	-	1,2	х	1	large amount of til		
					in deposit.		
107B~B15	1146	22.4					
107B-B16(R)	_	0.4					
107B-B17(R)	450	4.0					
106N-B1	-	_	x		till (frozen).		
106N-B2	1141	2.0					
106N-B3	1139a	_		x	poor quality bedroe		
106N-B4	1138	17.0					
1060-B1	1138	16.7					
1060-B2	1137	4.5					
1060-B3	1098	10.0					
1060-B4	1084, 1089	13.0					
1060-B5	1085	1.0					
1060-B6		5.0	x		large amount of til		
1060-B0 1060-B7	1057	12.0					
106P-B1	1049	1.4					
106P-B2	1050	5.5					
106P-B3	1047	4.2					
106P-B4	1047	9.3					
106P-B5(R)	1045	0.1			poor access and		
100F-D3(K)	10,52	0.1			quality,		
1061-B1	1035, 1036	35.0			1/		
	1032, 1030	2.5					
106I-B2	1022	6.2					
1061-B3	1022	1.8			too silty,		
1061-B4(R) 1061-B5(R)	-	2.0			too silty,		
106I - B5(R)	-	0.9					
1061 - B6(R) 1061 - B7(R)		1.0					
106I-B7(R)	1025	0.7					
106I-B8(R)	1 1						
106T - B9(R)	1003	7.6			too silty.		
1061-B10(R)	1006-	1.0			too silty,		
106I-B11(R) 106I-B12(R)	1006a	1.5					
1001-B12(K)	1153	12.0					
	ــ ــــــــــــــــــــــــــــــــــ		L				
TOTAL Granula		271.6					
- TOTAL Not rec							
000011	Mater		tan aubic	wardo			
= TOTAL		2,00.0	ion cubic y	yards.			

NOTE: The DIAND deposit number refers to the number assigned to each deposit that was investigated during the granular materials inventory as outlined in the following two sets of reports.

For numbers < 1000 - Ripley, Klohn and Leonoff International Ltd. 1972 & 1973. For numbers > 1000 - EBA Engineering Consultants Ltd. and F.F. Slaney & Co. Ltd. . 1974.

10. **RECOMMENDATIONS**

The 1975 CAGSL-NESCL borrow field program and previous borrow inventory programs have shown the distribution and characteristics of borrow deposits along the pipeline route through the Mackenzie Valley and the Yukon Coastal Plain. As the location of the pipeline and facilities and decisions on construction modes are finalized, a more accurate determination of borrow requirements should be made. Also, during this final design stage, a detailed field and office study of specific borrow deposits chosen to supply these requirements should be undertaken.

Final design field studies should obtain information on the quantity, quality, and stratigraphy of materials available in each deposit. This data should be collected by on-site geological and engineering observations and by drilling and test pitting. Geophysical methods should be used where feasible to provide subsurface information between drill holes. Also at this time additional data should be collected on the occurrence of permafrost in the borrow materials, the position of the water table in the deposit, access from the deposit to the pipeline route, and engineering aspects which might be useful during development of the borrow source.

It is recommended that final design field studies including biological, archaeological, land use, land availability, and socioeconomic factors of each deposit be conducted. A preliminary list of environmental design guidelines is given in Table II (see page 54).

Site specific borrow pit development plans using information from preliminary and final design studies should be produced prior to the exploitation of the borrow deposits.

TABLE II

PRELIMINARY ENVIRONMENTAL DESIGN GUIDELINES

- 1. Development activity in the vicinity of borrow deposits may be rescheduled during certain periods of the year to minimize disturbance of: migrating waterfowl (April-June) (August-October), wintering moose (December-April), staging waterfowl (August-September), spawning or migrating fish populations (April-September), migrating and calving caribou (April-June) fox and wolf (May-July), grizzly and black bears (May-October), and raptors (May-October).
- 2. In the final location of borrow deposits and facilities, productive forest land and merchantable stands of timber should be avoided, where possible, in favour of locations in lower productivity forest land.
- 3. Topsoil and/or the organic layer from all disturbed areas should be salvaged and stockpiled for use in deposit rehabilitation. Trees and shrubs may be salvaged either 'as cut' or chipped for use in erosion control, as dimension lumber or other project requirements.
- 4. A buffer strip should be maintained between waterbodies and the borrow deposit or support facilities such as roads, camps, etc. to minimize impact on aquatic ecosystems and to preserve important riparian wildlife habitat. The location and width of the buffer strip should be based on site specific data.
- 5. Any structure containing petroleum products or other toxic materials should be located so as to prevent the introduction of toxic materials into any waterbody inhabited by fish, waterfowl, and aquatic mammals, or any water course emptying directly into such water.
- 6. No borrow pits are proposed on active flood plain deposits in Mackenzie River tributaries. Where ancillary facilities such as haul roads cross active streams, precautions should be taken to protect stream banks and vegetation and to limit siltation.
- 7. Blasting operations at borrow deposits should be developed following den surveys at the site, to prevent adverse impact on denning species. Hibernating species should be relocated or taken by resident trappers if found in the proposed borrow deposit. Most blasting will be done during the winter period, thereby minimizing impact on the majority of wildlife.
- 8. Borrow deposits frequently represent prime denning habitat for bear, fox, wolf, and other denning species. During the final design field studies, active den sites and optimal potential denning habitats will be located. These areas should be protected where necessary from borrow development.
- 9. Adequate garbage handling and disposal measures will be required to prevent attracting bears and other scavenging wildlife to borrow deposits.
- 10. The likelihood of encountering archaeological sites is proportionately greater in well drained areas than in low-lying, poorly drained areas. Archaeological surveys will be conducted at all proposed borrow deposits prior to final design. Development activities will be monitoried by an archaeologist in the event that archaeological sites are encountered during development of the borrow deposit.

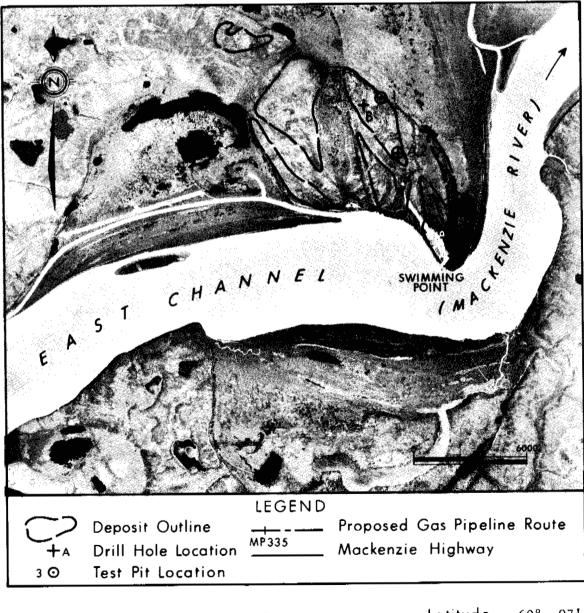
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The following is a list of individual site reports that are contained in this section.

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1061-B4(R)	561 565
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1061-B12(R)	597

- Physical Setting: Deposit 107C-B1 consists of large bars on a fluvial terrace located just west of Swimming Point and 8 miles east of milepost 25 on the right of way.
- Moterial: SAND well to poorly graded with occasional beds of gravel.
- Volume: 14,000,000 cubic yards.
- Assessment: Deposit 107C-B1 is a source of fair quality granular material suitable for general fill and backfill.



Airphoto No.A23476-128Approximate Scale:1" = 5100'

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Latitude: 69° 07' Longitude:134° 25'

DEPOSIT 107C-B1

PHYSICAL SETTING

Deposit 107C-B1 is located just west of Swimming Point on East Channel of the Mackenzie River, and is 8 miles due east of milepost 25 of the proposed pipeline route. The deposit corresponds to source number 222 in Ripley, Klohn, Leonoff DIAND Granular Materials Inventory Zone II (1972) report. A detailed investigation of this deposit has also been made by EBA in: "Geotechnical Evaluation of Granular Material, Mackenzie Delta Area", 1976.

This deposit consists of large bars on a fluvial terrace that stands 20 to 50 feet above the level of the Mackenzie River floodplain. The surface of the bars are flat except for gently sloping slip-off slopes. Old abandoned channels are 10 to 30 feet below the general level of the bars. Occasionally steep scarps define the edges of the bars.

Peat and silt may range up to 4 feet thick on the bars and drainage is good to imperfect. In the abandoned channels and on some lower parts of the terrace, peat and icy silt varies between 5 to 10 feet and drainage is imperfect to poor.

The surrounding terrain, which consists of floodplain and low terraces along the East Channel, contains standing water, indicating very poor drainage.

In mid-August the active layer is from 1 to 6 feet deep, below that the deposit is frozen with very little excess ice. EBA drill holes encountered visible ice in silt and fine sand layers of the deposit.

BIOLOGICAL SETTING

The vegetation at this site consists of dwarf birch, grass and lichen with sedges and scattered alder in wetter areas. Arctic ground squirrel dens were observed at the site. The habitat is suitable for fox, wolf, and grizzly bear. A reindeer antler was found on the site. The area provides habitat for upland and passerine bird species. Waterfowl are present in the area throughout the summer season and stage during the mid-August to late September period. No suitable fish habitat is found in the immediate vicinity of the site.

MATERIAL

On the basis of our preliminary investigation and the detailed investigation by EBA the material in this deposit is of fair quality and consists mainly of coarse, well graded to poorly graded sand and gravel with occasional silty beds. Lenses composed mainly of gravel ranging up to 6 feet in thickness were scattered throughout the deposit.

VOLUME

Based on an area of 930 acres and a conservative depth estimate of 9 feet, the total volume of material available is approximately 14,000,000 cubic yards.

As a result of the detailed investigation of this deposit recently done by EBA in which 44 test holes were advanced it should be noted that the recoverable volume would be about 6,000,000 cubic yards. Water level of the adjacent lakes is the limiting factor for this lower volume.

DEVELOPMENT AND REHABILITATION

Deposit 107C-B1 is a source of fair quality granular materials and could be used for general fill and backfill in pipeline construction. Since a detailed investigation has been carried out at this deposit, further test holes and pits may be needed only in areas where proposed development will take place. No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the deposit may be achieved by barge to Swimming Point and overland from there to the deposit, a distance of approximately 1 mile. Material would be loaded on trucks and hauled over ice on the Mackenzie River to the pipeline right of way at Tununuk junction. Alternatively, access to the pipeline right of way from the deposit may consist of an access road of about 8 miles. Overland access during the winter season would consist of snow roads.

Initially the peat cover and overburden would be stripped from the area to be excavated, and stockpiled around the edge of the site.

Development of this deposit would involve excavating borrow material in stages from raised gravel bar areas down to a grade so that good drainage would be established over the deposit. Depths of overburden varies and must be determined before specific sections are exploited. To prevent slumping of ice rich material along slopes, borrow material close to the river banks or steep slopes should not be excavated. An adequate buffer zone should be left to prevent this situation from occurring. Development of this borrow site could be accomplished by using blasting or conventional earthmoving techniques depending on site drainage and the degree of ice cementation. The excavated material may have to be stockpiled, thawed, and drained before it is used. Siltation controls should be used to prevent thaw water run-off from stockpiles draining into adjacent water courses.

Equipment required for development would be dozers, rippers, end dump trucks and front end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

GRAPHIC LOG SAMPLE CONDITION **GROUP SYMBOI** å ICE GRAPHIC LOG CONDITION LABORATORY TEST DATA NRC ICE TYPE VISUAL ICE % CORE RUN & % RECOVERY (FT.) ۰ŏ DEPTH (FT.) SAMPLE TYPE OTHER REMARKS DESCRIPTION DEPTH Plastic limit ------ Liquid limit TEST DATA CORE 60 80 100 120 140 📥 SOIL SOIL 80 100 🖸 20 40 60 19:30 PEAT-fine fibrous, dark brown, 3 UF 1.0 wet, spongy 1 0 - 19:36 ⁺Pt F Ę 2 SAND - fine, uniform, grey, (trace silt) 35 SP 4 (4.5) SILT-trace fine sand, dark brown ML 60 6 SAND - medium to fine, trace coarse, trace fine gravel, orange, yellow 10 and black grains 8.0 - 19:38 8 SP some grinding and 9.0 gravel chips 10 11.0 °°° GRAVEL - fine to coarse, little coarse sand, trace fine sand 12 bо ° 00 GP 00 <u>14.0___</u> Ьο increasing fine sand 14 100 TEST HOLE 0 TEST HOLE No. PROJECT : 13011 LOGGED BY FACILITY 1.1.8. No. 1975 BORROW INVESTIGATION LAT. & LONG 69⁰06'50''N, 134⁰24'26''W ELEVATION CHKD D,6. N75-PIPE MILEAGE NORTHERN ENGINEERING SERVICES AIRPHOTO No. : A 23476-127 N75-107C-B1-A DRWN. BY: jJ.₩.B. COMPANY LIMITED 4⁰.C AIR TEMP CALGARY ALBERTA CHKD RIG : D. O. HELI-DRILL 107C ENGINEERS FOR METHOD : ALR SHEET 1 OF FINISH : D 08 M 08 Y 75 TIME: 20:00 CANADIAN ARCTIC GAS STUDY LIMITED 2 D 09 M 08 Y 75 TIME: 19:30 START: ω

TEST HOLE LOG

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PC-9,5K37

TEST HOLE LOG

DEPTH (FT.)	SOIL GROUP SYMBOI	SOIL GRAPHIC LOG		DESCRIF	TION		ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Dry de	ABORAT Insity (po limit H 80 40	:f) 1	0 w	imit 14	% 40 ▲ 00 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FI.)	REMARKS
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GRAPHIC LOG GROUP SYMBOI ICE GRAPHIC LOG SAMPLE CONDITION Š CONDITION LABORATORY TEST DATA NRC ICE TYPE VISUAL ICE % 0 & CORE RUN & % RECOVERY DEPTH (FT.) ۰ð (FT) ▲ Dry density (pcf) ○ Water content % OTHER SAMPLE TYPE DESCRIPTION REMARKS DEPTH Plastic limit ⊢ ----- Liquid limit TEST DATA CORE 60 80 100 120 140 📥 SOIL SOIL 20 40 60 80 100 🖸 Peat-fine fibrous, dark brown, moist .Ö 2 Ľ۴ 21:20 SW SAND - fine to coarse, some gravel, light brown, fine fibres to 2.5' depth, pebbles to 3" 2 -2.5___ occasional cobble, 4", moist from depth 5.0' 4 6 6.5 F 8 10 11.0____ increasing gravel 12 -21:45 hole sloughing 3.5 SAND -fine, uniform 14 14 TEST HOLE SP End of hole 28.0 22:05 TEST HOLE No. ş PROJECT : LOGGED BY J.J.S; FACILITY 13011 1975 BORROW INVESTIGATION ELEVATION : CHKD LAT. & LONG 69⁰07'21''N, 134⁰25'13''W 0.0. N75-107C-NORTHERN ENGINEERING SERVICES DRWN. BY: AIRPHOTO No. PIPE MILEAGE : J. M. B. A 23476-127 THE N75-107C-B1-B COMPANY LIMITED 4⁰C HELI-DRILL AIR TEMP D. C. RIG : CHKD: CALGARY ALBERTA ENGINEERS FOR METHOD : AI R SHEET 1 OF 1 FINISH : D 08 M 08 Y 75 TIME: 22:05 CANADIAN ARCTIC GAS STUDY LIMITED START: D 08 M 08 Y 75 TIME: 21:20 œ

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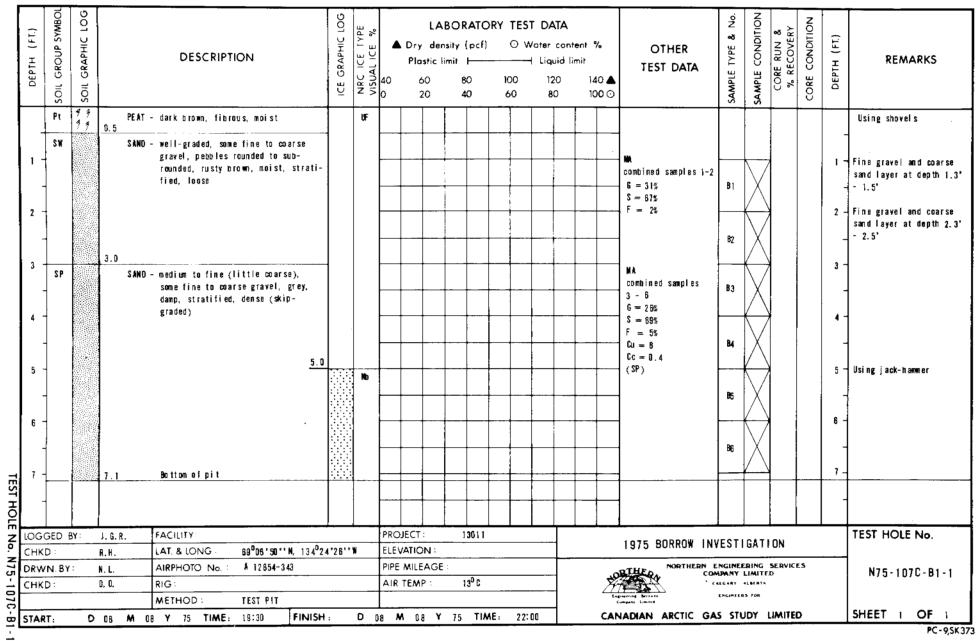
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TEST HOLE LOG

PC-9,5K373

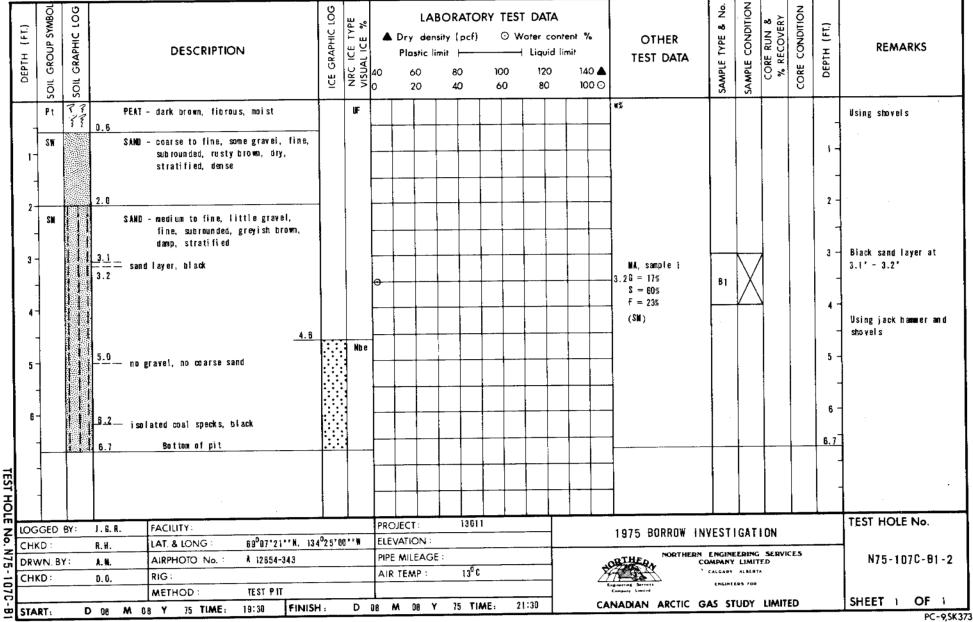
TEST HOLE LOG



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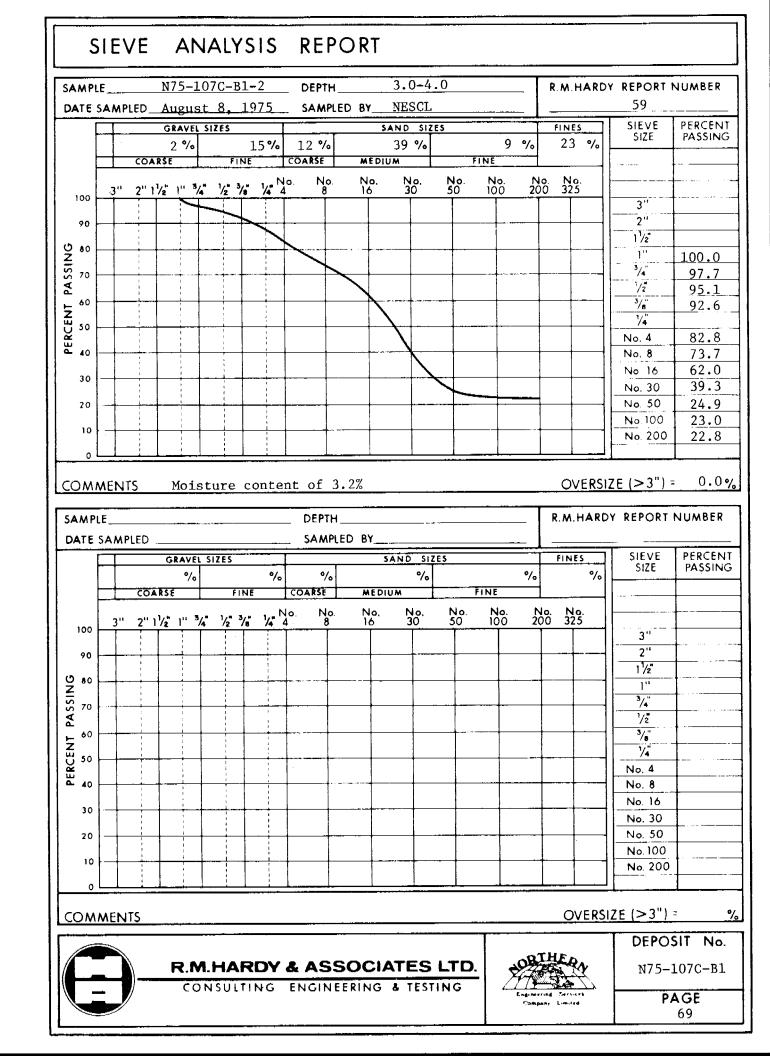


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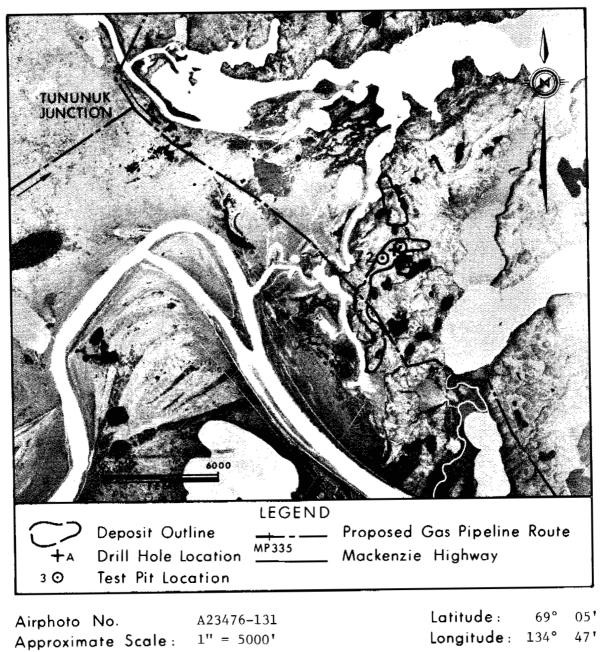
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- Physical Setting: Deposit 107C-B2 is part of an esker complex located 5 to 6 miles northwest of Tununuk Point and crossed by the right of way at milepost 23.
- Material: SAND and GRAVEL stratified, uniform to well graded sand and poorly graded gravel.
- Volume: 1,000,000 cubic yards.

Assessment: Deposit 107C-B2 is a source of good quality material suitable for general fill, backfill, and building pads. Haul distances would be short as the deposit is crossed by the right of way.



DEPOSIT 107C-B2

PHYSICAL SETTING

The deposit is situated 5 to 6 miles northwest of Tununuk Point. The proposed Cross Delta Route crosses the southern end of deposit at milepost 23. The deposit corresponds to source number 226 in Ripley, Klohn, Leonoff DIAND Granular Materials Inventory Zone II (1972) report.

The deposit consists of the western end of an esker complex that continues five miles to the east past the southern end of Ya-Ya Lake where gravel is currently being extracted. The esker is superimposed on fluvial sands which contain thick layers of massive ice.

The surface of the deposit is rolling with local relief to 30 feet and moderate slopes. Subsurface ice wedges have locally created mounds 20 to 30 feet across, separated by trenches 2 to 5 feet deep. Thermokarst has formed relief of about 100 feet in the sand on which the esker is superimposed, and as a result, steep slopes are present in the surrounding area.

Overburden is less than 1 foot over most of the deposit and drainage is good except in a few flat imperfectly drained depressions. The active layer varies between 2 and 7 feet and the deposit material is low to medium in ice content.

The Mackenzie Delta lies northwest of the deposit. A major inlet to Ya-Ya Lake is immediately west of the esker. To the southeast, hummocky ice-cored topography is present except in a marshy abandoned channel.

BIOLOGICAL SETTING

The surface of the esker is partly covered by patches of dwarf birch and willow. In low areas, the ground cover is mainly sedges with scattered alder. The general area provides year-round habitat for fox,

- 73 -

wolf, grizzly bear and caribou. Arctic ground squirrel dens are abundant at the site. Nearby lakes provide low productivity habitat for muskrat. The site provides habitat for ptarmigan and passerines. Waterfowl are present in the area throughout the summer season and stage during the mid-August to late September period.

MATERIAL

Test pits 107C-B2-1 and 2, drill hole 107C-B2-A and DIAND Granular Materials Inventory Zone II reports indicate that the deposit is composed of stratified, uniform to well graded sand and subrounded to rounded, poorly graded gravel. The test hole and test pit logs indicate a wide variation in material quality.

VOLUME

Based on a depth of 10 feet and an area of 100 acres the total estimated volume is approximately 1,000,000 cubic yards. It can be expected that at least half the material will be gravel.

DEVELOPMENT AND REHABILITATION

Deposit 107C-B2 is a source of good quality granular material, and could be used for general fill, backfill in pipeline construction, and building pads. The material cannot be recommended at this time for use in concrete aggregate as more extensive testing is required to define amounts of deleterious material. Tests from DIAND Granular Materials Inventory Zone II report and this report indicate that the chert in the aggregate may make it unsuitable for use in concrete production.

Equipment could be staged to the area by barging the equipment from Tununuk Point via river channels to the granular deposit. Haul of borrow material would be short as the pipeline right of way crosses the deposit at milepost 23. Access would involve building a winter snow

- 74 -

road from the deposit to the pipeline right of way. Care would have to be taken to avoid exposing slopes of their vegetative cover in order to insure that bimodal flows are not initiated.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Initially the peat cover and overburden, although minimal, would be stripped from the area to be excavated, and stockpiled around the edge of the site.

Development of this deposit would involve excavating borrow material evenly from the higher, well drained areas so that good drainage would be established over the deposit. As massive ice layers are present within this deposit, care should be taken to leave sufficient cover over the ice to prevent thermal degradation. This type of development could be accomplished by using blasting or conventional earthmoving techniques depending on the degree of ice cementation. The excavated material would have to be stockpiled, thawed, and drained before it is used. Crushing and/or screening of the material may be required to produce quality construction aggregates.

Equipment required for development would be dozers, rippers, end dump trucks, front end loaders, as well as screening and crushing plants if required.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

LOG **GROUP SYMBOI** ICE GRAPHIC LOG SAMPLE CONDITION SAMPLE TYPE & No. CONDITION LABORATORY TEST DATA NRC ICE TYPE VISUAL ICE % 0 & CORE RUN & % RECOVERY (FT.) (FT.) GRAPHIC ▲ Dry density (pcf) ○ Water content % OTHER DESCRIPTION DEPTH REMARKS DEPTH --- Liquid limit Plastic limit + TEST DATA CORE 140 📥 60 80 100 120 SOIL SOIL 0 100 🖸 20 40 60 80 0.2 PEAT-coarse fibrous, dark brown, damp 21 77 UF 10:15 SP SAND - fine to coarse, little fine gravel, 4 1/4 Walmac (trace silt) 2 3.0 F 4 35 5.0____ medium sand (approx. 70%) 40 trace fine gravel, to 3/4 6 7.0 7.0 I CE ICE + ICE-with lenses of poorly graded Ju 3 7/8' Walmac at |+ |sp sand (approx. 75% ice) 8 -8 1 9.0 12 12 13.0 193.6 13.0 I CE ICE 1 C E 19 0 at 10:46 14 (traces of fine sand) TEST HOLE 10:52 29 End of hole 29.0 29.0 29 PROJECT TEST HOLE No. LOGGED BY: FACILITY 13011 No. 1.1.8 1975 BORROW INVESTIGATION CHKD : LAT. & LONG : 69⁰05'07"'N, 134⁰47'48''W ELEVATION : D.O. J. N.B. AIRPHOTO No. : A 23476-13D PIPE MILEAGE NORTHERN ENGINEERING SERVICES DRWN, BY: N75-107C-B2-A σ COMPANY LIMITED 7° C AIR TEMP. CHKD: RIG : CALGARY ALBERTA D. O. HEL1-DRILL ENGINEERS FOR METHOD : AI R c FINISH : TIME: 10:52 CANADIAN ARCTIC GAS STUDY LIMITED SHEET 1 OF 1 D 09 M 08 Y 75 TIME: 10:40 D 09 M 08 ¥ 75 START:

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TEST HOLE LOG

TEST HOLE LOG

DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Dry	densit [.] tic limit	y (pcf		ST DATA Water co H Liquid 120 80	intent %	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FT.)	REMARKS
-	Pt	111	0.5	PEAT_dark brown, fibrous, moist.		UF									1			+	<u> </u> .	Using shovels
1 -	SW			SAND_coarse to fine; and gravel, mainly fine, subrounded to						_										
-		0000	1.3	rounded ; rusty brown, damp, stratified, loose.					_	+				MA, combined 1 & 2 G = 62% S = 35%	B1	\mathbb{N}	1			
2 -	GW			GRAVEL-mainly fine, subrounded; and sand, coarse to fine; fusty			┣					+		F = 3%		$\left\{ -\right\}$		1	2 -	4
			2.5	brown,wet, stratified, isolated cobbles to 5'' loose.					_						82	X			-	
3 -				some coarse to medium sand					-+	1		+ +	+ +			/`			з -	
4			4.0	light rusty brown Bottom of pit. ♥ 3.8															-	Water level at 3.8
OGGE			J.G.R.	FACILITY			PROJ			13011	I			1975 BORROW INV	ESTI	CATI				TEST HOLE No.
HKD RWN	I. BY :	: I	R. H. I. J. M. D. D.	LAT. & LONG : 69 ⁰ 05'07''N, 134 ⁰ 47' AIRPHOTO No. : <u>A 23476-130</u> RIG : METHOD : TEST PIT	'12''		PIPE	ATION MILEAC TEMP: 1		15.5 ⁰	C			NORTHERN E		RING : LIMITEI	SERVIC	ES		N75-107C-82-1
TART	1	D	08 M 0	8 Y 75 TIME: 22:20 FINISH :		D ₀	8 M	08	Y 75	TIM	E: 23:	50	CAN	ADIAN ARCTIC GA	s stu	DYI	.IMITEI	D		SHEET I OF I

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TEST HOLE No. N75-107C-82-1

001 SOIL GROUP SYMBOI ICE GRAPHIC LOG SAMPLE CONDITION ŝ CORE CONDITION LABORATORY TEST DATA CORE RUN & % RECOVERY TΥΡΕ Ε % DEPTH (FT.) ø (FT) SOIL GRAPHIC ▲ Dry density (pcf) O Water content % OTHER SAMPLE TYPE NRC ICE T VISUAL ICE DESCRIPTION REMARKS DEPTH Plastic limit ⊢ — Liquid limit TEST DATA 60 80 100 120 140 📥 20 100 🔿 40 60 80 ?? ?? ∎% Using shovels Pt PEAT - dark brown, fibrous, moist UF 0.5 Some fibres to depth 2,8' 0,0 GW GRAVEL - mainly fine, subrounded to ° rounded, and sand, coarse to °°, WA. combined. 1 medium, light brown, damp, samples 1 & 2 ۰° stratified, isolated cobbles to G = 62% B1 00 5"', | cose \$ = 37% ° • • F = 1% 2 -2 (6₩) Ω 2 B2 0.0 <u>ر</u> ، ۲ 1 ົດຈ 3 -3. 00 MA. combined ٦ 1 samples 3 & 4 SP SAND - mainly medium to fine, greyish e 6 G = 53 \$ B3 brown, damp, dense S = 42% 1 4 F ≈ 5%, o (GW) ₽, GW GRAVEL - fine to coarse, and cmf sand, Θ 84 3 00 subrounded, light brown, damp, isolated cobbles to 6'', dense 5 CLAY - silty, medium plastic, grey, damp, CI MA, combined 00 stiff samples 5 - 7 GW G B5 G = 53%GRAVEL - fine to coarse, and cmf sand, light 00 S = 45%brown, wet, stratified, dense 6-6 F = 2%5 00 86 7. 1-Using jack-hammer TEST HOLE 7.2 Nb ю B7 Bottom of pit 8.0 B LOGGED BY: FACILITY PROJECT : 13011 TEST HOLE No. 8 J. G. R. 1975 BORROW INVESTIGATION CHKD LAT. & LONG 69⁰05'02''N, 134⁰47'19''W ELEVATION R.H. N75-DRWN, BY: AIRPHOTO No. : A 23476-130 PIPE MILEAGE : F. 8. NORTHERN ENGINEERING SERVICES COMPANY LIMITED N75-107C-B2-2 CHKD RIG : AIR TEMP : 0.0. 15.5⁰C CALGARY ALBERTA 1070-ENGINEERS FOR METHOD : TEST PIT Lumited. START: FINISH : D 09 M 08 Y 75 TIME: 11:25 D 08 M 06 Y 75 TIME: 22:50 CANADIAN ARCTIC GAS STUDY LIMITED SHEET I OF

TEST HOLE LOG

-B2 - 2

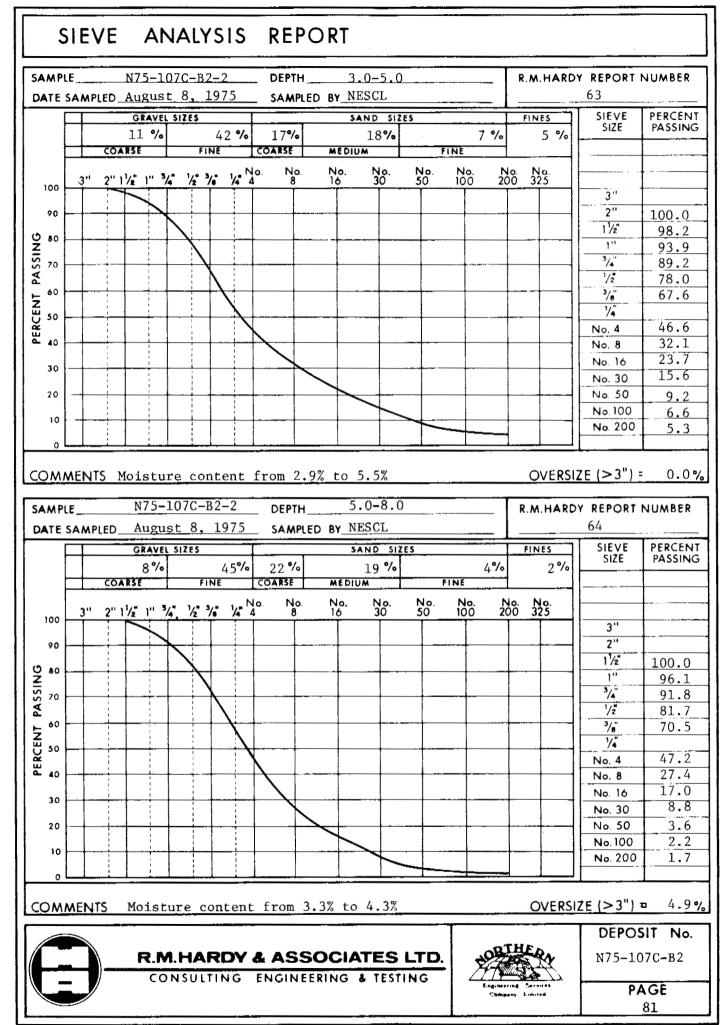
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PC-9,5K373

SIEVE		NAL	(SIS	REP	ORT							
SAMPLE	N75-	-107C-	B2-1	_ DEPTH_	1	.0-3.0)			.M.HAR	Y REPORT	NUMBER
DATE SAMPLED	Augu	ust_8,	1975	_ SAMPLE	D BY_N	ESCI.					139	
		L SIZES				AND SIZ	ES		+	FINES	SIEVE	PERCENT
	26 %		36 %	13%		15%		7		3 %	SIZE	PASSING
cc	ARSE	FI	NE	COARSE	MEDIU			FINE	-	- , -		
			N	lo. No.	No.	No	No	No.	No	No		
100 3" 2"	1 ¹ /2 1" 3	<u>/4 /2</u>	/ /4 4	8	16	No. 30	No. 50	100	200	No. 325		
											3"	100.0
90	N					<u> </u>			· · · 		2"	97.9
O 80	$+ \times$										11/2	90.8
0 80 BA SSING											<u> </u> "	79.5
S 70		\mathbf{N}				-	-+				3/4 1/2	73.5
												63.3
Z I		`	K								3/8 7/4	55.1
20 50 00 00 00 00 00 00 00 00 00 00 00 00	1											20 /
ظ ₄₀			\vdash								No. 4	38.4 26.5
				\mathbf{X}							No. 16	17.8
30						1			-		No. 30	$\frac{17.8}{12.9}$
20		 							_		No. 50	7.1
					+-						No. 100	4.0
10									·		No. 200	3.3
												5.5
SAMPLE DATE SAMPLED				•	1. D BY NE	0-3.0 SCL			R	.M.HARD	Y REPORT	
	GRAVEL	SIZES	1		5 A	ND SIZE	5			FINES	SIEVE	PERCENT
	20 %		42 %	14%		15%		8 •	/•	1 %	SIZE	PASSING
co	ARSE	Fi	NE	COARSE	MEDIU	M	F	INE				
	.1/= .u 3	/* 1/= 3	. 1. N	o. No.	No.	No.	No.	No. 100	No . 200	No. 325		
100 3. 2.	11/2 1" 3	4 /2 /	8 /4 4	8	16	30	50	100	200	325		
90	\mathbf{X}										3"	100.0
										11	$\frac{2}{1/2}$	96.6
9 00						 -				-	- 1/2	93.2
9 80 VISS 70 VISS 70		\mathbf{N}									3/4	86.4
A A											14	66.4
		$\vdash \mathbb{N}$							_		3/8	56.4
			\mathbf{X}								/* /*	
					1						No. 4	38.3
▲ 40							+				No. 8	25.4
30											No. 16	18.1
				\mathbf{N}							No. 30	12.5
20	+ ;									<u> </u>	No. 50	4.9
10											No. 100	2.0
											No. 200	1.3
0						1	1					
COMMENTS	Moist	ure c	ontent	s range	from	1.6% t	o 2.0	%		OVERSI	<u>ZE (>3") =</u>	0.0 %
									лтн	5.	DEPOS	IT No.
()				LASS ENGINEE				20			N75-10	
								Capit Cal	mpany L	mited		GE 0



	OF LABORATORY TE FOR OF AGGREGATES IN	
	2 DATE SAMPLED : August 8, DATE TESTED : February,	
SOUNDNESS OF AGG SULPHATE TEST	REGATE	ORGANIC IMPURITIES
COARSE AGGREGATE	: LOSS = 3.96 % : LOSS = 7.67 %	NUMBER : 4+ COAL REMOVED : 4+
LOS ANGELES ABRAS	SION TEST	COAL & ROOTLETS REMOVED : 4+ COAL CONTENT : 0.01%
PERCENT LOSS =	18.7 %	SIGNIFICANCE :
SUMMARY OF ROCK TYP	ES, COARSE AGGREGATE. (P	ETROGRAPHIC ANALYSIS)
ROCK TYPE	CLASSIFICATIONS	TOTAL WEIGHTED COMPONENT %
		COMPONENT /6
Quartzite	Strong to very strong, Good	44.7
Quartzite Granite	Strong to very strong, Good	
		<u>44.7</u> 0.05
Granite	Strong to very strong, Good Strong, Good	44.7 0.05
Granite Sandstone Siltstone Chert	Strong, Good	44.7 0.05 8.6 2.0 3.1
Granite Sandstone Siltstone Chert Flint	Strong, Good Potentially Reactive, Fair	44.7 0.05 8.6 2.0 3.1 2.75
Granite Sandstone Siltstone Chert Flint Friable Sandstone	Strong, Good Potentially Reactive, Fair Soft, Weak, Poor	44.7 0.05 8.6 2.0 3.1 2.75 0.15
Granite Sandstone Siltstone Chert Flint Friable Sandstone Ironstone	Strong, Good Potentially Reactive, Fair Soft, Weak, Poor Very soft, Deleterious	44.7 0.05 8.6 2.0 3.1 2.75 0.15 0.35
Granite Sandstone Siltstone Chert Flint Friable Sandstone Ironstone	Strong, Good Potentially Reactive, Fair Soft, Weak, Poor	44.7 0.05 8.6 2.0 3.1 2.75 0.15 0.35
Granite Sandstone Siltstone Chert Flint Friable Sandstone Ironstone PN = 125 INTERPRET COMMENTS : Strength of coarse	Strong, Good Potentially Reactive, Fair Soft, Weak, Poor Very soft, Deleterious	44.7 0.05 8.6 2.0 3.1 2.75 0.15 0.35 1 61.7 nt constitutes approx. 10% of alkaline reactivity
Granite Sandstone Siltstone Chert Flint Friable Sandstone Ironstone PN = 125 INTERPRET COMMENTS : Strength of coarse	Strong, Good Potentially Reactive, Fair Soft, Weak, Poor Very soft, Deleterious ATION : Fair quality aggrega tests required. Cherty compone component, further examination	44.7 0.05 8.6 2.0 3.1 2.75 0.15 0.35 0.35 1 0.35 0.17 0.18 0.197 0.197 0.197 0.197 0.197 0.197 0.197 0.197 0.197 0.197 0.197 0.197 0.197 0.197

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	OF LABORATORY TE		
SUITABILITY	OF AGGREGATES IN	CONCR	ETE
	DATE SAMPLED : August 8, 1 DATE TESTED : February, 1		
SOUNDNESS OF AGGI SULPHATE TEST	REGATE	ORGANI TEST	C IMPURITIES
COARSE AGGREGATE FINE AGGREGATE	: LOSS = 4.96 % : LOSS = 6.78 %		R : 5 EMOVED : 5
LOS ANGELES ABRAS	SION TEST	+ - ·	ROOTLETS D : 5
PERCENT LOSS =	19.7 %		CONTENT 0.01%
SUMMARY OF ROCK TYPE	ES, COARSE AGGREGATE. (F	ETROGRAP	HIC ANALYSIS)
ROCK TYPE	CLASSIFICATIONS		TOTAL WEIGHTED COMPONENT %
Quartzite Granite	Very strong, Good		32.1 0.32
Sandstone	-		8.9
Siltstone Limestone	Strong, Good		3.7 0.17
Flint Chert	Potentially reactive, Fair	-	3.65 3.4
Soft Sandstone	Friable, Weak, Poor		0.08
Clay	Soft, Deleterious		0.17
Ironstone	Solt, Deleterious		0.91
PN = 145 INTERPRETA	ATION : Poor quality		53.4

COMMENTS: Chert stability should be tested plus treatment for organic contamination. Caution: failed to meet strength requirements of CSA A23.1-5.3.2.2(b) (92%)



R.M.HARDY & ASSOCIATES LTD. CONSULTING ENGINEERING & TESTING **DEPOSIT No.** N75-107C-B2

PAGE 83

_	RY OF LABORATORY TE FOR Y OF AGGREGATES IN	
JULABILI	T OF AGGREGATES IN	CONCRETE
SAMPLE No. N75-107C- DEPTH (FT.): 5-8	32-2 DATE SAMPLED : August 8, 1 DATE TESTED : February, 1	
SOUNDNESS OF AG	GREGATE	ORGANIC IMPURITIES
COARSE AGGREGA FINE AGGREGATE	TE : LOSS = 4.96 % : LOSS = 6.78 %	NUMBER : 5 COAL REMOVED : 5
LOS ANGELES ABR	ASION TEST	COAL & ROOTLETS REMOVED : 4+
PERCENT LOSS =	18.7 %	COAL CONTENT :0.017 SIGNIFICANCE :
SUMMARY OF ROCK TY	PES, COARSE AGGREGATE. (P	ETROGRAPHIC ANALYSIS
ROCK TYPE	CLASSIFICATIONS	TOTAL WEIGHTED COMPONENT %
Quartzite		37.0
Granite	Very strong, Good	0.1
Sandstone		10.0
Siltstone	Medium strong to strong, Go	ood 3.15
Limestone		
		0.1
		0.1
Chert		0.1
Chert Flint	Potentially reactive	
·····	Potentially reactive Weak, Friable, Deleterious	2.75
Flint Ironstone		2.75 1.85 0.15
Flint Ironstone PN ₱ 126 INTERPR COMMENTS : Chert subord:	Weak, Friable, Deleterious	2.75 1.85 0.15 ce 55.1 d amongst minor and
Flint Ironstone PN ₱ 126 INTERPR COMMENTS : Chert subord:	Weak, Friable, Deleterious ETATION : Fair quality aggregat is the unfavourable rock type found inate components of the sample. St so page 85.	2.75 1.85 0.15 te 55.1 d amongst minor and trength tests required. DEPOSIT No
Flint Ironstone PN ₱ 126 INTERPR COMMENTS : Chert subord:	Weak, Friable, Deleterious ETATION : Fair quality aggregat is the unfavourable rock type found inate components of the sample. St	2.75 1.85 0.15 1.85 0.15 1.85 0.15 1.85 0.15 1.85 DEPOSIT No

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SUMMARY	OF LABORATORY TE	ST DATA
SUITABILITY	OF AGGREGATES IN	CONCRETE
SAMPLE No. N75-107C-B2-2 DEPTH (FT.): 5-8	DATE SAMPLED: August 8, 1 DATE TESTED : February, 1	1975 SAMPLED BY : NES 1976 TESTED BY : RMF
SOUNDNESS OF AGGR SULPHATE TEST	EGATE	ORGANIC IMPURITI
COARSE AGGREGATE FINE AGGREGATE		NUMBER :
LOS ANGELES ABRAS		COAL & ROOTLETS REMOVED : 4 COAL CONTENT : 0
PERCENT LOSS =	18.7 % PES, <u>FINE</u> AGGREGATE. (SIGNIFICANCE : PETROGRAPHIC ANALYS
ROCK TYPE	CLASSIFICATIONS	TOTAL WEIGHTED COMPONENT
Quartzite, Quartz	Very strong, Good	33.78
Sandstone Siltstone	Strong, Good	1.87
Chert Flint	Potentially reactive, Fair	3.78 3.34
	Potentially reactive, Fair Soft, Weak, Deleterious	
Flint Ironstone		3.34 0.125
Flint Ironstone	Soft, Weak, Deleterious	0.125
Flint Ironstone PN = 126 INTERPRETA	Soft, Weak, Deleterious	3.34 0.125 e 44.9 DEPOSIT

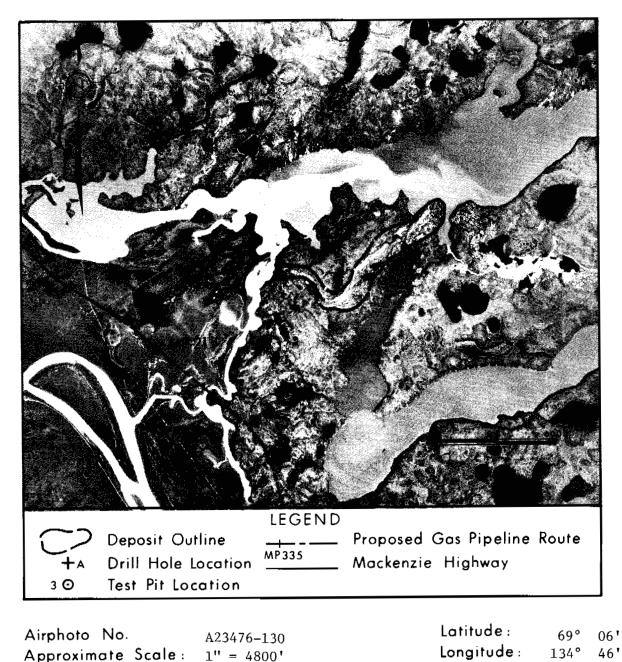
Physical Setting: Deposit 107C-B3(R) which is part of the western end of the Ya-Ya esker is located about 2 miles northeast of milepost 22.5 of the proposed pipeline right of way.

Moterial: SAND and GRAVEL - well graded.

Volume: 7,900,000 cubic yards.

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Assessment: Deposit 107C-B3(R) is a source of good quality granular material with access being relatively short via Ya-Ya Lake. Granular material from this deposit may be used for general fill, backfill, building pads, and possible concrete aggregate.



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DEPOSIT 107C-B3(R)

PHYSICAL SETTING

This deposit is part of the western end of the Ya-Ya esker. It is located close to the south shore of Ya-Ya Lake about 2 miles northeast of milepost 22.5 of the proposed pipeline right of way. The deposit corresponds to source number 225 in the Ripley, Klohn, Leonoff DIAND Granular Materials Inventory Zone II (1972) report, and Area "A" of EBA Engineering Consultants Limited Ya-Ya Granular Resources Study Volume I (1975) report.

The esker stands about 50 feet above the surrounding terrain which is hummocky and underlain by icy sand. The esker ridge has a rolling crest with steep flanks, thus the surface is well drained. Overburden is nonexistent except in depressions that contain 5 to 10 feet of peat and silt. Ice contents appear to vary from low in the sand beds to high in the silt. Massive ice is expected within the deposit.

BIOLOGICAL SETTING

Vegetation on this esker is found only in poorly drained depressions, where dwarf birch, alder and sedge predominate. The area provides year-round habitat for fox, wolf, and grizzly bear. Arctic ground squirrel dens and nesting passerines were observed at the site. The site lies within potential grizzly bear denning habitat. Waterfowl are present in the area throughout the summer season and stage during the mid-August to late September period. Nearby Ya-Ya Lake supports several fish species including pike, suckers, and whitefish.

MATERIAL

EBA Engineering Consultants Limited Ya-Ya Granular Resources Study Volume I report indicates that much of the material in this source is well graded sand and gravel. Sporadic lenses of fine sand and silt occur throughout the deposit.

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VOLUME

Results of the Ya-Ya Granular Resources Study indicate a total volume of 7,900,000 cubic yards. Massive ice, water levels of surrounding ponds, and overburden may limit the actual recoverable volume.

DEVELOPMENT AND REHABILITATION

Deposit 107C-B3(R) is a source of good quality granular material. This deposit was only investigated on a reconnaissance basis, but others have done more detailed investigations on it. Location of areas to possibly be exploited will be dictated by material requirements, the presence and position of massive ice, and insitu material quality. More drilling and test pitting will be required to delineate areas of better quality material, depth of overburden, and areas of massive ice. Haul distances to the pipeline right of way are in excess of 2 miles over gently rolling terrain. However, lake and channel surfaces are available for winter haulage across flat ice surfaces. Granular material from this deposit may be used for general fill, backfill in pipeline construction, and building pads. Suitable aggregate for concrete prooduction may be produced from this deposit.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the deposit with equipment may be achieved by barge to Ya-Ya Lakes camp and overland from there to the deposit, a distance of one mile. Alternatively, the equipment may be staged via the pipeline right of way to the deposit. In order to minimize environmental damage, snow roads would be built to transport the borrow material from the deposit to haul points on the right of way.

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Overburden varies in thickness from 0 to 10 feet and some stripping would be required at this site.

Development of this deposit would involve excavating borrow material evenly from the higher, well drained areas so that good drainage would be maintained over the deposit. Excavations would be kept away from Ya-Ya Lake to protect the lake from siltation. This type of development could be accomplished by using blasting or conventional earthmoving techniques depending on the degree of ice cementation. Some massive ice may have to be wasted during development. The excavated material may have to be stockpiled, thawed, and drained before it is used. Crushing and/or screening of the material may be required to produce quality construction aggregates.

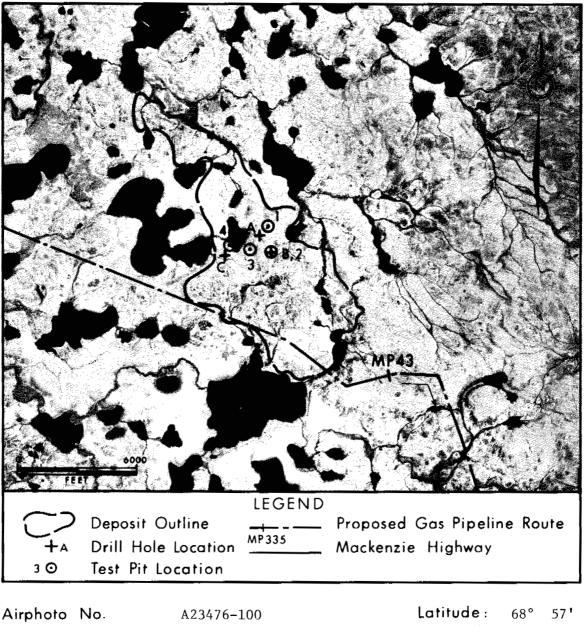
Equipment required for development would be dozers, rippers, end-dump trucks, front-end loaders, screens and concrete plants if required.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

- Physical Setting: Deposit 107B-B1 is an outwash plain modified by thermokarst. It is located 2 miles north of Wolverine Lakes and at pipeline milepost 42. The pipeline right of way crosses the southern portion of the deposit. Material: SAND and GRAVEL - stratified with little silt.
- Volume : 3,000,000 cubic yards.

B

Deposit 107B-B1 is a source of fair to good quality Assessment: material suitable for general fill and backfill. Further testing would be required to delineate favourable areas for development.



Approximate Scale: 1" = 4900'

Longitude: 134° 08'

DEPOSIT 107B-B1

PHYSICAL SETTING

Deposit 107B-B1 is an outwash plain modified by thermokarst. It is located about 2 miles north of the Wolverine Lakes, and the proposed pipeline right of way at milepost 42 passes through the southern portion. The deposit corresponds to source number 320 in Ripley, Klohn, and Leonoff DIAND Granular Materials Inventory Zone III (1972) report.

The outwash plain is hummocky to gently rolling with thermokarst lakes and depressions inset 100 feet below the general surface. The plain is also spotted with 20 to 30 foot knobs and ridges. Most slopes are gentle to moderate, but locally 40 to 100 foot scarps with slopes to 20 degrees are present.

Drainage is good over most of the deposit and there is negligible cover of peat and silt except in local swales. The active layer varies from 3 to 6 feet. Ice content in the sand and gravel is low but massive ice may be encountered anywhere from 7 to 27 feet below the ground surface.

BIOLOGICAL SETTING

Typical tundra vegetation covers the area with dwarf birch, willow, alder and lichen predominating. The area provides year-round habitat for Arctic ground squirrel, fox, wolf, and grizzly bear. Reindeer are common in the area and moose are occasionally present during the summer months. Ptarmigan, long-tailed jaegers and ground squirrel dens were observed at the site. A wide range of waterfowl, upland and passerine species occur during the summer months throughout the area. There is no suitable fish habitat in the vicinity of the site.

MATERIAL

Drill hole and test pit data as well as DIAND Granular Materials Inventory Zone II report show the deposit to be stratified gravel and sand, frequently silty. Uniform and well graded gravels were found in beds ranging from 1 to 25 feet thick. Sands are uniform to well graded, often with varying amounts of gravel. Since quality of the material varies greatly, further drilling will be required to define areas of higher quality material.

VOLUME

Although the DIAND report indicates a probable maximum volume of 1,500,000 cubic yards, investigations to date indicate that an estimated volume of 3,000,000 cubic yards, based on an average depth of 6 feet and the possibility that only $\frac{1}{4}$ of the deposit area of 1,280 acres consists of good quality granular material, is conservative.

DEVELOPMENT AND REHABILITATION

Deposit 107B-B1 is a source of fair to good quality granular material. Material requirements and insitu material quality will determine the amount of development that takes place on this deposit. Areas with thick overburden would be avoided. The deposit would be further investigated by drilling and test pitting to delineate areas of good quality material with the least amount of overburden. Granular material from this deposit is suitable for general fill and backfill in pipeline construction.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the deposit may be achieved by barge to Tununuk Point and overland from there via pipeline right of way to the deposit, a distance

- 96 -

of 14 miles. In order to minimize environmental damage, snow roads would be built to transport the borrow material the short distance to haul points on the right of way. Care would have to be taken not to start bimodal flows along the valley walls in this area.

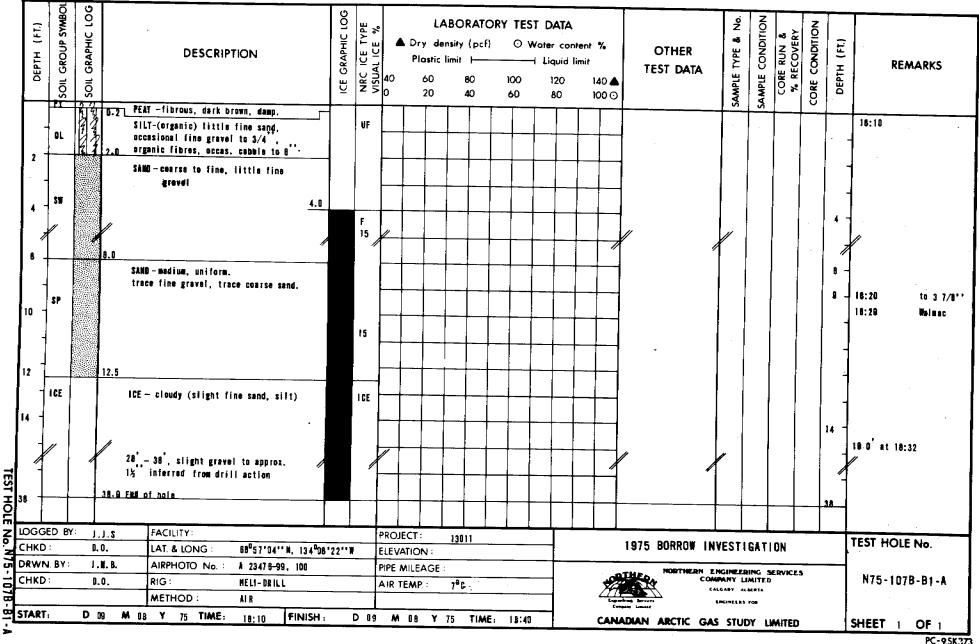
Initially the peat cover and overburden would be stripped from the area to be excavated, and stockpiled around the edge of the site.

Development of this deposit would involve excavating borrow material evenly from the higher, well drained knobs and ridges so that good drainage would be maintained over the area. Excavations would be kept away from any of the nearby lakes and streams to avoid siltation. Excavations close to massive ice also would be avoided. Development of this source would be accomplished by using blasting or conventional earthmoving techniques depending on the degree of ice cementation. The excavated material may have to be stockpiled, thawed, and drained before it is used. Natural mixing during excavation would be adequate to obtain gradations for the purposes intended.

Equipment required for development would be dozers, rippers, end-dump trucks, and front-end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

TEST HOLE LOG



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PC-9.5K373

ро ICE GRAPHIC LOG SAMPLE TYPE & No. SAMPLE CONDITION CONDITION NRC ICE TYPE VISUAL ICE % 0 & LABORATORY TEST DATA CORE RUN & % RECOVERY DEPTH (FI.) GRAPHIC OTHER DESCRIPTION Plastic limit |------- Liquid limit TEST DATA CORE 100 120 140 📥 60 80 sol 100 🖸 20 40 60 80 0.2 PEAT - dark brown, damp. 19;20 UF SILT-little fine sand, light brown oxidization 1.5 SAND - fine to coarse. 3.0 3.0 excavated by shovel to 3 F SILT-trace fine sand, low plastic, determine depth of medium brown active layer 7.0 000 GRAVEL - coarse to fine, 000 some fine sand, pebbles to 2', occas. 3' 10 00 Poorly graded, gravel to approx. 1½' some coarse to line sand ٥

13011

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D 09 M 08 Y 75 TIME: 20:45

PROJECT

ELEVATION

AIR TEMP.

PIPE MILEAGE :

68⁰56'56''N, 134⁰08'04''W

FINISH :

A 23476-99, 100

HELI-DRILL

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TEST HOLE LOG

OF 2

TEST HOLE No.

SHEET 1

N75-107B-B1-B

1975 BORROW INVESTIGATION

CANADIAN ARCTIC GAS STUDY LIMITED

NORTHERN ENGINEERING SERVICES

COMPANY LIMITED

CALGARY ALBERTA

ENGINEERS FOR

REMARKS

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1.M.B.

FACILITY

RIG :

LAT. & LONG

METHOD :

D 09 M 08 Y 75 TIME: 19:20

AIRPHOTO No. :

TEST HOLE

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- 99

TEST HOLE LOG

DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG	DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0		NBORATO nsity (pcf) limit ⊢ 80 40	Ο γ	T DATA Voter co I Liquid 120 80	ntent limit	% 140 ▲ 100 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FT.)	R	EMARKS
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-					10	-					+	+1						-	1	
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26-	F	. ° ° d	(coarse gravel,+3 ^{'')}			-	+				+							-	-	
-	ľ	ໍ່	<u>27.0</u> cobble, approx. 6"				╇╌╂─				-	+						-		
28							+	-	+		-						i	28 -	19:50	Hew 3 7/8
+			29.0 End of hole															29	20:45	Walmac
		Ì																		Seizing at 2 swivel jumpi
																				from skids. Reamed hole;
1												Π								abandoned.
oggi		Y:	J.J.S. FACILITY:			PRC	DJECT :	13011				k	1975 BORROW II	IVEST	1047	 104			TEST H	DLE No.
HKD		_	9.0. LAT. & LONG : 88 ⁰ 56*56*1, N, 134 ⁰ 0; L.N.B. AIRPHOTO No. : A 23478-98, 180	8'04''	1		VATION : E MILEAGE												4	
HKD			<u>қ м.в.</u> Аіярното №.: А 23478-99, 100 D.O. Rig: Hell-Gaill				TEMP. :	"A ⁰ , C	-			¥0	(/) · · · · · · · · · · · · · · · · · · ·	ALGABY	LIMITE		-3		N75-1	07B-01-8
			METHOD AIR									Engin	narring Servers impany Limited	LINGINEEN	5 708					

00 ŝ SOIL GROUP SYMBOI GRAPHIC LOG SAMPLE CONDITION CORE CONDITION NRC ICE TYPE VISUAL ICE % O & LABORATORY TEST DATA CORE RUN & % RECOVERY ۰ŏ DEPTH (FL) DEPTH (FL) GRAPHIC ▲ Dry density (pcf) O Water content % SAMPLE TYPE OTHER REMARKS DESCRIPTION - Liquid limit Plastic limit + TEST DATA 140 🔺 80 100 120 60 Щ SOIL 100 🖸 20 40 60 80 33 Pt 10;30 ÜF PEAT - fine fibrous, dark brown, moist 3 pebbles at 0.3 SAND - medium to coarse, silty, S below surface some gravel to 1½'' 4%, ₩almac 2 -3.0 F 4.0_____ little coarse sand, fine grave! 4 10 6 SAND - fine grained, silty, medium grey. 8 To 3 7/8" 10:38 9 Wal nac 10:42 10 25 12 11 13.0 13.0 ICE I CE ICE 14 TEST HOLE 18 16 TEST HOLE No. No. FACILITY: PROJECT LOGGED BY: 13011 1.1.8 **1975 BORROW INVESTIGATION** 68°56'56''W, 134°09'12''W ELEVATION : CHKD LAT. & LONG D.O. N75-107B-B1-C PIPE MILEAGE : NORTHERN ENGINEERING SERVICES AIRPHOTO No. : DRWN. BY: 9. M. B. A 23476-99 N75-107B-B1-C COMPANY LIMITED 9°C AIR TEMP. RIG : CALGARY ALBERTA CHKD: 0.0. HELI-DRILL ENGINEERS FOR METHOD : AL R SHEET 1 OF 3 FINISH : D 10 M 08 Y 75 TIME: 11:00 CANADIAN ARCTIC GAS STUDY LIMITED 08 Y 75 TIME: 10:30 START: M D 10

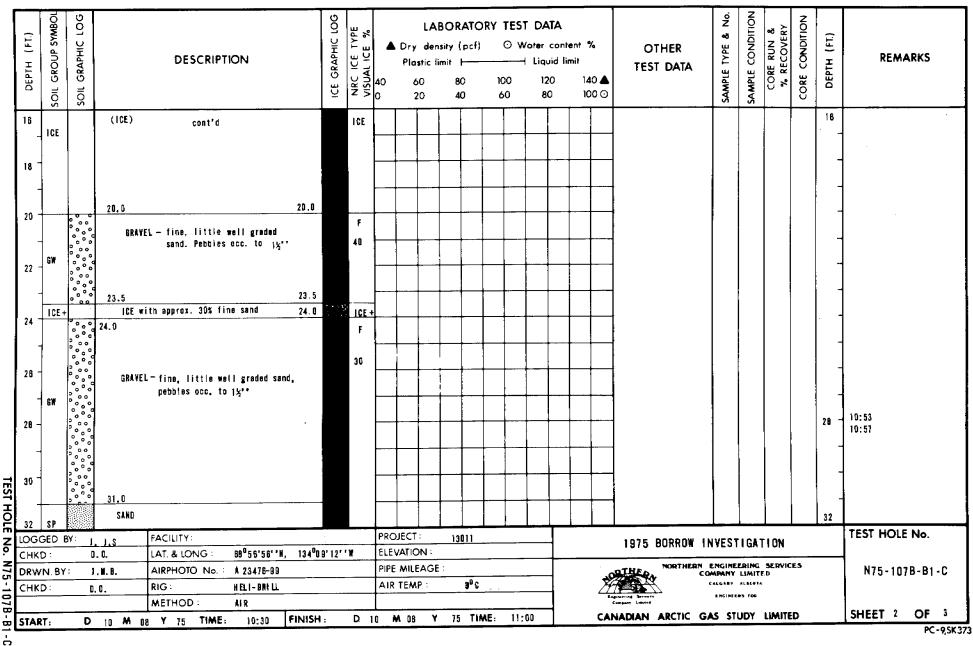
TEST HOLE LOG

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PC-9,5K373

TEST HOLE LOG

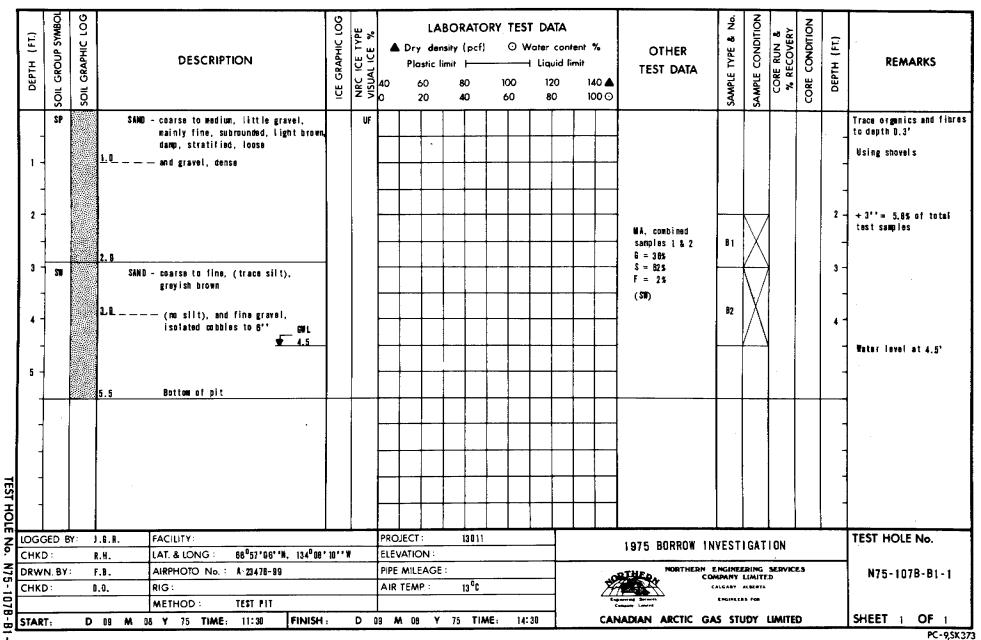


- 102 -

	DEFTH (FL.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 Q	Dry	densi t fic lim i)	y (pci	f) (∋ w₀ 0	DATA Her conv Liquid I 120 80	imit L	% 40 ▲ 00 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FL)	REMARKS
3	2	SP			(cont'd) unilerm, medium (trees coarse) End of hole		F 35 45															32 - - - 38	11:00
TEST HOLE No.	- • - • - • - • - • - •				Circulation failing. Ico noticed on bit. Toeth on bit badly chipped.																	-	
<u>s</u> i	HKC	N. BY		J.J.\$ D.0. J.M.B. D.0.	FACILITY: LAT. & LONG : 00°58'58'18, 134 ⁰ 0 AiRPHOTO No. : 4 23476-89 RIG : NELI-DRILL METHOD : AiR) 9' 12'		ELE	VATION MILEA TEMP	GE ·	130 0 ⁴ C					Ž	222 N. NY	INGINE IPANY	ERING LIMITS ALBERTA	SERVK	CES		TEST HOLE No. N75-107B-B1-C
	TAR	T:	D	10 M	R6 Y 75 TIME: 10:30 FINISH	i :	Dı	• •	M 08	¥ j	15 TI	ME :	11:00			CAN	NADIAN ARCTIC GA	s st	UDY	LIMIT	ED		SHEET 3 OF 3 PC-9,5K3

TEST HOLE LOG

PC-9,5K373



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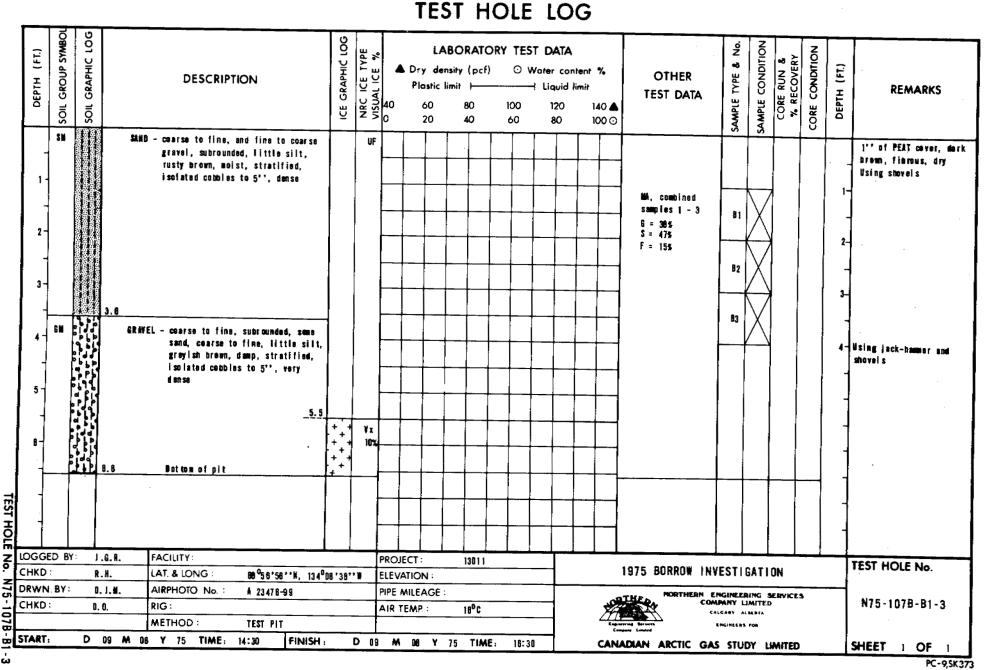
TEST HOLE LOG

Ŝ SAMPLE CONDITION CONDITION 100 ICE GRAPHIC LOG SOIL GROUP SYMBOI RECOVERY LABORATORY TEST DATA TYPE E % ۰Ö DEPTH (FI.) DEPTH (FT.) GRAPHIC ⊙ Water content % ▲ Dry density (pcf) SAMPLE TYPE OTHER NRC ICE 1 VISUAL ICE REMARKS DESCRIPTION - Liquid limit Plastic limit -TEST DATA CORE CORE % 140 📥 100 120 80 60 SOIL 100 🖸 80 20 40 60 Using shovels ١F GRAVEL-mainly fine, subrounded to GP 00 rounded, and sand, coarse to fine, ۰°, 0.7 rusty brown, moist, loose. 1 SAND-coarse to fine; trace gravel, fine, 1 SW subrounded: light brown, moist, stratified, loose. 1.5 °.° GRAVEL-mainly fine, subrounded; and sand,coarse to medium; light brown, damp, stratified, isolated 2 MA, combined ° ° ° 2 samples 1-3 00 **B**1 coppies to 5", loose GW 3 G = 52%ົດ° ດັ 3 00 S = 48%0.00 F = 2% 0 4 4 00 ° 。 ° **B**2 °°° • 0,0 5.0 5 , ° ° ° and sand. 5 °°°, ... B3 0 8 **B**.... 6 -• Excessive sloughing. 00 1 1 00 TEST HOLE Permatrost at 7.6' ° ° ° Bottom of pit Frozen at 7.5' <u>`</u>`` 7.5 TEST HOLE No. PROJECT FACILITY 13011 INVESTIGATION LOGGED BY: No. J.G.R. 1975 BORROW ELEVATION 68⁰56'56''N,134⁰08'04'' W LAT. & LONG : CHKD 8.9. NORTHERN ENGINEERING SERVICES PIPE MILEAGE N75-107B-B1-2 N75-1078-81 THE AIRPHOTO No. COMPANY LIMITED DRWN. BY: A. M. A 23476-99 AIR TEMP. Approx. 13⁰C CALGARY ALBERTA D. C. RIG : CHKD ENGINEERS FOR METHOD : Located TEST PIT OF SHEET 1 CANADIAN ARCTIC GAS STUDY LIMITED M 08 Y 75 TIME: 16:30 FINISH : D 85 D 09 M 08 Y 75 TIME: 14:45 START: PC-9,5K373

TEST HOLE LOG

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00 SAMPLE CONDITION **GROUP SYMBOI** ICE GRAPHIC LOG SAMPLE TYPE & No. CORE CONDITION NRC ICE TYPE VISUAL ICE % LABORATORY TEST DATA CORE RUN & % RECOVERY (FT.) (FT.) GRAPHIC I ▲ Dry density (pcf) ○ Water content % OTHER DESCRIPTION DEPTH REMARKS DEPTH Plastic limit + ----- Liquid limit TEST DATA 60 80 100 120 140 📥 SOIL sol 20 40 60 80 100 🖸 33 0.2 UF Using shovels PEAT - black, fibrous, moist Pt ۴, SAND - coarse to fine, some gravel, mainly SWfine, subangular, little silt, S rusty brown, moist, dense 1 -_1<u>.3</u> __ and gravel, color changes to light grey 11 1.9_ isolated cobbles to 4'', little gravel; 2- few fibres to depth 2.4' 2 dark grey, damp, very dense 6.2 B1 O MA, combined 3 3 samples 1 - 3 6 = 31% S = 58% F = 11% 4 11 5-5 5.5 Using jack-hammer **B**2 no silt, wet, dense 2.2 Θ ŧŧ 6-6-6.2 B3 l b Ð 3.7 7-7 TEST HOLE No. 11 Bottom of pit 7.4 11 TEST HOLE No. PROJECT : 13011 FACILITY LOGGED BY: J.G.R. 1975 BORROW INVESTIGATION 68056'56"'N, 134009'12" W ELEVATION CHKD LAT. & LONG R.H. N75-PIPE MILEAGE NORTHERN ENGINEERING SERVICES DRWN, BY: AIRPHOTO No. A 23476-99 D.J.M. N75-107B-B1-4 COMPANY LIMITED 16⁰C AIR TEMP RIG : CHKD: D.O. CALGARY ALBERTA 107B ENGINEERS FOR METHOD : TEST PIT SHEET 1 OF 1 FINISH : D 09 M 08 Y 75 TIME: 19:45 CANADIAN ARCTIC GAS STUDY LIMITED ÷ START: D 89 M 08 Y 75 TIME: 16:45

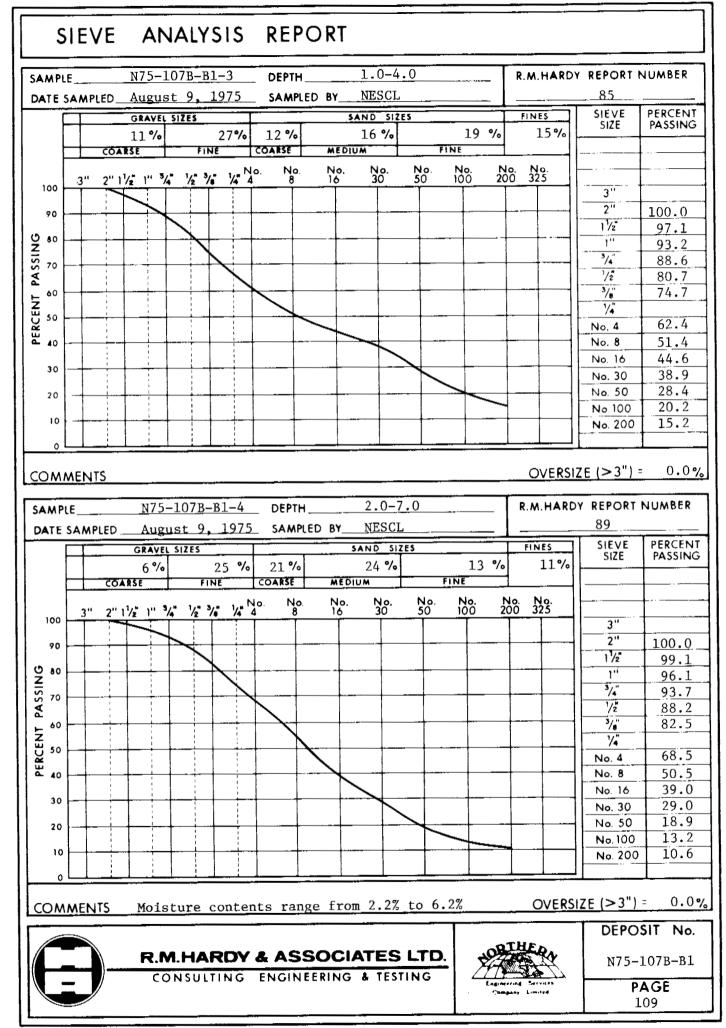
TEST HOLE LOG

PC-9,5K373

<u> </u>	51	EVE		NAL	.YS	IS	RE	PC	RT						· · · · · · · · · · · · · · · · · · ·	
SAM	PLE		N75	-107	B-B1	-1	_ DEF	•тн		2.5-5.	0		.	R.M.HARD	Y REPORT	NUMBER
DATE	E SA	MPLED_	Aug	ust	9,1	<u>975</u>	SAA	MPLED	BY]	NESCL			. .		42	
	_	· ·	GRAVE	L SIZES	;				5,	AND SIZ	S			FINES	SIEVE	PERCENT
			9%		2	7%	19	%		27 %		16	%	2%	SIZE	PASSING
	-	CÔA	RSE	<u> </u>	FINE		COARS		MEDIU			FINE		2 / 1		
						N		No.	No.	Na	No.					
100		3" 2"1	¹ /z 1" 3	14 1/2	∛"	1/4 4	0. 1	8	16	No. 30	50	No. 100	No. 200	No. 325		
															3"	100.0
90	·			\mathbf{N}		+		+	<u> </u>						2"	98.0
0.00															11/2"	96.7
PERCENT PASSING 05 00 02 08	· · ·				$\overline{\mathbf{N}}$			1	-+						1''	93.0
S 70	-			\downarrow				+	_ _						3/4	90.6
L ₹															1/2	86.3
⊨ °°		1 1			+	<u>+</u>		+	-						3/8	81.2
1 50															74	
l ä			1					\mathbf{k}			_				No. 4	63.8
a 40		+ + +	_		-+	+ +		+							No. 8	47.5
30															No. 16	37.4
J 30								T		$\overline{}$					No. 30	26.8
20	-	╉╼┊┨		+ +						$-\lambda$					No. 50	9.6
															No. 100	3.2
10	-				+			1		_					No. 200	2.0
0								<u> </u>					_			2.0
		MPLED_	Augus	st 9,	<u>, 19</u>				8Y_1	NESCL					Y REPORT	
	\vdash		GRAVEL						54	ND SIZI	S			FINES	SIEVE SIZE	PERCENT PASSING
			12%	1		%	16 °			22 %		8 '	%	2%		
		COAL	ISE		FINE		COARSE		MEDIU		الغنيب	INE				
		3" 2" 1	/2 1" 3/	/= ¹ /s"	1	1/2 N	o. N	io. 8	No.	No.	No.	No. 100	No.	No.		
100						<u> </u>		<u> </u>	Ť		<u> </u>	<u> </u>				
90						1 I									2"	
		<u> </u>			_	4		+							3"	100.0
					-			+	_		_				2"	100.0
	-														2" 1½	97.0
													-		2" 1½" 1"	97.0 92.5
					$\overline{\mathbf{x}}$										2" 1 ¹ /2" 1" 3/4"	97.0 92.5 88.0
PASSING															2" <u>1¹/2"</u> <u>1''</u> <u>3'/4</u> <u>7'</u> 2"	97.0 92.5 88.0 78.5
PASSING															2'' 1'/2" 1'' 3/4" '/2" 3/6"	97.0 92.5 88.0
PASSING															2'' 1'/2" 1'' 3/4 	97.0 92.5 88.0 78.5 69.5
PASSING															2'' 1'/2" 1'' 3/4 7/2" 3/6" 7/4 No. 4	97.0 92.5 88.0 78.5 69.5 47.7
PASSING 20 20															2'' 1'/2" 1'' 3'/4" '/2" 3'/6" '/4 No. 4 No. 8	97.0 92.5 88.0 78.5 69.5 47.7 33.8
PASSING 20 20															2" 1½ 1½ 3/4 ½ 3/6 ½ No. 4 No. 8 No. 16	97.0 92.5 88.0 78.5 69.5 47.7 33.8 24.3
60 00 00 00 00 00 00 00 00 00 00 00 00 0															2" 1½ 1½ 3/4 ½ 3/6 ½ No. 4 No. 8 No. 16 No. 30	97.0 92.5 88.0 78.5 69.5 47.7 33.8 24.3 16.2
PERCENT PASSING															2" 1 ¹ /2" 1 ¹ /2" ³ /4 ¹ /2" ³ /8" ⁷ /4" No. 4 No. 4 No. 8 No. 16 No. 30 No. 50	97.0 92.5 88.0 78.5 69.5 47.7 33.8 24.3 16.2 6.7
60 00 00 00 00 00 00 00 00 00 00 00 00 0															2" 1 ¹ /2" 1 ¹ /2" 3/4 ¹ /2" 3/6" ¹ /4 No. 4 No. 4 No. 8 No. 16 No. 30 No. 50 No. 100	97.0 92.5 88.0 78.5 69.5 47.7 33.8 24.3 16.2 6.7 3.4
00 00 00 00 00 00 00 00 00 00 00 00 00															2" 1 ¹ /2" 1 ¹ /2" ³ /4 ¹ /2" ³ /8" ⁷ /4" No. 4 No. 4 No. 8 No. 16 No. 30 No. 50	97.0 92.5 88.0 78.5 69.5 47.7 33.8 24.3 16.2 6.7
080 70 80 80 80 80 80 80 80 80 80 80 80 80 80		NTS												OVERSIZ	2" 1 ¹ /2" 1 ¹ /2" 3/4 ¹ /2" 3/6" ¹ /4 No. 4 No. 4 No. 8 No. 16 No. 30 No. 50 No. 100	97.0 92.5 88.0 78.5 69.5 47.7 33.8 24.3 16.2 6.7 3.4 2.4
000 000 000 000 000 000 000 000 000 00		NTS												OVERSIZ	2" 1 ¹ / ₂ " 1" 3/ ₄ " 1/ ² 3/ ₆ " 7/ ⁴ No. 4 No. 8 No. 16 No. 30 No. 50 No. 100 No. 200	97.0 92.5 88.0 78.5 69.5 47.7 33.8 24.3 16.2 6.7 3.4 2.4 0.0 %
00 00 00 00 00 00 00 00 00 00 00 00 00		NTS												OVERSIZ	2" 1 ¹ / ₂ 1 ^{''} 3 ['] / ₄ ['] / ₂ ³ / ₆ ['] / ₄ No. 4 No. 8 No. 16 No. 30 No. 50 No. 100 No. 200 ['] / ₆ ['] / ₂ ['] / ₂	97.0 92.5 88.0 78.5 69.5 47.7 33.8 24.3 16.2 6.7 3.4 2.4 0.0 %

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-	Y OF LABORATORY TE FOR ' OF AGGREGATES IN		
SAMPLE No. N75-107B-B1 DEPTH (FT.): 0-3	-3DATE SAMPLED : August 9, DATE TESTED : February,		PLED BY: _{NESCL} ED BY : _{RMHA}
SOUNDNESS OF AGG SULPHATE TEST	REGATE	ORGANI TEST	C IMPURITIES
COARSE AGGREGATE	E : LOSS = 3.36 % : LOSS = 3.02 %		R : 5 EMOVED : 4
LOS ANGELES ABRA	SION TEST	REMOVE	ROOTLETS D:3+ CONTENT:Trace
PERCENT LOSS =	19.8 %		CANCE :
SUMMARY OF ROCK TYP	ES, COARSE AGGREGATE. (F	PETROGRAP	HIC ANALYSIS)
ROCK TYPE	CLASSIFICATIONS	5	TOTAL WEIGHTED COMPONENT %
Quartzite	Very strong, Good		
Sandstone Siltstone	Strong, Good		5.7 1.05
Chert Flint	Potentially reactive, Fair		1.25 2.35
Ironstone	Soft, Poor		0.45
PN = 130 INTERPRET recommend and absorpt	further examination of alkaline	aggregate, reactivity	37.6
COMMENTS : Further	tests recommended. Chert compon d further examinations. Strengt	-	
POBTHE O	CONSULTING ENGINEER		DEPOSIT No. N75-107B-B1
Engineering Servet Company Limited			PAGE 110

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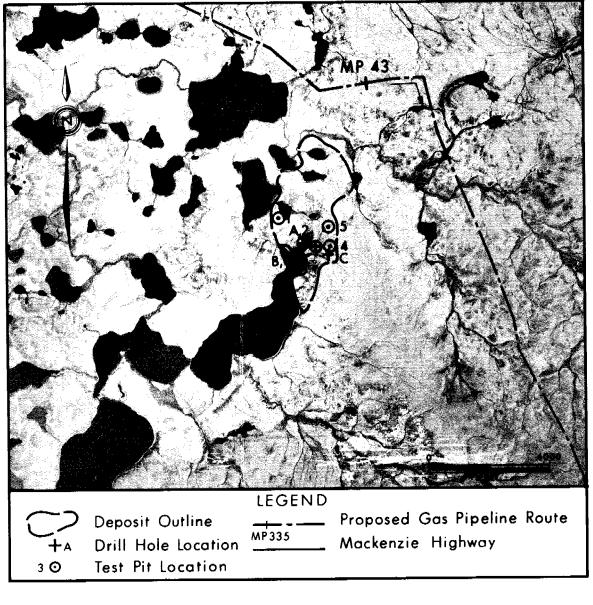
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beds of silt and clay.

Physical Setting: Deposit 107B-B2 consists of two parts: the northern
portion is an outwash plain modified by thermokarst,
the southern portion is a series of gravel benches along
an escarpment.
Material: SAND and GRAVEL - interbedded, well graded, with occasional

Volume: 5,400,000 cubic yards.

Assessment: Deposit 107B-B2 is a source of fair to good quality granular material. Areas exploited will be dictated by the thickness of overburden. Haul distance to the pipeline right of way is in excess of ½ mile across a small valley. Material is suitable for general fill, backfill, building pads and possible concrete aggregate.



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Airphoto No.A23476-100Approximate Scale:1" = 4900'

Latitude : 68° 54' Longitude : 134° 06'

DEPOSIT 107B-B2

PHYSICAL SETTING

Deposit 107B-B2 is located at the northern end of the Wolverine Lakes, approximately 40 miles north-northwest of Inuvik. The proposed pipeline right of way passes about 2 miles to the north and east of the deposit. This deposit corresponds to source number 319 in the Ripley, Klohn, Leonoff DIAND Granular Materials Inventory Zone III (1972) report.

This deposit consists of two separate parts. The southern tip of the deposit is a series of gravel benches along the edge of a 200 foot escarpment, which flanks a meltwater channel. These benches are composed of erosional Tertiary remnants, kame terraces or slump blocks. The benches have flat to gently sloping surfaces separated by steep slopes. The flat upper surfaces are dotted with 10-foot gravel knobs. Except for local patches of silt, this area has a negligible amount of over-burden and the drainage is generally good.

The northern portion of the deposit is an outwash plain modified by thermokarst. Relief is gently rolling with lakes inset 20 to 60 feet below the general surface level. The area is moderately well to imperfectly drained, with variable cover of up to 10 feet of silt and peat. It would be safe to assume that about half of the plain has less than 3 feet of overburden. Depending on the ground cover, the active layer varies from 2 to 7 feet.

BIOLOGICAL SETTING

The surface of the deposit, except for bare gravelly patches along the southern escarpment, is mainly covered by dwarf birch, willow and lichen with sedges in poorly drained areas. Reindeer occur in the area throughout the year and moose are occasionally present during the summer season. Numerous Arctic ground squirrel dens were observed at the site. Grizzly bears used the area, as was indicated by diggings at ground squirrel dens. The area provides year-round habitat for foxes and wolves. The lower slopes of the site provide good passerine nesting habitat. Adjacent lakes provide water-fowl habitat during the open-water season. Wolverine Lake supports several species of fish including lake trout, whitefish, pike and burbot.

MATERIAL

NESCL drill holes and test pits, plus the DIAND Granular Materials Inventory Zone III report, show the deposit to consist of interbedded sand and gravel with occasional beds of silt and clay. Sand and gravel is well graded and usually subrounded. Ice is abundant in sands and gravel and massive ice was encountered in nearly all test holes. The quality of material varies greatly throughout the deposit. Petrographic analysis of gravel from one DIAND test hole showed sound material including quartzite (81%), a marginal sandstone (11%), with quartz (5%), chert and a trace of ironstone (8%).

VOLUME

In the southern portion (terraces), ice appears at depths of 5 to 20 feet. Total estimated volume, based on 30 acres and 10 feet of materials, is 400,000 cubic yards. In the approximately 340 acres of outwash modified by thermokarst, sand and gravel appears to be present to depths of more than 35 feet, and volume is estimated to be 5,000,000 cubic yards. Total volume is therefore 5,400,000 cubic yards.

DEVELOPMENT AND REHABILITATION

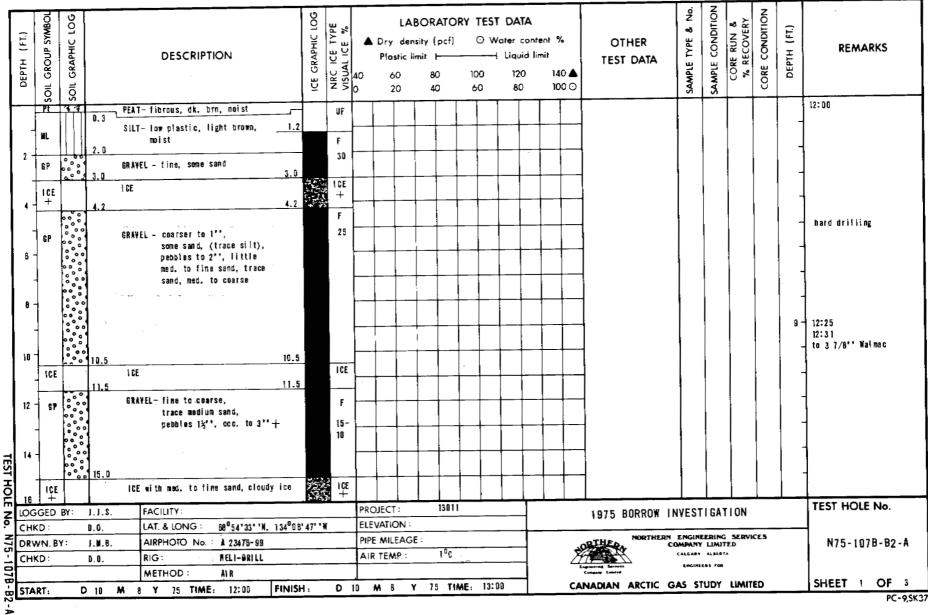
Deposit 107B-B2 is a source of fair to good quality granular material. Areas to be exploited will be dictated by the amount of peat and overburden cover as well as insitu material quality and ice contents. Granular material from this deposit may be used for general fill, backfill in pipeline construction, building pads, and concrete aggregate production if the material is found to be suitable. No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

The equipment may be staged via the pipeline right of way to the deposit. Haul distances from the deposit to the pipeline right of way are in excess of half a mile. A small valley between the deposit and the right of way would have to be crossed. In order to minimize environmental damage, snow roads would be built to transport the borrow material from the deposit to haul points on the right of way.

Initially, the peat cover and overburden would be stripped from the area to be excavated, and stockpiled around the edge of the excavation.

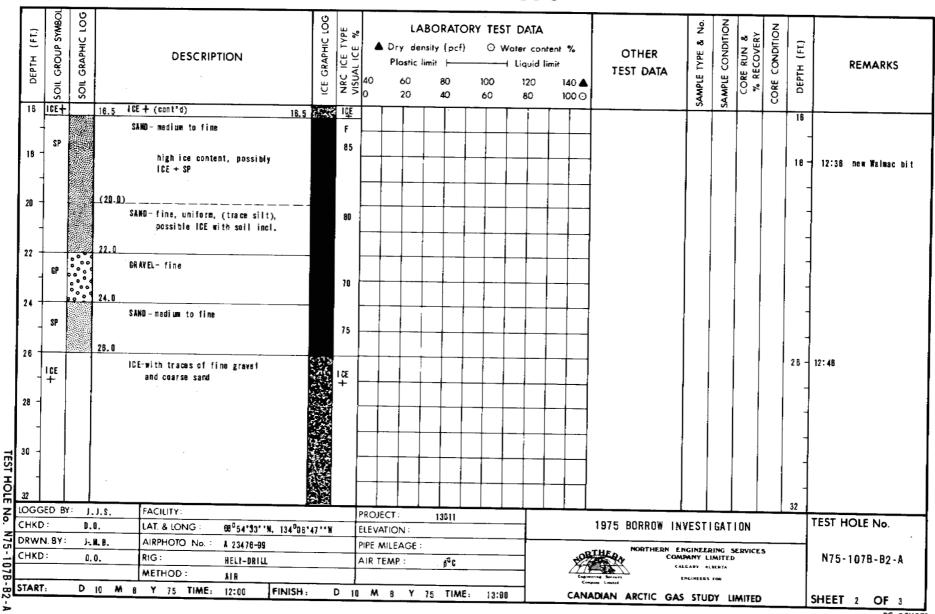
Development of this deposit would involve excavating borrow material evenly from the higher, well drained knobby areas so that good drainage would be established over the area. Excavations would be kept away from Wolverine Lake and any drainage channels so that siltation would not take place. This type of development could be established by using blasting or conventional earthmoving techniques, depending on the degree of ice cementation. The excavated material may have to be stockpiled, thawed, and drained before it is used. Crushing and/or screening of the material may be required to produce quality construction aggregates. The effects of the borrow excavation on the thermal degradation of the insitu material will require careful consideration in view of the massive ice sheets at relatively shallow depths.

Equipment required for development would be dozers, rippers, end dump trucks, front end-loaders; as well as screening, drying, crushing and concrete plants, if required. A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.



TEST HOLE LOG

PC-9,5K373



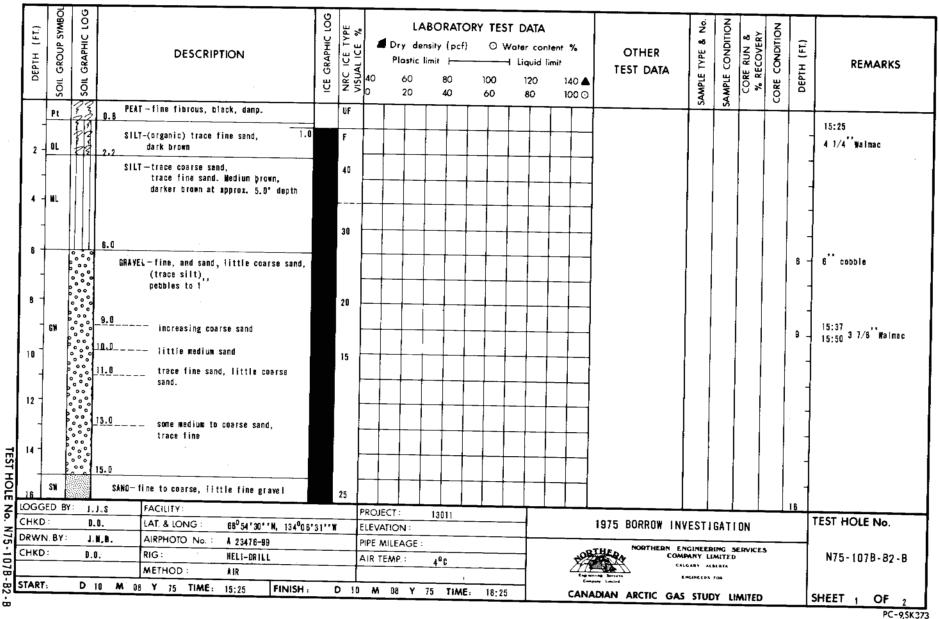
TEST HOLE LOG

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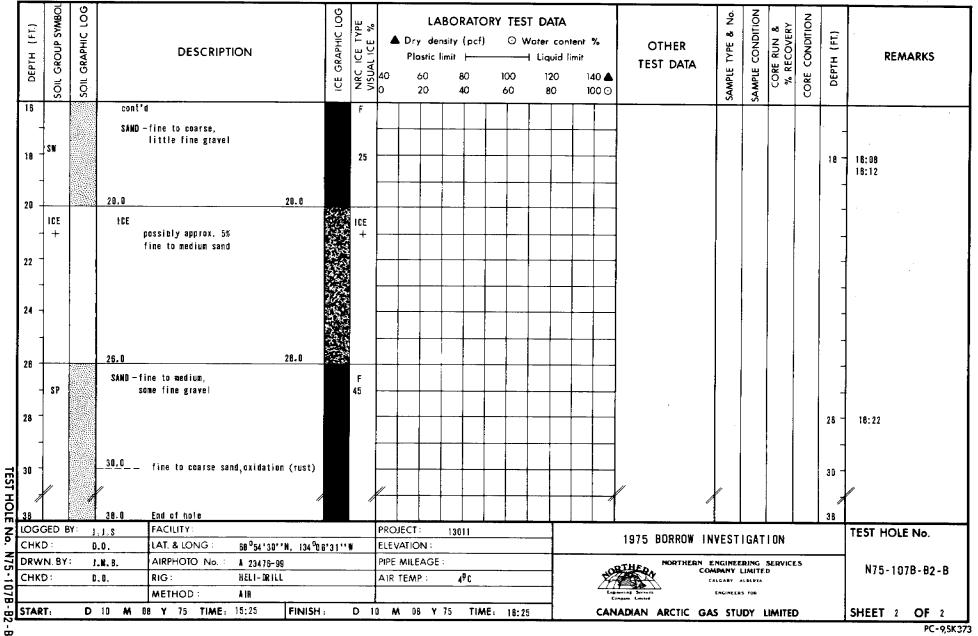
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CEDTU (ET)		SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	▲ 40 0	Dry	dens stic lir 0	ity (p	ocf)	O	₩0 -	DATA ter co Liquid 120 80	ntent limit 1.	% 40 ▲ 00 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
3	2	61 -		CLA	Y-medium plastic, white (creamy)		F 10									-							_	
3	4-			35,0		-								_									-	
	16 +	SP		36.0 SAN	iD-medium, uniform		10		_			\rightarrow	_			+							36	1 3: 00
				End	i of hole					_				_									-	
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		GED I		J.J.S.	FACILITY				JECT		1	3811						1975 BORROW I	IVEST	IGAT	TION			TEST HOLE No.
z⊢	HK			0.0.	LAT. & LONG : 68 054"33" N, 1340 AIRPHOTO No. : 4 23476-99	0 6' 47'		+	VATIC MILE		:				-+			NORTHERN	ENGIN	ERING	SERVI	CES		NTE 1078 PO 4
75	HK	N. BY		Í.M.B. D.D.	AIRPHOTO No. A 23476-99 RIG: HELL-DRILL				TEM			1°C					×		CALGARY					N75-107B-B2-A
SI.				P. V.	METHOD : AIR	_		\square		-							Δ_i	Agnassing Servers Company Limited	ENGINE	LAS 709				
÷, s	TAR	T:	D	10 M E	8 Y 75 TIME: 12:00 FINISH	1:	D	10	M 8	Y	75	TIN	E: 1	13:00			CA	NADIAN ARCTIC G	AS ST	UDY	LIMIT	ED		SHEET 3 OF 3 PC-95K3

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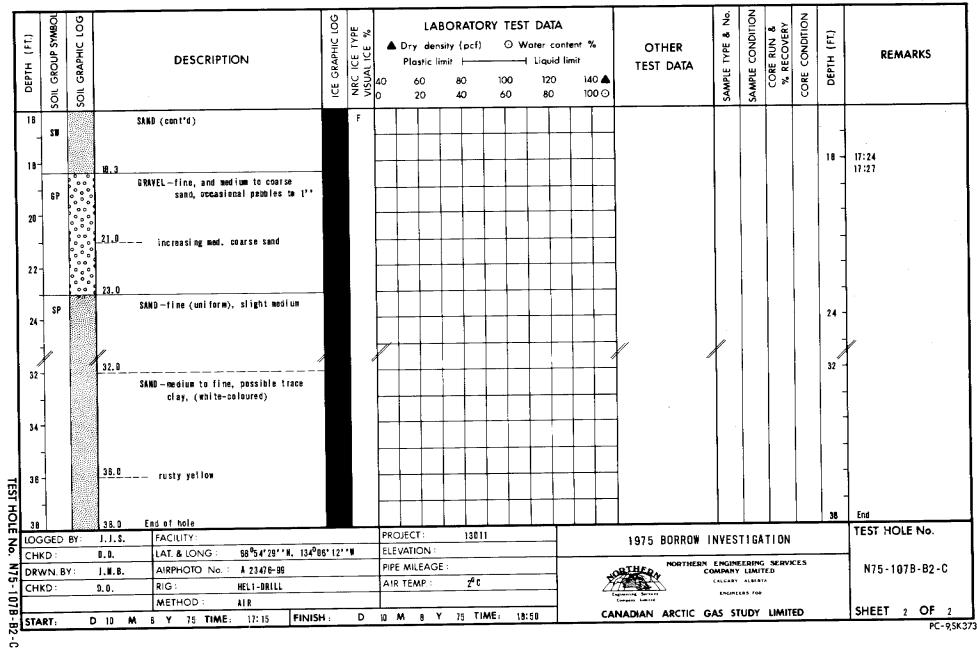
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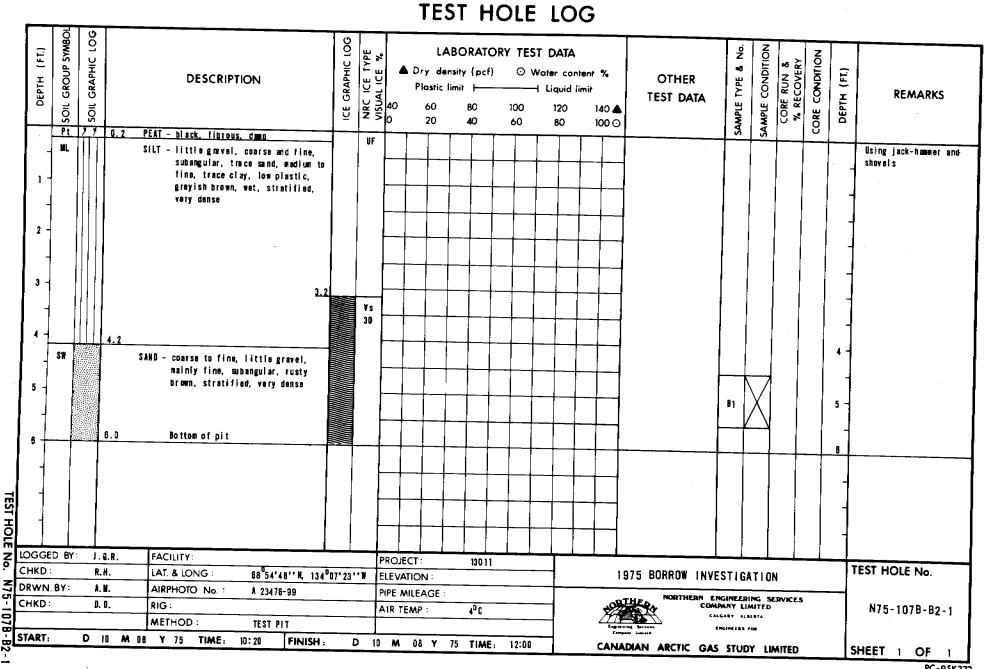
DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	L/ Dry de Plastic 60 20	ensity limit	(pcf)		Nater H Liqu 124 80	conte id lim D			OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
	Pt	320	0.8	PEAT-fibrous, black,moist		UF			-									1-	<u> </u>		<u> </u>	18:55
2 -		a la la	2.5	SILT-(organic), little fine gravel, <u>1.</u> trace fine sand, low plastic, dafk brown	3	F 20															1.3 - -	- 17:15 4½'' Walmac
4 -	GP			GRAYEL-fine to coarse, some medium to coarse sand, rusty (oxidized), pebbles to 1½**		10															-	
8 - -				no oxidization											_						-	
8 -	SP		10.0	SAND — wedium to coerse					-												- 9 -	17:19 Chert and 17:22 quartzite
10 + - 12 -				GRAVEL-fine (3/4"),little medium sand																	-	p ebb le s
14 - _ 18	SW		3.5S	SAND-fine, medium to coarse, (no gravel)		15														1	-	
LOGG	ED BY	landid	J.S.	FACILITY			PROJE	CT :		13011		<u></u>		I							16	TEST HOLE No.
CHKD	:	D.	0.	LAT & LONG 68054"28" W, 13406	12""		ELEVA	TION :								1975 BORROW IN		IGAL	1 UN			
DRWN CHKD		J. D.	N. B. D.	AIRPHOTO No. A 23478-99 RIG: HEL1-DRILL METHOD: AIR			PIPE A AIR T	AILEAGE	E :	2 ⁰ C				2	TOR TOR		NGINEE PANY I LGARY A	LIMITE		ES		N75-107B-B2-
START		<u> </u>	10 64	8 Y 75 TIME: 17:15 FINISH			L	• v	76	TIME	18:5			~		ADIAN ARCTIC GAS	сти					SHEET I OF

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No. Z 2 07B

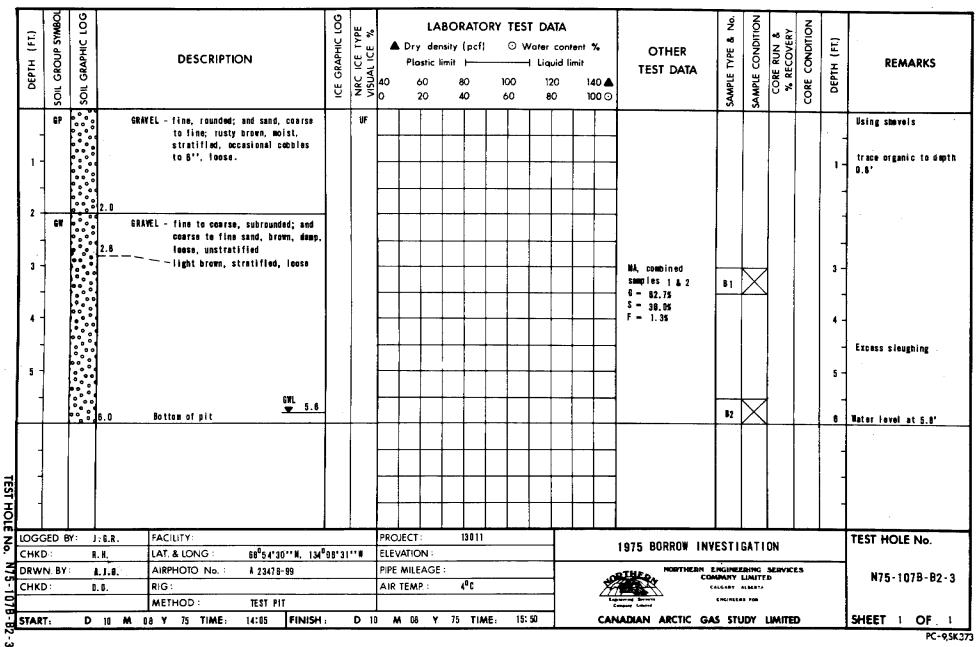
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PC-9,5K373

8 No. SAMPLE CONDITION 500 ICE GRAPHIC LOG CORE CONDITION **GROUP SYMBOI** LABORATORY TEST DATA CORE RUN & % RECOVERY TYPE E % DEPTH (FT.) (FT.) ⊙ Water content % GRAPHIC ▲ Dry density (pcf) SAMPLE TYPE OTHER NRC ICE VISUAL ICE REMARKS DESCRIPTION - Liquid limit Plastic limit + DEPTH TEST DATA 120 140 📥 60 80 100 soll SOIL 100 🖸 20 40 60 80 Using shovels UF SAND - coarse to fine; some gravel, mainly SW fine, subangular, brown, moist, stratified, loose. . 0 GRAYEL - mainly fine, subrounded; and sand, 6P 00 coarse to fine; brown, damp, stratified, isolated cobbles to 2 4'', dense. 81 3 з 4 B2 SAND - coarse to fine; and gravel, fine, SW subrounded; trace silt, greyish 5 5 brown, damp, dense. SAND - coarse to fine; little silt; trace 51 1 fine gravel, low plastic, grey, wet, dense. 6 SAND - coarse to fine; little gravel, SW mainly fine, subrounded, greyish 7 -7. TEST HOLE brown. 1.5 Using jack-hammer and shovels **H** B3 Bottom of pit TEST HOLE No. PROJECT 13011 LOGGED BY: FACILITY No. J.G.R. 1975 BORROW INVESTIGATION 68⁰54'33''N, 134⁰06'47''W ELEVATION : LAT. & LONG CHKD R. H. N75 NORTHERN ENGINEERING SERVICES PIPE MILEAGE : A 23476-99 N75-1078-B2-2 AIRPHOTO No. A.J.B. DRWN. BY: COMPANY LIMITED 4⁰C CALGARY ALBERTA AIR TEMP RIG : D.O. CHKD: 107B ENGINEERS FOR TEST PIT METHOD : SHEET 1 OF 13:00 CANADIAN ARCTIC GAS STUDY LIMITED D 10 M 08 Y 75 TIME FINISH M 08 Y 75 TIME: 10:30 - B2 D 10 START PC-9.5K373

TEST HOLE LOG

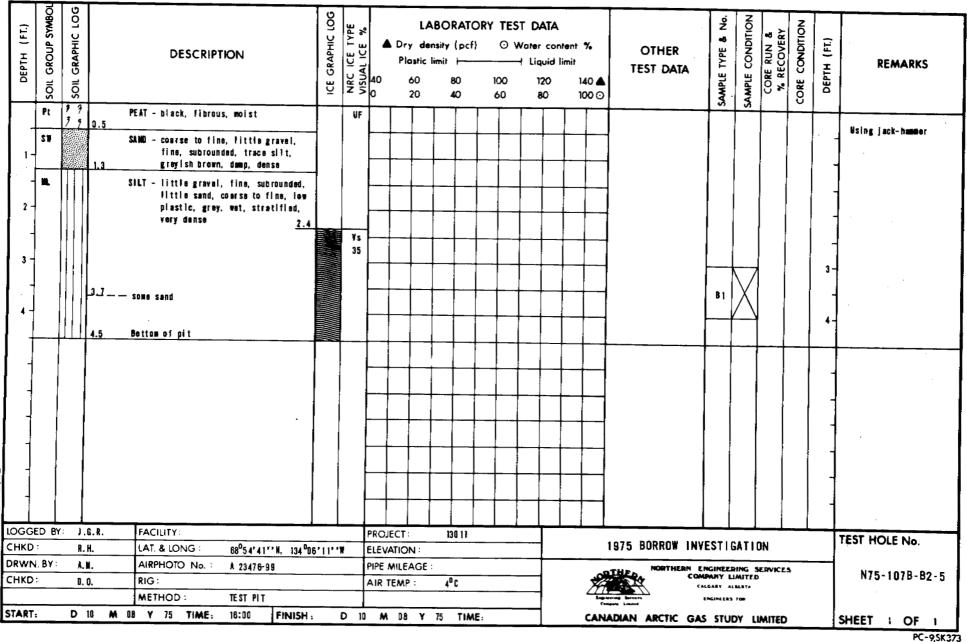


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DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %		Dry d	ABORAT ensity (po : limit		Nater cont Liquid li 120 80	-	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
	SW		SAND	 coarse to fine, and gravel, fine, trace silt, rusty brown, damp, isolated cobbles to 7^{**}, loose 		UF						-						Using shovels
1 -	CH I			L - coarse and fine, subrounded, and sand, coarse to fine, light brown, damp, occasional cobbles to 7'									B1	X			- 1 -	ford laws (PD) and it
2 -													B2				2 -	Sand layer (SP), medil at 2.0' - 2.3'
3 -			3.7										B3 B4	X	*			
4 -	SW		SAND	 coarse to fine, and gravel, fine, subrounded, greyish brown, damp, loose 								S = 40.8% F = 1.2%	85	X				
5												_	B6	X	*		5 -	
6 -	1						\vdash			-			87	X	Y		8 - 8.5	
			6.5	Bottom of pit												1	-	
-												_						
	GED	BY :	J.G.R.		Deeter				130	11		1975 BORROW	INVES	TIGT	ION			TEST HOLE No.
CHK DRV CHK	VN. B	BY :	R.H. A.J.B. D. O.	LAT. & LONG : 86 ⁰ 54'31' 'N, 134 AIRPHOTO No. : A 23476-99 RIG :	-06-12	<u></u>	PIP		GE :	тох. 4 ⁰ С		 NORTHER	ENGIN COMPANY CALGARY	LIMIT	°F.D	CES		N75-107B-B2-
STA		0		METHOD: TEST PIT	H :	Ð	T		¥ 75			 ANADIAN ARCTIC		UDY	LIMIT	ED		SHEET 1 OF PC-9



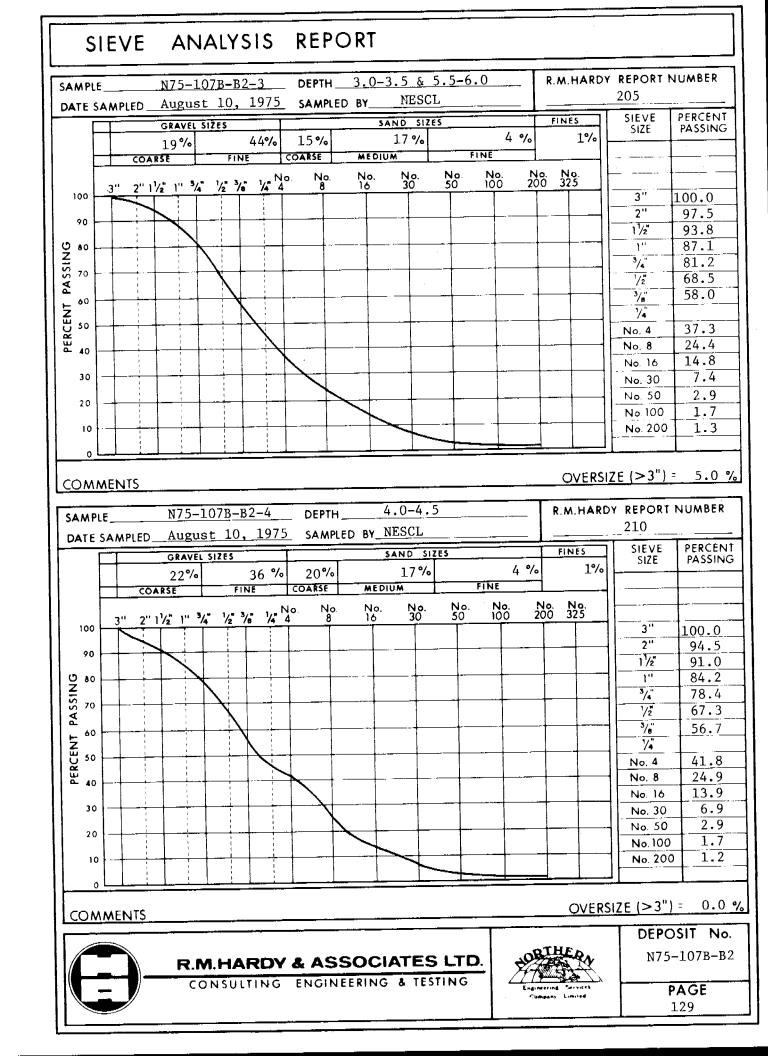


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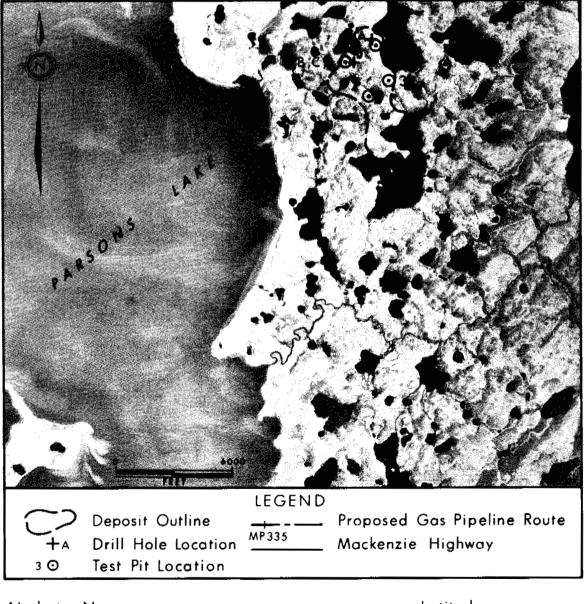
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TEST HOLE No. N75-1078-

B2-5



- Physical Setting: Deposit 107B-B3 is an outwash plain modified by thermokarst located 1.5 miles east of the northeast corner of Parsons Lake. Local relief within this deposit is 120 feet.
- Material: GRAVEL well graded and sand with minor amounts of silt and isolated cobbles.
- Volume: 6,000,000 cubic yards.
- Assessment: Deposit 107B-B3 is a source of an excellent quality granular material. Access from the deposit to the right of way is 6 miles in length across hilly ice cored terrain, or across Parsons Lake. Granular material from this deposit may be used for general fill, backfill, building pads and possible concrete and asphalt aggregate.



Airphoto No. A23476-104 Approximate Scale: 1" = 5000'

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Latitude: 69° 59' Longitude: 133° 30'

DEPOSIT 107B-B3

PHYSICAL SETTING

This deposit is an outwash plain modified by thermokarst. It is located 1.5 miles east of the northeast corner of Parsons Lake and is 6 miles north of the Parsons Lake lateral. The Ripley, Klohn, Leonoff DIAND Granular Materials Inventory Zone III (1972) report refers to this deposit as Source 309.

The outwash plain may have been a kame and kettle complex originally, but the topography has been modified by thermokarst and its original geomorphic form is difficult to determine.

Local relief within this deposit is 120 feet. Although most depressions have steep slopes, the deposit is generally characterized by a gently rolling surface with isolated superimposed ridges and knobs standing 15 to 50 feet above the general level of the deposit.

Overburden varies from negligible on knobs, ridges, steep slopes and some gently sloping areas, to 3 to 8 feet in most depressions and on level areas. Drainage is generally good over most of the deposit but locally, it may be moderately good to imperfect. The active layer ranges from 1 to 6 feet and the ice content in the glaciofluvial material is low.

The terrain between the deposit and the proposed pipeline right of way is hummocky with ice cored hills.

BIOLOGICAL SETTING

This site is covered by dwarf birch, willow, alder, sedge, moss, and lichen. The site is located in a reindeer calving area. Arctic ground squirrel dens were observed on the site together with grizzly bear diggings. Caribou and occasional moose also use the area. A lake to the west of the site supports a small Arctic tern colony. Twelve birds were observed during the 1975 survey. Ptarmigan, passerines, and waterfowl occur throughout the area. Immediately adjacent bodies of water do not appear to support fish populations.

MATERIAL

The materials in this deposit are well graded gravel and sand with minor amounts of silt and isolated cobbles. The gravel appears to be concentrated in the knobs and ridges, but is not confined to them. The glaciofluvial material at the site is probably underlain by preglacial sand, gravel, and silt containing abundant ground ice. The DIAND report and drill holes 107-B3-A and C show massive ice at 8 to 30 feet below the surface.

VOLUME

The total estimated volume of sand and gravel based on 200 acres and 20 foot thickness is 6,000,000 cubic yards. This volume would be decreased if only the knobs and ridges of granular material are considered.

DEVELOPMENT AND REHABILITATION

Deposit 107B-B3 is a source of an excellent quality granular material. Areas to be exploited will be dictated mainly by length of haul, environmental restrictions, local ground ice conditions and overburden. Granular material from this deposit may be used for general fill, backfill in pipeline construction, building pads, and concrete and asphalt aggregate production. The gravel will require further testing prior to use in concrete production. More drilling and test pitting would be required to delineate the areas of best quality material.

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No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

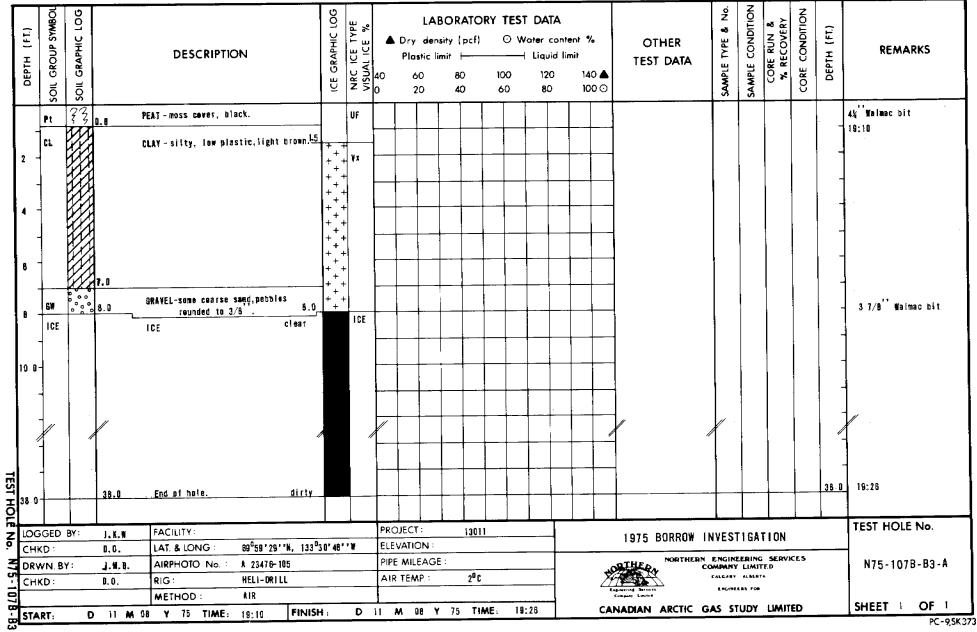
A 6 mile access snow road would have to be constructed from the pipeline right of way to the deposit. This road would cross hilly, ice cored terrain, or the ice on Parsons Lake. If crossing the hilly terrain, care should be taken not to initiate bimodal flows on slopes.

Initially the peat cover and overburden would be stripped from the area to be excavated, and stockpiled around the edge of the site. Borrow material would then be excavated evenly from the knobs and ridges to a grade such that good drainage would be maintained over the area. Excavations would be kept away from the lakes and creeks in the area to prevent siltation. This type of development could be accomplished by using blasting or conventional earthmoving techniques depending on the degree of ice cementation. The excavated material may have to be stockpiled, thawed, and drained before it is used. Natural mixing during excavation will provide adequate good gradations. Crushing and/or screening of the material may be required to produce quality construction aggregates.

Equipment required for development would be dozers, rippers, end dump trucks, front-end loaders, as well as screening, drying, crushing, concrete and asphalt plants if required.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

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DEPTH (FT.)	SOIL GROUP SYMBOI	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40	▲ Dry Pla: 6 2	dens stic lin	ORAT(ity (pcf sit 80 40	;) 1	οw	T DAT (ater c) Liquid 120 80	onten 1 limit		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FI.)	REMARKS
2 -	67	• • • • • • • • • • • • • • • • • • •	6	PEAT - mossy BRAVEL - fine to coarse little cmf. sand, pabbies to 1 5, rounded.clean, rusty brown,moist,occasional cobbles to 6 End of hole		ÜF												S				4% "Welmac bit. pit dug to overcome caving of unfrazen gravels, unsuccessfu because permafrost too deep.
				Refusai due to unfrozen gravel caving into kole.																		20:28
LOGGE CHKD		D.	0.	FACILITY: LAT. & LONG : 88 ⁰ 58' 18' 'N, 133 ⁰ 31'	<u>' </u>]''' 		ELE			13011	!				<u> </u>	1975 BORROW INV	ESTI	GATI	ON			TEST HOLE No.
CHKD). D.		AIRPHOTO No.: A 23476-105 RIG: HELI-DRILL METHOD: AIR			_	TEMP.		2 ⁰ C						al X	GINEER ANY LI SARY AL	MITF.D	ERVICE	3		N75-107B-B3-B
START:		D	1 M	08 Y 75 TIME: 20:00 FINISH:		D 1	1	80 N	Y	5 TIM	E	20:26		_	CAN	ADIAN ARCTIC GAS	STUC	уц	MITED			SHEET I OF

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ŝ SAMPLE CONDITION CORE CONDITION ICE GRAPHIC LOG **GROUP SYMBOL** GRAPHIC LOG CORE RUN & % RECOVERY LABORATORY TEST DATA NRC ICE TYPE VISUAL ICE % O & ۰ð (FT.) DEPTH (FT.) ▲ Dry density (pcf) O Water content % OTHER SAMPLE TYPE REMARKS DEPTH DESCRIPTION Plastic limit |-TEST DATA 140 📥 120 60 80 100 SOIL SOIL 80 100 🖸 60 20 40 4½ Walmac bit. ŬF PEAT - non-woody, roots, brown-black, 33 Pt clear ice at 1.0 1.0 10:14 ICE TCE ÎCF 34 + Pt 33-37 PEAT ¥X 2 + (+ + 3.0 3.0 GRAVEL-fine grained, silty, peobles to F GM ¥, rounded,occasional cobbles, 1°p1 4 rounded to 8 at 5.0 5.0 6 3 7/8 Walmac bit 8.0 cobble to 6 ___ 8 10:17 10 increasing in size ٩. 12.0 100 12 ໍໍໍໍ SRAYEL - fine to coarse, poorly graded, GP little fine sand, trace silt, 00 occasional cobbles, pebbles rounded to 1.0 14 TEST HOLE 3 7/8 tricone bit boulder to 12 10:30 16.0 TEST HOLE No. PROJECT : FACILITY 13011 LOGGED BY: 1975 BORROW INVESTIGATION Š J.K.W 69⁰59'11''N, 133⁰30'26''W ELEVATION : LAT. & LONG D.O. CHKD NORTHERN ENGINEERING SERVICES PIPE MILEAGE : N75-107B-B3-C AIRPHOTO No. A 23476-105 N75-1.1.9. DRWN. BY: COMPANY LIMITED 2⁰ C -----AIR TEMP : RIG : HEL !- DRILL CHKD R.H. ENGINEERS FOR 107B-B3-C METHOD : AI R SHEET 1 OF 2 CANADIAN ARCTIC GAS STUDY LIMITED D 12 M 8 Y 75 TIME: 11:25 FINISH : D 12 M 8 Y 75 TIME: 10:10 START:

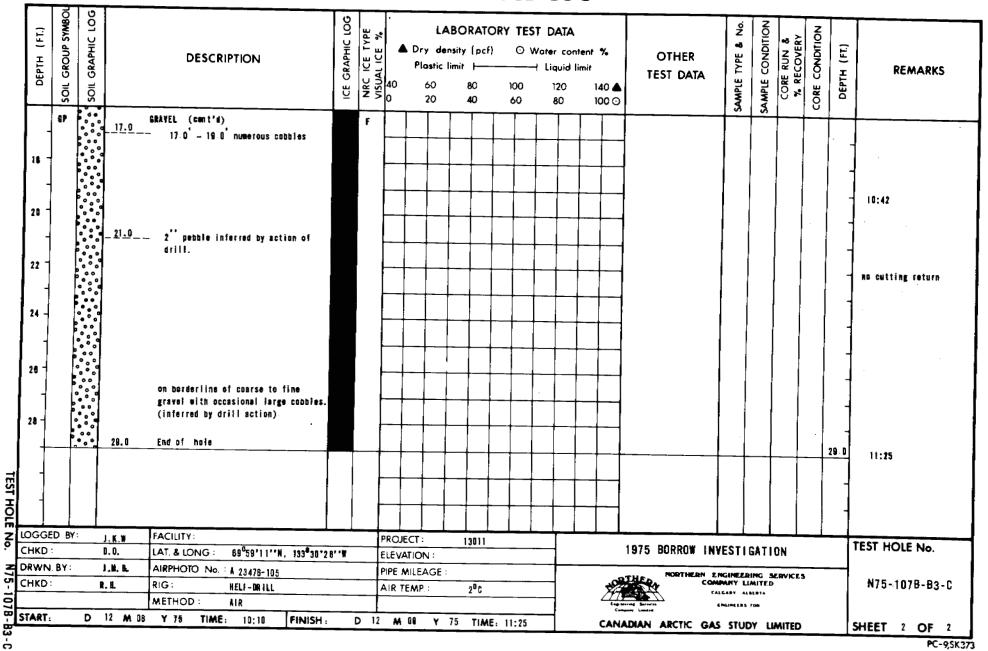
TEST HOLE LOG

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> TEST HOLE No.

> > 1078-

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SAMPLE CONDITION SAMPLE TYPE & No. CORE CONDITION ICE GRAPHIC LOG SOIL GROUP SYMBOL GRAPHIC LOG CORE RUN & % RECOVERY NRC ICE TYPE VISUAL ICE % LABORATORY TEST DATA DEPTH (FT.) DEPTH (FT.) b ▲ Dry density (pcf) O Water content % OTHER REMARKS DESCRIPTION - Liquid limit Plastic limit + TEST DATA 80 100 120 140 📥 60 SOIL 100 🖸 80 20 40 60 Using jack-hammer 39 ÜF PEAT - black, fibrous, damp Ρt \$ \$ No samples taken 0.5 SILT - some fine sand, little gravel, ML. fine, subangular, low plastic, ۱ light brown, wet, stratifled, firm 1.5 ۲s occasional ice lenses to 3'' 50 2 2.2 ---- little sand, to grey Bottom of pit 3.0 TEST HOLE No. TEST HOLE No. PROJECT : 13911 FACILITY LOGGED BY: J.G.R. 1975 BORROW INVESTIGATION ELEVATION : LAT. & LONG : 69°59'29''N, 133°30'48''W CHKD R.H. NORTHERN ENGINEERING SERVICES PIPE MILEAGE N75-107B-83-1 N75-1078-B3-1 AIRPHOTO No. : A 12918-266 DRWN. BY: A.J.B. COMPANY LIMITED Approx. 7⁰C AIR TEMP : CALGARY ALBERTA RIG : CHKD: D. O. -----TEST PIT METHOD : SHEET 1 OF CANADIAN ARCTIC GAS STUDY LIMITED D 11 M 08 Y 75 TIME: 14:00 FINISH : 08 Y 75 TIME: 12:00 D 11 M START: PC-9,5K373

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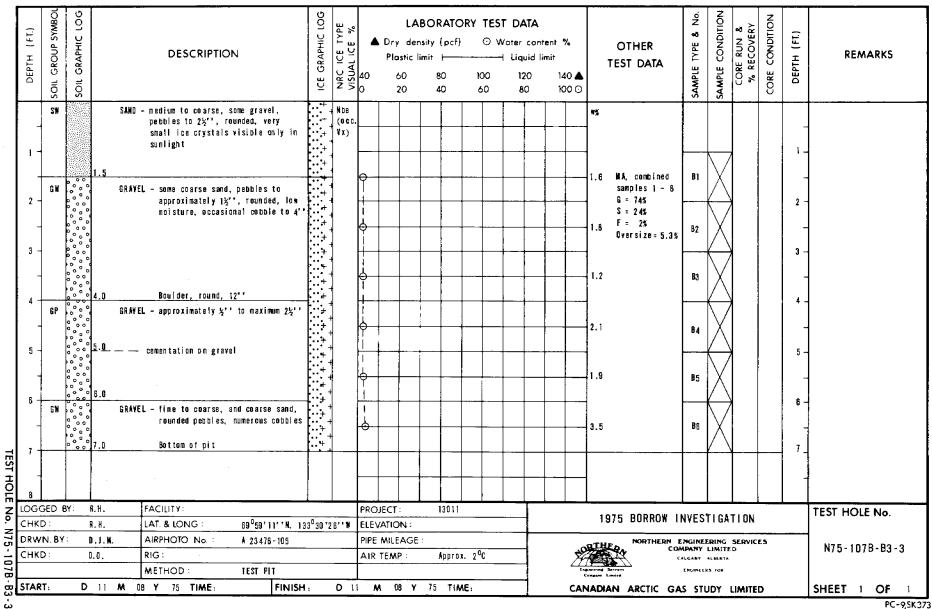
TEST HOLE LOG

DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG			DESCR	IPTION			ICE GRAPHIC LOG	NRC ICE TYPE	4		dens stic lin 0	iORATi ity (pef nit } 80 40		⊙ wa ko	DATA Inter con Liquid 120 80	i lent limit 1/	% ₩ ₩	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
	Pt	17	0.3		black, fibro					Uf	1							Τ-			- 3	8		0	_	Materia I.
1-	C¥		1	GRAVEL -	- fine to co fine to co dry, loose	erse sand , isolata	l, ligh id cebb	t brown.				├ ─┼								M A			2		· -	Using shovels
					7", numeri	ous fibre	\$									_	_			MA, combined samples 1 - 3 oversize = 3.6% 6 = 71%	B 1	\mathbb{N}			1- -	
2-															┢─┦	-+-				S = 275					2 -	
- 3-														_	$\left \right $					F = 2%	B2	X				
			3.5																			K			3 -	
4-	8P			GRAYEL -	mostly coar rounded, ii dry, loose	se (½** - ttle sand	- 3'*) I, lig	t brown,																	-	
5+			5.0		Bottom of p	it										-			_		83	X				
		·														+					╂──┦	<u> </u>			5 -	
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OGGE	DBY	:].	6. R.	FAC	ILITY:						PROJE	ECT :		13011			┿┙									
CHKD		R.	H.	LAT	& LONG :	690	⁰ 59'18'	'N, 133 ⁰	31'11'			TION	:				-1		1	975 BORROW IN	VESTI	GATI	ON :			TEST HOLE No.
DRWN.	·		<u>j. N</u>		PHOTO No.	· 12	3476-1	05			PIPE N	AILEAC	GE :				+			HE NORTHERN	NGINEER	LING S	ERVICES			
		<u> </u>	0.	RIG	: THOD :						AIR T	EMP. :		App rox.	7°C				H	CO CO	APANY LI	IMITED				N75-107B-B3-2
TART		D	11 M	_	75 TIME		T PIT	FINISH :		 D 11	M	08	Y 75	5 TIM	: 14	16	_		Lugaman Compa	MAN ARCTIC GA	ENGINEERS					SHEET I OF 1

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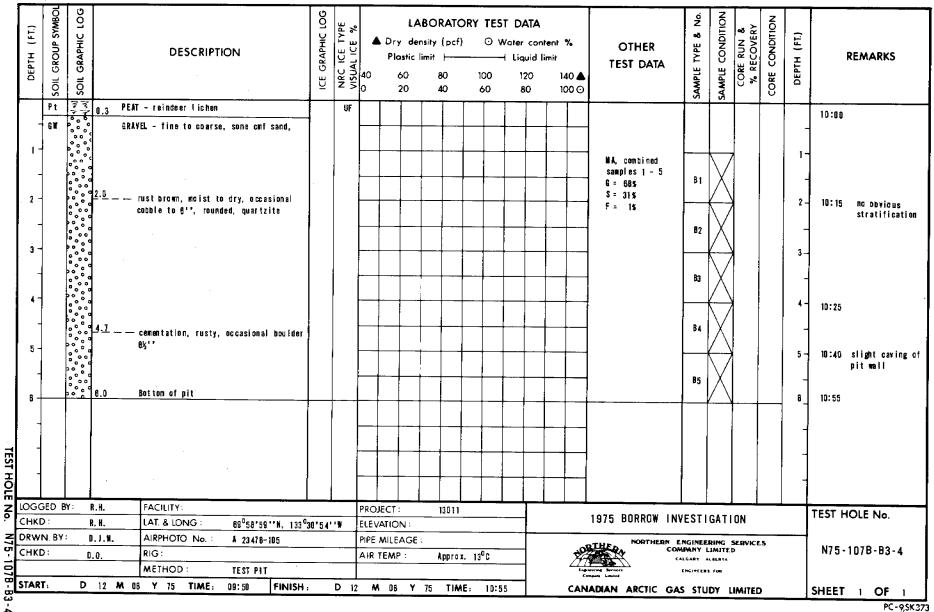
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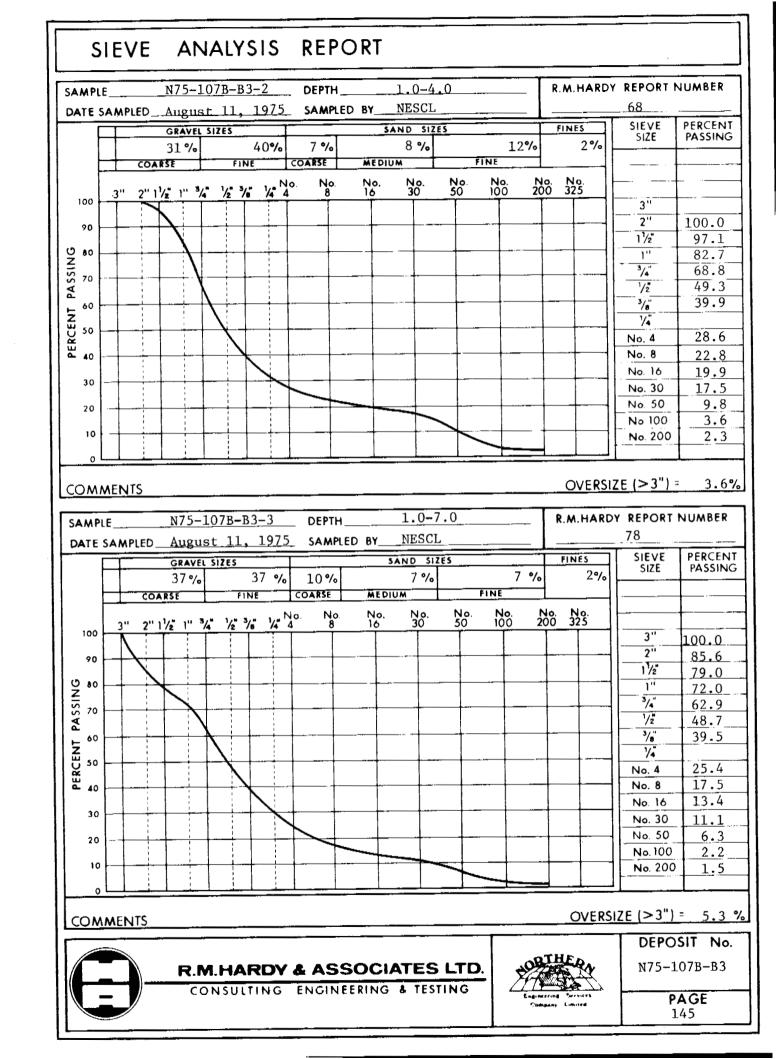
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	OF LABORATORY TE FOR OF AGGREGATES IN		
	DATE SAMPLED : August 12, DATE TESTED : March, 1976		
SOUNDNESS OF AGGE SULPHATE TEST	REGATE	ORGANI TEST	C IMPURITIES
COARSE AGGREGATE FINE AGGREGATE			R : 4 REMOVED : 3
LOS ANGELES ABRAS	ION TEST	REMOV	ROOTLETS ED : 3 CONTENT :Trace
PERCENT LOSS =	13.8 %		CANCE :
SUMMARY OF ROCK TYPE	S, COARSE AGGREGATE. (P	ETROGRAP	HIC ANALYSIS
ROCK TYPE	CLASSIFICATIONS		TOTAL WEIGHTED COMPONENT %
Quartzite	Very strong, Good		37.39
Sandstone Siltstone	Strong, Hard, Good		16.91 8.31
Limestone Altered Siltstone	Strong, Good		0.28
Chert Flint	Potentially reactive, Fair		1.89
Ironstone	Soft, Friable, Deleterious		0.07
PN = 115 INTERPRETA			68.00
COMMENTS : Satisfactor	ry, See also page 148.		
Engineering Services	R.M.HARDY & ASSO		N76 1075 D2
Company Limited			PAGE 147

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CI 11 T A D 11 1 T V	FOR		
SUITABILITY	OF AGGREGATES IN	N CONCRE	TE
SAMPLE No. N75-107B-B3- DEPTH (FT.): 1-6	-4 DATE SAMPLED: August 12, DATE TESTED : March, 197		ED BY : NESCL D BY : RMHA
SOUNDNESS OF AGG SULPHATE TEST	REGATE	ORGANIC TEST	IMPURITIES
COARSE AGGREGATE		NUMBER COAL RE	: 4 MOVED : 3
LOS ANGELES ABRAS	SION TEST		ROOTLETS
PERCENT LOSS =	13.8 %		ONTENT Trace
JMMARY OF ROCK TY	PES, <u>fine</u> aggregate.	PETROGRAP	HIC ANALYSIS
ROCK TYPE	CLASSIFICATIONS		TOTAL WEIGHTED COMPONENT %
Quartzite	Very strong, Good		20.72
Condatono			2.60
Sandstone			·····
Siltstone	Strong, Hard, Good		3.67
Siltstone Limestone			3.67 0.15
Siltstone	Strong, Hard, Good Strong, Soft, Good		3.67
Siltstone Limestone Altered Siltstone			3.67 0.15
Siltstone Limestone Altered Siltstone Chert			3.67 0.15 0.15
Siltstone Limestone Altered Siltstone	Strong, Soft, Good		3.67 0.15 0.15 2.05
Siltstone Limestone Altered Siltstone Chert	Strong, Soft, Good		3.67 0.15 0.15 2.05
Siltstone Limestone Altered Siltstone Chert Flint	Strong, Soft, Good Potentially reactive, Fair		3.67 0.15 0.15 2.05 2.59
Siltstone Limestone Altered Siltstone Chert Flint Calcareous coating Ironstone	Strong, Soft, Good Potentially reactive, Fair Soft, Weak, Poor		3.67 0.15 0.15 2.05 2.59 0.06
Siltstone Limestone Altered Siltstone Chert Flint Calcareous coating Ironstone PN = 115 INTERPRET	Strong, Soft, Good Potentially reactive, Fair Soft, Weak, Poor Friable, Soft, Deleterious ATION : Good		3.67 0.15 0.15 2.05 2.59 0.06 0.01
Siltstone Limestone Altered Siltstone Chert Flint Calcareous coating	Strong, Soft, Good Potentially reactive, Fair Soft, Weak, Poor Friable, Soft, Deleterious ATION : Good		3.67 0.15 0.15 2.05 2.59 0.06
Siltstone Limestone Altered Siltstone Chert Flint Calcareous coating Ironstone PN = 115 INTERPRET	Strong, Soft, Good Potentially reactive, Fair Soft, Weak, Poor Friable, Soft, Deleterious ATION : Good ry. See also page 147.		3.67 0.15 0.15 2.05 2.59 0.06 0.01 32.00
Siltstone Limestone Altered Siltstone Chert Flint Calcareous coating Ironstone PN = 115 INTERPRET	Strong, Soft, Good Potentially reactive, Fair Soft, Weak, Poor Friable, Soft, Deleterious ATION : Good		3.67 0.15 0.15 2.05 2.59 0.06 0.01

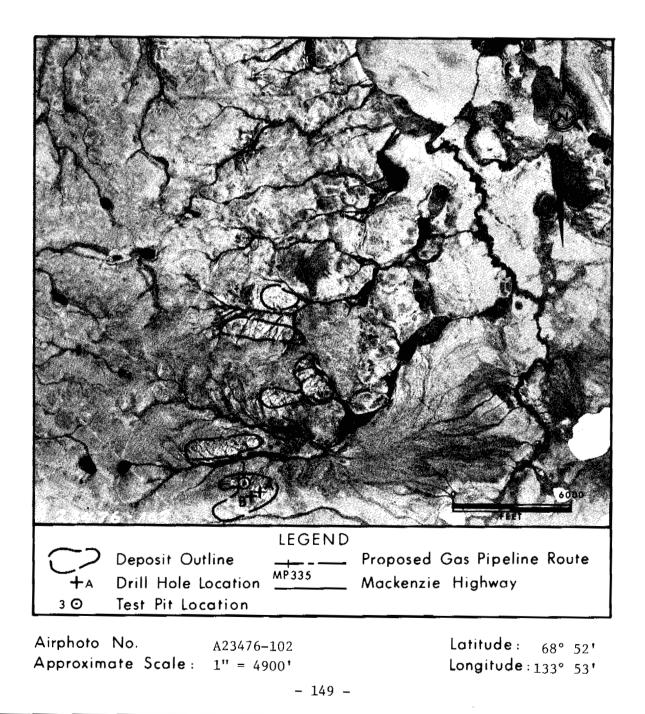
Physical Setting:Deposit 107B-B4 consists of exposed Tertiary strata located
6 miles east of Wolverine Lakes, about 40 miles north of
Inuvik and about 2 miles east of milepost 48 of the proposed
pipeline route.Material:SAND
approally woll emoded interhedded with emovel and

SAND - generally well graded, interbedded with gravel and some silt.

Volume: 10,000,000 cubic yards.

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Assessment: Deposit 107B-B4 is a source of good to excellent quality granular material suitable for general fill, backfill, building pads and possible concrete aggregate. Haul distance from the deposit is about 2 miles.



DEPOSIT 107B-B4

PHYSICAL SETTING

Deposit 107B-B4 is 6 miles east of Wolverine Lakes and about 40 miles north of Inuvik. The deposit is approximately 2 miles east of the proposed pipeline milepost 48. The Ripley, Klohn, Leonoff DIAND Granular Materials Inventory Zone III (1972) report refers to this deposit as Source 315.

This deposit consists of exposed benches of Tertiary gravel and sand on the eastern flank of the North Storm Hills. These benches, which are between 150 and 250 feet above the lowland to the east, slope gently eastward and are broken by 10 to 20 foot scarps.

The benches are well drained and free of overburden except for their western edges where some icy silt may overlie the gravel and sand. The active layer in mid-August is more than 6 feet under bare gravel, but shallower where vegetative cover is present.

The terrain near the deposit consists of gently rolling moraine with fens along drainage ways; and imperfectly to poorly drained gently sloping alluvial fans; and poorly drained lacustrine areas.

BIOLOGICAL SETTING

The benches are sparsely covered with patches of dwarf birch, willow and lichen. The site is low quality, large mammal habitat. A small number of Arctic ground squirrel dens were observed at the site. The site may be an important raptor perching, nesting or feeding area, as eagle feathers and owl pellets were found at the site. Plover, longtailed jaeger and ptarmigan were also observed in the area. There is no nearby suitable fish habitat.

MATERIAL

The deposit is primarily interbedded sand and gravel with some silt. NESCL drill holes and test pits plus the DIAND information shows that the well graded sand and generally fine gravel both have low ice contents. Local ice bodies were encountered within 15 feet of the surface.

VOLUME

Fifteen to 20 feet of gravel and sand is the minimum amount of granular material available over most of this deposit, approximately half of the area has granular material in excess of 30 feet in thickness.

The estimated total volume, based on 460 acres and 15 feet thickness, is 10,000,000 cubic yards. One quarter of this volume (2,500,000 cubic yards) is considered to be gravel.

Although the volume could be increased by extending the deposit to the west, deeper overburden would have to be removed to expose the deposit in that direction.

DEVELOPMENT AND REHABILITATION

Deposit 107B-B4 is a source of good to excellent quality granular material and is suitable for general fill, backfill in pipeline construction, building pads, and concrete and asphalt aggregate. However, the gravel will require further testing before use in concrete production. The DIAND report indicates that the high proportion of sandstone particles will make the material unsuitable for high quality concrete.

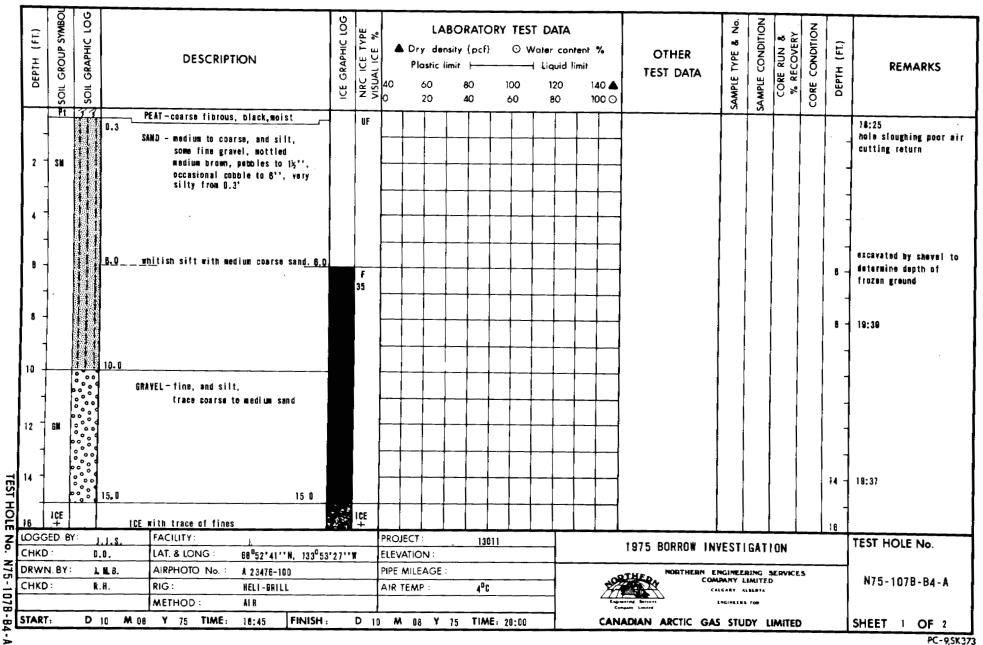
No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the deposit would probably be along the pipeline right of way. A 2 mile snow road would have to be built to transport material to haul points on the right of way across gently rolling morainic hills. Initially, the peat cover and overburden, although minimal, would be stripped from the area to be excavated and stockpiled around the edges.

Development of this deposit would involve excavating borrow material evenly from the higher, well drained areas to a grade such that good drainage would be established over the area. Terracing would make it possible to excavate the steeper slopes of this deposit. This type of development could be accomplished by using blasting or conventional earthmoving techniques depending on the degree of ice cementation. The excavated material may have to be stockpiled, thawed, and drained before it is used. Crushing and/or screening of the material may be required to produce construction aggregates. The long term effects of thermal degradation will have to be considered because of the presence of local, massive ice bodies.

Equipment required for development would be dozers, rippers, end dump trucks front-end loaders, as well as screening, drying crushing, concrete and asphalt plants if required.

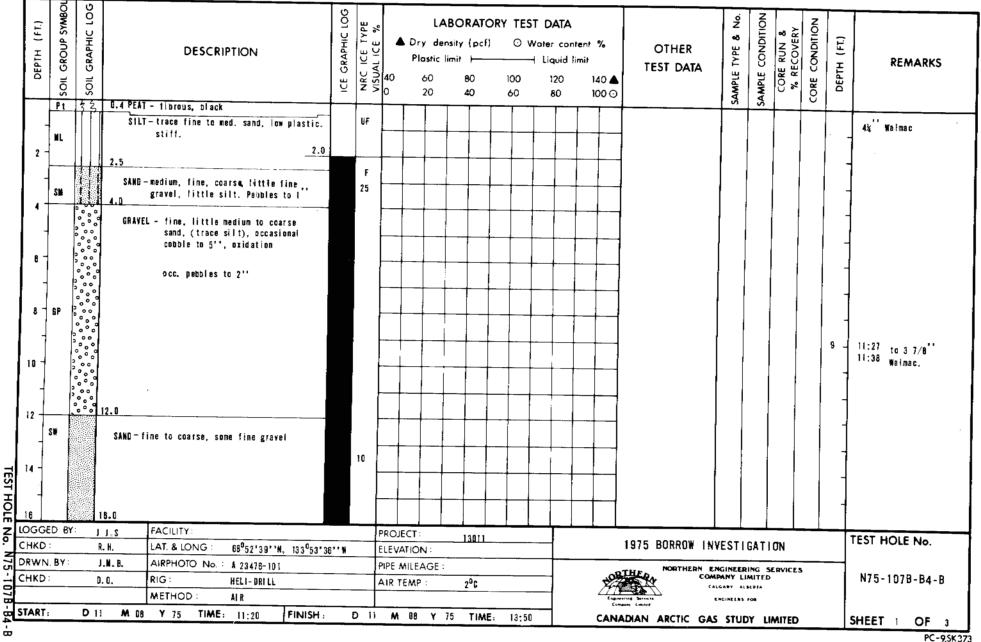
A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.



DEPIM (FL)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG			DESCRIPT	ION ⁻		ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Plo: 6	den		pcf} 		₩ote — L	ATA r cont quid li 120 80	mit 14(OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FL)		REMARKS
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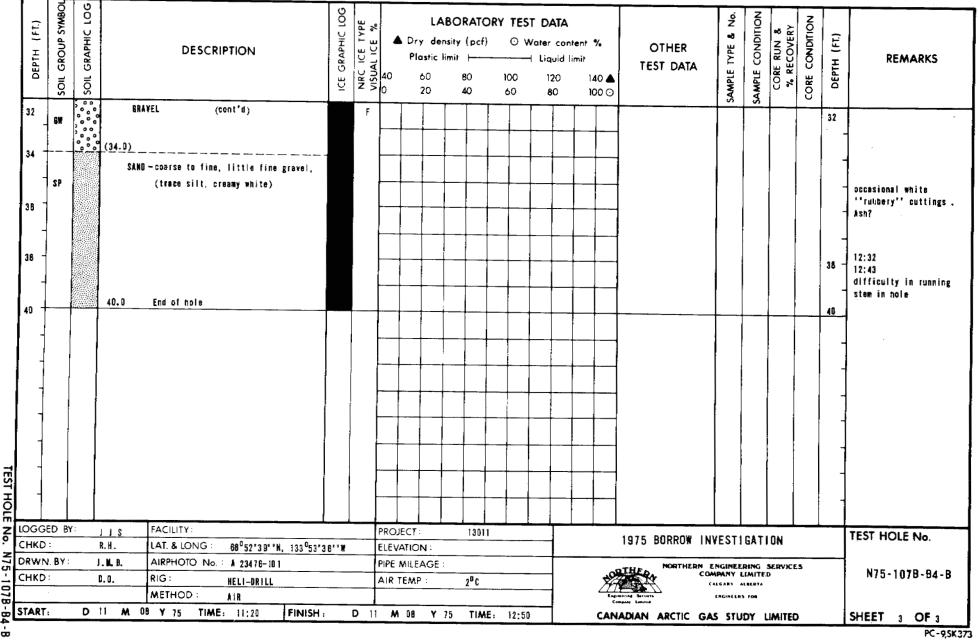
PC-9,5K373

	DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Dry	density ic limit	(pcf)	O	ST DAT Woter co 	ontent % d limit 14	% 10 ▲ 10 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REM/	ARKS
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	- 20 - 1			<u>_20.0</u>	gravel to 3/4		i				-												-
	22				whitish fines																		
	24			_24-0	little gravel to 1½, medium_coarse sand. Pebbles to 1½						_						5						
	28			26.5	some fine gravel																-		
	28 -			1	WEL - coarse, to 1%"																28 -	il:56 New 12:22 Waim hole	3 7/0 nac. Ream e. Difficult
TEST HOLE No.	30 -	GW		GRJ	NYEL - fine, little cmf sand, pebbles to 1½''																-		run stem n hole.
핑			, ° ° °		rust coloured														<u> </u>				
z		GED	BY:	1.1 5	FACILITY				JECT :		3011					1975 BORROW LI	VEST	I GAT	TION			TEST HOL	E No.
	снк			R. H.	LAT. & LONG : 68052'39'' H, 13305	3'36'	•₩		VATION							NORTHERN							
킼	DRW	N. BY D: RT:	Y:	J.N.B.	AIRPHOTO No. : A 23476-101		_	TEMP		2 ⁰ C				*	CC CC		LIMIT	E.D			N75-107	7B-84-8	
<u> </u>	снк	D:		D.O.	RIG: HELI-DRILL			1 CMP		1.0				2	Automa Suranes		LAS FOR						
밁					METHOD : AIR IN Y 75 TIME: 11-20 FINISI			1	M 04	¥ 75	TI	ME: 1	3:50		CAP	Company Longited NADIAN ARCTIC G	AS SI	UDY	LIMIT	ΈD		SHEET 2	OF 3
٣	STAR	<u>स</u> ः	D	<u>11 M (</u>	11:20 FINIS		<u> </u>	11	•• Uð				0.00							-			PC-9,SK3

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> N75-107B - B4 - B

LOG ŝ SAMPLE CONDITION **GROUP SYMBOI** GRAPHIC LOG CONDITION NRC ICE TYPE VISUAL ICE % 0 5 LABORATORY TEST DATA CORE RUN & % RECOVERY (FT.) ۰Ö DEPTH (FI.) GRAPHIC ▲ Dry density (pcf) ① Water content % OTHER SAMPLE TYPE REMARKS DESCRIPTION DEPTH - Liquid limit Plastic limit H TEST DATA CORE 60 100 120 140 📥 60 40 Щ SOIL SOIL 100 🖸 80 20 40 60 ° † ° MA, sample 1 Using shovels GW-GRAVEL - fine to coarse, subangular, and UF 6 = 48% GM mfc sand, brown, moist, B 1 |**°**0° borderline gravel/sand S = 44% stratified, loose F = 8% 1 -(GW- GM) 82 <u>_</u>___ 2 -- some sand. 2 ໍາ B3 3 3 84 4 85 ÷. 5 5 88 6 6 ိုစ် SW SAND - coarse to fine; and gravel, fine, 87 subangular; light brown, damp, dense. Permafrost at 7.2" 1 -7 Bottom of pit TEST HOLE No. 1.2 TEST HOLE No. **PROJECT** : 13011 FACILITY LOGGED BY J.G.R. 1975 BORROW INVESTIGATION 68°52'41''N, 133°53'27"'W ELEVATION : LAT. & LONG CHKD R.H. N75-1 NORTHERN ENGINEERING SERVICES PIPE MILEAGE : A. J. B. DRWN. BY: AIRPHOTO No. A 23476-101 N75-107B-B4-1 oTHE COMPANY LIMITED Approx. 4⁰C AIR TEMP CALGARY ALBERTA CHKD RIG : D. O. 107B ENGINEERS FOR METHOD : TEST PLT SHEET 1 CANADIAN ARCTIC GAS STUDY LIMITED OF D 10 M 08 Y 75 TIME: 22:10 FINISH : è 18:00 START: D 10 M 08 Y 75 TIME:

TEST HOLE LOG

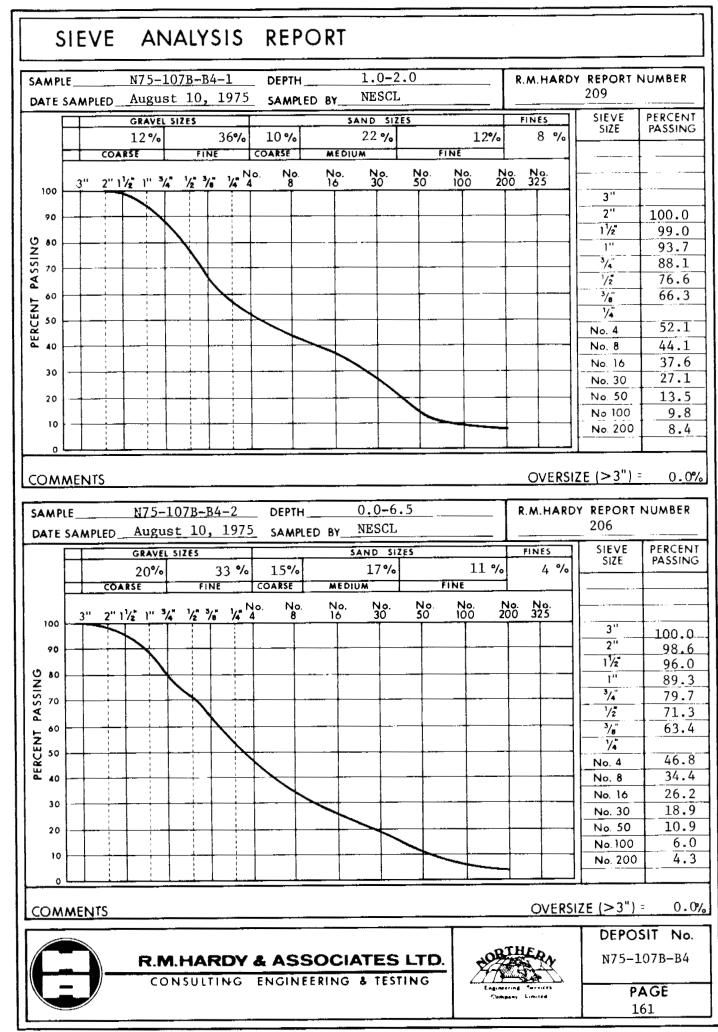
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PC-9,5K373

DEPTH (FT.)	SOIL GROUP SYMBOL	Sol I		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Pla: 6	dens	BORAT sity (pcf nit 80 40	i) O	ST DATA Water co Liquid 120 80	ntent %		SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FL)	REMARKS
-	GP		9 9 9	GRAVEL – mainly fine, subrounded; and sand, coarse to fine, light grey, moist, stratified, loose.		UF								MA, combined samples 1 - 7 G = 53.2% S = 42.5%	B1	X				Using shovels
2 -									_					F = 4.3%	B2	X				
3 -	SP			SAND - mainly medium to fine; little gravel, fine, subrounded; light grey, moist, stratified, loose.											B3	X			2	
4 -	GP		3.8	GRAVEL - fine, subrounded; little sand,											84	X			3 -	
5 -			9	coarse and medium; light grey, damp, loose.	į										B 5	X			4 -	
8 -															60	X			- 6 -	
		•	8.4	Bottom of pit											B7	X				
	ED B		J. G. R.	FACHITY			PROJ	IECT :		1301									-	TET HOLEN
HKD			ì.Н.	LAT. & LONG : 88 ⁰ 52'45''N, 133 ⁰ 5	3 43			ATION	1:					1975 BORROW IN	VESTI	GATI	ON			TEST HOLE No.
	WN. BY: A. J. B. AIRPHOTO No. I 23478-101 IKD: D. D. RIG:						MILEA TEMP		App r	0 X. 4 ⁰ C		X		ENGINEEI MPANY L ALGABY AN ENGINEERS	IMITE.	SERVICE	1.5		N75-107B-84-2	
ART		D	10	M 08 Y 75 TIME: 18:00 FINISH:		D 10	M	08	Y	75 TIA	AE: 20:	20	CAN	ADIAN ARCTIC GA			IMITER	•		SHEET I OF I

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TEST HOLE No. N75-1078-84-2



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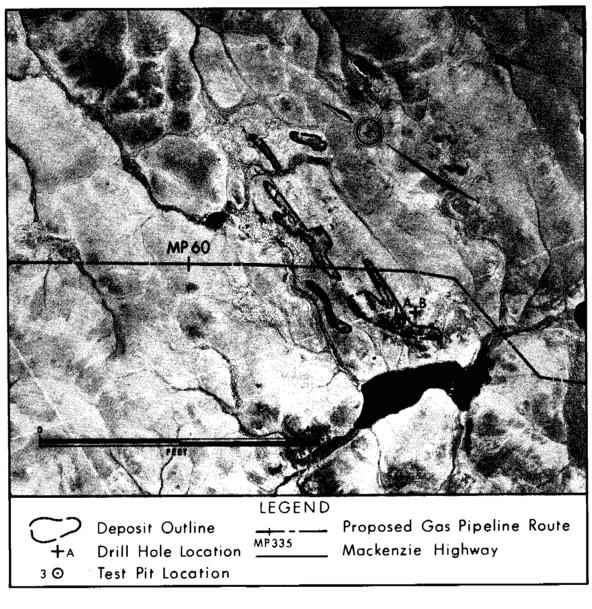
Physical Setting: Deposit 107B-B5 consists of kame terraces located 11.5 miles NNW of Noell Lake, 9 miles east of Reindeer Depot and crossed by the right of way at milepost 60.

Moterial: SAND - interbedded with silt and clay, and with some gravel.

Volume: 300,000 cubic yards.

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Assessment: Deposit 107B-B5 is generally a source of poor quality granular material suitable only for general fill and backfill. It is crossed by the right of way and thus local use is expected.



 Airphoto No.
 BR74404-97
 Latitude:
 68°
 42'

 Approximate Scale:
 1" = 2050'
 Longitude:
 133°
 45'

DEPOSIT 107B-B5

PHYSICAL SETTING

Deposit 107B-B5 is 11.5 miles north-northwest of Noell Lake and 9 miles east of Reindeer Depot. The pipeline right of way crosses the deposit near milepost 60.

The deposit consists of narrow flat-topped kame terraces which border the western edge of a north-south trending meltwater channel. The western edges of the terraces are generally formed by short scarps. The kame terraces are free of significant cover and are well drained. The active layer under bare gravel surfaces is approximately 5 feet thick.

BIOLOGICAL SETTING

Scattered clumps of vegetation on the terraces consist of dwarf birch and lichen with cottongrass in poorly drained areas. The site provides low quality, large mammal habitat. Reindeer, grizzly and black bear, Arctic ground squirrel, fox and wolf are found in the area. The area provides generally poor quality habitat for both waterfowl and terrestrial birds. Arctic loons were observed nesting on the small lake northwest of the site in 1975. Nearby lakes and streams do not appear to support fish populations.

MATERIAL

Test pit 107B-B5-1 showed good well graded gravel and coarse sand to a depth of 5 feet. Drill hole logs show interbedded sand, silt and clay. The test pit was located on one of the knobs indicating gravel is concentrated in these areas. Over the entire deposit the quality of the material is poor, but pockets of good quality gravel are present.

VOLUME

An average depth of 5 feet of good quality material for the area outlined on the airphoto is probably an optimistic figure. The total estimated volume, based on 40 acres and 5 feet depth is 300,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 107B-B5 is, for the most part, a source of poor quality granular material and is only suitable for general fill and backfill in pipeline construction. Despite the varied quality and small quantity of aggregate at this site, development for local use is expected as the pipeline right of way crosses the western end of the deposit and overburden and vegetative cover are minimal.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Since this is a small intermediate deposit, development would not be extensive and could be carried out by equipment available along the pipeline right of way. In order to minimize environmental damage, snow roads would be built the short distances to the pipeline.

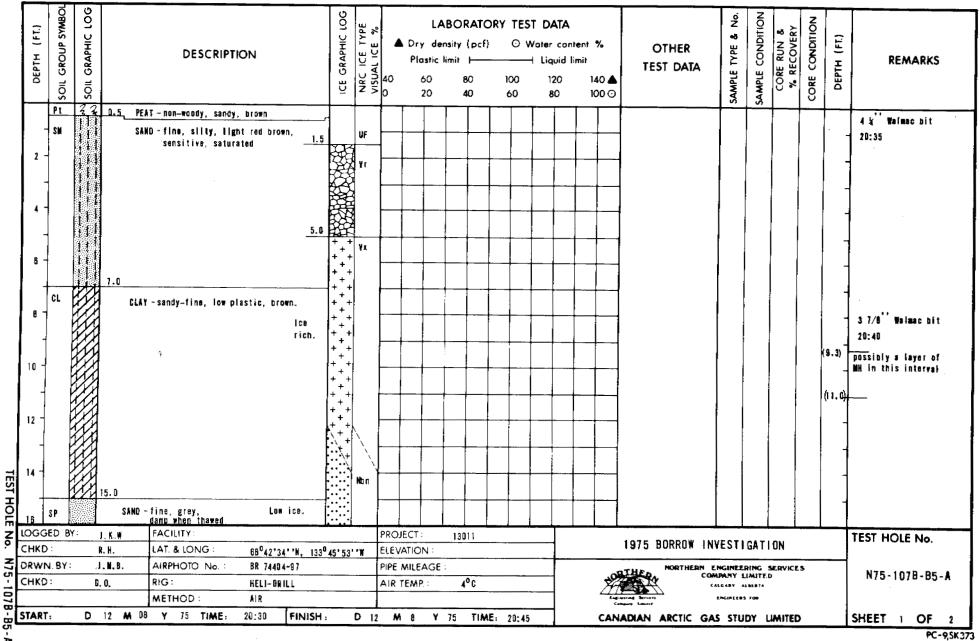
Development at this deposit would first involve locating all the small areas of good quality gravel by extensive drilling and test pitting. Initially the sparse vegetation would be removed and harvested according to land use regulations. Since this deposit is essentially free of overburden, stripping of the excavation area would be minimal. Excavation of the best areas would follow by removing borrow material evenly from these isolated pockets to a level whereby good drainage is maintained throughout the area.

Conventional earthmoving techniques would probably be all that is required for development; however, blasting techniques could be used if areas of high ice cementation are encountered.

The excavated material may have to be stockpiled, thawed and drained before it is used.

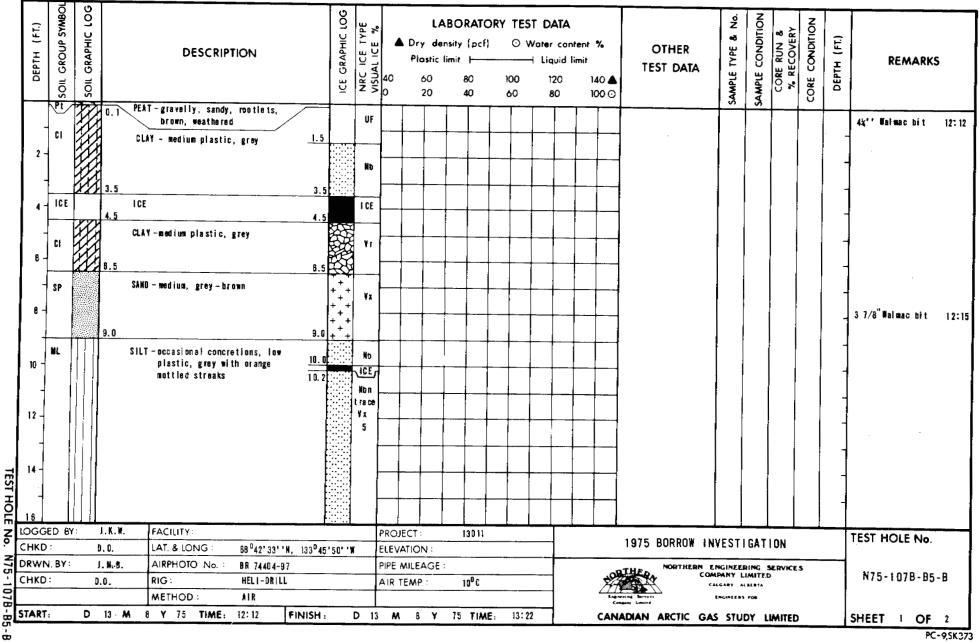
Equipment required for development would be dozers, rippers, end-dump trucks, and front-end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.



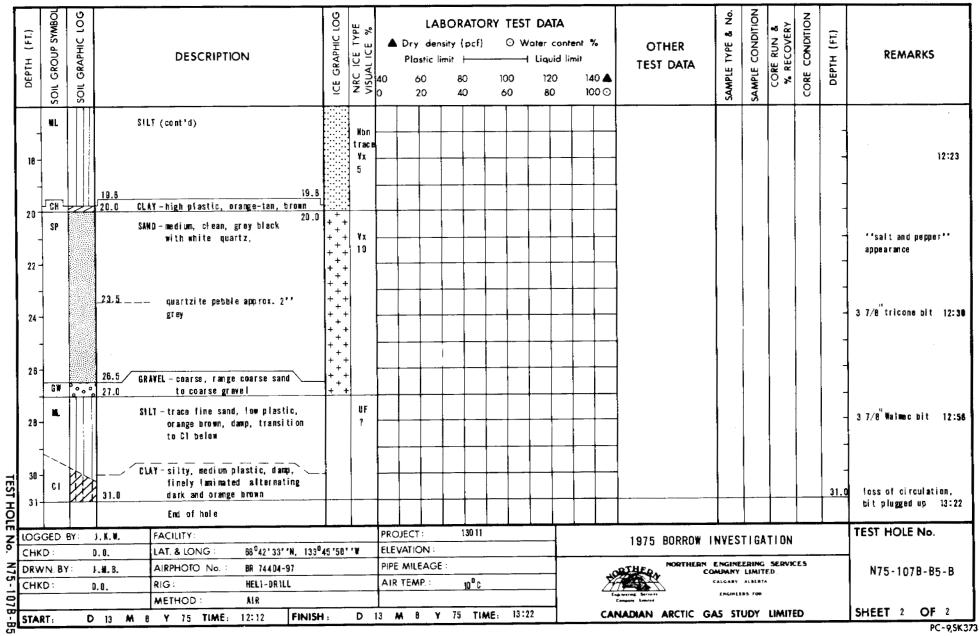
DEPTH (FT)		SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Dry d	ensity : limit	(pcf)	ΟV	T DATA Vater com I Liquid I 120 80	limit 14	% 10 ▲ 00 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
Γ	s	IP		17.0	SAND - (cont'd)		Nba															
		n		18-0	CLAY - some medium sand, low plastic, chocolate brown.																18.0	20:45
13 TEST HOLE No.					End of hole																	
Z LO			Y: J.		FACILITY: LAT. & LONG : 88 ⁰ 42*34**N, 133 ⁰ 4						13011					1975 BORROW IN	IVEST	IGAT	ION			TEST HOLE No.
N75-1078	IKD :	. BY :) 9	H. M. R. . O.	AIRPHOTO No. : BR 74404-97 RIG : HEL1-BRILL METHOD : AIR			PiPf AIR	TEMP.	GE :	4 ⁰ C	45 00			20	and Services	Enginer	LIMIT ALBERT	F.D			N75-107B-B5-A
¦g_S⊺ ∽	ART:		D	12 🛤	88 Y 75 TIME: 20:30 FINIS	H: _	D	12	M 08	¥ 15	TIA	AE: 28:	45		CAN	NADIAN ARCTIC G	AS ST	UDY	LIMIT	.0		PC-9,5K3

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> <u>No</u>. N75 107B

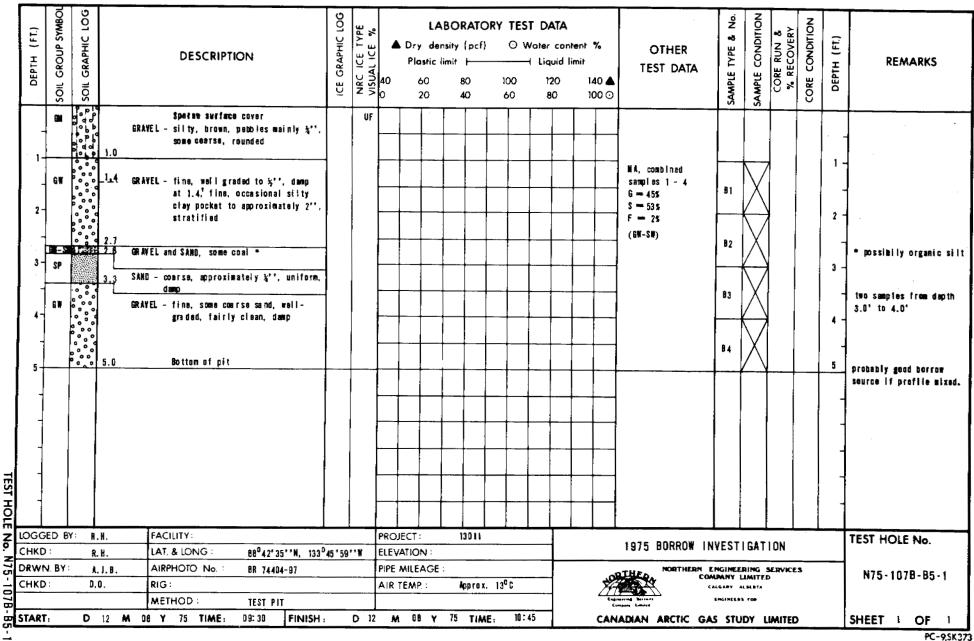


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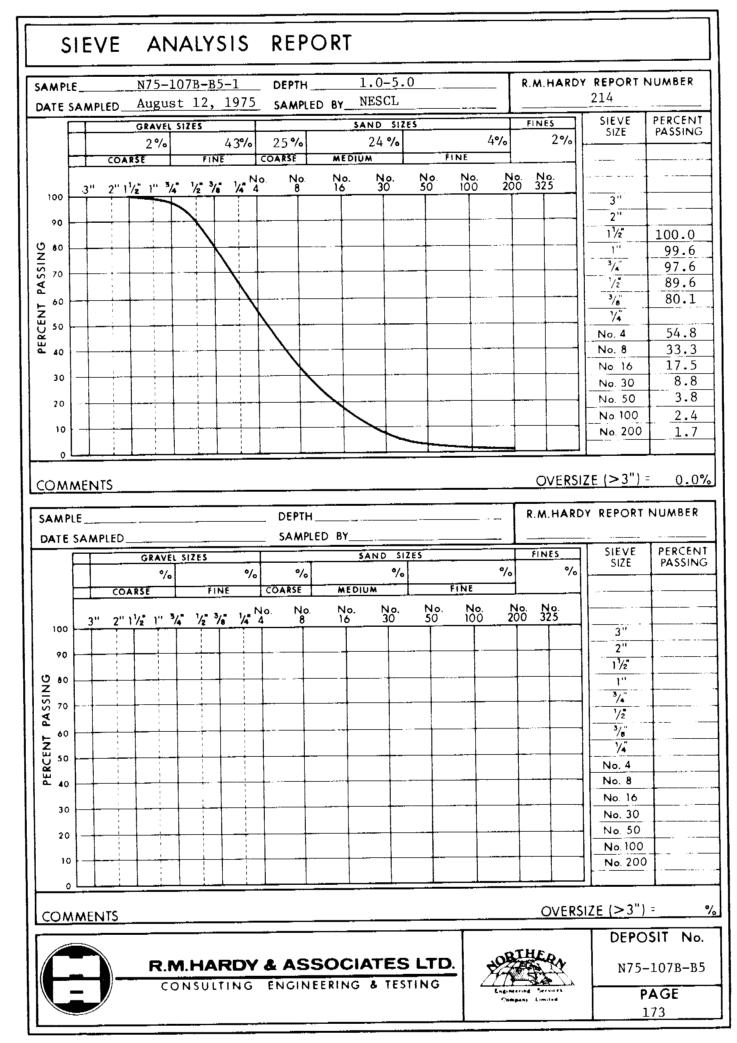
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> TEST HOLE No. N75



Physical Setting: Deposit 107B-B6 is a lacustrine plain located on the southern edge of Jimmy Lake just 4.5 miles NNE of Noell Lake and 2 miles northeast of the right of way.

Material: GRAVEL - poorly graded.

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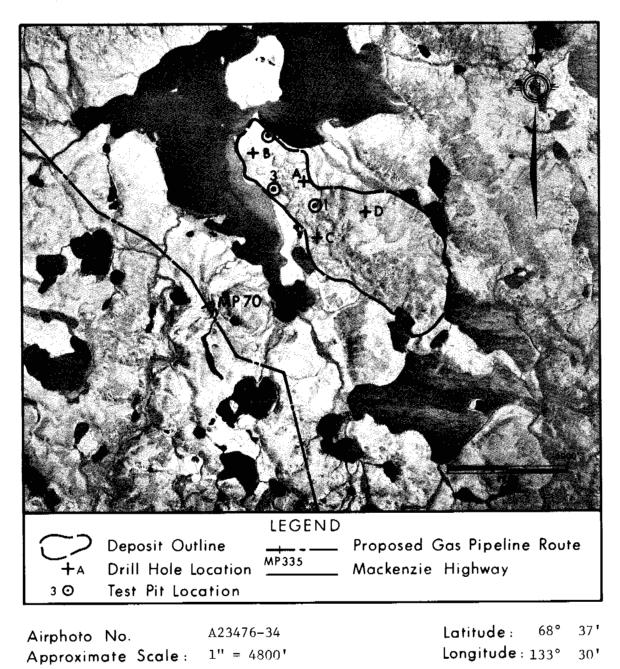
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Volume: No volume calculated due to the thick overburden.

Assessment: Deposit 107B-B6 is not recommended for development due to its poor quality granular material and the thick overburden.



DEPOSIT 107B-B6

PHYSICAL SETTING

This deposit is a lacustrine plain at the southern edge of Jimmy Lake. It is 4.5 miles north-northeast of Noell Lake and 2 miles northeast of milepost 70 on the proposed pipeline right of way.

The plain is gently to moderately rolling and its edge is defined by 20 to 50 foot scarps formed by meltwater and thermokarst activity. The surface of the plain is moderately well to imperfectly drained. In mid-August the active layer was generally less than 1 foot in depth.

BIOLOGICAL SETTING

Vegetation typical of the forest-tundra transition occurs on this plain. Common species on the northern portion are bog birch, willow and alder with a ground cover of moss and lichen. The southern part has scattered black spruce up to 20 feet in height and sedges in wet depressions. The site is located in low quality, large mammal habitat. Occasional black bear may occur in the area. Jimmy Lake provides nesting and moulting habitat for waterfowl. A pair of swans were observed on the lake during the 1975 survey. Several species of passerines were observed nesting at the site. It is not known whether Jimmy Lake supports fish populations. There is no other potential fish habitat in the immediate vicinity.

MATERIAL

The deposit consists of 2 to 10 feet thick layers of poorly graded gravel. The material is of poor quality and is overlain by 10 to 20 feet of icy lacustrine sediments with zones of ground ice.

VOLUME

The volume of recoverable material can be considered nil due to the depth of icy clays, silts and massive ice overlying the gravel.

DEVELOPMENT AND REHABILITATION

Deposit 107B-B6 is not recommended for development because the granular material in this deposit is of poor quality and is overlain by thick overburden.

GROUP SYMBOL GRAPHIC LOG ICE GRAPHIC LOG SAMPLE CONDITION SAMPLE TYPE & No. CONDITION NRC ICE TYPE VISUAL ICE % O & LABORATORY TEST DATA CORE RUN & % RECOVERY (FT.) (FT.) O Water content % ▲ Dry density {pcf} OTHER DEPTH DESCRIPTION DEPTH REMARKS Plastic limit + ---- Liquid limit TEST DATA CORE 60 80 100 120 140 📥 SOIL SOIL 20 100 🖸 40 60 80 33 PEAT-fine fibrous, amorphous, woody 4½ Waimac bit 0.8 UF Pt 0.8 inclusions, black 15:15 + 34 ÷ SiLT-(organic) low to non plastic. 0L '+ + ¥X. black. 2 + + + + 1 11 4 + CLAY-silty, trace fine gravel, high ice CL. rust brown, in part mottled + + grey, pebbles subangular to + 3/8 , (till-like) + 6 + 7.0 47.0 14 A. 101 ICE ICE + SILT + 3 7/6 Walmac bit. + 15:20 10 almost clear 12.0 pebbles, 2 - 3 . 12 14 TEST HOLE 15.5 <u>ہ ہے</u> GRAVEL e P TEST HOLE No. PROJECT : No. LOGGED BY: FACILITY: 13011 J.K.W 1975 BORROW INVESTIGATION ELEVATION : CHKD R.H. LAT & LONG : 68°37'36''N, 133°31'50''W N75 AIRPHOTO No. : 1 23478-34 PIPE MILEAGE : NORTHERN ENGINEERING SERVICES DRWN. BY: J. H. B. N75-107B-B6-A COMPANY LIMITED AIR TEMP. HELI-DRILL 10⁰ C CHKD RIG : D.O. CALGARY ALBERTA 07B-B6 ENGINEERS FOR METHOD : AL R SHEET 1 OF 2 CANADIAN ARCTIC GAS STUDY LIMITED START: D 13 M 08 Y 75 TIME: FINISH : D 13 M 08 Y 75 TIME: 18:08 15:15

TEST HOLE LOG

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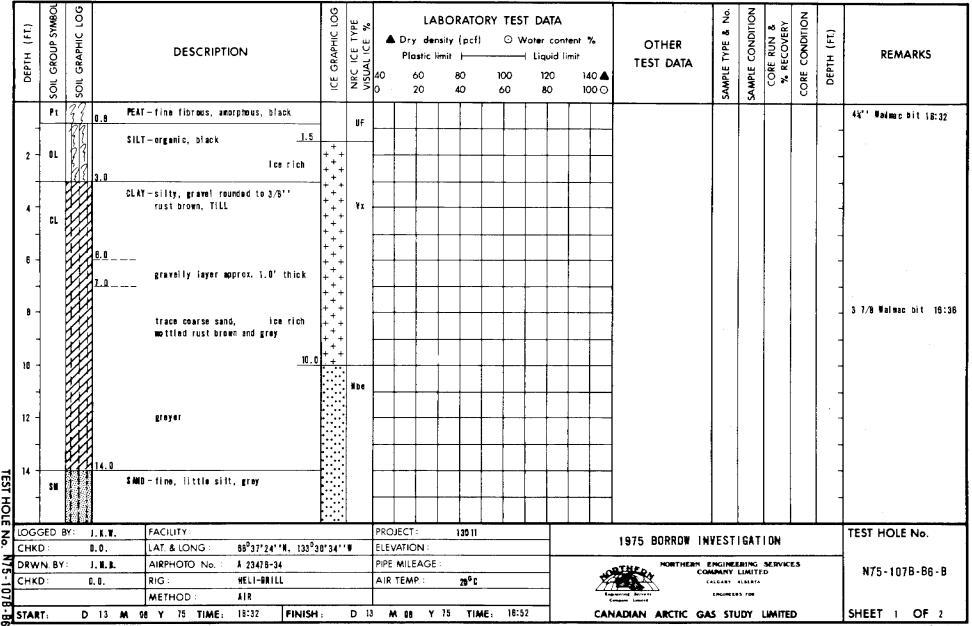
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DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPI	FION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Dry	density c limit	/ {pcf		ST DA Water 	id lim	1	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FI.)	REMARKS
18 -	GP		GRAYEL :	(cont'd) - coarse grained, c granita, sandstor	accasional cobbies. ne, siitstone.		F														-	3 7/8" Tricone bit 15:30
20 -			21.5	and users fine mend	nebble et																-	
22 - - 24 -	NIL GP NIL		22.5 : GRAVEL - 24.8	and very fine sand. 22 - coarse grained	fine sand. cs rich.						-										-	
- 26 -	ICE			CE cobble - hard End of Hole	grey cloud		ICE	 													- 27.0	16:00
			27.0																		-	
-																					-	
	ED B		K.W	FACILITY:				<u> </u>	JECT :		3011				* 	1975 BORROW II	NVEST	IGAT	ION			TEST HOLE No.
HKC RW1 HKC	N. BY	R. : J. D.(K. W.	LAT. & LONG : AIRPHOTO No. : RIG : METHOD :	HELI-DRILL	' 50 ' ' N		PIPE	VATION MILEA		10 ⁰ C						ENGINEE MPANY ALGABY ENGINEER	LIMITE.		ES		N75-107B-B6-A
TAR	T :	D	13 M 08		AIR 15:15 FINISH	l :	D	1 <u>3</u> A	VI 08	¥ 75	j T1/	ME: 16	:08		CANA	ADIAN ARCTIC GA	us stu	IDY i	IMITE	D		SHEET 2 OF 2 PC-9,5

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TEST HOLE No. N75-1078-B6-A

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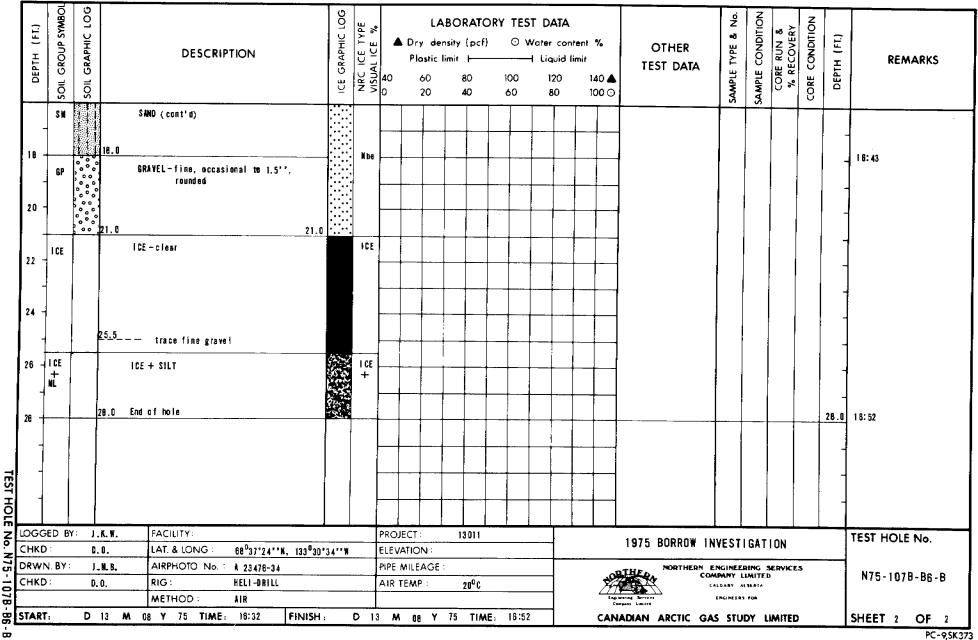
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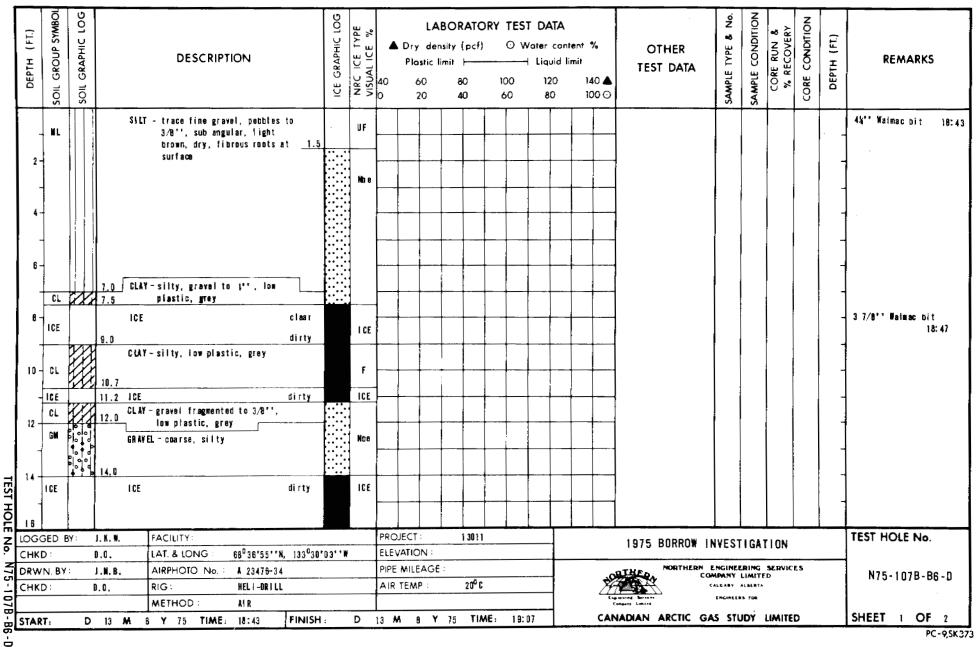
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DEPTH (FT.)	SOIL GRAPHI			DESCRIPTI	N			NRC ICE TYPE VISUAL ICE %	▲ 40 0	Dry de	ensity ((pcf) 	ΟW	T DATA Fater cor Liquid 1 120 80	ntent limit	% 40 ▲ 00 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
Pt	122.12	2	PEA 1.0	LT - fine fibrous, amo brown, becoming l																			4% Walmac bit 17:30
2 - NL	-17	ļ		.T-trace fine sand, light grey brown	low plastic,	2.0		UF					-										
4			5.0								-											-	
6 - -		HH HH		AY-silty, trace fine occasional fine g sand, medium plas grey brown	ravel to coa			Hbn												-		-	
8 - - 10 -				grey																			bit plugged up 3 7/8'' Waimac bit 17:45
12 -			2.0. End	1 of hole																		12.0	Loss of circulation 17:58
-																						-	
															†							-	
		Ļ	V IN	FACILITY					PROJ	ECT:													TEST HOLE N
LOGGEL CHKD		J. D.	K.W. 0.	LAT. & LONG :	68937'19''N	1. 133929'1	5"	¥		ATION		13011					1975 BORROW I	NVES	T I GA	TION			TEST HOLE No.
DRWN	BY:		N.B.	AIRPHOTO No. :	A 23476-34					MILEAG	E :					-1	OTHEN NORTHERN				E S		N75-107B-B6-C
CHKD		D.		RIG :	HELI-DRILL				AIR T	EMP :		20 ⁰ C				20		MPANY	AL BERTA	D			M/3-10/0-06-C
				METHOD	AIR											E 14	inering Bernies ampany Limited	ENGINEE					
START:		D 1	3 M	08 Y 75 TIME:	17:30	FINISH :		D	3 M	88	Y 75	TIME	E: 17:5	8		CAN	ADIAN ARCTIC GA	s st	UDY	LIMITE	0		SHEET 1 OF 1

PC-9,5K373



- 184 --

SOIL GROUP SYMBOL GRAPHIC LOG ICE GRAPHIC LOG SAMPLE CONDITION ŝ CORE CONDITION LABORATORY TEST DATA CORE RUN & % RECOVERY ТҮРЕ Е % (FT.) SAMPLE TYPE & DEPTH (FI.) OTHER NRC ICE T VISUAL ICE DESCRIPTION DEPTH REMARKS Plastic limit |---Liquid limit TEST DATA 120 140 📥 60 80 100 SOIL 20 40 60 80 100 🖸 1CE ICE (cent'd) t CE 17.0 inferred by drilling ML SILT action 10:55 18 F 19, 0 ICE ICE iCE clear 20 22 -24 -26.0 26.0 26 ML. SILT 28.5 28.5 F clear ICE I CE 1CE 28.0 28.0 19:07 28-End of hole TEST HOLE LOGGED BY FACILITY PROJECT 13011 TEST HOLE No. J.K.W. 20 1975 BORROW INVESTIGATION LAT. & LONG : ELEVATION : CHKD D. O. 68°36'55''N, 133°30'03''W PIPE MILEAGE : DRWN.BY: 3. M. B. AIRPHOTO No. : NORTHERN ENGINEERING SERVICES A 23476-34 THE N75-107B-B6-D COMPANY LIMITED 20°C CHKD: D. O. RIG : HELI-DRILL AIR TEMP CALGARY ALBERTA 078-86 ENGINEERS FOR METHOD : AL R 19:07 SHEET 2 OF 2 D 13 M 8 Y 75 TIME: 18:43 FINISH : D 13 M B Y 75 TIME: CANADIAN ARCTIC GAS STUDY LIMITED START:

TEST HOLE LOG

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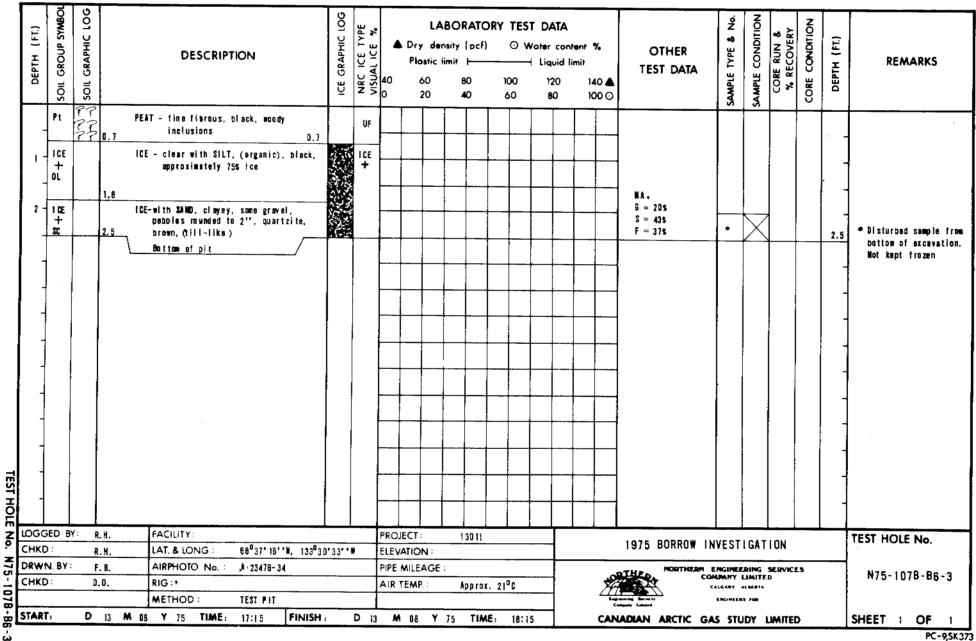
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DEPTH (FI.)	DIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40	Dry den Plastic li 60	imit 80	F) C 100	Wate — Li	r cont quid li 120	mit 14(•▲	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FI.)	REMARKS
	Sol		<u> </u>		Ĕ		0	20	40	60		80	100	00		₹	SA		8		
	Pt	39		PEAT - annorphous, fine fibrous, black, woody inclusions	↓ -,	UF	{														No samples taken
1	OL	77		SILT (organic) - non-plastic, black	[++	1					+	+								-	1
		77	1.0	ice rich 1.0		50															· .
רו	I CE+ \01_/		1.25	ICE-with SILT (organic)	1.50		1													-	columnar crysta
-				ICE-clear, columnar		ICE				+										-	spectrum coloui
	I CE		2.0	Bottom of pit																2.0	
2 -			1	Abandon ed			\vdash					1		+		t	<u> </u>	<u> </u>	<u> </u>	2.0	
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-		-		Note: Refer also to test hole N75-1078-88-4				<u> </u>		++		+ i		-				-		-	4
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066	ED B	Y:	A. H.	FACILITY	<u> </u>		PRO	JECT :	130	1 I		╈								L	TEST HOLE No.
HKD			R. H .	LAT. & LONG : 68037"45" N, 1330	31 '17'	' W	ELEN	ATION :				1			1975 BORROW IN	VEST	IGAT	IUN		ſ	
RWN	N. BY :		A. M.	AIRPHOTO No. : A 23476-34			PIPE	MILEAGE	:						THE NORTHERN				ES		N75, 1070 Do
HKD			D, C.	RIG:			AIR	TEMP. :	k an	ro x. 18 ⁰	C	1		ter ter		MPANY ALGARY		D		ſ	N75-107B-B6
				METHOD : TEST PIT								1		<u>لللا</u> دون	Nerring Berrith	E=G1=1 E8	S FOR			ſ	
TART			1.0	M 08 Y 75 TIME: 15:00 FINISH		D .		A 08 Y	15 TI	ME	16: 30	-			ADIAN ARCTIC GA	S STI	YOL		D	ľ	SHEET 1 OF

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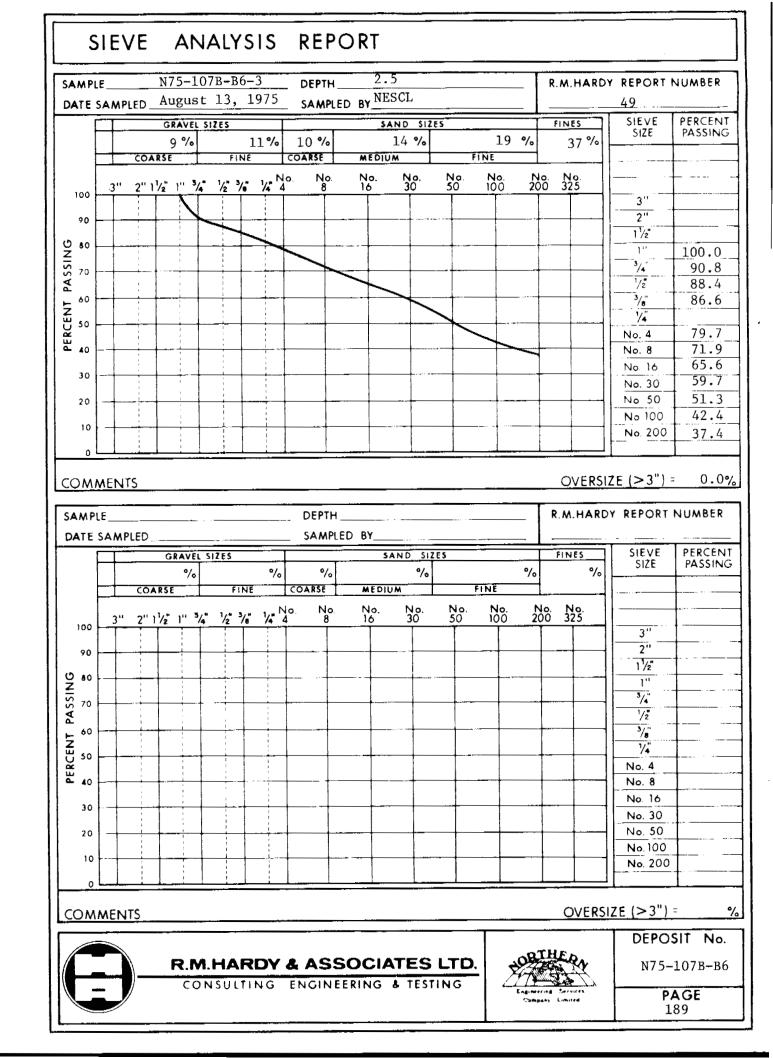
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TH (FT.)	GROUP SYMBOI	GRAPHIC LOG		DESCRIPTION	GRAPHIC LOG	ICE TYPE	L ICE %	▲ Dry Plas	dens		f) O	EST DAT Water a	onten		OTHER TEST DATA	TYPE & No.	SAMPLE CONDITION	CORE RUN &	CONDITION	DEPTH (FL)	REMARKS
DEPTH	SOIL GF	SOIL GF			ICE G	NRC		6 2	0	80 40	100 60			140 ▲ 100 ⊙		SAMPLE TYPE	SAMPLE	S. %	CORE	DEP	
	Pt	33	0.5	PEAT - amorphous, fine fibrous, black, woody inclusions		UF										T					No samples taken
	OL	1-1-	0.9	SILT (organic), non-plastic, black	+++++++++++++++++++++++++++++++++++++++	+ 50														1	
1 -	1 CE +	1		ICE with SILT (organic)		10 +	E													-	
-			1.8	Bottom of pit										_			 			1.8	-
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ЭG	GED	BY :	R.H.	FACILITY				ROJECT		130	111				1975 BORROW II	WEST	IGA	T I ON			TEST HOLE No.
			R. H.	LAT. & LONG 98 ⁰ 37'22'''N, 1	<u>33°31'22</u>	2''₩	-+-	EVATIC	_						NORTHERN				CES		
	VN.B (D:	T :	A. N. D. O.	AIRPHOTO No. : A 23476-34 RIG :				IR TEM			oro x. 21 ⁰	C		<u><u></u></u>		CALGARY					N75-107B-B6-
			0.0.	METHOD : TEST PIT										<u>/ / /</u> Lag C:	J. Januaring Seconds company Limited	ENGINE					
TAI	RT:	0	13	M 08 Y 75 TIME: 17:00 FIN	ISH :	D	13	M 0	6 Y_	75 T		17:30		CAN	ADIAN ARCTIC G	AS ST	UDY	LIMIT	ED .		SHEET 1 OF 1 PC-9



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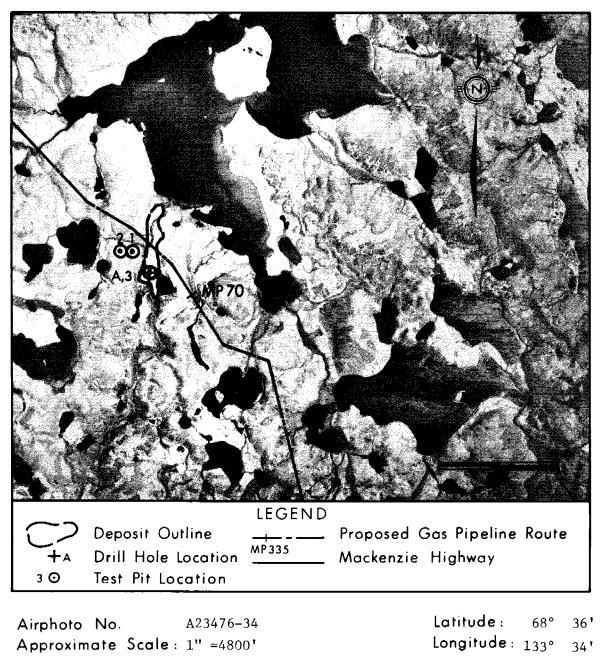
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DEPOSIT 107B-B7

- Physical Setting:Deposit 107B-B7 consists of small fluvial terraces
located 3 miles north of Noell Lake and just north
of milepost 70 on the right of way.Material:SAND silty, overlain by thick peat and silt.Volume:No volume calculated, non-granular material.
- Assessment: Deposit 107B-B7 is not recommended for development because of its lack of acceptable granular material.



DEPOSIT 107B-B7

PHYSICAL SETTING

This deposit consists of small fluvial terraces located 3 miles north of Noell Lake and just north of milepost 70 on the proposed pipeline right of way.

The terraces are 5 to 15 feet above the low, marshy floodplain of a small creek which flows from Noell Lake to Jimmy Lake. This creek dissects the southern end of the deposit. The site is moderately well to imperfectly drained. The active layer appears to be less than 1 foot over most of the area.

BIOLOGICAL SETTING

The common shrubs on the terraces are willow and alder with a lichen and moss ground cover. The flood plain is dominated by sedges and bog birch. The site is located in generally poor quality wildlife habitat. Several ptarmigan including two broods were seen at the site. Occasional fox, wolf, grizzly and black bear may occur in the area. The creek which dissects the site does not appear to support fish populations.

MATERIAL

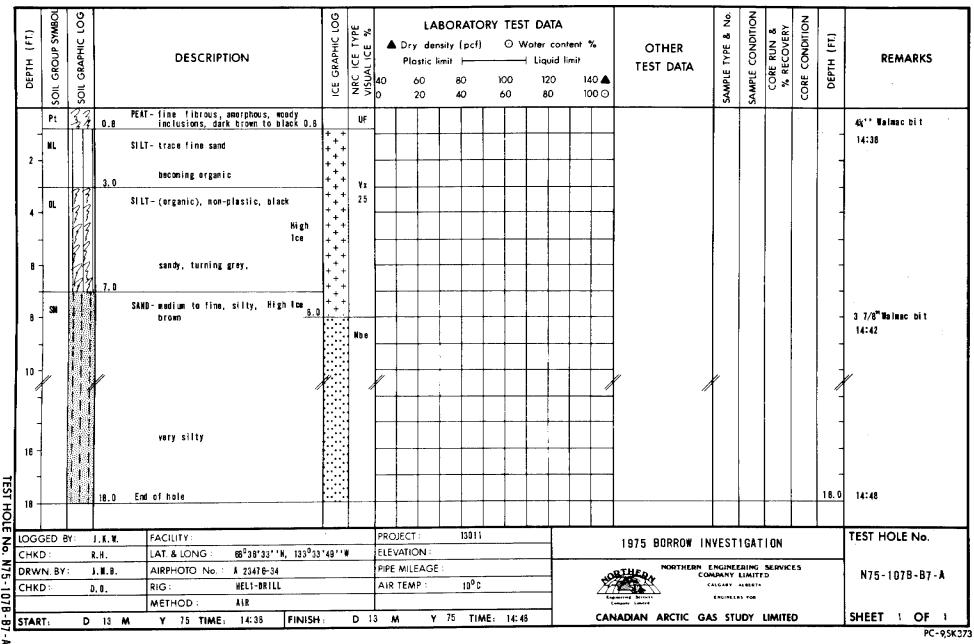
Drill hole 107B-B7-A shows 7 feet of peat and icy organic silt over 11 feet of silty sand.

VOLUME

Material of acceptable granular quality was not encountered.

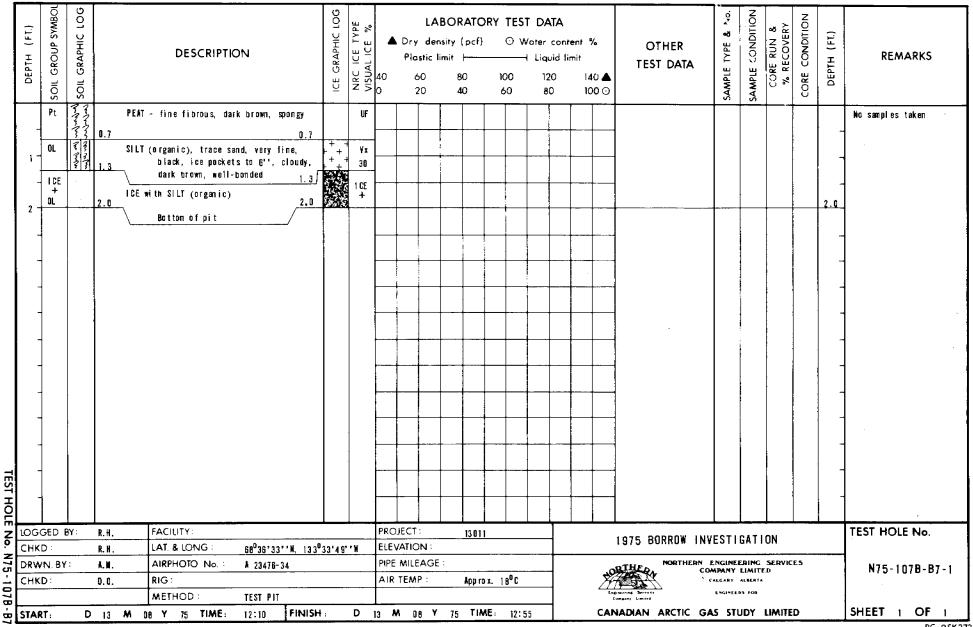
DEVELOPMENT AND REHABILITATION

Deposit 107B-B7 is not recommended for development.



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DEPTH (FT.)	IL GROUP SYMBOL	DIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40	Dry Plas	density tic limit D	y (pcf }) © (100	GT DATA Water con ⊣ Liquid I 120	imit 140 🔺		SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FT.)	REMARKS
	SOIL	SOIL				~ ^	0	2		40	60	80	100 🖸	·	SA	Š		Ŭ		
-	Pt	la la su	0.7	PEAT - moss cover, amorphous, fine fibrous with woody inclusions, dark brown, spongy		UF			-					4					-	No saaples taken
1 -	Q.	77	1.0	SILT-(organic), black	+	¥x 25	1										L_		1.0	
• -				Bottom of excavation at 1.0" Note: Adjacent area tested by geophysics										-					-	
-				- results negative, therefore axcavation abandoned						•								-	-	
-																1			-	
-														-					-	
-							 												-	
-					19.1									-					-	
GG	GED B	BY :	R. H.	FACILITY			PRC	DJECT :		1301	1									TEST HOLE No.
нка			R. H.	LAT. & LONG : 68 36'42""N, 133	⁰ 34 ' 12	••₩	ELE	VATIO	N÷					1975 BORROW IN	VESTI	GATI	ON			4
₹WI	N. BY D :		A.N. D. D.	AIRPHOTO No. : A 23476-34 RIG :				E MILE/		Ap p	19 ⁰ C		Ž		CALGABY		F.D	ES		N75-107B-B7
_				METHOD: TEST PIT M DR Y 75 TIME: 13:00 FINISH					Y		ME: 13:			Company Limiter	EMGINEE					SHEET 1 OF

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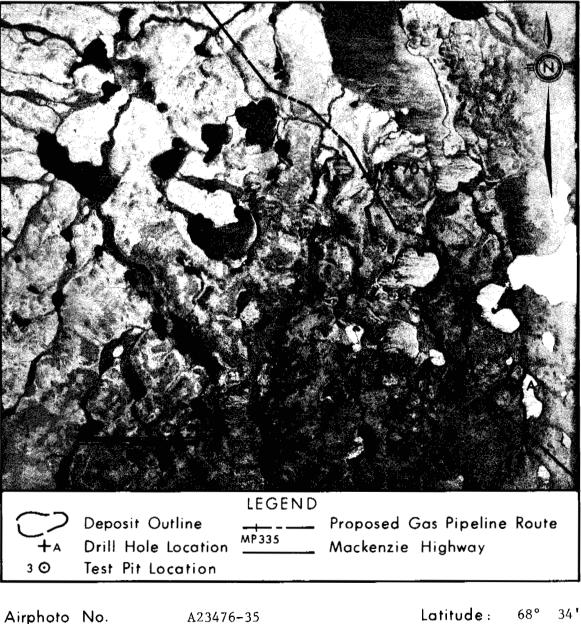
Physical Setting: Deposit 107B-B8 is a lacustrine veneered outwash plain located 2 miles northeast of Noell Lake and adjacent to the right of way between milepost 72 and 73.

Moterial: GRAVEL - silty, fine, and sand.

Volume: 1,000,000 cubic yards.

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Assessment: Deposit 107B-B8 is a source of fair to poor quality granular material suitable for general fill and backfill. It is not recommended for development due to thick overburden and massive ground ice.



Approximate Scale: 1" = 4800'

Latitude: 68° 34' Longitude: 133° 29'

DEPOSIT 107B-B8

PHYSICAL SETTING

Deposit 107B-B8 is a lacustrine veneered outwash plain deposit located two miles northeast of Noell Lake and adjacent to the pipeline right of way between mileposts 72 and 73.

The plain is a remnant of a more extensive lacustrine plain that has been greatly modified by thermokarst. At this site, the lacustrine sediments overlie outwash. Most of the surface of this deposit is gently rolling, but moderate to steep slopes are found at its edges. Overburden on the average is 5 feet thick and drainage is moderately good. The active layer is generally less than 1 foot. The sand and gravel have low ice contents, but massive ice is present in underlying sediments.

BIOLOGICAL SETTING

This plain is located in the forest-tundra transition zone. Vegetation is made up of scattered black spruce with bog birch, willow, alder and lichen. Reindeer and moose are present. The area is also moderately productive habitat for fox, wolf, grizzly and black bear. The site provides habitat for passerines and ptarmigan. Waterfowl are present in the area throughout the open-water season. The immediately adjacent small ponds and streams appear to be unsuitable fish habitat. Noell Lake supports a native domestic fishery.

MATERIAL

The drill hole and test pit at this location show up to 5 feet of peat, clay and silt over 8 feet of fine gravel and sand. Both gravel and sand are silty with occasional small amounts of clay.

VOLUME

Total estimated volume of gravel and sand based on 90 acres and a thickness of 8 feet is 1,000,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 107B-B8 is a source of fair to poor quality granular material, suitable for general fill or backfill in pipeline construction. Even though this deposit is close to the pipeline right of way, development is not recommended due to the thick overburden and the existing massive ground ice beneath the thin layer of silty sand and gravel. Poor quality and low volume also reduce its feasibility as a possible source of borrow material.

GRAPHIC LOG ź SAMPLE CONDITION **GROUP SYMBO** ICE GRAPHIC LOG CONDITION LABORATORY TEST DATA CORE RUN & % RECOVERY түрЕ Е % (FT.) ۰ö (FT) ▲ Dry density (pcf) O Water content % OTHER SAMPLE TYPE NRC ICE VISUAL ICE DESCRIPTION REMARKS DEPTH DEPTH Plastic limit -I Liquid limit TEST DATA CORE 120 40 60 80 100 140 📥 SOL SOIL 20 40 60 80 100 🖸 PEAT-fine fibrous, amorphous, black, ÜF 22 Pt. 8.5 4½ Waimac bit woody inclusions 18:43 C٤ CLAY - some fine sand, low plastic, wet when thawed Nbe 2 4 GM GRAVEL-fine, silty, and coarse sand, pebbles to 我 , sub angular. Nbn 6 ٥þ 7.5 ... 3 7/8 Walmac bit. 11 8 Nhe SAND - medium to fine, silty, some fine •• SM 19:46 •• 000 gravel, dark grey brown. ¥X 10 12 13,0 clear ICE I CE I C E 14 TEST HOLE TEST HOLE No. PROJECT : LOGGED BY: FACILITY: 13011 1.8.8 20 1975 BORROW INVESTIGATION CHKD LAT & LONG 68 034 41 'N, 133 29 26 'W ELEVATION : R. H. NORTHERN ENGINEERING SERVICES AIRPHOTO No. 3 A 23476-34 PIPE MILEAGE : DRWN.BY: J.M.B. N75-1078-B8-A COMPANY LIMITED 18⁰ C HELI-DRILL AIR TEMP CHKD: 0.0. RIG : CALGARY ALBLETA ENGINEERS FOR ALR. METHOD : SHEET 1 OF 2 FINISH : D 13 M 88 ¥ 75 TIME: 19:57 CANADIAN ARCTIC GAS STUDY LIMITED M DB Y 75 TIME: 19:43 START: D 13 C13

TEST HOLE LOG

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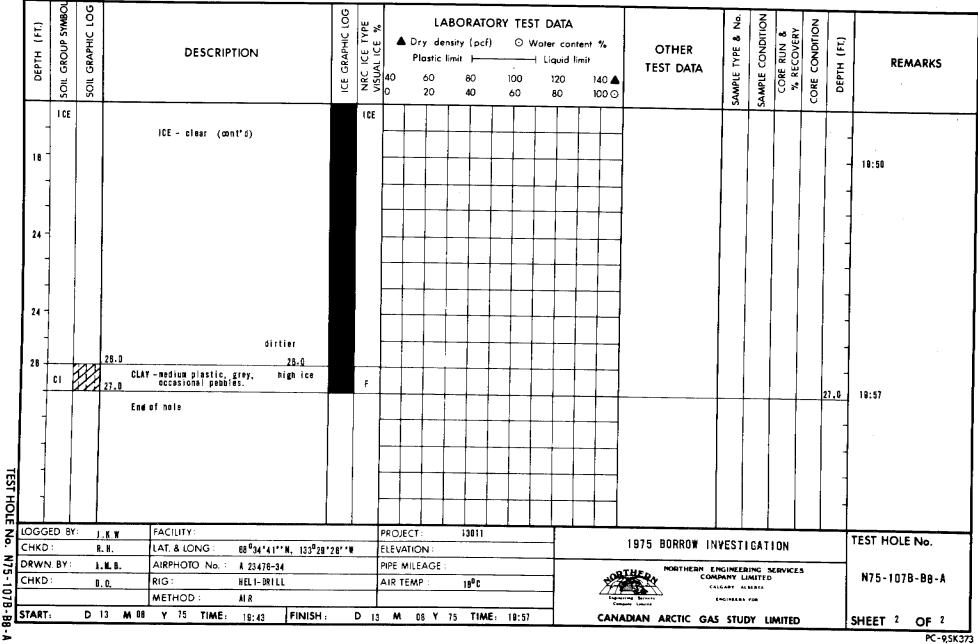
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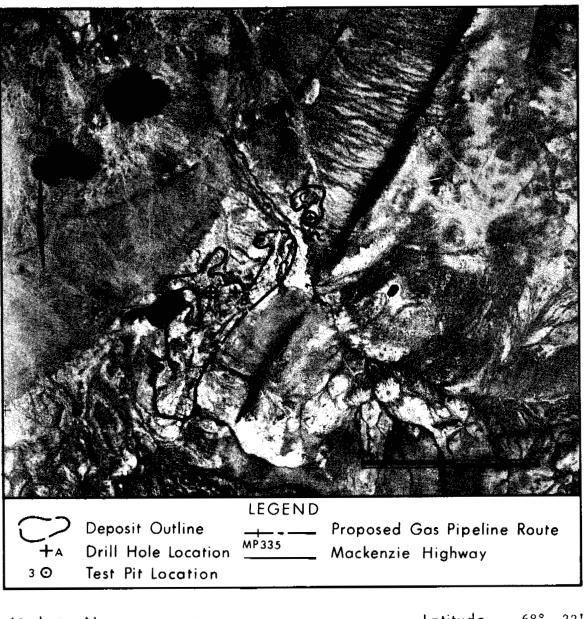
DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Pla ć	den	sity (p	ocf)	οw	F DATA (ater con) Liquid I 120 80	limit 12	% 40 ▲ 50 ⊙ ;	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
+			D.2 PEA	lT - moss cover, amerphous, fine		UF							Г									No samples taken
-	CL	\mathcal{M}		fibrous, woody inclusions									ļ								_	
		XX	1.0	brown, wet, soft, occ. peaty layer[.0	1															1		
1+	NE.			T - clayey, peobles rounded to 3/8**	+ +	H Yx	1															
-				ice to 3" pockets	+ +	H							<u></u>	-						1	-	
			2.0	Bottom of pit	+ +	₽															2.0	
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ເວດ	ED F	L 3Y :	R.H.	FACILITY	.	-L.	PRC	JECT	:	1	30 11		<u> </u>		<u> </u>			CAT	ON N			TEST HOLE No.
СНК			R.H.	LAT. & LONG : 68034'41"", 1330	29'26	' 'W	ELE	VATIC	DN :							1975 BORROW INV	6911					
DRW			A. N.	AIRPHOTO No. : A 23476-34			PIPE	MIL	EAGE							ATHED NORTHERN E		ERING	SERVK ED	ES.		N75-107B-B8-1
СНК			D. O.	RIG :			AIR	TEM	NP. :	4	p p ro x.	. 21 ⁰ C			Å		ALGARY	ALBERT				
				METHOD : TEST PIT											En	nginaering Berries Campany Limited	ENGINEI					
STAR			13 M	08 Y 75 TIME: 19:00 FINISH		D	13	W 0	8 Y	75	TIM	E: 20:	00		CAP	NADIAN ARCTIC GA	S ST	UDY	LIMIT	ED		SHEET I OF I

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Physical Setting: Deposit 107B-B9 is a kame terrace complex located 2.5 miles south of Sitidgi Lake and 6 miles northeast of milepost 96 on the right of way.

Moterial: SAND and GRAVEL - interbedded fine sand and gravel with a little silt.

- Volume: 5,800,000 cubic yards.
- Assessment: Deposit 107B-B9 is a source of fair quality granular material suitable for general fill, backfill and building pad subgrade.



Airphoto No. A12918-30 Approximate Scale: 1" = 3250'

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Latitude: 68° 22' Longitude: 132° 44'

DEPOSIT 107B-B9

PHYSICAL SETTING

Deposit 107B-B9 is a kame terrace complex about 2.5 miles south of Sitidgi Lake. The deposit is 6 miles northeast of milepost 96 on the proposed pipeline right of way. This deposit corresponds to source number 452 in Ripley, Klohn, and Leonoff DIAND Granular Materials Inventory Zone IV (1972) report.

The terrace complex consists of ridges and hills located along the eastern edge of a lowland occupied by Sitidgi Lake. The topography in the area is gently to moderately rolling with local relief of about 50 feet and occasional slopes to 20 degrees.

Overburden is normally thin, but peat and silt may vary between 1 and 3 feet in low areas. Drainage on hills, ridges and most slopes ranges from moderately good to good, but depressions are poorly drained. The active layer is from 1 to 5 feet thick. Below the active layer the deposit is frozen with varied but generally low ice content.

Terrain between the deposit and the pipeline right of way is a drumlinized morainic plain with a few peat-filled marshy drainageways.

BIOLOGICAL SETTING

Most of the site is covered by white spruce up to 40 feet high and a thick understory of dwarf birch, willow, crowberry and lichen. Low, wet areas are covered with sedges. The site provides low quality habitat for fox, wolf, and moose but good habitat for reindeer and caribou. A pair of swans was observed nesting on the adjacent lake in 1975. The nearby lake does not appear to support fish populations.

MATERIAL

Drill hole and test pit logs and the DIAND report indicate this deposit is mainly interbedded fine sand and gravel with a small amount of silt. In test pit 107B-B9-1 ablation till was encountered at 4.2 feet. Massive ice appeared at a depth of 10 feet in drill hole 107B-B9-B and therefore, may occur elsewhere in the deposit.

VOLUME

Total estimated volume, based on 270 acres and a maximum depth of 30 feet under ridges is 5,800,000 cubic yards. The DIAND report giving a lower volume calculation of 1,500,000 cubic yards is based on a smaller area and shallower depth.

DEVELOPMENT AND REHABILITATION

Deposit 107B-B9 is a source of fair quality granular materials in an area where good granular deposits are scarce. More drilling is needed to outline the best portions of the deposit. This deposit could be used for general fill and backfill in pipeline construction and building pad subgrade material.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socio-economic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

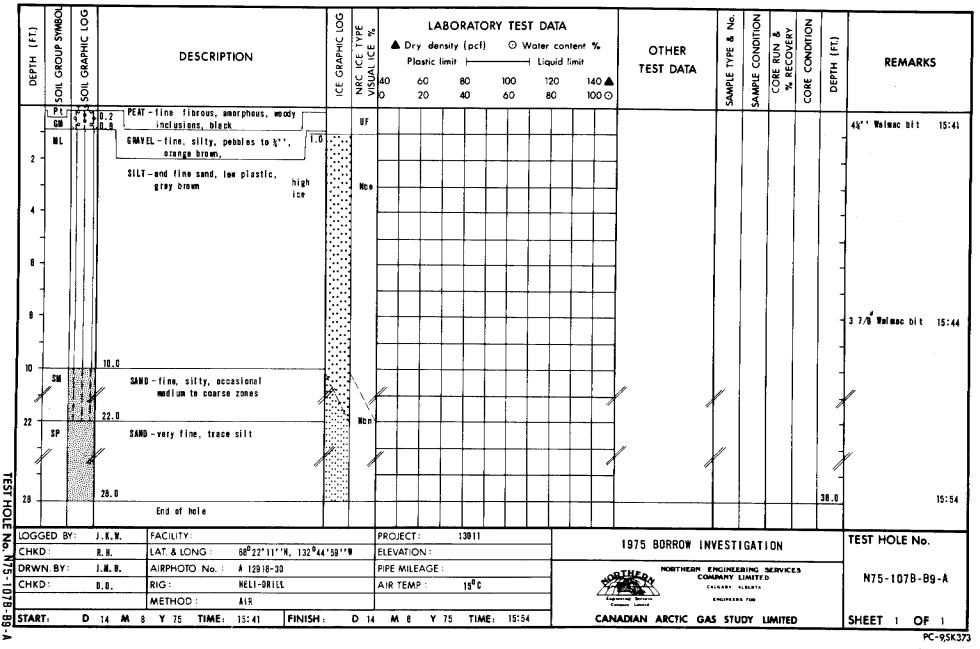
Access to the deposit would probably be accomplished via the pipeline right of way. A 5 mile snow road from the pipeline right of way would be necessary to reach the deposit.

Tree and shrub cover would have to be removed from areas to be excavated and disposed of in accordance with land use regulations. The peat cover and overburden would then be stripped from the area and stockpiled around the edge of the excavation.

Development of this deposit would involve excavating borrow material in stages from the higher, well drained areas so that good drainage would be maintained. This development could be accomplished by blasting techniques or conventional earthmoving techniques depending on the degree of ice cementation. Care would have to be taken to leave sufficient material over areas with massive ice in order to prevent thermal degradation. The excavated material may have to be stockpiled, thawed, and drained before it is used.

Equipment required for development would be dozers, rippers, end-dump trucks, and front-end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.



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ŝ SAMPLE CONDITION ICE GRAPHIC LOG CONDITION GROUP SYMBOL GRAPHIC LOG CORE RUN & % RECOVERY NRC ICE FYPE VISUAL ICE % LABORATORY TEST DATA SAMPLE TYPE & DEPTH (FI.) DEPTH (FT.) O Water content % ▲ Dry density (pcf) OTHER REMARKS DESCRIPTION - Liquid limit Plastic limit + TEST DATA CORE 100 120 140 📥 80 60 SOIL SOIL 80 100 🖸 0 40 60 20 4%'' Walmac bit 16:58 PEAT-fine fibrous, amorphous, woody ₽t UF inclusions, roots, dark brown 1.0 S 1.5 SAND-fine, silty ICE 2.0 I CE TEF 2 SAND - fine, silty 31 Nbe 4.0 OCC. GP 00 GRAVEL-fine, trace fines, pebbles ¥x to 3/41", sub rounded, ovate 6 3 7/8" Walmac bit 17:00 8 00 9.0 Ice rich SAMD-medium, grey black SP 10. 0 10.0 10 ICE clear ICE 1 CE TEST HOLE 28.0 17:09 clear 28.0 28 End of hole TEST HOLE No. PROJECT : 13011 FACILITY J.K.W. LOGGED BY 1975 BORROW INVESTIGATION z ē ELEVATION : LAT. & LONG 68⁰22'16''N, 132⁰44'37''W CHKD R.H. NORTHERN ENGINEERING SERVICES PIPE MILEAGE N75 -AIRPHOTO No. A 12918-30 N75-1078-89-8 DRWN, BY: J.M.B. COMPANY LIMITED 2 2⁰ C CALGARY ALBERTA AIR TEMP. HELI-DRILL CHKD D. O. RIG ENGINEERS FOR 078-89-METHOD : AIR SHEET 1 OF 1 CANADIAN ARCTIC GAS STUDY LIMITED D 14 M 8 Y 75 TIME: 17:09 16:58 FINISH : D 14 M 8 Y 75 TIME: START: PC-9,5K373

TEST HOLE LOG

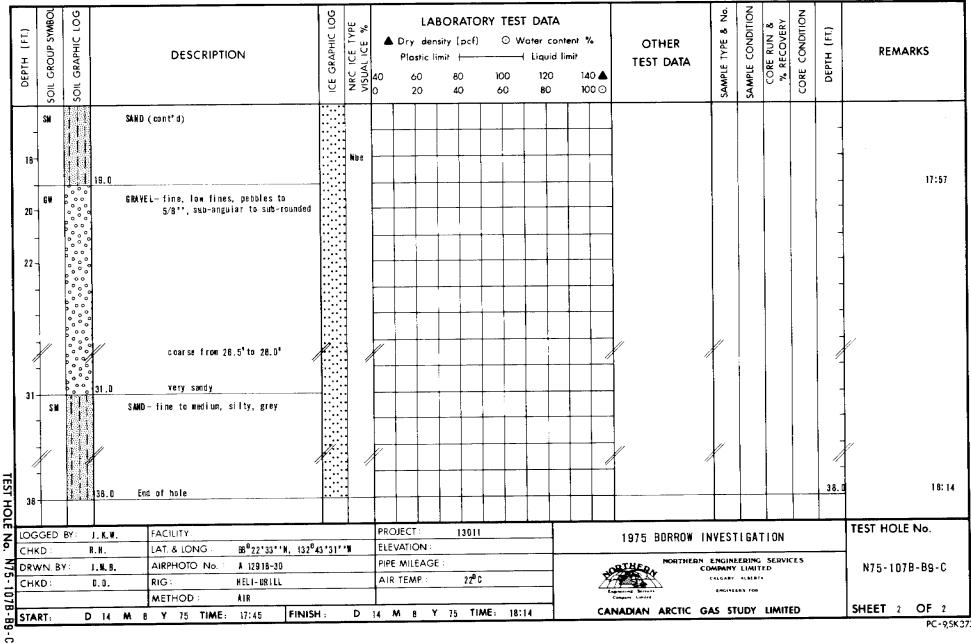
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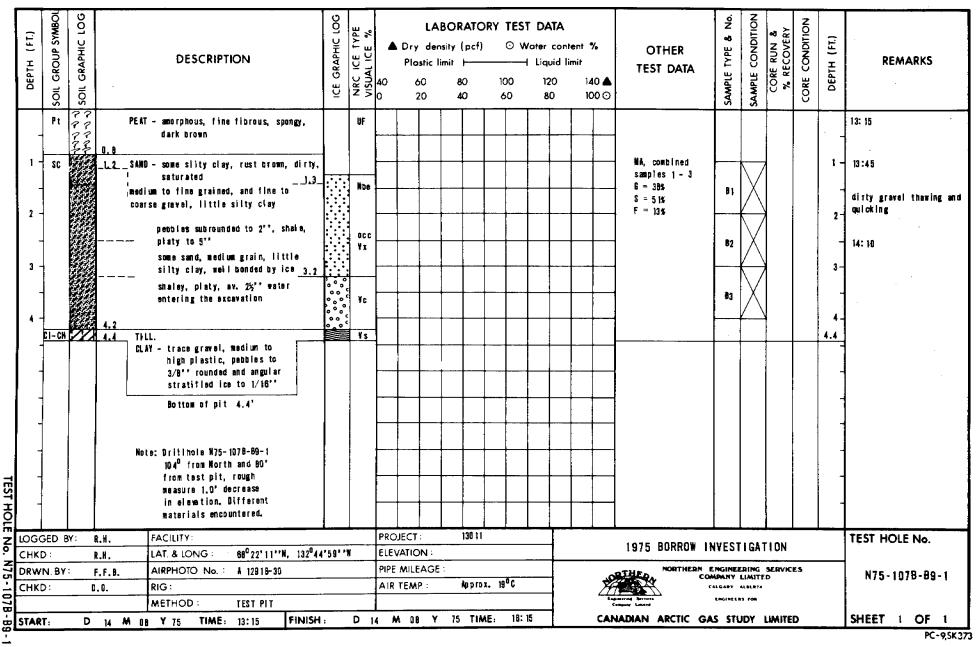
DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION			NRC ICE TYPE VISUAL ICE %	A Dru	densit _i itic limil 0	(pcf)	ΟV	T DATA Vater con 1 Liquid I 120 80	imit 14	% 10 ▲ 10 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
2	SM		2.0	D~fine, silty, trace gravel, pebbles to 3/0°°, orange, damp			UF														4%;"Walmac bit 17;
	NL		SIL 1. 3.0	T- trace fine samd, low plastic	3.0															-	
4-			GRA 5.0	¥EL— fine, si≹ty, poorly sorted			¥be		_											-	
8			SAN	D-fine to medium, silty, grey with orange band from 6' - 7'																-	
8-	1												;								37/8 ⁷⁷ Walmac bit 17
10-			_10.0	- pebble to 1.5"		· · · · · · · · · · · · · · · · · · ·															
- 14-			_14.0	less silty (possibly SP)																	
16																				-	
	GED B		.K.W.	FACILITY			PI	ROJECT		1 30 11			<u></u>		1975 BORROW IN	VEST	1647				TEST HOLE No.
		R.		LAT. & LONG : 68 ⁰ 22*33**N, 133	2 ⁰ 43'31'	' W		EVATION													
CHKD	N.BY:	: J. D,	N. B 0.	AIRPHOTO No. : A 12918-30 RIG : HELI-DRILL	<u>-</u>	<u> </u>		PE MILEA		2 2 ⁰ C				+0 <u>8</u>		APANY I	IMITE.		5		N75-107B-B9-C
				METHOD: AIR			-f			22.6					Irring Surveys	ENGINEER:					
STAR	۲:	D	14 M 8		ISH :	D	 14	M 8	Y 75	TIME	. 18:1			CAN/	ADIAN ARCTIC GA	с сти	ר אט	IMAITE	`		SHEET 1 OF 2

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PC-9,5K373



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00 **GROUP SYMBOI** ICE GRAPHIC LOG SAMPLE CONDITION Š CONDITION NRC ICE TYPE VISUAL ICE % O & LABORATORY TEST DATA CORE RUN & % RECOVERY (FT.) SAMPLE TYPE & (FT.) **GRAPHIC** OTHER DESCRIPTION REMARKS DEPTH DEPTH Plastic limit |-------- Liquid limit TEST DATA CORE 60 80 100 120 140 🔺 SOIL SOIL 20 40 60 80 100 🖸 770.2 Pt PEAT - fine fibrous, brown, woody UF 17:20 MA, combined 0.2 inclusions samples 1 & 2 GM GRAVEL - coarse to fine, little fine to Oversize 3.0% 81 ູ່ໃດ medium sand, little silt, G = 66%1-17:55 gravel platy to 5"", rust S = 17% brown, dry, "gap-graded" F = 17% d 0 1.5 82 occasional quartzite cobble, rounded to 8** 2.0 2 18:50 2 damp 19:05 MA, sample 3 З 3-6 = 12% S ≈ 65% BB SH SAND - fine-grained, some silt, brown, damp F = 23% Bottom of pit 4 19:45 4 TEST HOLE No. FACILITY PROJECT TEST HOLE No. R.H. 13011 LOGGED BY: 1975 BORROW INVESTIGATION 68⁰22'33''N, 132⁰43'31''W ELEVATION : CHKD LAT. & LONG R.H. N75-1 PIPE MILEAGE : AIRPHOTO No. NORTHERN ENGINEERING SERVICES DRWN. BY: A.M. A 12918-30 N75-107B-B9-2 COMPANY LIMITED AIR TEMP Approx. 21⁰C CHKD: 0.0. RIG : * CALGARY ALBERTA 1078-89-2 INGINEERS FOR METHOD : TEST PIT Longit SHEET 1 OF 1 FINISH : D 14 M 08 Y 75 TIME: 19:45 CANADIAN ARCTIC GAS STUDY LIMITED D 14 M 08 Y 75 TIME: START: 17:20

TEST HOLE LOG

PC-9,5K373

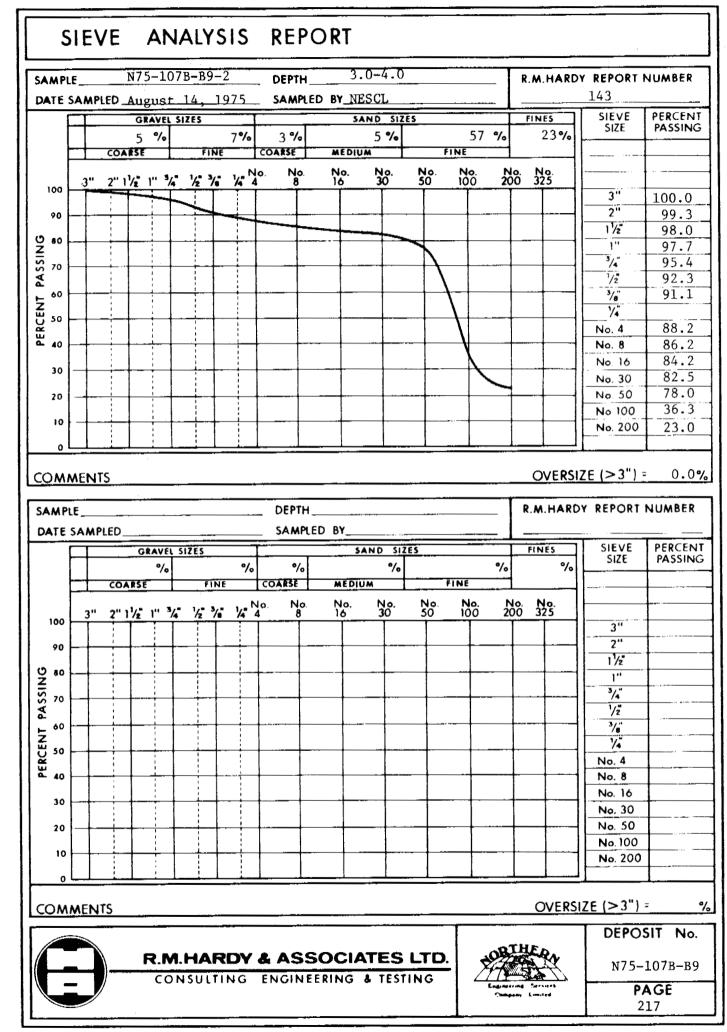
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SAM	PLE_	N75	5-107B-	-B9-	1	_ DEF	PTH	1	.0-4.0)			R.M.HARI	DY REPORT	NUMBER
DAT	e sa	MPLED Aug	gust 14	i. 1	975	_ SA/	MPLED	BY_N	ESCL			_		136	
			AVEL SIZES						AND SIZ	ES		<u> </u>	FINES	SIEVE	PERCENT
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20)			-+	+						<u> </u>			No. 50	20.6
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90 04 70 70		40 COARSE	%	2) FINE		COARSI	E	MEDIU No.	5 % M	No.	FINE No.) %	17 %	SIZE	PASSING 100.0 94.2 84.6 68.0 60.1 50.7
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PASSING		40 COARSE	%	2) FINE		COARSI	E	MEDIU No.	5 % M	No.	FINE No.) %	17 %	SIZE	PASSING 100.0 94.2 84.6 68.0 60.1 50.7 44.7
ERCENT PASSING 05 09 02 08 06		40 COARSE	%	2) FINE		COARSI	E	MEDIU No.	5 % M	No.	FINE No.) %	17 %	SIZE 3'' 1\/2 1\'2 1\'2 1\'' 3\4 1\2 3\6 1\4 1\2 3\6 1\4 No. 4	PASSING 100.0 94.2 84.6 68.0 60.1 50.7 44.7 34.4
ENT PASSING		40 COARSE	%	2) FINE		COARSI	E	MEDIU No.	5 % M	No.	FINE No.) %	17 %	SIZE 3'' 2'' 1/2 1'' 3/4 1/2 3/6 1/2 3/6 1/2 No. 4 No. 8	PASSING 100.0 94.2 84.6 68.0 60.1 50.7 44.7 34.4 32.4
ERCENT PASSING 05 09 02 08 06		40 COARSE	%	2) FINE		COARSI	E	MEDIU No.	5 % M	No.	FINE No.) %	17 %	SIZE 3'' 2'' 1'/2 1'' 3'/4 1/2 3'/6 1/2 3'/6 1/2 3'/6 1/2 1/2 No. 4 No. 4 No. 8 No. 16	PASSING 100.0 94.2 84.6 68.0 60.1 50.7 44.7 34.4 32.4 29.8
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PERCENT PASSING 05 05 04 08 05 05 04 08		40 COARSE	%	2) FINE		COARSI	E	MEDIU No.	5 % M	No.	FINE No.) %	17 %	SIZE 3'' 1'/2 1'' 1'/2 1'' 3'/4 1/2 3'/6 1/2 3'/6 1/2 3'/6 1/2 1/2 3'/6 1/2 3'/6 1/2 3'/6 1/2 1/2 3'/6 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2	PASSING 100.0 94.2 84.6 68.0 60.1 50.7 44.7 34.4 32.4 29.8 27.4 24.6 21.1
90 00 00 00 00 00 00 00 00 00 00 00 00 0		40 COARSE	%	2) FINE		COARSI	E	MEDIU No.	5 % M	No.	FINE No.) %	17 %	SIZE 3'' 2'' 1\/2 1\'2 1\'2 3\'6 \'4 \'4 No. 4 No. 4 No. 8 No. 16 No. 30 No. 50	PASSING 100.0 94.2 84.6 68.0 60.1 50.7 44.7 34.4 32.4 29.8 27.4 24.6
90 00 00 00 00 00 00 00 00 00 00 00 00 0		40 COARSE 3" 2" 1½" 1	%	2) FINE		COARSI	E	MEDIU No.	5 % M	No.	FINE No.) %	17 %	SIZE 3'' 1'/2 1'' 1'/2 1'' 3'/4 1/2 3'/6 1/2 3'/6 1/2 3'/6 1/2 1/2 3'/6 1/2 3'/6 1/2 3'/6 1/2 1/2 3'/6 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2	PASSING 100.0 94.2 84.6 68.0 60.1 50.7 44.7 34.4 32.4 29.8 27.4 24.6 21.1 17.3
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90 80 70 80 80 80 80 80 80 80 80 80 80 80 80 80		40 COARSE 3" 2" 1 1/2" 1 3" 2" 1 1/2" 1 NTS R	%				5SO		5 %) %	17 %	SIZE 3" 2" 1½ 1½ 3/4 1/2 3/4 1/2 3/6 1/2 3/6 1/2 3/6 1/2 3/6 1/2 3/6 1/2 3/6 1/2 3/6 1/2 3/6 No. 4 No. 4 No. 4 No. 4 No. 50 No. 50 No. 100 No. 200 ZE (>3") = DEPOS N75-10	PASSING 100.0 94.2 84.6 68.0 60.1 50.7 44.7 34.4 32.4 29.8 27.4 24.6 21.1 17.3 3.0 %

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Physical Setting: Deposit 107B-B10 is an esker with a kame delta at its eastern end. It is located 4 miles east of Campbell Lake and 3.5 miles west of milepost 94 on the right of way. Material:

SAND - fine to medium with variable silt content.

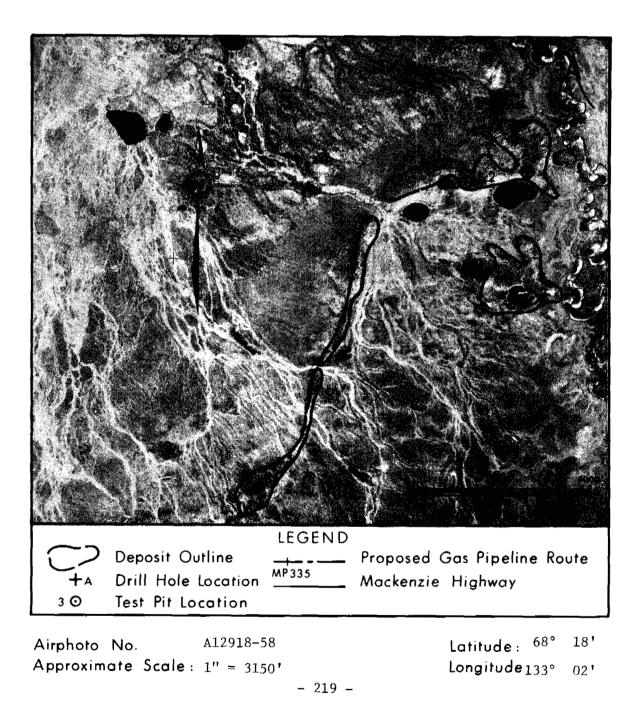
Volume : 9,400,000 cubic yards.

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Assessment: Deposit 107B-B10 is a source of fair quality granular material suitable for general fill and backfill. Access to the deposit is fair over poorly drained moraine and lacustrine plain.



DEPOSIT 107B-B10

PHYSICAL SETTING

This deposit begins approximately 4 miles east of Campbell Lake and runs in a northeasterly direction for about 4 miles. The northeast end of the deposit is 3.5 miles west of milepost 94 on the proposed pipeline right of way.

The deposit consists of a broad esker with a probable kame delta at its eastern end. The crests of the esker and kame delta stand 40 to 80 feet above the surrounding lowlands with side slopes of 15°. Fresh scarps around the lake within the kame delta indicate active thermokarst is occurring.

Overburden is generally less than 1 foot and drainage varies from moderately good to good. The active layer is about 3 feet deep, below this the deposit is frozen with low to moderate ice content. Scattered ground ice can be expected throughout the kame delta.

The terrain west of the deposit is a poorly drained flat to gently sloping moraine and lacustrine plain. Poorly drained fluvial terraces and a small creek border the eastern end of the deposit and a poorly drained moraine plain lies between the stream and the pipeline right of way.

BIOLOGICAL SETTING

The crests and south-facing slopes of the esker and delta support mixed black spruce and white birch up to 30 feet in height, with pure black spruce on north-facing slopes. The understory on both slopes is fairly uniform and consists of dwarf birch, willow, labrador tea, and lichen. The area provides low productivity habitat for fox, wolf and snowshoe hare. The site lies within the winter range of the Mackenzie Reindeer Herd. Good moose habitat occurs around the small lake adjacent to the site and along the nearby tributary of Norris Creek, but moose populations in the area are low. No evidence of beaver was seen in the adjacent stream or lakes. The area is important waterfowl habitat although no waterfowl were observed on the nearby lakes. The fish potential of the adjacent creek is not known.

MATERIAL

The drill hole and test pit logs from this deposit indicate the material is mainly fine to medium sand with varying silt content. Six feet of silty gravel is present at site 107B-B10-3 in the kame delta. Further drilling will be required to define areas of better quality material.

VOLUME

An estimate of total volume based on an area of 390 acres and 30 foot depth is 9,400,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 107B-B10 is a source of fair quality granular material which could be used for general fill and backfill in pipeline construction.

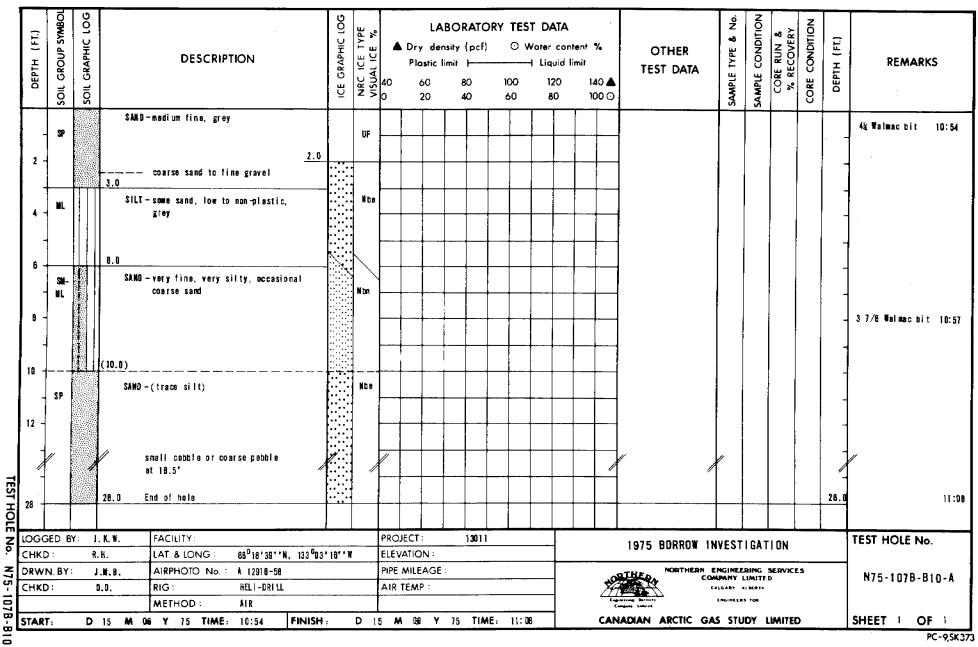
No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the deposit could be obtained via the pipeline right of way. In order to minimize environmental damage, snow roads would be built to transport the borrow material from the deposit to haul points on the right of way, a distance in excess of 4 miles. Access would be over poorly drained moraine and lacustrine plain and care would have to be taken not to disturb the drainage and initiate thermokarst subsidence. Tree cover would have to be removed, both from areas to be excavated and the haul road right of way, and disposed of or harvested in accordance with current land use regulations. The peat cover and overburden would then be stripped from the area to be excavated, and stockpiled around the edge of the excavation area.

Development of this deposit would involve excavating borrow material evenly from the higher, well drained areas so that good drainage would be maintained. This type of development could be accomplished by using blasting or conventional earthmoving techniques depending on the degree of ice cementation. The excavated material may have to be stockpiled, thawed, and drained before it is used. A buffer zone would have to be maintained, between the nearby creek and the excavation, to ensure that thermokarst subsidence and siltation of the stream is prevented.

Equipment required for development would be dozers, rippers, end-dump trucks, and front-end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.



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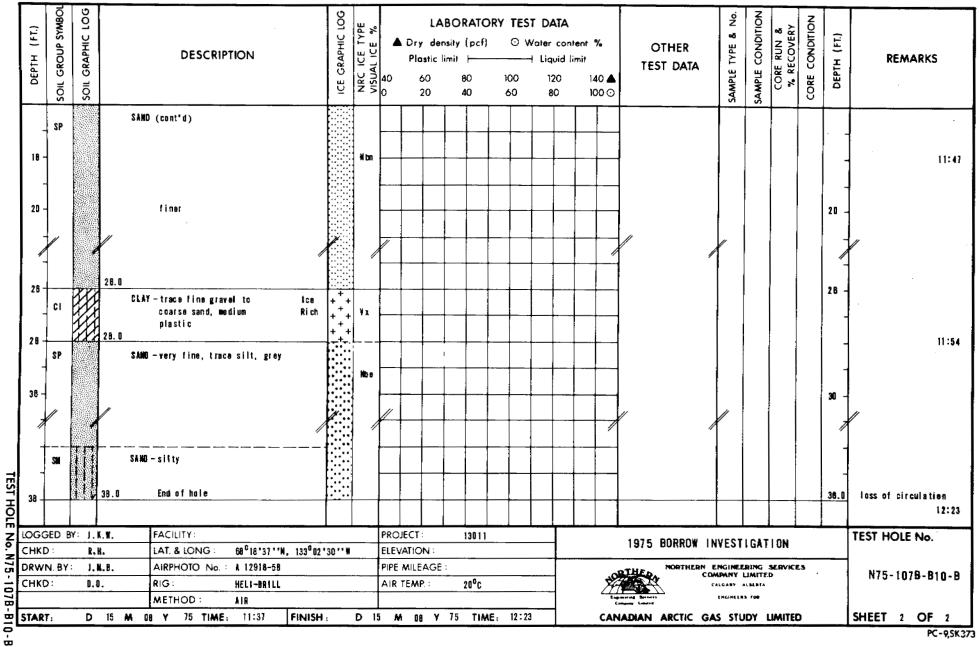
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DEDTU (ET)			SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40	Dry	densit tic lim)		C C) Wot L)	DATA er contr .iquid lit 120 80		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FL)	REMARKS
		. 19	20	SAND -	-fine, silty, rusty brown													<u>s</u>				4% ⁺⁺ Walwac bit 11:37
	2 - SP		1 4		-very fine grained, wet, soft to 3.0', brown		UF			· .	_										-	
	4-				3.0 slight trace silt		Nbe									-					-	
	6 -				brown to grey								- 1								-	
	8			<u>(11.0)</u>	Bish																	3 7/8'' Wai mac bit 11:42
Я Z	OGGE	ED BY		J.K.W.	FACILITY: LAT. & LONG : \$80°18'37''K, 133°0		······································				130	1		_		1975 BORROW I	NVES	TIGA	TION			TEST HOLE No.
N75-1	HKD DRWN CHKD	: I. BY : :		R.H. J.H.B. D.O.	LAT. & LONG : 88 ⁰ 18'37' ¹ N, 133 ⁰ 0 AIRPHOTO No. : A 12918-58 RIG : HELI-DRILL	2.30.	Ħ	PIP	E MILE R TEMI	AGE	200	C			Ź	NORTHERN CI	CALGAN	r liwe	TE.D	ICES		N75-107B-B10-B
078-B	TART	 1	D	15 M D	METHOD: AIR 8 Y 75 TIME: 11:37 FINIS	H:	D	15	M 81	8 Y	75 1	IME:	12:23		C/	ANADIAN ARCTIC G			LIMI	TED		SHEET 1 OF 2 PC-9,5K37

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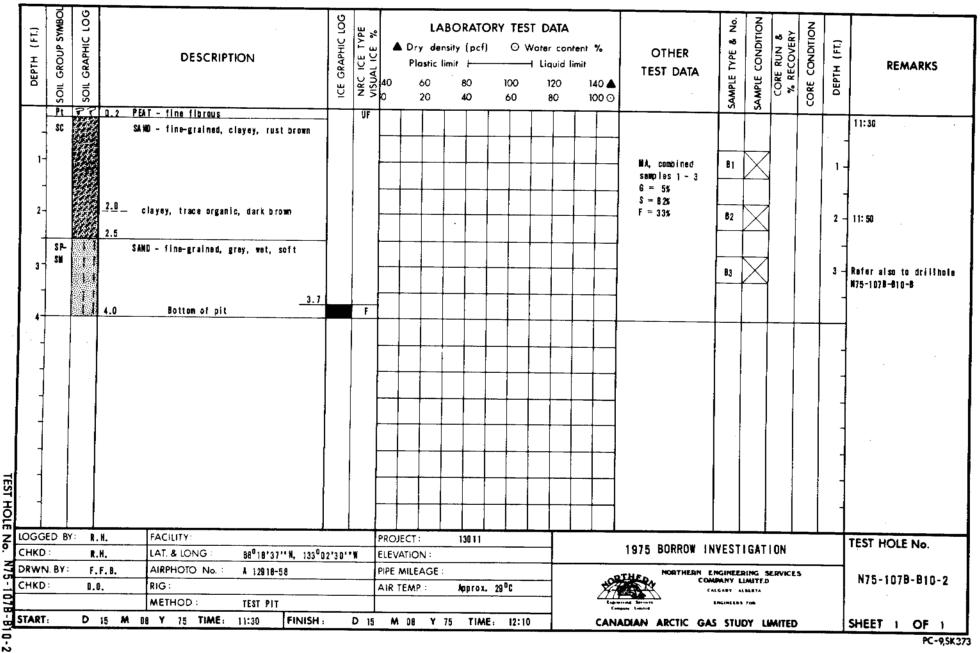
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> N75 -107B-B

DEPTH (FL)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Dry de	nsity {p	cf)	οw	T DATA Vater cont Liquid li 120 80		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (Ft.)	REMARKS
		33 1/1		amorphous, fine fibrous, occasional woody inclusions, dark brown to	1	UF													-	10:45 No samples taken
1-				black silty, little sand, medium to fine, rust brown					: 	_	-								1.3	11:00
-		~ ~ ~		Bottom of pit (ICE) Frozen at Abandoned bottom of pit		(F)														
-				Note: Refer also to drillhole N75-1078-810-4															-	
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CHE	KD : NN. BY		R. H. A. M.	LAT. & LONG : 68 18 39' 1, 133 AIRPHOTO No. : 1 12918-58	03 10	н п	+	MILEAG	E :					OTHEN NORTHERN	ENGINE	ERING	SERVIO	ES		N75-1078-B10-1
CHI			D.O.	RIG:		<u> </u>	+	TEMP :		orox.	18 ⁰ C		<u>t</u>		CALGARY	ALSERT				
				METHOD : TEST PIT									<u> </u>	ng-nerating Sur-rites Company Lamited	E 961 ME 8					
STA	RT:	D	15 M I	08 Y 75 TIME: 10:45 FINIS	1:	D	15 🖡	V 08	/ 75	TIME	11	: 00	<u>CA</u>	NADIAN ARCTIC GA	ls st	UDY	LIMITI	ED		SHEET 1 OF 1

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106 **GROUP SYMBOL** SAMPLE CONDITION ICE GRAPHIC LOG Š CORE CONDITION NRC ICE TYPE VISUAL ICE % LABORATORY TEST DATA CORE RUN & % RECOVERY DEPTH (FT.) ۰ð (FT.) SOIL GRAPHIC OTHER SAMPLE TYPE REMARKS DEPTH DESCRIPTION Plastic limit |------ Liquid limit TEST DATA 100 120 140 🔺 60 RO. SOIL 20 40 60 80 100 🔿 33 UF Pt PEAT - amorphous, fine fibrous, woody 33 0.4 GM GRAVEL-and silt, pebbles, angular to 3''. roots, brown 0.9 1 °. 6P -GRAVEL-and coarse grained sand, stratified, layer approximately 0.4' SP ٥ 2 MA, combined 2 samples 1 & 2 Sir-SAND - coarse, medium, fine, and fine to G = 41% **B**1 SC coarse gravel, trace fines (clayey) S = 50%possibly cemented, peobles sub-F = 9% 3 З rounded to 2½'', platy to approx. 15'' * 5'' 4 82 5 6 6 occasional oversize to 7" Face exposed to 7.0' 7 TEST HOLE below top of lake bank TEST HOLE No. PROJECT : 13011 FACILITY 2 o LOGGED BY: R.H. 1975 BORROW INVESTIGATION 68⁰17'59''N, 133⁰02'16''W ELEVATION : CHKD R. H. LAT, & LONG N75-1078-B10-3 PIPE MILEAGE : NORTHERN ENGINEERING SERVICES AIRPHOTO No. DRWN. BY : D.J.M. A 12918-58 N75-107B-B10-3 COMPANY LIMITED AIR TEMP Approx. 27 °C RIG : CALGARY ALBERTA CHKD: D. G. ENGINEERS FOR METHOD : TEST PIT SHEET i OF CANADIAN ARCTIC GAS STUDY LIMITED FINISH D 15 M 08 Y 75 TIME: 16:00 1 START: D 15 M 08 Y 75 TIME: 15:00

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TEST HOLE LOG

PC-9,5K373

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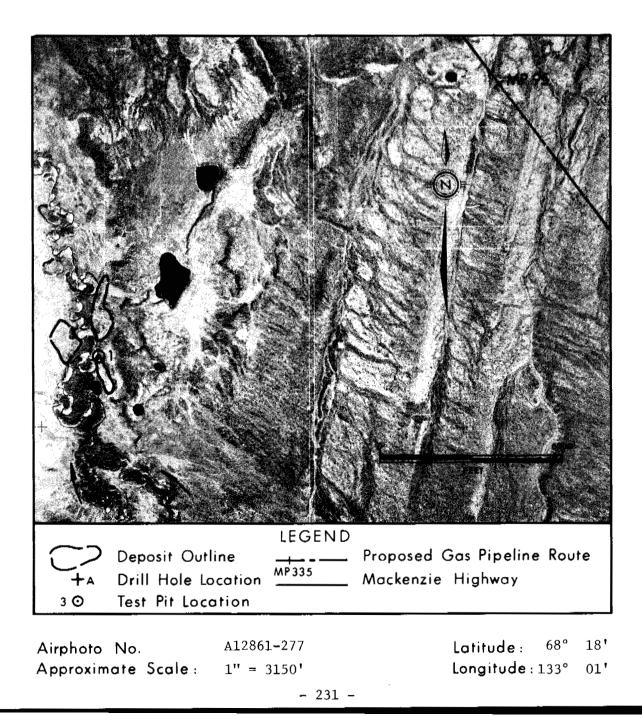
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Physical Setting: Deposit 107B-Bll is a fluvial terrace located 6.5 miles east of Campbell Lake and 3.5 miles west of milepost 94 on the right of way.

Material: GRAVEL - interbedded with sand, scattered boulders.

Volume: 800,000 cubic yards.

Assessment: Deposit 107B-Bll is a source of good quality granular material suitable for general fill, backfill, building pads and possible concrete aggregate.



DEPOSIT 107B-B11

PHYSICAL SETTING

This deposit is a fluvial terrace located 6.5 miles east of Campbell Lake and approximately 3.5 miles west of milepost 94 of the proposed pipeline right of way.

The terrace stands about 12 feet above the floodplain of a stream which bissects the deposit. Overburden varies between 1 and 5 feet and drainage is imperfect. The active layer is probably between 1 and 3 feet thick, increasing where overburden is thin.

Terrain between the deposit and the pipeline right of way is a poorly drained, gently rolling morainic plain.

BIOLOGICAL SETTING

The vegetation at the site is stunted black spruce. The understory consists of dwarf birch, willow, labrador tea, and lichen, with sedges in depressional areas. The area provides low productivity habitat for fox, wolf and snowshoe hare. No evidence of beaver was seen in the stream or lakes. The site lies within the winter range of the Mackenzie Reindeer Herd. Good moose habitat occurs around the small lake adjacent to the site and along the tributary of Norris Creek. Moose populations in the area are low. The area is important waterfowl habitat although no waterfowl were observed on the nearby lakes. The fish potential of the creek is not known.

MATERIAL

The test pit log shows 10 feet of interbedded gravel and sand with scattered boulders up to 8 inches in diameter. The platy nature of the gravel indicates high shale contents.

VOLUME

Total estimated volume based on 60 acres and a 10 foot depth is 800,000 cubic yards. The volume of this deposit could be greatly increased by including adjacent poorly drained terraces that appear to be covered by a moderate thickness of overburden.

DEVELOPMENT AND REHABILITATION

Deposit 107B-Bl1 is a source of good quality granular material based on the results of one test pit excavated at the deposit. More drilling and test pitting would be required to determine overburden thickness, the extent, and quality of the material in this deposit. Granular material from this deposit could be used for general fill, backfill in pipeline construction, building pads, and possibly concrete aggregate.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the deposit from the pipeline right of way would have to cross poorly drained terraces and a stream, but could follow an esker ridge for a portion of the way. Care would have to be taken not to initiate thermokarst subsidence in the poorly drained area between the deposit and the pipeline alignment.

In order to minimize environmental damage, snow roads would be built to transport the borrow material from the deposit to the right of way, a distance in excess of 3 miles.

Tree cover would have to be removed, both from areas to be excavated and along the haul road right of way, and disposed of in accordance with current land use regulations. The peat cover and overburden would then be stripped from the area to be excavated and stockpiled around the edge of the excavation.

Development of this deposit would involve excavating borrow material evenly from the higher, well drained areas so that good drainage would be established over the area. Care would have to be taken to avoid siltation of nearby streams. This could be accomplished by a buffer zone between the stream and the borrow pit. This source could be developed by using blasting or conventional earthmoving techniques depending on the degree of ice cementation. The excavated material may have to be stockpiled, thawed, and drained before it is used. Crushing and/or screening of the material may be required to produce quality construction aggregates.

Equipment required for development would be dozers, rippers, end-dump trucks, front-end loaders, as well as screening, crushing and concrete plants if required.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHI		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %		-	dens stic fir 0		ORY TE f) O 100 60		ntent %		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FL)	REMARKS
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00 ŝ SAMPLE CONDITION ICE GRAPHIC LOG GROUP SYMBOI CONDITION LABORATORY TEST DATA CORE RUN & % RECOVERY NRC ICE TYPE VISUAL ICE % 0 & (FT.) SAMPLE TYPE & DEPTH (FL) GRAPHIC ▲ Dry density (pcf) ⊙ Water content % OTHER REMARKS DESCRIPTION Plastic limit 🕒 - Liquid limit DEPTH TEST DATA CORE 100 120 140 📥 60 60 SOIL SOIL 20 40 60 80 100 () 8.2 SAND - medium, silty, rust brown and grey UF 8 SM W.L B3 SAND, medium grain, poorly graded SP 1 - 4 cont'd 9 9 9.2 °.° B GRAVEL - some sand, medium, oversize B4 ° ° ° platy 9'' x 1岁'' 10 00 Discontinued at approximately 4' above stream level Stream bed, cobbies & platy gravei TEST HOLE TEST HOLE No. PROJECT : 130 11 LOGGED BY: FACILITY R.H. Z 1975 BORROW INVESTIGATION ELEVATION : LAT. & LONG 68⁰18'19''W, 133⁰01'03''W CHKD : R.H. PIPE MILEAGE NORTHERN ENGINEERING SERVICES AIRPHOTO No. : N75-107B-B11-1 DRWN. BY: A 12861-277 D.J.M. AHTO COMPANY LIMITED c AIR TEMP : Approx. 27°C CALGARY ALBERTA RIG : CHKD: D. O. ENGINEERS FOR c METHOD : TEST PIT SHEET 2 OF 2 œ CANADIAN ARCTIC GAS STUDY LIMITED FINISH : D 15 M 08 Y 75 TIME: 13:50 12:15 D 15 M 08 Y 75 TIME: START: PC-9,5K373

TEST HOLE LOG

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DEPOSIT 107B-B12

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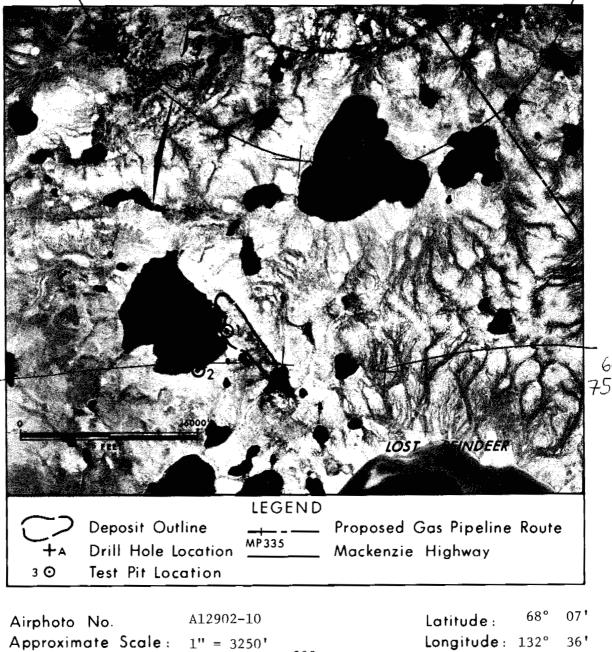
Physical Setting: Deposit 107B-B12 is a kame located 1 mile northwest of Lost Reindeer Lake and 2 miles southwest of the right of way at milepost 111.

Material: GRAVEL - well graded, and fine to medium sand.

Volume : 500,000 cubic yards.

Deposit 107B-B12 is a source of good quality granular Assessment: material suitable for general fill, backfill, building pads and possible concrete aggregate. 601000 E 7561000 N

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600000E 7559000NL

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DEPOSIT 107B-B12

PHYSICAL SETTING

This deposit is a kame located 1 mile northwest of the western Lost Reindeer Lake and 2 miles southwest of milepost 111 on the proposed pipeline right of way.

The complex consists of a low ridge with gentle to moderate slopes. A slump, that has developed on the edge which borders a small lake, suggests this deposit is ice cored. The depth of overburden was not determined but probably ranges between 1 to 3 feet over most of the deposit. Drainage is moderately good to imperfect.

The terrain between the pipeline right of way and the deposit is gently undulating to rolling, poorly drained moraine with peat in swales and depressions.

BIOLOGICAL SETTING

The vegetation at this site consists of scattered black spruce with an understory of willow, alder and bog birch and a ground cover of lichen and moss. The area provides good reindeer and caribou habitat but is only moderately productive habitat for lynx, fox, marten and wolf. Grizzly and black bear occur infrequently in the area. The western Lost Reindeer Lake is used by a wide range of waterfowl during the open-water season. Arctic terns were observed nesting on the lake during the 1975 survey. Ptarmigan and passerines are common in the area. Lost Reindeer Lake is inhabited year-round by pike, burbot, and grayling.

MATERIAL

The 2 test pits on this site show the material to consist of well graded gravel and fine to medium sand. Near surface gravel is silty and at

depth it is composed of soft, incompetent rock fragments. Further drilling is required to determine a more accurate estimate of quality and thickness of the deposit.

VOLUME

Total estimated volume based on an area of 60 acres and a 6 foot depth is 500,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 107B-B12 is a source of good quality granular materials. Areas to be exploited will be dictated by overburden thickness, insitu material quality and material requirements in the area. Further drilling and test pitting are required to determine overburden thickness, to define the quantity and quality of material within this deposit and delineate any massive ice that may be present before development commences. Initial indications are that the granular material from this deposit could be used for general fill, backfill in pipeline construction, building pads and concrete aggregate production with some processing.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Equipment could be staged to the deposit along the pipeline right of way and then to the deposit across 2 miles of gently undulating to rolling poorly drained moraine. When crossing this terrain care should be taken not to initiate thermokarst subsidence or disturb drainage. In order to prevent environmental damage snow roads would be built to transport the borrow material from the deposit to haul points on the right of way. Tree cover would have to be removed from access roads and excavation areas and harvested in accordance with current land use regulations. The peat cover and overburden then would be stripped from the area to be excavated and stockpiled around the edge of the site.

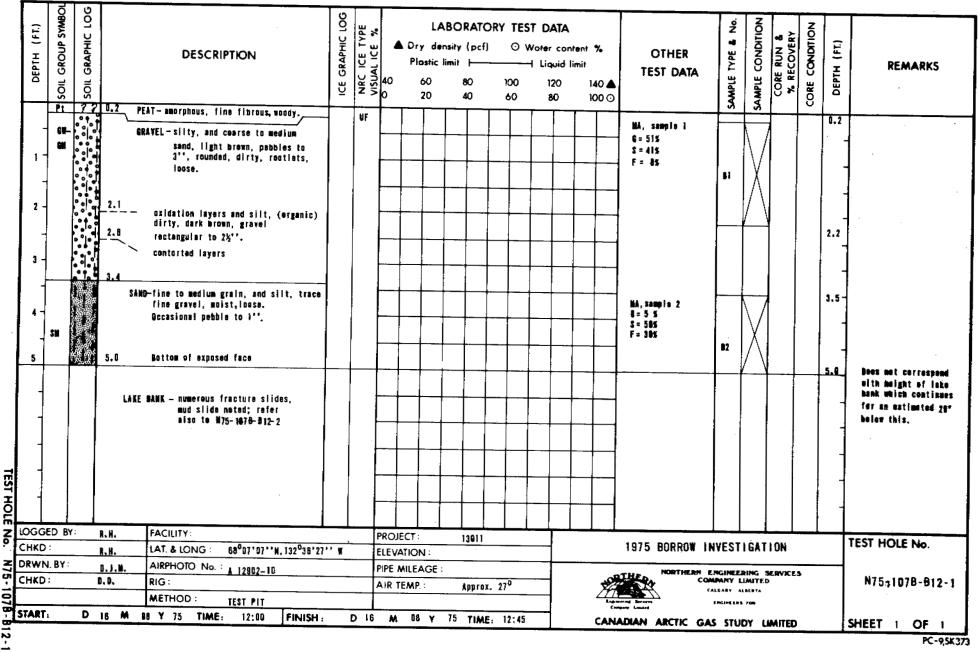
Development of this deposit would involve excavating borrow material evenly from the higher, well drained areas so that good drainage would be maintained over the area.

This type of development could be accomplished by using blasting or conventional earthmoving techniques depending on the degree of ice cementation. The excavated material may have to be stockpiled, thawed, and drained before it is used.

Equipment required for development would be dozers, rippers, end-dump trucks and front-end loaders as well as screening, crushing and concrete plants if required.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.





LOG Ŝ SAMPLE CONDITION **GROUP SYMBOL** ICE GRAPHIC LOG CONDITION CORE RUN & % RECOVERY LABORATORY TEST DATA TYPE E % (FT.) SAMPLE TYPE & DEPTH (FT.) GRAPHIC OTHER NRC ICE 1 VISUAL ICE 0 5 REMARKS DESCRIPTION DEPTH ----- Liquid limit Plastic limit +-TEST DATA CORE 80 100 120 140 📥 60 SOIL SOIL 20 40 60 80 100 🖸 Top of bank Approximately å 5*__ Bulk samples at 5', 10' GRAVEL - fine to coarse, and sand, ູ່ໃ 5 -5 6W-Md, combined 81 oxidized. \$ 23'. GM Samples 1 - 3 6 50% S 415 • u .___ as above 84 10 soft racky 10 F 82 may abrade easily. 15 15 29 20 23 * approximately 5' from lake water distances estimated from 23 83 l evel top of hank. BRAVEL -soft" rock , black 25 28 * Bottom of excevation • NOTE: not measured accurately due to insufficient time and difficult terrain. Possible better source of gravel (quantity) than \$75-1078-012-1 TEST HOLE TEST HOLE No. PROJECT FACILITY LOGGED BY: 13011 z R.H. 1975 BORROW INVESTIGATION ELEVATION : CHKD : LAT, & LONG : 86⁰07'04"'N, 132⁰38'38'' W R. H. NORTHERN ENGINEERING SERVICES PIPE MILEAGE : AIRPHOTO No. : N75 -DRWN. BY: A. N. A 12902-10 N75-107B-B12-2 COMPANY LIMITED AIR TEMP : Approx. 30⁰C CALGARY ALMARTA CHKD: 0.0. RIG : -----107B-1 METHOD : TEST PLT SHEET 1 OF 1 CANADIAN ARCTIC GAS STUDY LIMITED FINISH : D 16 M 08 Y 75 TIME: 08 Y 75' TIME: --START: D 18 M

TEST HOLE LOG

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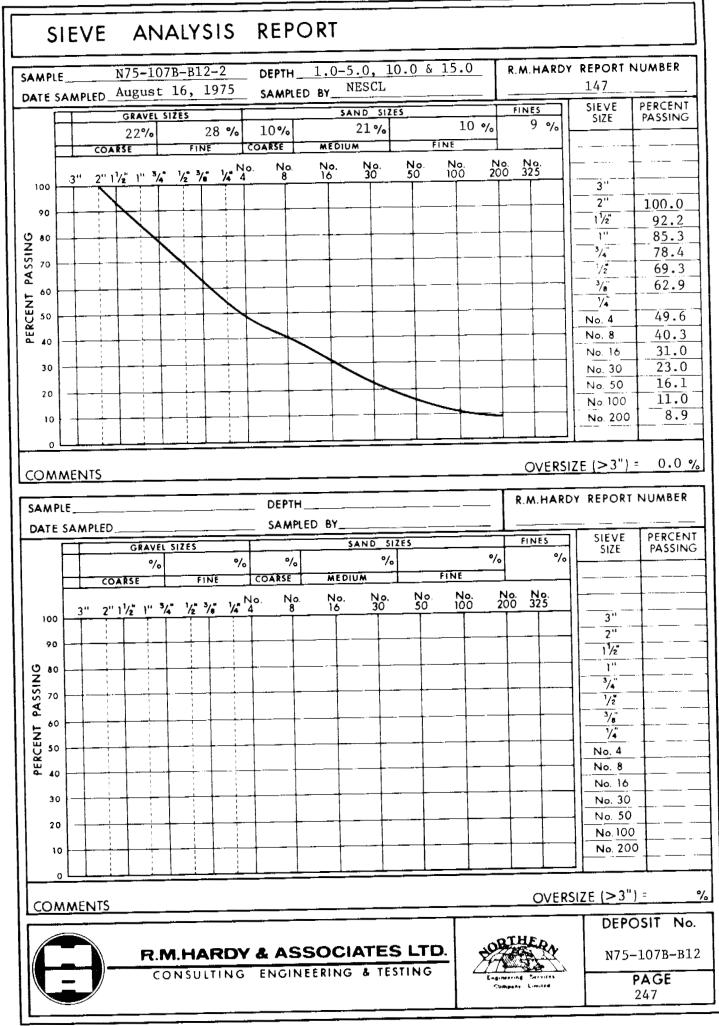
PC-9,5K373

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DEPOSIT 107B-B13

Physical Setting: Deposit 107B-B13 is a kame and kettle complex bordering the northwestern corner of Lost Reindeer Lake and is about 3 miles from milepost 112 on the right of way.

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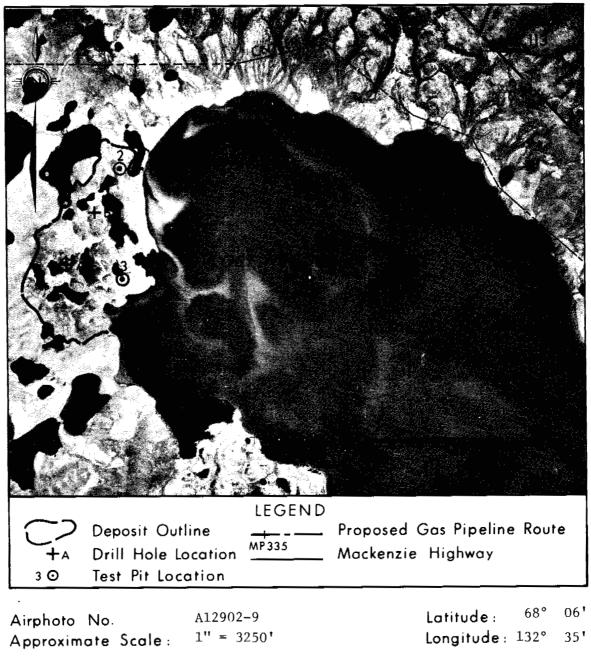
*see site # 1153-1

Moterial: GRAVEL - well graded, and sand.

Volume: 4,600,000 cubic yards.

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Assessment: Deposit 107B-B13 is a source of good quality granular material suitable for general fill, backfill and building pads; although it is not considered suitable for concrete aggregate.



DEPOSIT 107B-B13

PHYSICAL SETTING

This deposit is a kame and kettle complex bordering the northwestern corner of the most western Lost Reindeer Lake. It is approximately 3 miles southwest of milepost 112 on the proposed pipeline right of way. This deposit corresponds to source number 1153a in the EBA DIAND Granular Materials Inventory (1974) report.

The kame and kettle complex consists of hills rising up to 100 feet above intervening depressions. Maximum slopes are about 20 degrees. Peat and silt on hills and ridges varies from 0 to 1 foot in thickness, however in the depressions they may be more than 10 feet thick.

The deposit is well drained except for marshy depressions, and small lakes scattered throughout the area. In August the active layer ranges from 2 to 6 feet. Below this active layer the deposit is frozen with low to moderate ice content.

Terrain between the deposit and the pipeline route is a flat to rolling moraine plain with occasional patches of peat. Drainage is moderate to imperfect and there is a possibility that massive ice is present in the rolling moraine.

BIOLOGICAL SETTING

Better drained portion of the site support black spruce up to 30 feet in height. The understory consists of willow, alder, and bog birch, with a ground cover of lichen and moss. Depressions have a thick moss cover and scattered stunted black spruce. The site provides marginal moose habitat but potentially good reindeer and caribou habitat. Reindeer and caribou populations in the area are low. Habitat is low to moderately productive for fox, lynx, marten, and wolf. Grizzly and black bear occur infrequently in the area. Arctic terns were observed nesting on the western Lost Reindeer Lake. The degree of waterfowl utilization of this and nearby small lakes is not fully known. Lost Reindeer Lake is inhabited year-round by pike, burbot and grayling.

MATERIAL

Drill hole and test pit logs indicate the material at this deposit is well graded gravel and sand. Silt content varies throughout. Drill hole 107B-B13-A encountered a washed till with boulders 10 to 12 inches in diameter.

VOLUME

Only the hills and ridges on the area outlined on the airphoto are considered in the volume calculation. Total estimated volume based on 160 acres and a maximum depth of 40 feet is 4,600,000 cubic yards. Approximately 50 percent of the material can be assumed to be gravel.

DEVELOPMENT AND REHABILITATION

Deposit 107B-B13 is a source of good quality granular material, but is not considered suitable for concrete aggregate. Areas to be exploited will be dictated by material requirements, insitu material quality, and overburden thicknesses. Granular material from this deposit may be used for general fill, backfill in pipeline construction and building pads. Extensive drilling and test pitting would be required to delineate the boundaries of the better quality granular material prior to development.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socio-economic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year. Access could be gained from the pipeline right of way to the deposit by crossing the ice on Lost Reindeer Lake in the winter. This would make a haul distance of 4 miles from the deposit to the pipeline right of way.

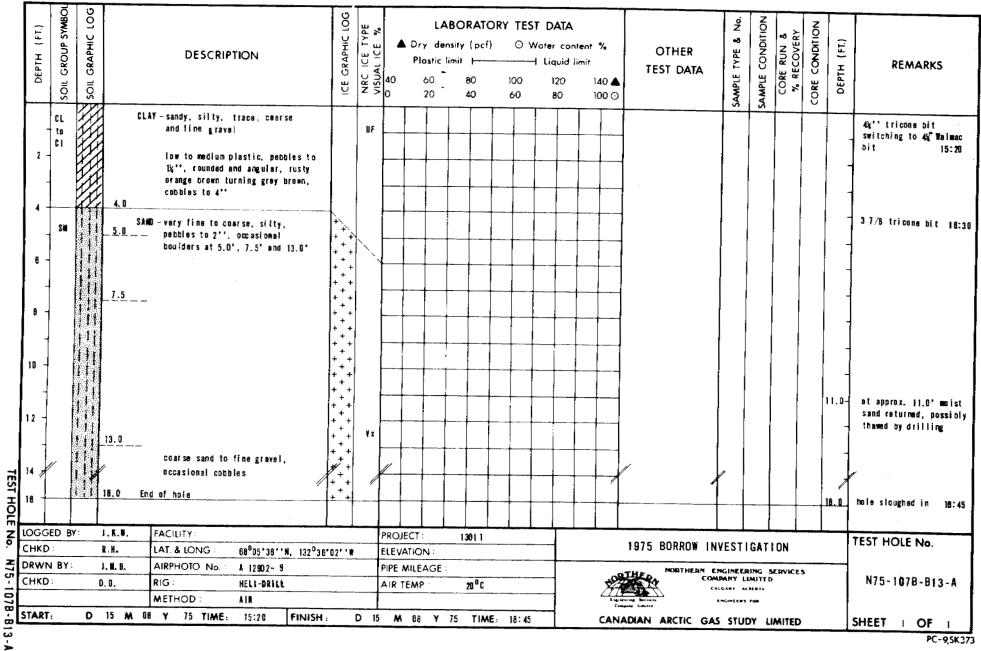
Vegetative cover would be removed from pit areas in accordance with land use regulations. The peat cover and overburden would then be stripped from the area to be excavated and stockpiled around the perimeter of the site.

Development of this deposit would involve mining the borrow material in stages from the steep side slopes of the kames. A buffer zone should be established to avoid siltation of Lost Reindeer Lake and protect the shoreline environment from thermokarst subsidence. Some gentle to moderate slopes of the deposit will probably be developed by excavating material evenly so that good drainage is maintained. Sufficient cover would be left on massive ice layers to prevent thermal degradation. Either type of development could be accomplished by using blasting or conventional earthmoving techniques depending on the degree of ice cementation. The excavated material may have to be stockpiled, thawed, and drained before it is used. Natural mixing during excavation will be adequate to obtain good gradations.

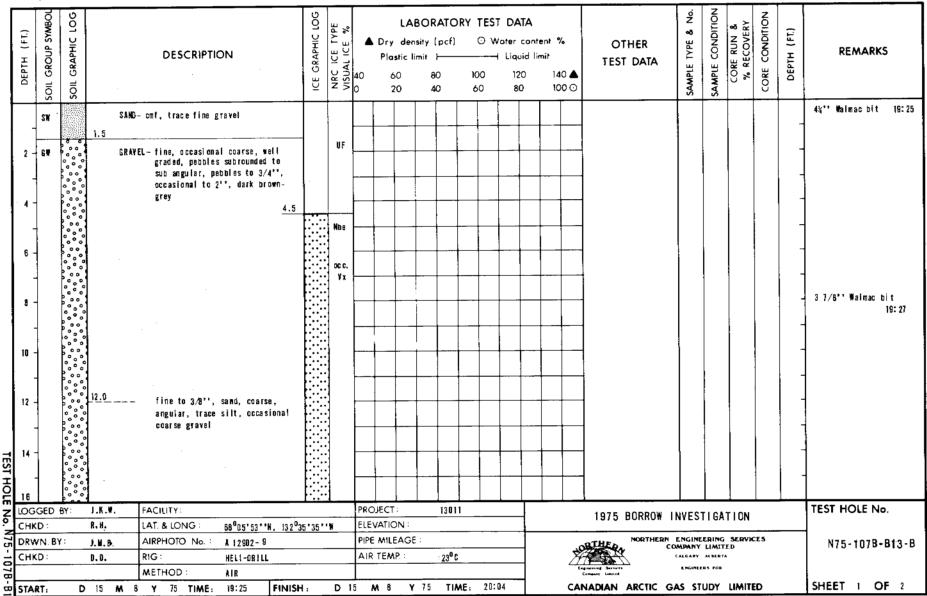
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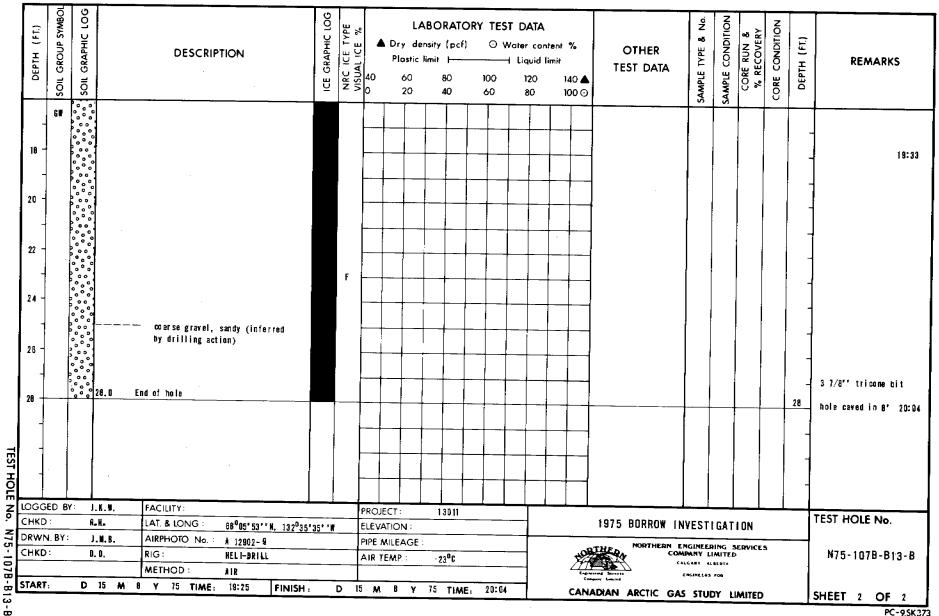
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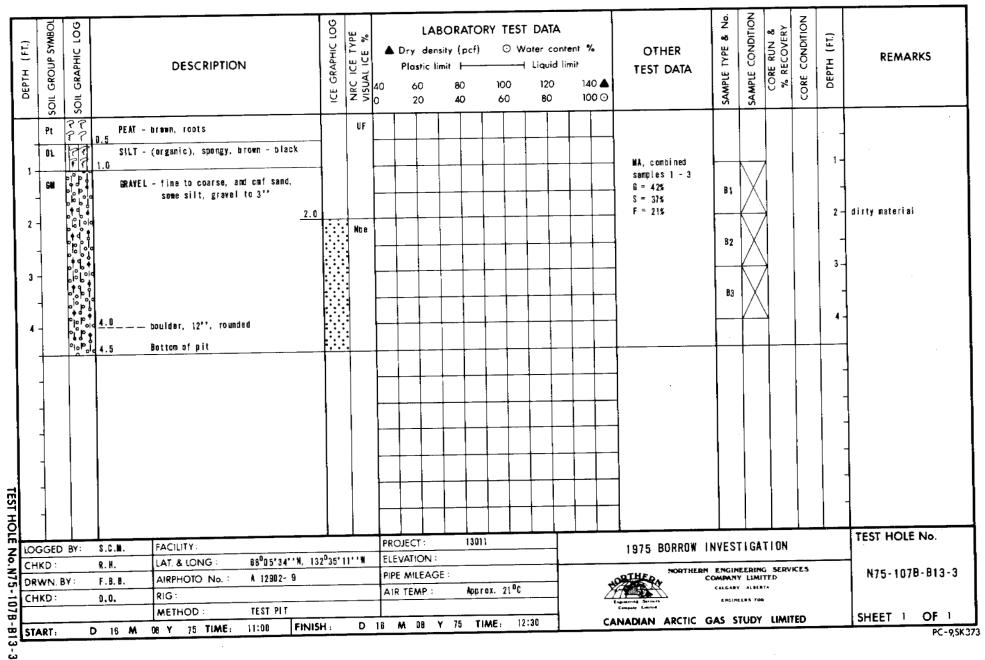


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o L									13.5
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								1"	83.2
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		HARDY &				HOBTH	Ear)7B-B13
	//			•		Engineering Company L	tervices. .imited	PA 26	

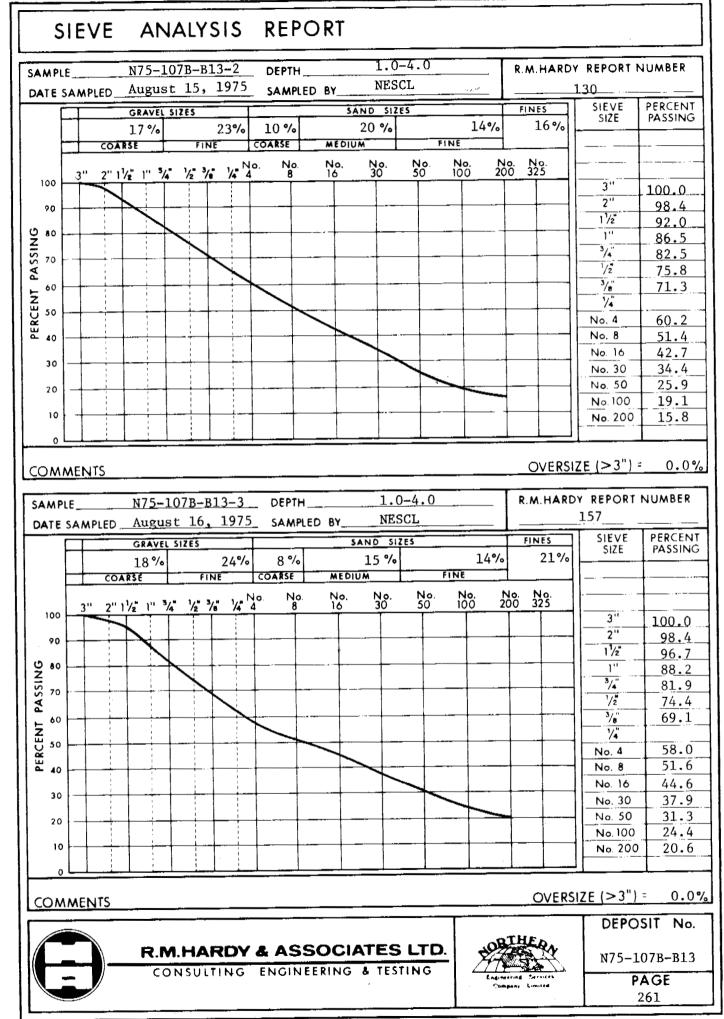
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SUMMARY OF LABORATORY TEST DATA FOR SUITABILITY OF AGGREGATES IN CONCRETE SAMPLE No.N75-107B-B13-3DATE SAMPLED : August 16, 1975 SAMPLED BY : NESCL DEPTH (FT.): 1-4DATE TESTED : January, 1976 TESTED BY : RMHA SOUNDNESS OF AGGREGATE ORGANIC IMPURITIES SULPHATE TEST TEST COARSE AGGREGATE : LOSS = 28.97 **%** NUMBER : 2 FINE AGGREGATE : LOSS = 24.33 % COAL REMOVED : Nil COAL & ROOTLETS LOS ANGELES ABRASION TEST : Nil REMOVED COAL CONTENT : Nil PERCENT LOSS = 21.5 % SIGNIFICANCE : SUMMARY OF ROCK TYPES, COARSE AGGREGATE. (PETROGRAPHIC ANALYSIS) TOTAL ROCK TYPE CLASSIFICATIONS

ROCK TTPE		WEIGHTED COMPONENT %
Quartzite		10.3
Granite	Strong to very strong, Good	3.35
Chaut		0.2
Chert		
Flint	Potentially reactive, Fair	0.5
Ironstone		3.55
Sandstone		12.05
Siltstone	Medium strong, Friable, Fair	8.4
Limestone		3.45
Friable Clay	Deleterious	0.2
PN = 238 INTERPRETA	TION : Not suitable for use in concrete	42.0
COMMENTS : Not suitab	le	

Engineering Servers Conserve Limited

R.M.HARDY & ASSOCIATES LTD.

CONSULTING ENGINEERING & TESTING N75-1078-813

PAGE 262

DEPOSIT No.

BIH-A 605610 E 7549940N BIH-B 604210E 7550140N

UTM Zone 8 OUT OF STUDY AREA

DEPOSIT 107B-B14

Deposit 107B-B14 is a hummocky moraine and kame complex Physical Setting: located 2.5 miles south of Lost Reindeer Lake and 2.5 miles southwest of milepost 118 on the right of way.

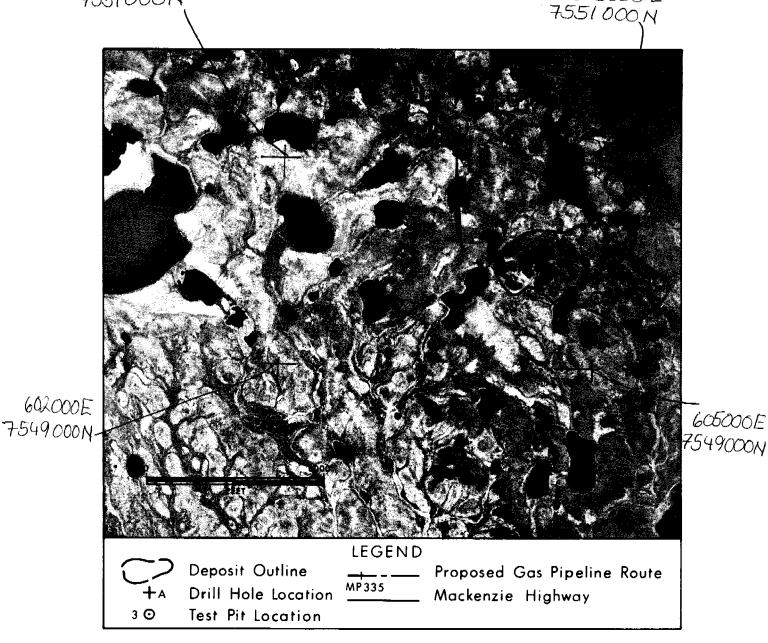
Material: TILL - primarily ablation till with some gravel and sand.

Volume :

7551000N

1,200,000 cubic yards.

Deposit 107B-B14 is a source of poor quality granular Assessment: material suitable only for marginal fill. It is therefore 602000E not recommended for development. 605000 E



Airphoto No. A12902-7 Approximate Scale: 1'' = 3250'

68° 03' Latitude : 31' Longitude : 132°

DEPOSIT 107B-B14

PHYSICAL SETTING

This deposit is a complex of hummocky moraine and kames located 2.5 miles south of the western Lost Reindeer Lake and 2.5 miles southwest of milepost 118 of the proposed pipeline right of way.

Relief over the deposit averages about 30 feet with gentle to moderate slopes. Locally steep sided hills stand 80 feet above bordering depressions. Overburden on most hills and slopes is negligible, whereas depressions may contain up to 10 feet of peat and icy organic silt. Drainage on most hills and south-facing slopes is good, on gentler north-facing slopes it is moderate to imperfect and in depressions poor. The active layer is normally less than 3 feet. Below the active layer the deposit is frozen with moderate ice contents.

Surrounding terrain consists of flat to gently rolling moraine with numerous boggy areas along poorly defined drainageways. High ground ice contents can be expected in the moraine.

BIOLOGICAL SETTING

Vegetation on hilltops and south-facing slopes at this site consist of white spruce up to 40 feet in height and a thick understory of willow, soapberry, rose, juniper, moss and grasses. North-facing slopes and low land are characterized by shrubs and black spruce. The area provides marginal moose and caribou habitat. Habitat is low to moderately productive for lynx, fox, marten, wolf, snowshoe hare, grizzly, and black bear. Little suitable habitat is available for beaver or muskrat. Owl pellets were found at the site. Ponds and lakes in the area do not appear to support fish populations.

MATERIAL

The material in this deposit is primarily a bouldery ablation till with some gravel and sand. Further drilling and test pitting are required to outline areas of adequate quality and volume.

VOLUME

The geomorphology of the deposit indicates maximum possible depths of 40 feet of granular material under some hills. Investigations to date reveal that no more than one quarter of the deposit may be fair to good quality granular material. Total estimated volume of granular material based on an area of 240 acres and 40 foot depth is 1,200,000 cubic yards.

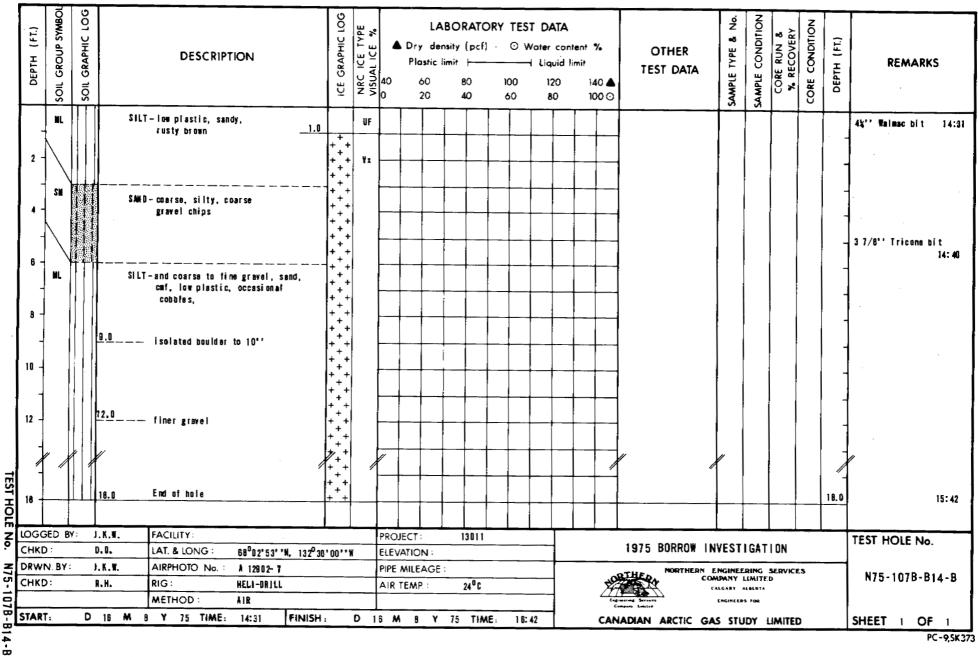
DEVELOPMENT AND REHABILITATION

Deposit 107B-B14 is a source of poor quality granular material and would be suitable only as marginal fill. Development of the deposit is not recommended unless extreme shortages of borrow exist in this area and extensive drilling and test pitting would be necessary to delineate the areas of better quality material before this deposit is developed.

Ŝ SAMPLE CONDITION GROUP SYMBOL GRAPHIC LOG ICE GRAPHIC LOG CONDITION LABORATORY TEST DATA CORE RUN & % RECOVERY түрЕ Е % (FT.) SAMPLE TYPE & DEPTH (FT.) O Woter content % ▲ Dry density (pcf) OTHER NRC ICE VISUAL ICE O D REMARKS DESCRIPTION Liquid limit DEPTH Plastic limit |-TEST DATA CORE 140 📥 60 80 100 120 SOIL SOIL 20 40 60 80 100 🖸 4%'' Walmac bit 11:50 ÜF SILT - and fine gravel, little NL. 1.0 coarse gravel, sand, fine to medium, trace clay, low to non plastic, occasional 2 . small cobbles, sedimentary and metamorphic 3 7/8" Walmac bit 11:57 4 6 8 Nb to ¥x 18 -— boulder 12'' - 14'' **+**: 3 7/8'' tricone bit нŰ 20 TEST HOLE 12:15 ۰, 41 13:25 22 22.0 22 End of hole 41 TEST HOLE No. PROJECT : 130 11 LOGGED BY FACILITY <mark>ک</mark> J.K.W. 1975 BORROW INVESTIGATION ELEVATION 68°D 2'48' 'N, 132°31'49''W LAT. & LONG CHKD D.O. N75-NORTHERN ENGINEERING SERVICES PIPE MILEAGE AIRPHOTO No. A 12902-0 N75-107B-B14-A DRWN. BY: 1.K.W. COMPANY LIMITED AIR TEMP. 21⁰C CALGARY ALBERTA HELI-DRILL RIG CHKD: D. 0. -----078 METHOD : A I R SHEET 1 OF CANADIAN ARCTIC GAS STUDY LIMITED - 1 D 16 M 8 Y 75 TIME: 13:25 FINISH : D 16 M 8 Y 75 TIME: 11:50 START: PC-9,5K373

TEST HOLE LOG

- B14-A



- 268 -

LOG ŝ SAMPLE CONDITION **GROUP SYMBOI** ICE GRAPHIC LOG CONDITION NRC ICE TYPE VISUAL ICE % LABORATORY TEST DATA CORE RUN & % RECOVERY (FT.) -8 (FT) GRAPHIC ▲ Dry density (pcf) O Water content % OTHER SAMPLE TYPE DESCRIPTION DEPTH REMARKS DEPTH Plastic limit + - Liquid limit TEST DATA CORE 60 80 100 120 140 🛦 SOIL SOIL 20 40 60 80 100 🖸 11 15:40 Ρt PEAT - amorphous, fine fibrous, woody ŬF No samples taken inclusions 11 11 0.5 0.5-+ ٧x 40 CLAY - trace gravel, medium plastic, C) pebbles to ¾", clear ice to 2" + pockets 18:00 1.0 -+ — 1.2', little gravel, rectangular to + 3'' + ¹−1.4', boulder rounded to 11" 1.5 1.8 1.5 GH Difficult to excavate Noe 1.8 GRAVEL - very silty, some fine sand, peobles to 1", subangular and platy, black, till ?, wellbonded by ice Bottom of pit TEST HOLE No. TEST HOLE No. FACILITY PROJECT : 13011 LOGGED BY: R.H. 1975 BORROW INVESTIGATION 68°02'46''N, 132°31'49''W LAT. & LONG ELEVATION : CHKD R.H. N75-A 12902-7 NORTHERN ENGINEERING SERVICES PIPE MILEAGE : AIRPHOTO No. : DRWN, BY: A.J.B. oTHE N75-107B-B14-1 COMPANY LIMITED Approx. 29⁰C AIR TEMP. D.O. RIG : CALGARY ALBERTA CHKD: ENGINEERS FOR 078-B TEST PIT METHOD : SHEET 1 OF FINISH : D 16 M 08 Y 75 TIME: 18:40 CANADIAN ARCTIC GAS STUDY LIMITED - 1 D 18 M 08 Y 75 TIME: 15:40 START: PC-9,5K373

TEST HOLE LOG

4

DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Dry	density ic limit	/ (pcf	DRY TE:	Woter (conten id limit D		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
1	Pt CP	10.00	9.4 634¥ 1.3-7 L.bes	- coarse fibrous, roots EL - fittle coarse sand, angular peobles to B'' x 1'', companyation on gravel, graylsh white fider, rounded, 15''		UF									WA, 1.5' to 2.5'					· - 1-	Sample is a mixture of
2			SMO	- modium grain, silty, brown Dottom of pit											B = 35% S = 43% F = 22%	81	X			2.5 3.0	teo strata
	-																	- - - - -			
																				1	
TES																				-	
	GED	BY: R.	N.	FACILITY			PRO	JECT :		130 1 1										_	TEST HOLE No.
z	D : N. BY	R. 1: F.	H. F. B. O.	LAT. & LONG : 80 ⁰ 02' 37"" 1, 132 ⁰ 31 AIRPHOTO No. : A 12902-7 RIG : METHOD : TEST PIT	'05' 'I		ELEV PIPE	MILEA	GE :		x. 27 ⁰ C			Ž			LIMITE	SERVICE	23		N75-107B-B14-2
STAI	IT:	Ð	18 M E	a Y 75 TIME: 15:30 FINISH	:	D 18	, N	08	¥ 15	i TI	ME: 17:	00		CAN	ADIAN ARCTIC GA	s sru	JDY	Limitei	0		SHEET 1 OF 1 PC-9,5K37

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- 270 -

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SAMPLE CONDITION SOIL GROUP SYMBOL GRAPHIC LOG SAMPLE TYPE & No. CORE CONDITION ICE GRAPHIC LOG CORE RUN & % RECOVERY NRC ICE TYPE VISUAL ICE % 0 & LABORATORY TEST DATA DEPTH (FI.) DEPTH (FT.) ▲ Dry density (pcf) O Water content % OTHER REMARKS DESCRIPTION Plastic limit ⊢ ----- Liquid limit TEST DATA 140 🔺 60 80 100 120 SOIL 60 80 100 🔾 20 40 14:45 7 7 0.2 UF Pt. PEAT - anorphous, fine fibrous, woody, CL inclusions, black No samples taken CLAY, - silty, little fine sand, low to medium plastic, rust brown and 1mottled grey <u>1.5</u> – peaty layers, black to dark brown <u>.u</u>.... soft, saturat≉d 2 -2.5 15:00 Bottom of pit 2.5 I CE poorly drained ۱CE م + at depth 2.5' **TEST HOLE** TEST HOLE No. PROJECT FACILITY 13011 LOGGED BY R. H. 1975 BORROW INVESTIGATION ō ELEVATION 66°02'44''N, 132°30'23''W LAT. & LONG CHKD R. H. NORTHERN ENGINEERING SERVICES COMPANY LIMITED N75 PIPE MILEAGE N75-107B-B14-3 DRWN. BY: A.N. AIRPHOTO No. 1 A 12902-0 CALGARY ALBERTA AIR TEMP.: Арр го х. <u>29⁰ С</u> RIG : CHKD: D. D. ENGINEERS FOR 107B METHOD : TEST PIT SHEET I OF CANADIAN ARCTIC GAS STUDY LIMITED M 08 Y 75 TIME: 15:00 FINISH : D 18 D 16 M 08 Y 75 TIME: 14:45 START: D

TEST HOLE LOG

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PC-9,5K373

	SI	EV	E	A	NA		1S	IS	R	REF	0	RT										
SAMP DATE											1		5-2.5 ESCL				-	R.M	HAR		REPORT 44	NUMBER
				38AVE 15% E			20 NE) %	COA	7 % RSE		S. MEDIL	13%	ES	FIN	23 E	%	FIN	es 22%		SIEVE SIZE	PERCENT
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DATE	- NA								c .								-					
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			OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%		%		SIEVE SIZE	PERCENT PASSING
100			OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%		%		SIZE	
			OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%		%		SIZE	
90			OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%		%		3" 2" 1½	
90			OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%		%		3'' 2'' 1'/2"	
90			OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%		%		3" 2" 1½	
PA55ING			OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%		%		SIZE 3'' 2'' 1'/2' 1'' 3'4' 1'2' 3'/8'	
PA55ING			OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%		%		SIZE 3'' 2'' 1'/2" 1'' 3/4" '/2" 3/6" '/4"	
PASSING			OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%		%		SIZE 3'' 2'' 1 ¹ /2' ³ /4' ¹ /2' ³ /4' ¹ /2' ³ /8'' ¹ /4' ¹ /	
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PERCENT PASSING			OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%		%		SIZE 3'' 2'' 1 ¹ /2' ³ /4' ¹ /2' ³ /4' ¹ /2' ³ /8'' ¹ /4' ¹ /	
PERCENT PASSING 0 0 0 0 0 0 0			OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%		%		SIZE 3'' 2'' 1'/2' 1'' 3'4' 1'2' 3'4' 1'2' 3'4' 1'2' 3'4' No. 4 No. 4 No. 8 No. 16 No. 30 No. 50 No. 100	
PERCENT PASSING 0 <			OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%		%		SIZE 3'' 2'' 1'/2' 1'/2' 3/4' '/2' 3/8' 7/4' No. 4 No. 8 No. 16 No. 30 No. 50	
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		3" 2	OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%	N 32	%		SIZE 3'' 2'' 1'/2' 1'' 3'4' 1'2' 3'4' 1'2' 3'4' 1'2' 3'4' No. 4 No. 4 No. 8 No. 16 No. 30 No. 50 No. 100	
DERCENT PASSING 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		3" 2	OARS	RAVE %	SIZ	ES	NE	%	COA	%		S.A	ND SIZ		FIN		%	N 32	%		SIZE 3'' 2'' 1 ¹ /2' 1'' 3'/4' '/2' 3'/6' '/4' No. 4 No. 8 No. 16 No. 30 No. 50 No. 100 No. 50 No. 100 No. 200 (> 3'') =	
0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		3" 2		RAVE %	4" 			°%	сол о.	%			ND SIZ		FIN		%	N 32	%		SIZE 3" 2" 1 ¹ /2" 1 ¹ /2" ³ /4" ¹ /2" ¹ /4" ¹ /2" ³ /4" ¹ /2" ¹ /2"	PASSING

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BI5-A 612810 E 7546540N BI5-B 611870E 7547400N

Project No. 13011 A Proj Name: 1975 Pipeline Borrow Investigations Canadian Arctic Gas Study Ltd. ß ζ. EBA 1146 Tech BRA-17 Ω Tech B04-12 e F G H) 5 ĸ ì, Μ Ν JKW 0 LPB ρD P Q R 32' 5 7 Ů ٧ 7546540N 612810 E ω 15:58 X 75 08 19 ĭ 75 08 17 16:27 Z

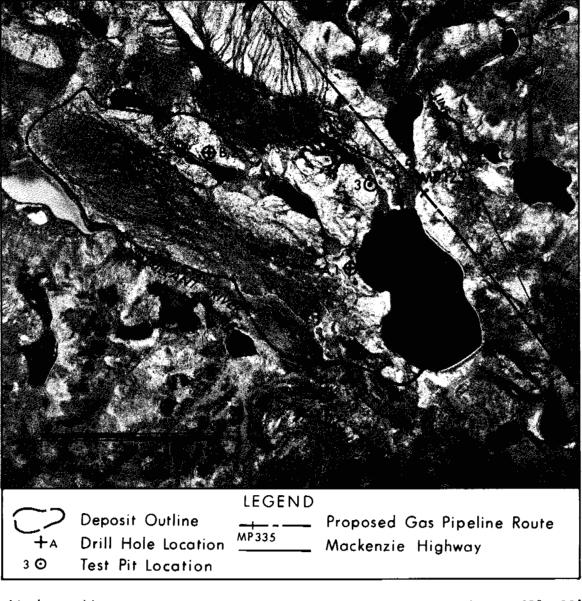
Physical Setting: Deposit 107B-B15 is an outwash plain located about 5.5 miles southeast of Lost Reindeer Lake and ½ mile west of the right of way at milepost 123.

+ see 1146-1

Moterial: GRAVEL - fine, and sand, variable silt content.

Volume: 22,400,000 cubic yards.

Assessment: The eastern part of deposit 107B-B15 is a source of good quality granular material whereas the remainder is fair to poor quality. The material is suitable for general fill, backfill, building pads and possible concrete aggregate.



Airphoto No. A12760-182 Approximate Scale: 1" = 3250' Latitude: 68° 00' Longitude: 132° 18'

DEPOSIT 107B-B15

PHYSICAL SETTING

This deposit is an outwash plain approximately 5.5 miles southeast of the eastern most Lost Reindeer Lake and $\frac{1}{2}$ mile west of the pipeline right of way. This deposit corresponds to source number 1146 in EBA DIAND Granular Materials Inventory Volume IV (1974) report.

The outwash plain has a very gentle southern slope with a few channels and lakes inset 10 to 20 feet below its surface. Overburden of peat and icy organic silt varies between 1 and 10 feet and is thinnest in the southern section. Drainage varies from moderately good to imperfect on the outwash plain itself and is poor in the inset channels. The active layer is generally less than 2.5 feet and the frozen material below has low to moderate amounts of ice. The outwash material is underlain by clay with massive ice. Terrain between the deposit and pipeline right of way consists of an imperfectly drained, gently sloping till plain.

BIOLOGICAL SETTING

Vegetation on this plain consists of black spruce with an understory of willow and labrador tea and a ground cover of lichen. The site is located in good reindeer and caribou winter range. Ungulate sign was observed in the area, including a well-worn trail along the lakeshore. The area is good potential marten habitat although no furbearers were seen. Grizzly and black bear are found occasionally throughout the area. The adjacent lake is utilized by waterfowl throughout the openwater season. Ptarmigan winter in the area and a wide range of passerines occurs. The lake and associated Travaillant River system support several fish species including humpback whitefish, ninespine stickleback, longnose suckers, Arctic grayling and pike.

MATERIAL

Drill holes, test pits and the DIAND report show this deposit consists of 15 to 20 feet of gravel and sand. Gravels are generally fine, silty, sandy and poorly graded. The fine to medium grain sized sand has variable amounts of silt and gravel. Massive ice was encountered at shallow depths (1 to 2 feet) in test pits 107B-B15-2 and 107B-B15-4.

VOLUME

A total estimated volume based on 1390 acres and 20 foot thickness over half the area is 22,400,000 cubic yards. This volume would be reduced to 7,000,000 cubic yards if development is restricted to areas of shallow overburden.

DEVELOPMENT AND REHABILITATION

Portions of deposit 107B-B15 are a source of good quality granular material, the remainder of the deposit being fair to poor quality material. The eastern portion of the deposit appears to be the best part to develop, as drill hole and test pit data indicates thick overburden and massive ice exist in the western portion. Material from this deposit would be suitable for general fill, backfill in pipeline construction, building pads, and possibly concrete aggregate.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

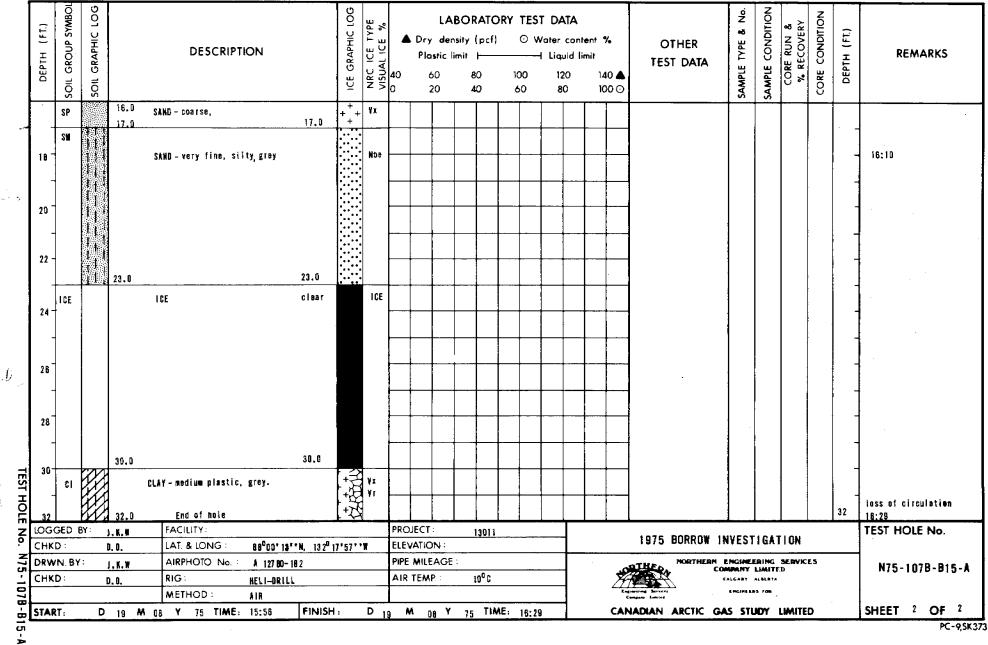
Access to the deposit would probably be achieved along the pipeline right of way. From the pipeline right of way to the deposit a 0.5 mile snow road over gentle to moderate slopes would probably be used. The vegetation would be removed and disposed of in accordance with land use regulations. The peat cover and overburden would then be stripped from the area to be excavated, and stockpiled around the perimeter of the site.

Development of this deposit would involve extensive drilling and test pitting to locate areas of better quality material with the least amount of overburden. Excavations would then proceed over these areas and involve removing borrow material evenly from the better quality areas. Proper drainage would have to be maintained and sufficient cover left over areas with massive ice. This type of development could be accomplished by using blasting or conventional earthmoving techniques depending on the degree of ice cementation. The excavated material may have to be stockpiled, thawed, and drained before it is used. Crushing and/or screening of the material may be required to produce quality construction aggregates.

Equipment required for development would be dozers, rippers, end-dump trucks, front-end loaders, as well as screening, crushing, and concrete plants if required.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

DEPTH (FT.)	GROUP SYMBO	GRAPHIC LOG		DESCRIPTION	GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	•		densit	y (pcf)	ORY TE	Water	conte		OTHER TEST DATA	TYPE & No.	SAMPLE CONDITION	CORE RUN &	CONDITION	DEPTH (FL)	REMARKS
	soll	soit G			ICE G	NRC	40 0	60 20		80 40	100 60	12 8	20 0	140 ▲ 100 ⊙	1	SAMPLE TYPE	SAMPLE		CORE	DEPT	•
-				EAT-weedy, fibreus, reats ILT-trace sand, lew plastic, light brown.		UF														· -	4k** Weiner bit 15:56
2-	-			AMD-medium coarse, silty, some fine <u>2.5</u> to medium gravel					+	-										-	• •
4						F									4						
-									_	_					-					-	•
•			0,5							-		·									
				EL- fine, silty, occasional coarso, posalos subrounded to sub angular to 2'', for platy pieces, for posalos to 1.5''.																	3 7/8** Wolmes bi 15:58
10															- -						
- 12-									_	-					•					-	
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CHK	GED D:	DY	J.K.¥ 9.0.	FACILITY: LAT. & LONG : 89°80 * 13*** II, 132 ⁰	17'57'	•••	PROJ ELEV/		:	13011	· · · · ·		· ·		1975 BORROW I	NVEST	I GA1	ION		` . 	TEST HOLE No.
· · · ·	- /N. 8Y	't. '	J. K. W	AIRPHOTO No. : # 12788-182			PIPE /	MILEA	GE :						THE NORTHERN				LS		NTE 1678 84
СНК	D:		1.8.	RIG: MELI-BRILL METHOD: AIR			AIR 1	EMP. :		18 ⁸ C		· · ·		Ž		CALGARY -	AL BERTA	.			N75-1079-81
STAR		D		E Y 75 TIME: FINISH	;	D	A M	18	¥ 1	5 TIN	IE 1		1	CA	NADIAN ARCTIC G	AS STU	JOY I	UMITE	D	· ·	SHEET I OF



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DEPTH (FT.)	SOIL GROUP SYMBO	SOIL GRAPHIC LOG		DESCRIP	[ION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %			BORATO sity (pcf) mit (0 \	T DATA Voter cor I Liquid 120 80	ntent % limit 14	• • ▲ : • •	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FI.)	REMARKS
	<u> </u>		0.2 PEAT	-fibrous, noody i	nclusions, <u>U.5</u>		UF									13	S				4%'' Walmac bit
-	ML			dark brown -trace fine sand,			٧r														14:38
2 -	1		3111	gravel, low plas			in Noe													.	
_				¥".																	
			4.0																	-	
4 -	OL	33	SILT -	(organic) black	lce															-	
-	1	33			rich		OCC. Yx						+ 1	-+						-	1
8 -	-	23							_			$\left \right $	+							-	
-																				_	
8 -		27																			3 7/8'' Walmac bit
Ű.	[2 9	9.0																	-	14:45
10	GP to GN		GRAYE		rse gravel, pebbles sub rounded to ½°°,		F											-			
12																				-	
-																				-	
14			8								<u> </u>		+							-	
-																					
16																					
	GED E			FACILITY				PROJE		1301 1					1975 BORROW IN	VEST	GAT	ION			TEST HOLE No.
) : N. BY		D. D.	LAT. & LONG : AIRPHOTO No. :	66 ⁰ 00*51**N, 132 ⁰ 19	*47**	R	ELEVAI PIPE M	ILEAGE	:			<u></u>		NORTHERN	ENGINEE	RING	SERVIC	ES		
СНК			R.H.	RIG:	HELI-DRILL			AIR TE		10 ⁰ C				XO		MPANY		D			N75-107B-B15-
				METHOD :	ALR									Lago	maring Sarupet	LMGINEER	5 708				
TAR	۲:	D	15 M 08	Y 75 TIME:	14:38 FINISH	:	D 1	M (08 Y	75 T1N	NE: 15:1	9		CAN	ADIAN ARCTIC GA	S STU	IDY	LIMITE	D		SHEET 1 OF

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ŝ SAMPLE CONDITION ICE GRAPHIC LOG CONDITION SOIL GROUP SYMBOI GRAPHIC LOG CORE RUN & % RECOVERY NRC ICE TYPE VISUAL ICE % O A LABORATORY TEST DATA SAMPLE TYPE & DEPTH (FT.) DEPTH (FI.) O Water content % ▲ Dry density (pcf) OTHER REMARKS DESCRIPTION Plastic limit + - Liquid limit TEST DATA CORE 140 🛦 100 120 **1**40 60 80 SOIL 80 100 🖸 20 40 60 GRAVEL - (cont'd) 6P olo to gets dirtier with depth GM 14:50 F 18 20 21.0 appears finer 22 24 tess of circulation 26.0 28 28 3 7/8"" Walmac bit CLAY-modium plastic, grey CL 15:00 Dz 28 End of hele 15:19 29.0 TEST HOLE TEST HOLE No. PROJECT : LOGGED BY: FACILITY 13011 3.K.W **N**0 1975 BORROW INVESTIGATION ELEVATION : LAT. & LONG 88⁰00'51"'N, 132⁰19*47"'W CHKD D. O. 07N NORTHERN ENGINEERING SERVICES PIPE MILEAGE : AIRPHOTO No. 1 A 12780-182 N75-1078-B15-B DRWN. BY: 1.8.8 COMPANY LIMITED AIR TEMP 1000 CALGARY ALBERTA RIG : HELS-ORALL CHKD R. H. 107B -----METHOD : A I R SHEET 2 OF 2 CANADIAN ARCTIC GAS STUDY LIMITED D 19 M 08 Y 75 TIME: 15:18 FINISH : D 19 M 08 Y 75 TIME: 14:39 START:

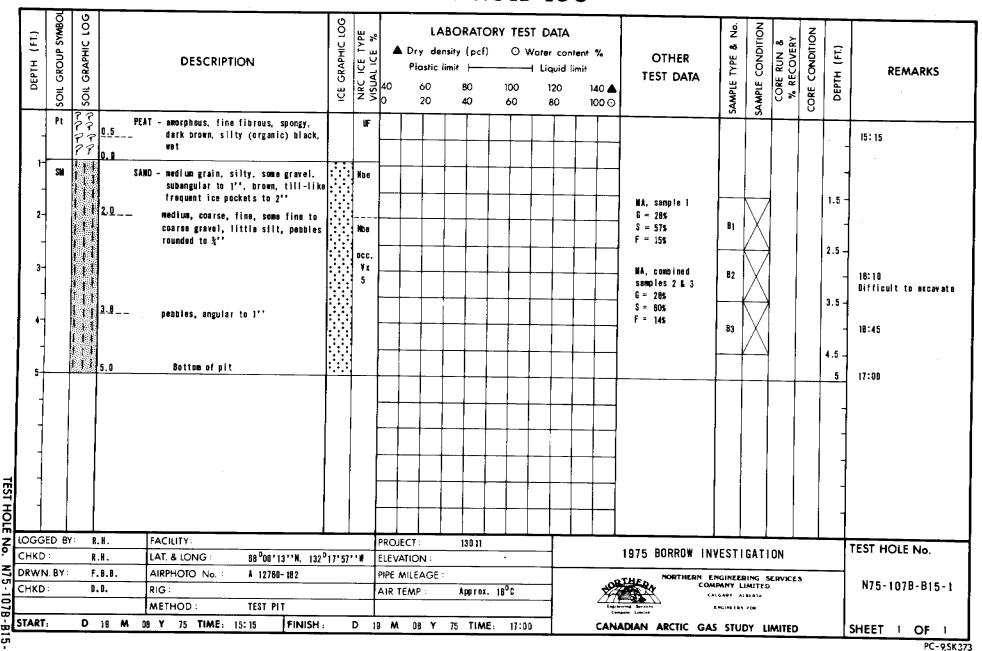
TEST HOLE LOG

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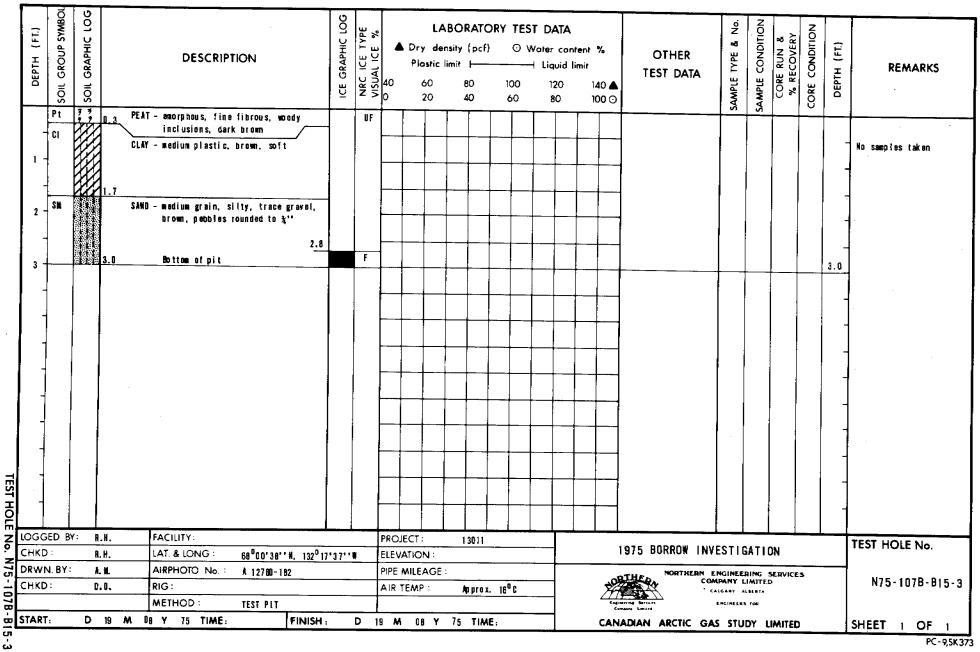
GROUP SYMBOI GRAPHIC LOG ICE GRAPHIC LOG SAMPLE CONDITION SAMPLE TYPE & No. CONDITION NRC ICE TYPE VISUAL ICE % LABORATORY TEST DATA CORE RUN & % RECOVERY (FT.) (FT.) ▲ Dry density (pcf) ○ Water content % OTHER DESCRIPTION DEPTH REMARKS DEPTH Plastic limit |----- Liauid limit TEST DATA CORE 60 80 100 120 140 📥 SOIL SOIL 20 40 60 80 100 🔿 17 Pt UF PEAT - amorphous, fine fibrous, spongy, 13:25 dark brown No samples taken 11 SM **B** SAND - medium grain, silty, wet 1 1 i 1.2 ICE with SILT (organic), nonplastic, black I CE I CE + + 0L 2 λī. 3.0 Bottom of pit ્રક્ 3.0 15:00 3~ TEST HOLE **Z** FACILITY PROJECT : 13011 LOGGED BY: R. H. TEST HOLE No. 1975 BORROW INVESTIGATION CHKD LAT. & LONG 68°00'51''N, 132°19'47''W ELEVATION : R. H. N75 DRWN, BY: A. H. AIRPHOTO No. : A 12760 - 182 PIPE MILEAGE : NORTHERN ENGINEERING SERVICES N75-107B-B15-2 COMPANY LIMITED - 1 0 7 B - B AIR TEMP. Approx. 16⁰C CHKD: **.**.. RIG : CALGARY ALBERTA ENGINEERS FOR METHOD : TEST PIT Longies 15:00 START: D 19 M 08 Y 75 TIME: 13:25 FINISH : D 19 M 08 Y 75 TIME: CANADIAN ARCTIC GAS STUDY LIMITED SHEET 1 **OF** 1 15-2

TEST HOLE LOG

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DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPT	ON	ICE GRAPHIC LOG	NRC ICE TYPE	VISUAL ICE %	▲ Dr Ph	y den	isity (pi	:f) 	⊙wa	DATA ater con Liquid I 120 80	imit 1.	% 40 ▲ 00 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
	Pt	77 77	PE) 0.5	NT - amorphous, fine f inclusions, black			UF	:															13:25
+ 1 - -	CL.			IN - trace fine sand, peaty layers, bla	brown, damp, soft,																	-	Neo samo,pies taken
2 -		\mathbb{Z}	2.1		2.	1				-		_										-	- 14:10
-	I CE + OL			i with SLLT (organic), black, trace orga clear ice about J	anic inclusions,		1 CE +	E							-							-	14:20
3 -						27 - 14 17 - 14 18 - 14	KEP		1														14:30
4 -			4 . D	Bettom of pit			573.5 (C)								-							4.0	14:40
-									_			-										-	Poorly drained
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-																							
-														1									
						-																	
	GED E	Y :		FACILITY		·		PI	ROJEC	 r:	1 30	11											TEST HOLE No.
нк			R.H.	LAT. & LONG :	68 ⁰ 01'19''N, 132	⁰ 20'32'	'W		LEVATIO								1975 BORROW IN	VEST	IGAT	ION			
	N. BY		A. N.	AIRPHOTO No.	A 12760-182			-	IPE MIL				- ⁰ - 0			<u>ک</u> ور		MPANY	LIMIT		E.S		N75-107B-815
нк):	<u>.</u>	0.0.	RIG : METHOD :	TEST PIT				IR TEN	NP :	V op	ro x. 1	5'6			Ž.		EALGARY ENGINEE					
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				121	S	RE	PO	RT							
	MPLED_									.5		R	M.HAR	NY REPORT 151	NUMBER
		5 %			•/。				ND SIZ 24 %		16		FINES	SIEVE SIZE	PERCENT PASSING
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۰L														No. 200	15.0
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90		3 %	F	INE	- (COARSE		MEDIU. No.	27 % M	No.	No.	%	14 %	SIEVE SIZE 3" 2" 1½ 1½ 1" 3/4	PERCEN PASSING 100.0 97.3
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90		3 %	F	INE	- (COARSE		MEDIU. No.	27 % M	No.	No.	%	14 %	SIEVE SIZE 3" 2" 1½ 1½ 1" 3/4" 1/2	PERCEN PASSINC 100.0 97.3 92.2 86.8 74.4
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90 80 70 60 50		3 %	F	INE	- (COARSE		MEDIU. No.	27 % M	No.	No.	%	14 %	SIEVE SIZE 3" 2" 1½ 1½ 1½ 3/4 1½ 3/6 1/2 3/6 1/2 3/6 No. 4 No. 8 No. 16	PERCEN PASSINC 100.0 97.3 92.2 86.8 74.4 57.3 41.9
90 80 70 60 50 40		3 %	F	INE	- (COARSE		MEDIU. No.	27 % M	No.	No.	%	14 %	SIEVE SIZE 3" 2" 1½ 1½ 1½ 3/4 1½ 3/4 1½ 1½ 3/6 2¼ No. 4 No. 8	PERCENT PASSINC 100.0 97.3 92.2 86.8 74.4 57.3 41.9 30.2
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90 80 70 60 50 40 30 20 10	3" 2" 1	3 %	F	INE	- (COARSE		MEDIU. No.	27 % M	No.	No.	%	14 %	SIEVE SIZE 3" 2" 1½ 1½ 1½ 3/4 ½ 3/6 1½ 3/6 1½ 1½ 3/6 1½ 1½ 3/6 1½ 1½ 2 3/6 1½ 1½ 2 3/6 1½ 2 1½ 2 1½ 2 1½ 2 1½ 2 1½ 2 1½ 2 1½	PERCENT PASSINC 100.0 97.3 92.2 86.8 74.4 57.3 41.9 30.2 21.5 16.3 13.6 .0.0
90 80 70 60 50 40 30 20 10 0	3" 2" 1	3 %	л. НА						27 % M		No.	%	14 %	SIEVE SIZE 3" 2" 1 ¹ /2" 1 ¹ /	PERCEN PASSINC 100.0 97.3 92.2 86.8 74.4 57.3 41.9 30.2 21.5 16.3 13.6 .0.0

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out of study area

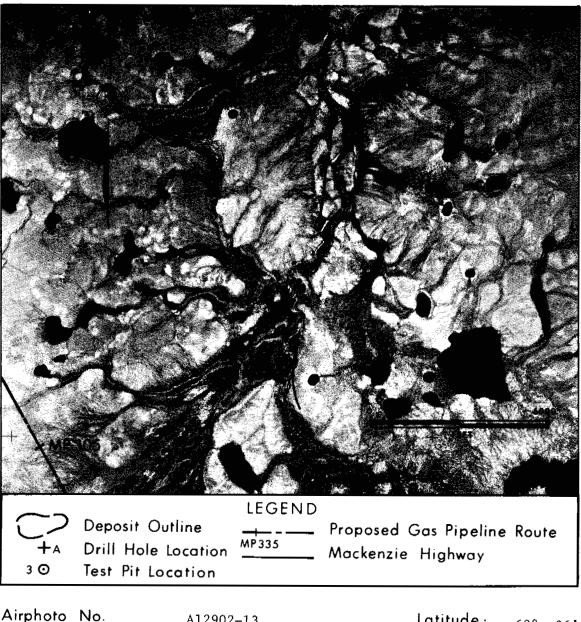
Physical Setting: Deposit 107B-B16(R) is a fluvial terrace located on the west side of Miner River and is approximately 2.5 miles east of milepost 104 of the proposed pipeline right of way.

Material: GRAVEL - silty, and rich in shale fragments.

Volume: 400,000 cubic yards.

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Assessment: Deposit 107B-B16(R) is not recommended for development because it consists of poor quality material.



Airphoto No. A12902-13 Approximate Scale: 1" = 3250* Latitude: 68° 36' Longitude: 132° 15'

DEPOSIT 107B-B16(R)

PHYSICAL SETTING

This deposit is a fluvial terrace on the west side of Miner River. It is approximately 2.5 miles east of milepost 104 on the proposed pipeline right of way.

The terrace slopes gently to the north except for a couple of minor swales which drain east to the Miner River. The site is moderately well drained, has moderate to high ice content, and overburden may be up to 10 feet thick.

Terrain between the pipeline and the deposit is rolling to hummocky moraine which is moderately well drained except in depressions.

BIOLOGICAL SETTING

This terrace is covered by dwarf birch, ericaceous shrubs, sedges, and lichens. Upland areas provide good quality reindeer and caribou habitat. Riparian areas provide moderately productive habitat for fox, wolf, bear and moose. There is little suitable habitat for muskrat and beaver. Swans were observed nesting along the Miner River. No other suitable waterfowl habitat is present at the site. The Miner River is used by grayling for spawning, rearing, and possibly over-wintering. Lakes and the headwaters of the Miner River support grayling, pike, and whitefish populations.

MATERIAL

Gravel exposed in the river bank is very silty and rich in shale fragments. This composition suggests overall poor quality gravel for construction purposes.

VOLUME

Deposit 107B-B16(R) covers an area of about 50 acres and has a total estimated volume of 400,000 cubic yards based on a thickness of 10 feet.

DEVELOPMENT AND REHABILITATION

Deposit 107B-B16(R) is a source of poor quality granular materials and the site is not recommended for development. Material is of poor quality and therefore of little use for construction materials. The possibility of thick overburden and moderate to high ice contents also make this deposit unfavourable for development. This deposit was only investigated on a field reconnaissance basis.

out of study area.

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DEPOSIT 107B-B17(R)

Physical Setting: Deposit 107B-B17(R) is part of an esker complex located 7.5 miles east of Campbell Lake and 2 miles west of milepost 94 of the proposed pipeline right of way.

Material: SAND - fine.

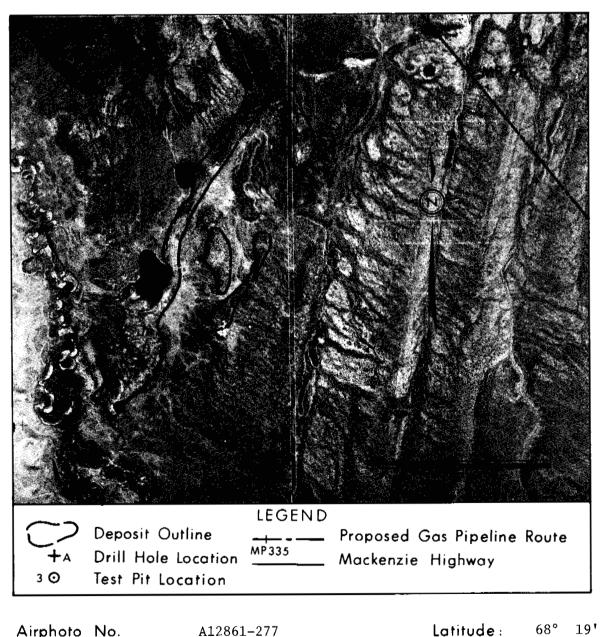
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Volume: 4,000,000 cubic yards.

Assessment: Deposit 107B-B17(R) is considered a source of poor quality granular material since is is composed of fine sand with a high ice content. It is therefore not recommended for development.



Approximate Scale: 1" = 3150' - 291 -Longitude: 133°

DEPOSIT 107B-B17(R)

PHYSICAL SETTING

This deposit is part of an esker complex located 7.5 miles east of Campbell Lake and 2 miles west of milepost 94 on the proposed pipeline right of way. Deposit 107B-B10 is also a part of this same complex. The Ripley, Klohn, Leonoff DIAND Granular Materials Inventory Zone IV-VI (1972) report identifies this source as number 450.

The crest of the esker complex is gently rolling and rises 30 to 100 feet above the surrounding terrain. Ridge crests are 200 feet or more across with steeply sloping sides. The site is moderately well drained and overburden is minimal, rarely exceeding 1 foot.

Terrain between the deposit and pipeline right of way is mainly imperfectly drained morainic plain with a thin cover of lacustrine sediments.

BIOLOGICAL SETTING

The majority of the esker complex is covered by mixed black spruce and birch up to 30 feet in height. Shrubs up to 4 feet in height are common in the understory with a ground cover of mosses and lichens. The area provides low productivity habitat for fox, wolf and snowshoe hare. The site lies within the winter range of the Mackenzie Reindeer Herd and also supports caribou. Streams, ponds, and lakes in the vicinity are used throughout the open-water season by a wide range of waterfowl and shore birds.

MATERIAL

The DIAND report indicates that this deposit is primarily fine sand with low to moderate ice content at the surface. Sands do contain a small amount of gravel, but in general this is poor quality material. Ice lenses are present at depth.

VOLUME

The total estimated volume, based on an area of 180 acres and an average depth of 30 feet, is 4,000,000 cubic yards over half the area. Only a portion of this volume may be readily accessible.

DEVELOPMENT AND REHABILITATION

Deposit 107B-B17(R) is a source of poor quality granular materials because it is primarily sand and has ice lenses immediately below the active layer. Therefore, it is not recommended for development because better material exists in deposits 107B-B10 and 107B-B11. This site could be developed for use as marginal fill if a shortage of granular material results in this area. This assessment is based only on a field reconnaissance of the deposit.

106N - BI-A 617100E 7540480N

X ref EBA 1141 Tech BD4-30

see site#1142

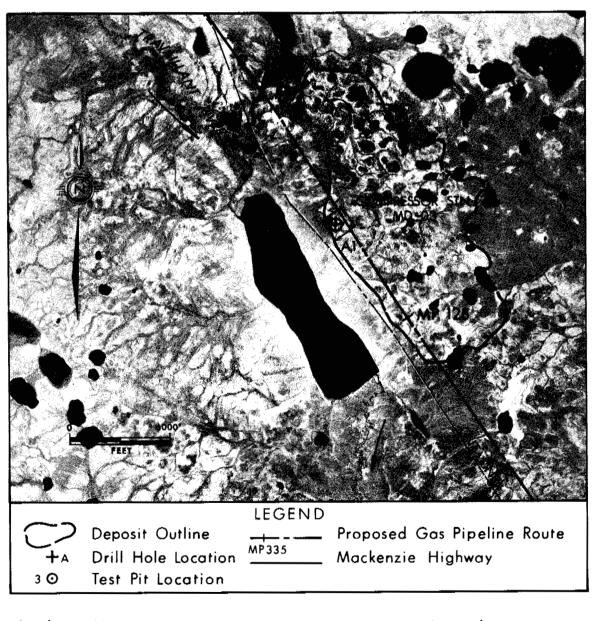
DEPOSIT 106N-B1

Physical Setting: Deposit 106N-B1 is a till covered area one half mile northeast of Fish Trap Lake at milepost 126 of the proposed gas pipeline right of way.

Material : TILL

Volume: No granular materials volume.

Assessment: Deposit 106N-B1 is not recommended for development either as a granular or a general fill borrow source because of poor material quality.



Airphoto No.A12583-30Latitude:67° 57'Approximate Scale:1" = 5700'Longitude:132° 12'

DEPOSIT 106N-B1

PHYSICAL SETTING

Deposit 106N-B1 is a till covered area one half mile northeast of Fish Trap Lake on or adjacent to the pipeline alignment near mile 126.

The slopes adjacent to Fish Trap Lake are moderately steep and lead up to a rolling morainic area. Drainage over the site is moderate, the overburden is thin, and ice content is high.

BIOLOGICAL SETTING

This site supports scattered black spruce with an understory of dwarf birch, willow and lichen. Moose use the area but the population is low. The area provides good marten habitat and marten sign was observed during the 1975 survey. Grizzly and black bear are occasionally present in the area. A limited number of waterfowl use Fish Trap Lake throughout the open-water season. There was no evidence of raptors in the area during the 1975 survey. Pike have been identified in Fish Trap Lake and it is likely that other species including humpback whitefish, grayling, burbot and lake trout, which are found in other lakes of the Travaillant Lake river system, are also present in the lake.

MATERIAL

Material in this deposit is till with a low pebble content.

VOLUME

There is no granular material available from this area. Unlimited poor quality fill would be available if this type of material was suitable for construction.

DEVELOPMENT AND REHABILITATION:

Deposit 106N-Bl consists of glacial till with high ice content and no granular material. It is not recommended for development either as a source of granular or general fill.

SAMPLE CONDITION SAMPLE TYPE & No. LOG CONDITION ICE GRAPHIC LOG **GROUP SYMBOI** CORE RUN & LABORATORY TEST DATA түрЕ Е % DEPTH (FT.) DEPTH (FT) O Water content % GRAPHIC ▲ Dry density (pcf) OTHER NRC ICE 1 VISUAL ICE 0 05 REMARKS DESCRIPTION - Liquid limit Plastic limit TEST DATA CORE 120 140 📥 80 100 60 SOIL SOIL 60 80 100 🖸 20 40 18:18 4%" insert bit UF CLAY-silty, occasional coarse sand, Ĉ I medium plastic, grey, soft Noe 2.0 000 2 -Wł ¥1 2.8 Ľ 4 5.8 WZ. -6 10:21 SILT-gravelly, pieces shale, low 1ce plastic 11.5 ¥s <u>j</u> t i ch **#**3 ? 12.5 12 13.0 13.0 1 CE 1CE ICE with silt inclusions . ' + + 14 H. F-15.0 ICE with clay inclusions ICE + 16 -C1 17.0 17.0 17.8 TEST HOLE No. CLAY-trace gravel (shale), medium to C1 -¥x + high plastic, saturated when 84 CH 10,5 18:55 18 + t haved 108 18.0 End of hole rich 19 19.0 TEST HOLE No. 13011 PROJECT FACILITY 1975 BORROW INVESTIGATION LOGGED BY: 1.8.8. ELEVATION : 87°57'30""N, 132°12"19""W LAT. & LONG D.D. CHKD : NORTHERN ENGINEERING SERVICES A 12583-30 PIPE MILEAGE : N75-106N-B1-A AIRPHOTO No. A.M. DRWN. BY : COMPANY LIMITED S AIR TEMP. 13⁰ C CALGARY ALBERTA 5-RIG : **KELI-DRILL** CHKD: 0.0. ENGINEERS FOR AIR 106N-B METHOD : OF 1 SHEET 1 CANADIAN ARCTIC GAS STUDY LIMITED D 19 M 88 Y 75 TIME: 18:55 18:19 FINISH : D 19 M 08 Y 75 TIME: START: PC-9,5K373

TEST HOLE LOG

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DEPTH (FT.)	SOIL GROUP SYMBOI	SOIL GRAPHIC LOG		DESCRIPTION		NRC ICE TYPE		A Dry d	ABORA ensity (p limit H 80 40	ocf)	0 v		ntent limit	% 40 ▲ 100 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FL)	REMARKS
	Pt	??	PE 0.5	AT - spongy, dark brown, woody inclusions		UF												1		<u> </u>	No samples taken
1-	CI		CL	AY - medium plastic, brown, trace gravel (≪5%)	1.0										1					-	
-						Nbe									1						•
2			2.5	Bottom of pit																2.5	
				Note: Granular material not encountered in adjacent drilinole			-	-												-	Poorly drained,flat
-																					
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ogge			. H.	FACILITY:	L		-	OJECT :	1	3011			<u> </u>	<u> </u>	1975 BORROW IN	1		<u> </u>			TEST HOLE No.
		_	L <u>H.</u> . N.	LAT. & LONG : 87 ⁰ 57'30'' N, AIRPHOTO No. : 1 12583-30	13201211	**₩	+	EVATION : PE MILEAG	F :						NORTHERN			_			-
HKD				RIG :			+	R TEMP.		pprox.	16 ⁰ C			zio E	co co	MPANY I	LIMITE.	D	- 3		N75-106N-B1
TART				METHOD: TEST PIT 08 Y 75 TIME: 18:30 FIN	NISH :		1	M 08 Y			19:3	_			IADIAN ARCTIC GA	ENGINEER				ľ	SHEET OF

106N-B2-A	623680E	7533740N
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See Site#1141

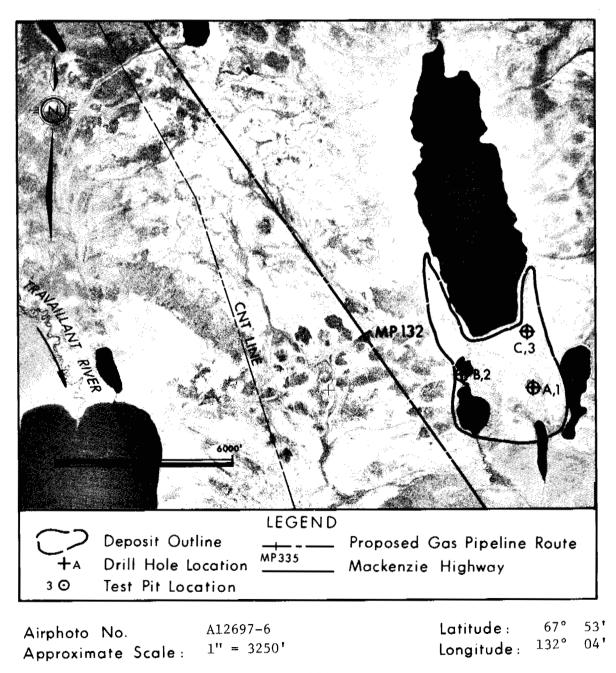
DEPOSIT 106N-B2

Physical Setting: Deposit 106N-B2 is a small outwash plain located 5 miles southeast of Fish Trap Lake and is close to the right of way.

Material: GRAVEL - well graded with some coarse sand.

Volume: 2,000,000 cubic yards.

Assessment: Deposit 106N-B2 is a source of fair to good quality granular material suitable for general fill, backfill and building pads. Access will involve crossing a small creek.



DEPOSIT 106N-B2

PHYSICAL SETTING

This deposit is a small outwash plain at the southern end of a small lake. It is about 5 miles southeast of Fish Trap Lake and the proposed pipeline right of way passes near the southwest corner of the deposit. This deposit corresponds to source number 1141 in the EBA DIAND Granular Materials Inventory Volume IV (1974) report.

The plain is about 3000 feet square with two narrow fingers extending part way along the sides of the lake. It has a gently undulating surface with local relief of 5 to 10 feet. A few small hills and scarps are moderately well drained, while the flatter areas and depressions are imperfectly to poorly drained. Overburden is generally less than 2 feet thick but may be thicker in low-lying areas. The depth of the active layer is about 1 foot in peat covered areas and more than 3 feet where cover is negligible. The deposit has a low ice content.

BIOLOGICAL SETTING

Vegetation on the small hills and slopes consists of black spruce up to 30 feet in height and ground cover of Labrador tea, cloudberry, blueberry and lichen. The poorly drained depressions and flat areas have a well developed peat layer covered with sedges and mosses. The site is located in good caribou habitat. An old beaver lodge was found in a small lake adjacent to the site. Evidence of trapping activity in the form of an old marten dead-fall trap was found. Grizzly and black bear are found occasionally throughout the area. The small ponds and lakes in the area provide suitable habitat for waterfowl. None of the adjacent water bodies appear to provide suitable fish habitat.

MATERIAL

Drill holes, test pits and the DIAND report show the outwash consists of well graded, rounded gravel from 2 to 10 feet thick. Some coarse sand,

a trace of silt and occasional cobbles and boulders are also present. One to 3 feet of peat, organic silt and ice cover the gravel which is underlain by lacustrine clay.

VOLUME

The total estimated volume, based on an area of 290 acres and average depth of 5 feet, is 2,000,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 106N-B2 is a source of fair to good quality granular materials. Areas to be exploited would be dictated by insitu material quality and depth of overburden. Granular material from this deposit may be used for general fill, backfill in pipeline construction and building pads.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access from the deposit to the right of way is about 1500 feet across a creek and care should be taken not to disrupt drainage and cause siltation in this creek. A snow road would be built to transport the borrow material over this distance from the deposit to haul points on the right of way. Initially trees and other vegetation covering the area of excavation and access road would be harvested and/or disposed of in accordance with land use regulations. The peat cover and overburden then would be stripped from the area to be excavated, and stockpiled around the edge of the site.

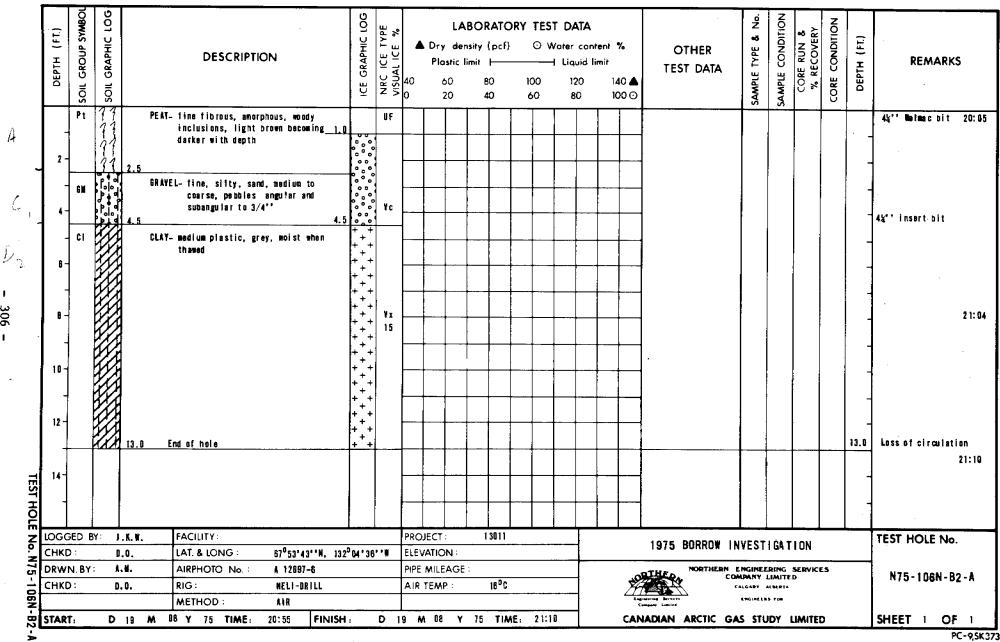
Development of this deposit would involve excavating borrow material evenly from the higher, better drained areas to a grade such that

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drainage is comparable to drainage before any excavation took place. The gravel is not deep and shallow excavations over large areas would take place. Care would be taken to avoid siltation of the lakes in the area. This type of development could be accomplished by using blasting or conventional earthmoving techniques depending on the degree of ice cementation. The excavated material may have to be stockpiled, thawed, and drained before it is used. Natural mixing during excavation would be adequate to obtain good gradations.

Equipment required for development would be dozers, rippers, end-dump trucks, front-end loaders, as well as screening, and crushing plants if required.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

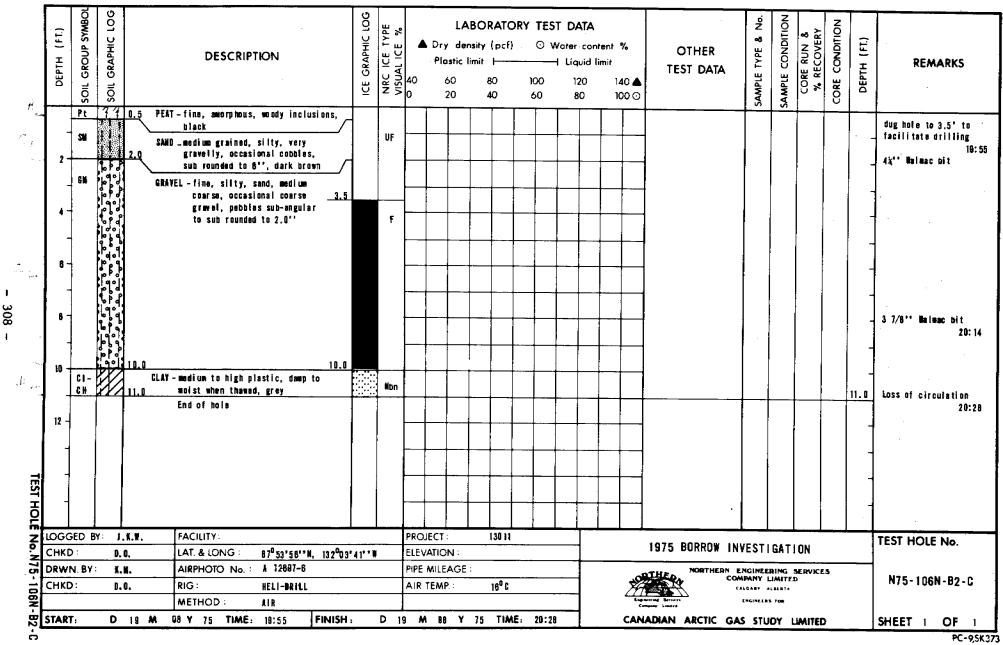


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LE No.	LOG		BY:).X.W	FACILIT					<u> </u>		OJECT		130	11	L	•		<u> </u>	1975 BORF	ROW IN	VEST	İĞAT		L	4,	TEST HOLE No.
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N75-	DRW		Ύ:			RIG	NO NO. :	HEL1-					R TEM		18	⁰ C				P O	THE ALL	co	CALGARY	LIMIT	FD			N75-106N-82-
						METHO	D :	ALR												<u>/ / </u> Engi Co	impany Limited		LNGIALE	#3 709				
06N-82	STAF	RT:		D 2	0 M	08 Y 7	5 TIME:	12:20	FINISH	1 :	D	20	M 8	8 Y	15	TIME	12:5	3		CAN	ADIAN ARC	TIC G	AS ST	UDY	LIMITE	D		SHEET 1 OF

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SOIL GROUP SYMBOL GRAPHIC LOG GRAPHIC LOG SAMPLE CONDITION ź CONDITION NRC ICE TYPE VISUAL ICE % LABORATORY TEST DATA CORE RUN & % RECOVERY DEPTH (FT.) ۰õ DEPTH (FL) ▲ Dry density [pcf] ○ Water content % OTHER SAMPLE TYPE DESCRIPTION REMARKS Plastic limit + ---- Liquid limit TEST DATA CORE 60 80 100 120 140 🛦 Щ SOIL 20 40 60 80 100 🖸 Noss cover Pt PEAT - dark brown, spongy UF 0.8 LT 1 73 1 Pt PEAT and SILT (organic) 73 Noe + 0L black 33 337 2.0 2.0 2 I GE ICE and PEAT, black 1 CE + + Pt 3 -3.3 3.3 3.3 MA, combined, \sim Non 6¥-GRAVEL - fine to coarse, some sand, little samples 1 - 3 : fines, peobles rounded to 3"" GN. G = 89% 4 2 4 28:80 S = 205 F = 11% 4.5___ occasional granitic pubble rounded to 2'' 13 Nettem of pit 5 28:45 5 FEST HOLE No. LOGGED BY: R.H. FACILITY PROJECT : 130 11 TEST HOLE No. 1975 BORROW INVESTIGATION CHKD R.H. LAT. & LONG 67⁰53'43''W, 132⁰04'36''W ELEVATION N75 DRWN. BY: A 12897-6 F.8.8. AIRPHOTO No : PIPE MILEAGE NORTHERN ENGINEERING SERVICES oTH & N75-106N-B2-1 COMPANY LIMITED RIG : CHKD: AIR TEMP : D.C. Approx. 18⁰C CALGARY ALBERTA 106N-B2-ENGINEERS FOR METHOD : TEST PIT START: D 19 M 08 Y 75 TIME: FINISH D 19 M 08 Y 75 CANADIAN ARCTIC GAS STUDY LIMITED SHEET I OF 17:30 TIME 20:45

TEST HOLE LOG

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	DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG			DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0		ensity	(pcf)	RY TES ⊙ v 100 60	Vater c	onte d lim		•	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FL)	REMARKS
	1	Pt	1-1-	0.6	PEAT	- anno rphous, fine fibrous, dark brown, spongy		ŰF																12:10 No samples taken
	ŀ	ML		1.5	SILT	- some very fine sand, non-plastic, brown ice to ¼'' at approx. <u>1.2</u> 1'' Spacing, clear, candled		V s 15	-														-	
					Nate	Moandoned Drillhole N75-106N-B2-Bon this site, did not encounter gravel to the depth drilled																		12:30
	1																							
TE	-			-																			1	
TEST HOLE No.	-																	-						
z			l¥:	R.H.		FACILITY	<u> </u>		PRO.			1 30 1 1		<u> </u>	<u> </u>			1975 BORROW INV	ESTI	GATI				TEST HOLE No.
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۳ ۲	снко			D.O.		RIG :			AIR	TEMP.		App ros	4. 22 ⁰ C			4	<u>×</u>	· ca	PANY L	LBLRTA	D			N75-106N-B2-2
р Бр	STAR	 [:	D	20		METHOD: TEST PLT Y 75 TIME: 12:10 FINISH	:	D :	20 M	08	Y 1	5 TIM	E: 12	30		c	CAN.	ADIAN ARCTIC GAS			IMITE	5		SHEET 1 OF 1
N75-106N-B2-2																								PC-9,5K37

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DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Plo ć	der	nsity (pcf)	RY TE ⊙ 100 60	Wote — Lir	r conte		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
	٩t	77	PEAT	- dark brown to black, spongy, roots		UF																
1 -	GN		GRAY	EL - silty, brown, peobles rounded to 3''			_						_			MA, combined			7		1-	
.	6#-		1.4 GR AV	EL - coarse to fine, some coarse to												samples 1 - 3 G — 70% S — 55%	Bl	IX			-	
2 -	BM			fine sand, trace silt, brown, cobbies rounded to 7°°						$\left \right $			-	+		S = 25% F = 5%		$\left(- \right)$	K		2 -	
-	1		2 <u>.8</u> Do	ulder to 18°' diameter												oversize = 11.8%	B2	X			3-	
3 -																	B3					
4	+ 	<u>°ā</u> •,	Eı	ttom of pit cavated into corner of test pit to tain a sample from 3° - 4°																		
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TEST HOLE	-										_]
7 1.0G	GED	BY:	 R.H.	FACILITY			PRO	JECT	1		13011	i I			<u> </u>	1975 BORROW IN	VECT	1641				TEST HOLE No.
	(D :		R.K.	LAT. & LONG : 87053'58'''N, 1320	03*41*	•₩		VATIO						1								4
ວກ 📖	VN.B	Y	F.F.B.	AIRPHOTO No. : A 12897-6				E MIL							فد	277 Bas 10 P	MPANY	LIMIT	F.D	CE5		N75-106N-B2-3
СНК	(D:		D.O.	RIG :			AIF	R TEM	IP. :		wpro	x. 24 ⁰ 0	i 	_	Ľ,	A Control of Control o	ALGART ENGINE	ALBERT	•			
<u> </u>				METHOD : TEST PLT			1			75	715	45 7	1:15	-		ADIAN ARCTIC GA			1.04.07	'ED		SHEET 1 OF 1
STA	RT:		19 M	08 Y 75 TIME: 20:00 FINIS		D	18	M 08		75		AC: 4	1 - 10			ALAN ARCINC OA			CUMU	2.07	·	PC-9,SK3

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SI	EVE AN	IALYSIS	REPO	RT				- ···· · · · · · · · · · · · · ·	
SAMPLE_	N75-10)6N-B2-1	DEPTH	3.5-5.0			R.M.HARD	Y REPORT	NUMBER
DATE SA	MPLED August	19, 1975	SAMPLED	BY_NESCL				153	
	GRAVEL	SIZES		SAND SIZ	5		FINES	SIEVE	PERCENT
	29%	40 %	6%	8 %		6 %	11%	SIZE	PASSING
		1		MEDIUM	F	INE	11/0		
		No). No.	No. No.	No.	No. N	lo No		
100	3" 2" 11/2" 1" 3/4"	1/2 / 1/4 4	8	16 30	50	100 20	o. No. 00 325		
								3"	100.0
90 -				-+				2"	97.7
0 80 -								11/2	90.4
5 80 BASSING								1"	79.7
S 70					-			3/4"	71.3
<u> </u>			-					1/2	58.7
IZ I								3/8 1/4	48.3
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₩ 40				+				No. 4 No. 8	31.3 24.7
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	N75-10 MPLED <u>Augus</u>	t 19, 1975		BY <u>NESCL</u>	·····		R.M.HARD	Y REPORT 145	NUMBER
	GRAVEL S		T	SAND SIZE	S		FINES	SIEVE	PERCENT
	38 %	32 %	10%	10%		5 %	5 %	SIZE	PASSING
	COARSE			MEDIUM	F	INE		j	····
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90								2"	98.3
	N							1/2	88.1
PASSING				-+				1"	71.8
SSI 102				<u>↓</u> ↓				3/4"	61.6
8								1/2	48.5
5 *								³ /#	41.6
U 50		\mathbf{X}						74	
ER I		N						No. 4	29.5
~ 40								No. 8	21.8
30		\rightarrow N		┥╴━┥━━				No. 16	15.5
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COMME	NTS						OVERSI		11.6 %
								DEPOS	IT No.
		HARDY &				POBT	HERN	N75-10)6N-B2
L		SULTING E	NGINEERII	NG & TESTI	٩G	Engineers	ng Services ng Limited		GE
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see site # 1139

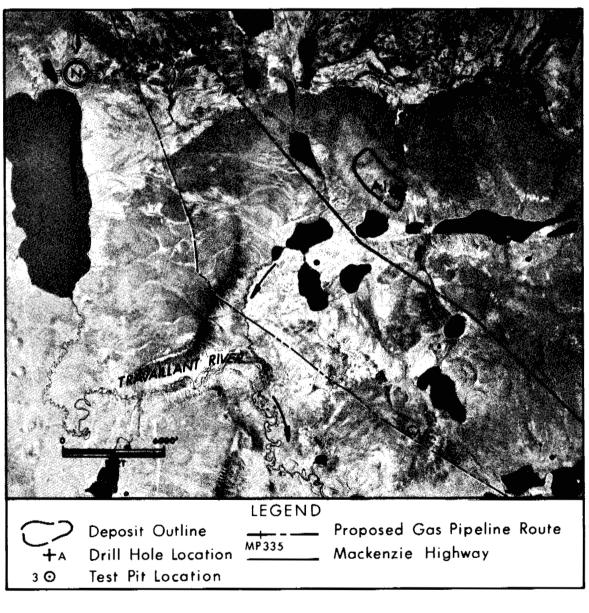
DEPOSIT 106N-B3

Physical Setting: Deposit 106N-B3 is a bedrock escarpment located 3 miles east of Wood Bridge Lake and less than 1 mile northeast of milepost 134 on the right of way.

Material: SHALE - poor quality.

Volume: Unlimited.

Assessment: Deposit 106N-B3 is a source of poor quality granular material and should probably not be considered for development.



Airphoto No.A21583-148Latitude:67° 52'Approximate Scale:1" = 5700'Longitude:132° 01'- 313 -- 313 -

DEPOSIT 106N-B3

PHYSICAL SETTING

This deposit is a bedrock escarpment 3 miles east of Wood Bridge Lake and less than 1 mile northeast of milepost 134 on the pipeline alignment. This deposit corresponds to source number 1139a in the EBA DIAND Granular Materials Inventory Volume IV (1974) report.

The 300 foot escarpment and the area adjacent to it are both considered part of this deposit. The escarpment slopes at about 30 degrees to the southwest, and the area behind the escarpment slopes very gently to the northeast. Drainage is good over the entire site and the active layer ranges from 3 to 5 feet in depth.

Terrain at the base of the escarpment is gently rolling and imperfectly drained.

BIOLOGICAL SETTING

The general area is part of an old burn which is now vegetated by black spruce and paper birch with an understory of willow, alder, cinquefoil, Labrador tea, and bilberry. Moose habitat at this site is marginal. Denning potential is considered good. Black and grizzly bear are found occasionally throughout the region. No evidence of beaver or other aquatic furbearers was observed in the adjacent lake. No raptor sign was observed in the vicinity of the escarpment. Waterfowl occur in the region throughout the open-water season. Small nearby ponds and lakes do not appear to support fish populations.

MATERIAL

About 20 feet of silty sand and gravel overlies shale along parts of the escarpment crest. In other areas 5 to 10 feet of till and colluvium

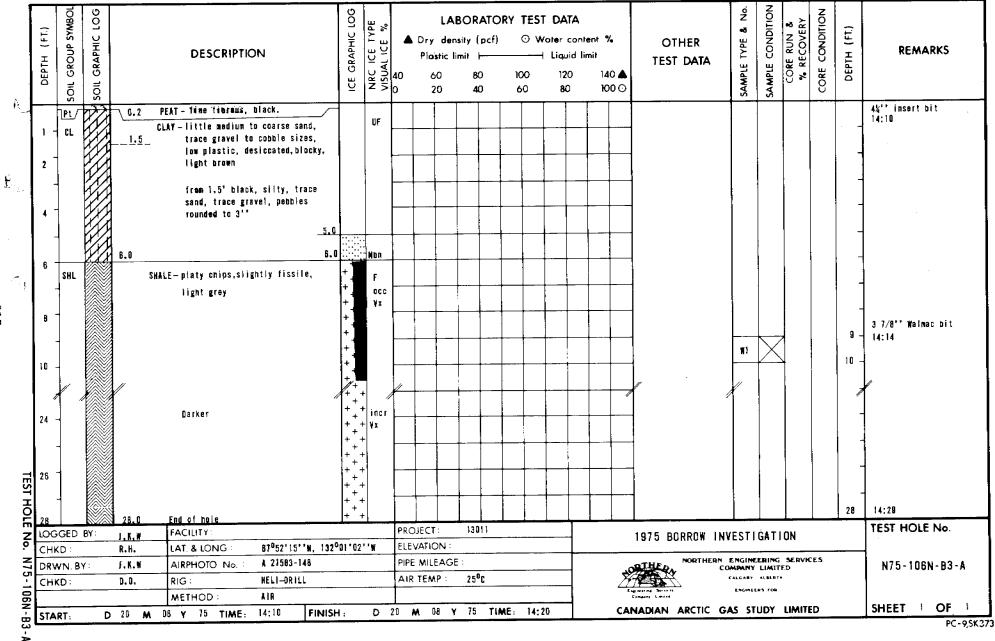
cover the shale. The shale contains occasional bentonitic beds and appears to be free of ice lenses. The sand and gravel, although not sampled, is probably also low in ice content (observed during geological field reconnaissance).

VOLUME

This escarpment and similar escarpments in the vicinity could provide an unlimited amount of poor quality borrow material.

DEVELOPMENT AND REHABILITATION

The shale found in deposit 106N-B3 is poor quality material for pipeline construction purposes and better borrow deposits exist closer to the pipeline right of way. This deposit should probably not be considered for development.



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DEPTH (FT.)		SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE	40	Dry Plas 61 21	densi stic lim 0	ORATC ity (pcf) iit	0	Water H Liq 1:	r cont			OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
	1	Pt	177	0 5	EAT - fine fibrous, dark brown, roots		UF	\uparrow										S	S.	<u>-</u>	Ĕ-		
1		CL			CLAY - some fine sand, nuggetted, dry to desiccated, damp at D.8', light brown		-										ſ				,		No samples taken
2				_}_8	silty, little fine sand, trace grave1, grey, moist					- -		- +		╞╶┤								-	
					pebbles rounded to 3'', occasional cobble to 7''																	-	
3	+	_	111	3.0	Bottom of pit	ļ	ļ															3.0	
TEST HOLE					Refer also to drillhole N75-106N-B3-A																		
	GED	BY	R	. H <i>.</i>	FACILITY			PRO.	JECT :		1301 1					-							TEST HOLE No.
	D: M		R	<u>. H.</u>	LAT. & LONG : 67°52'15'' N. 132°	01'02'	'₩		ATION							19	975 BORROW INVE	STI	GATI	ON			LOT HOLL NO.
	D:	51.	. <u> </u>	. M. . O.	AIRPHOTO No. : # 21583-148 RIG :				MILEA	GE :					کد	OBT	HE NORTHERN EN	GINEES		ERVICE	s		N75-106N-83-1
					METHOD : JEST PIT			AIR	TEMP		Approx.	245			Ž		CALG		BLRTA				
LOGI CHK DRW CHK	RT:	_	D	20 M (08 Y 75 TIME: 12:00 FINISH :		D 20	N	0.8	Y 7	5 TIME	: 13	30		CAI	NAC	DIAN ARCTIC GAS			MITED		_	SHEET 1 OF 1

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106N - B4 - A 625450E 7530470N 106N - B4 - B 624730E 7530470N

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see site # 1138

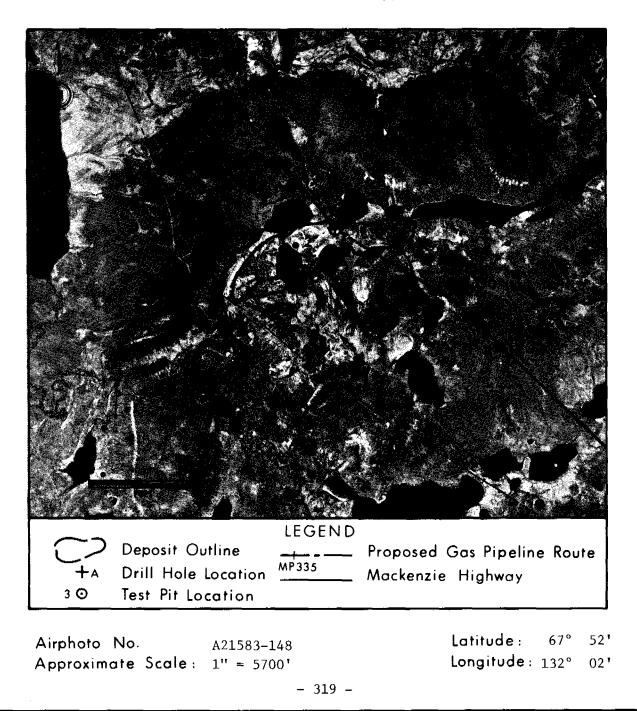
DEPOSIT 106N-B4

Physical Setting: Deposit 106N-B4 is an outwash terrace located 2 miles east of the south end of Wood Bridge Lake. The proposed pipeline alignment crosses the deposit near milepost 135.

Moterial: GRAVEL - well graded gravel to silty sand with variable silt content.

Volume: 17,000,000 cubic yards.

Assessment: Deposit 106N-B4 is a source of good quality granular material. Haul distance is short and granular material from this deposit may be used for general fill, backfill, in pipeline construction, building pads, and possible production of concrete aggregates.



DEPOSIT 106N-B4

PHYSICAL SETTING

This deposit is an outwash terrace located 2 miles east of the south end of Wood Bridge Lake. The proposed pipeline alignment crosses the deposit near milepost 135. This deposit has been previously documented as source 1138 in the EBA DIAND Granular Materials Inventory Volume IV (1974) report.

The terrace surface is flat to gently sloping, with maximum relief of 10 feet. Meltwater activity has formed a 20 foot scarp along its western and northern edges. Drainage near the scarp is moderate to good, but only fair to poor over the remainder of the site. Overburden near the scarp edge is negligible, but ranges from 3 to 10 feet over the rest of the deposit. Further drilling is required to determine the exact extent and thicknesses of overburden. The active layer varies between 1 and 8 feet. The deposit is overlain by icy peat and silt, but the gravel and sand has low ice content.

BIOLOGICAL SETTING

The site supports spruce up to 25 feet in height and a thick understory of willow, bog birch, and ericaceous shrubs. Ground cover consists of sedges and mosses. The area provides only marginal habitat for furbearers and large mammals. Grizzly and black bear are found occasionally throughout the region. No sign of beaver or other aquatic furbearers was evident in the adjacent lakes. Waterfowl occur in the region throughout the open-water season. Adjacent lakes do not appear to support fish populations.

MATERIAL

Material at this deposit is of good quality and ranges from well graded gravel to silty sand. Gravel is mainly rounded and exhibits variable silt content.

VOLUME

Total estimated volume, based on an area of 400 acres and a conservative depth of 30 feet of sand and gravel, is 17,000,000 cubic yards. Approximately half of this volume is estimated to be gravel.

DEVELOPMENT AND REHABILITATION

Deposit 106N-B4 is a source of good quality granular material. Areas to be exploited will be dictated by insitu material quality, overburden thicknesses, ice content and material requirements. Additional drilling and test pitting is required to define the areas with the least overburden and the best quality material. Granular material from this deposit may be used for general fill, backfill and pipeline construction, building pads, and possible production of concrete aggregates. Further testing would be necessary to determine material suitability for concrete.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socio-economic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the deposit would probably be achieved from the pipeline right of way as it is more than 40 miles inland from the Mackenzie River. The pipeline right of way crosses the deposit, making snow haul roads conveniently short.

In order to prevent environmental damage, development would be kept away from shorelines and streams near the deposit.

Vegetation would have to be harvested and disposed of in accordance with existing land use regulations. The peat cover and overburden then would be stripped from the area to be excavated, and stockpiled around the edge of the excavation.

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Development of this deposit could involve excavating borrow material evenly from the higher, well drained areas so that good drainage would be maintained over the area. Pit development by mining vertical faces could also be considered along the valleytrain. This would involve excavating material from the face of the scarp. Either type of development could be accomplished by using blasting or conventional earthmoving techniques depending on the degree of ice cementation which appears to be low. The excavated material may have to be stockpiled, thawed, and drained before it is used. Crushing and/or screening of the material may be required to produce quality construction aggregates.

Equipment required for development would be dozers, rippers, end-dump trucks, front-end loaders, as well as screening, drying, crushing, and concrete production plants if required.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

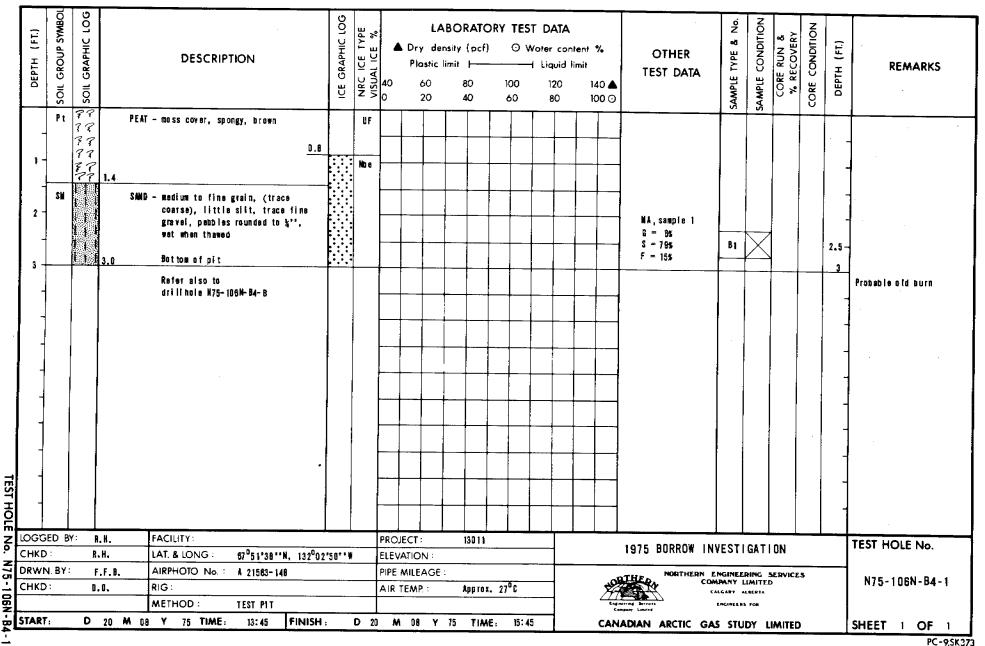
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•				weathered, dry	to desiccated																-]	
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		:	<u>R.H.</u> J.K.W	LAT. & LONG : AIRPHOTO No.	67 ⁰ 51'50''N, 132 ⁰ 00' <u>5</u> : A 21583-148	52''W			MILEAC							NORTHERN				ES			
CHKD			D.O.	RIG:	HELI-DRILL				TEMP.		27 ⁰ C				the second	CO CO	MPANY CALGARY	LIMITE			l	N7	5-106N-84-A
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DEPTH (FT.)		SOIL GROUP SYMBOL	SOIL GRAPHIC LOG			DESC	RIPTIO	N			ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Pla	den	3ORAT sity (pc mit ⊢ 80 40		Wate	DATA ar contr iquid lir 120 80			OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
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E 8		GM P				fine, sil occasiona boulder f intervals X ⁴⁺ , meta	il cobble o 10'' a :, pebble	is, iso t 7.0° s roun	lated , coar	ser		F															-	4%" Tricone bit 17:01
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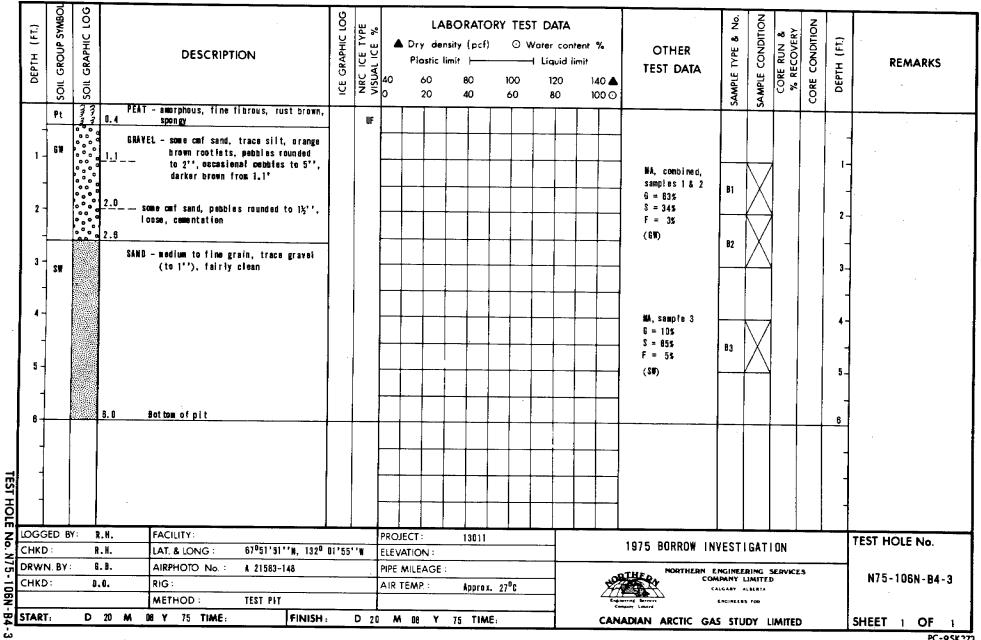
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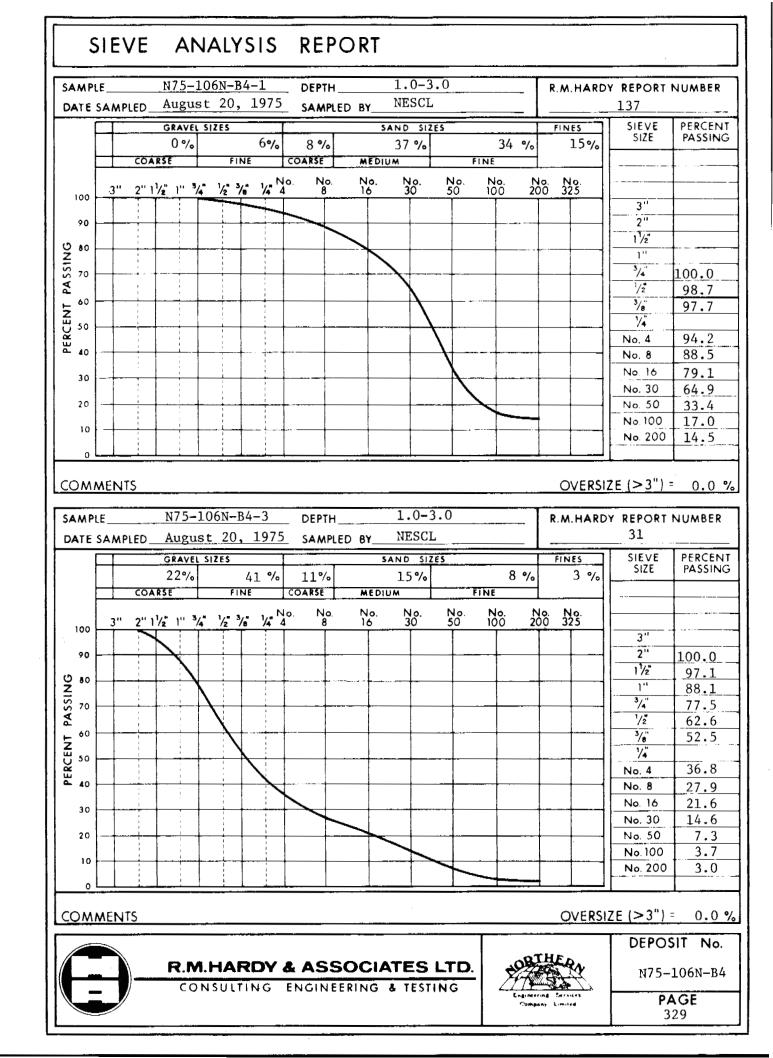
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	Pt + aL	7 37	1 1.0	PEAT with SILT (organic), black 1.0						i								-			
2 -	1 CE + 0L			CE to approximately 2'' with SILT (organic), black		1 CE +														-	17:30
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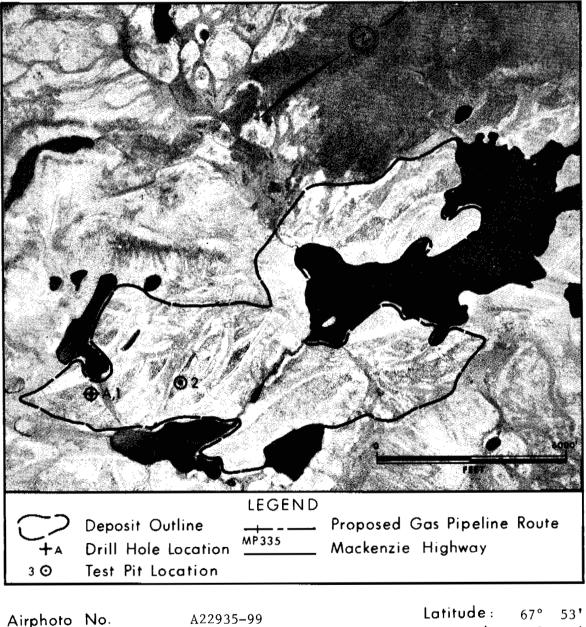
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Physical Setting: Deposit 1060-B1 is a channeled outwash plain located 11 miles north of Travaillant Lake and 4 miles northeast of milepost 137 on the proposed pipeline.

Material: GRAVEL - well graded, and sand.

- Volume : 16,700,000 cubic yards.
- Assessment: Deposit 1060-B1 is a source of good to excellent quality granular material suitable for general fill, backfill, building pads, and possible concrete and asphalt aggregate. The access to the right of way is fair.



1'' = 3100'Approximate Scale:

Longitude : 131° 53'

DEPOSIT 1060-B1

PHYSICAL SETTING

Deposit 1060-B1 is a channeled outwash plain located 11 miles north of Travaillant Lake and 4 miles northeast of milepost 137 on the proposed pipeline right of way. This deposit corresponds to part of source number 1138 in EBA DIAND Granular Materials Inventory Volume IV (1974) report.

The surface of the outwash plain is a mosaic of large bars and abandoned channels that are separated by 10 to 15 foot scarps. The bars have a negligible cover of peat and silt and are well to imperfectly drained. The abandoned channels are poorly drained and probably contain thicker overburden. The active layer ranges between 6 and 8 feet and material below this depth is frozen with low ice content.

Terrain between the pipeline route and the deposit consists of a flat, marshy plain with poorly defined drainage and a drift covered upland with rolling topography.

BIOLOGICAL SETTING

Vegetation on the bars consists of a dense stand of black spruce up to 20 feet in height with a thick shrub understory and a ground cover of moss and lichen. Abandoned channels are covered by sedges with scattered shrubs. This area provides winter range for caribou and moderately productive habitat for upland furbearers, black and grizzly bear and moose. No beaver lodges were observed in the adjacent lakes. The area provides limited denning opportunities for small mammals. No information is available on waterfowl use of the area or the fisheries potential of nearby streams, ponds and lakes.

MATERIAL

Drill hole and test pit logs plus the DIAND report indicate that this deposit consists of at least 18 feet of well graded gravel and sand.

Gravel is generally rounded and contains a trace of silt periodically. At the sites sampled there was less than 1 foot of peat covering the deposit. Water was encountered at 2.8 feet in test pit 1060-B1-2 and this could cause problems during development. Material quality is good to excellent.

VOLUME

The total estimated volume, based on an area of 1460 acres and a conservative depth estimate of 15 feet, is 16,700,000 cubic yards. Volumes could be doubled by including outwash along this valley to the north. The recovery of granular material may be restricted because of the relatively high water table.

DEVELOPMENT AND REHABILITATION

Deposit 1060-B1 is a source of good to excellent quality granular materials. Location of areas to be exploited will be dictated by haul distances, overburden thicknesses, insitu material quality, and material requirements. Depth of water table is about 3 feet or less in places and this will also be a factor in locating areas for development. Granular material from this deposit may be used for general fill, backfill in pipeline construction, building pads, and concrete and asphalt aggregate. The gravel will require further testing before use in concrete.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socio-economic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

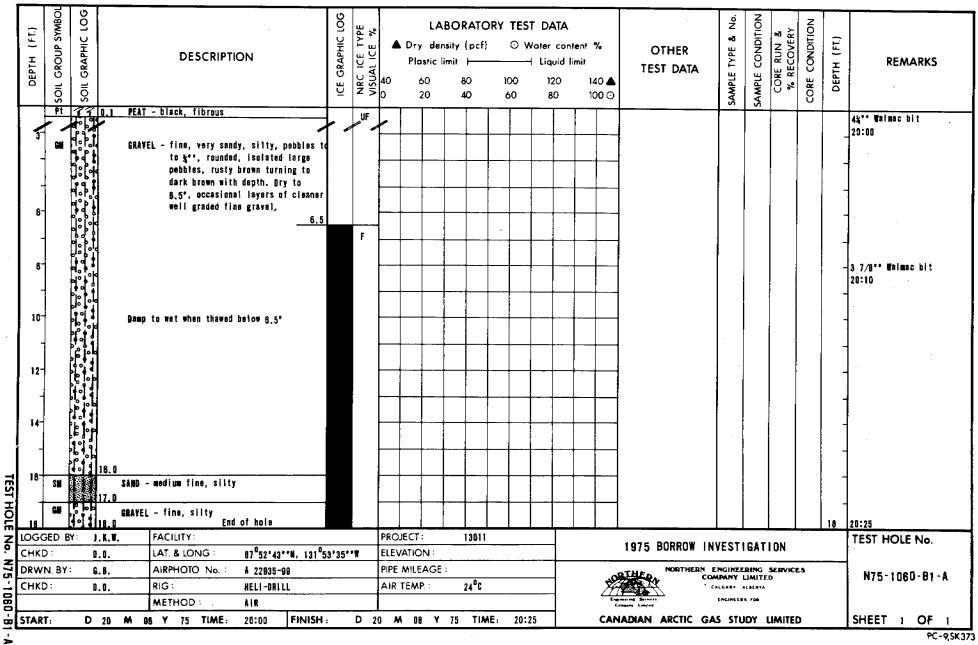
Access to the deposit would probably be via the pipeline right of way. In order to minimize environmental damage, snow roads would be built to transport the borrow material from the deposit to haul points on the right of way, a distance of at least 4 miles across a flat marshy area and a drift covered upland.

Trees and vegetative cover would have to be removed and disposed of or harvested in accordance with existing land use regulations. Peat cover and overburden is negligible at this site, therefore minimizing stripping.

Development of this deposit would involve excavating borrow material in stages from the higher, better drained bars. If very large quantities of borrow are required, dugout pit development could be established depending on the depth of water table. Either type of development could probably be accomplished by conventional earthmoving techniques since ice contents are low. The excavated material may have to be stockpiled, thawed, and drained before it is used. An adequate buffer zone would have to be maintained between the excavation and any water courses or lakes to prevent siltation. Crushing and/or screening of the material may be required to produce quality construction aggregates.

Equipment required for development would be dozers, rippers, end-dump trucks, front-end loaders, as well as screening, crushing, concrete and asphalt plants if required.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.



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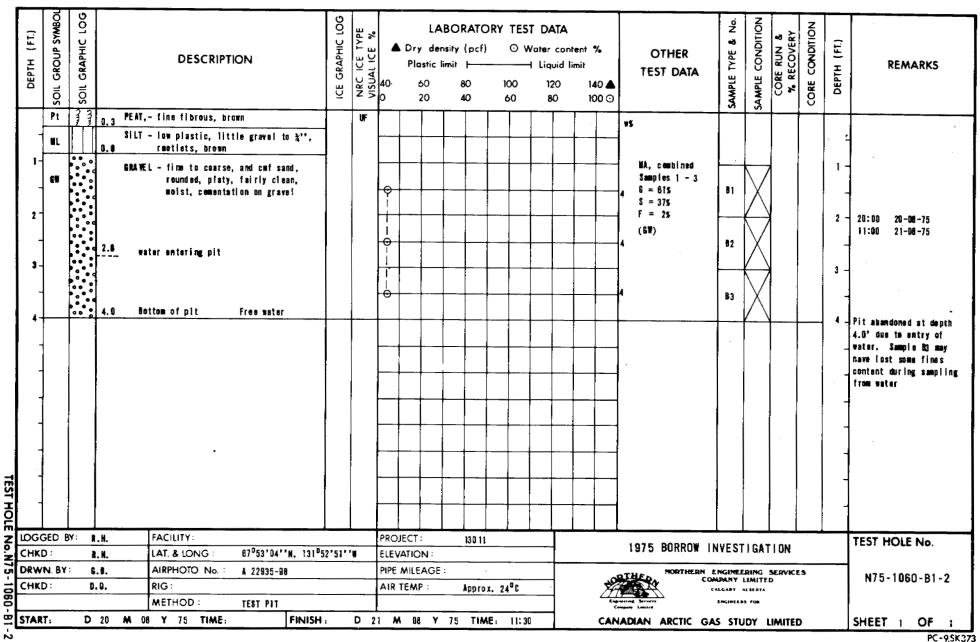
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500 SOIL GROUP SYMBOL ICE GRAPHIC LOG ŝ SAMPLE CONDITION CONDITION NRC ICE TYPE VISUAL ICE % O & LABORATORY TEST DATA CORE RUN & (FT.) SAMPLE TYPE & GRAPHIC DEPTH (FT) A Dry density (pcf) O Water content % OTHER DESCRIPTION DEPTH REMARKS Plastic limit 1 Liquid limit -1 TEST DATA CORE 60 80 100 120 140 🔺 SOIL 20 40 60 80 100 🖸 14.14 Pt PEAT - fine fibrous, dark brown UF 04 85 10 0 01 10 0 01 GM GRAVEL - silty, roots, orange brown 0.9 ٩, ٥٩, 1 GW GRAVEL - and cmf sand, trace fines, MA. combined cementation on gravel, brown, samples 1 - 2 Ð 81 moist 6 = 59%S = 39- 2 2. F = 2% 82 3.0 MA, sample 3 2 1. 13:30 S = 28% SAND - medium to coarse, some gravel to SW S = 89% 2"", cementation on peoples Ŋ F = 3% 4.0 Bottom of pit 13:50 (SW) 4 NOTE: Bottom of pit was cleared and is either a large flat rock or sandstone bedrock **TEST HOLE** LOGGED BY R.H. FACILITY PROJECT: 130.11 TEST HOLE No. **Z 1975 BORROW INVESTIGATION** CHKD R. H. LAT. & LONG 87°52'43''W, 131° 53'35''W ELEVATION AIRPHOTO No. A 22835-99 DRWN. BY: F. B. PIPE MILEAGE : IORTHERM ENGINEERING SERVICES N75-1060-B1-1 COMMANY LIMITED CHKD: AIR TEMP. D.O. RIG : Approx. 24⁰C CALGARY AUBLRIA **METHOD:** TEST PIT -----FINISH : START: D 21 M 08 Y 75 TIME: -D 21 M 08 Y 75 TIME: 13:50 CANADIAN ARCTIC GAS STUDY LIMITED SHEET 1 OF

TEST HOLE LOG

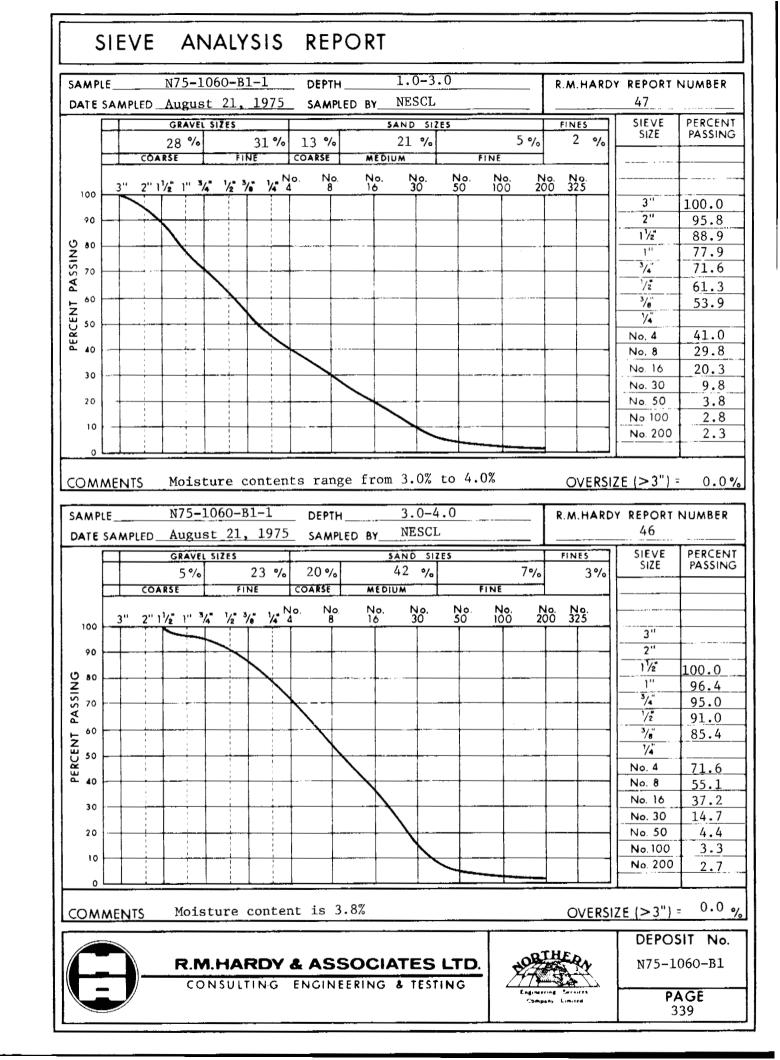
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PERCENT PASSING	70				\mathbb{N}															1"	78.2
A S	70				1															3/4 1/2	69.9
F	60	\vdash	+ +			$ \rightarrow $												\rightarrow		3/8	58.7
N N N	50	ł		1]													ĺ	<u> </u>	51.4
1 2 2	50																			No. 4	39.2
P	40			+	+ +	;	+							<u> </u>		Tala				No. 8	29.7
	30	_	1											1						No. 16	29.7
	50							1												No. 30	11.1
	20		+	+	-		-		+		\rightarrow			_				_		No. 50	4.1
	10																- i -			No. 100	3.0
	10		r 		T	1			T			~			- †		+	_†		No. 200	2.4
	0		<u>l :</u>	<u> </u>	<u>. </u>	. !			<u> </u>					1							<u> </u>
			MPLED													- <u> </u>	F	R. M. H	ARD	Y REPORT I	NUMBER
			T																		
			+	GR	AVEL	SIZES						SAND	SIZE	s				FINE	5	SIEVE	PERCENT
			<u> </u>	GR	%	SIZES		%		%		SAND	\$1ZE %	s		•	<u> </u>	FINE	%	SIEVE SIZE	PERCENT
			co	GR. ARSE		SIZES	FINE		COA		ME	SAND			INE	۰,	<u> </u>	FINE			
				ARSE	%		FINE		COA		No.	DIUM	%	f	No		/o No.		%		
۱	100				%		FINE		COA	RSE		DIUM			INE No 100		6	No 325	%	SIZE	
				ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE	
	100 90			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE	
				ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE 3" 2" 1½	
	90			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE 3" 2" 1½ 1"	
SING	90 80			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE 3" 2" 1½ 1" 3/4"	
PASSING	90 80			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE 3" 2" 1 ¹ /2 1" 3/4" 1/2	
PASSING	90 80 70			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE 3" 2" 1½ 1½ 1" 3/4" 1/2 3/6"	
ERCENT PASSING	90 80 70 60 50			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE 3" 2" 1 ¹ /2 1" 3/4" 1/2	
ERCENT PASSING	90 80 70 60			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE 3" 2" 1 ¹ /2" 1 ¹ /2" 1 ¹ /2" 3/4" 7/2" 3/6"	
PERCENT PASSING	90 80 70 60 50			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE 3" 2" 1 ¹ /2 1" 3/4" 1/2 3/6" 7/4 No. 4	
PERCENT PASSING	90 80 70 60 50 40			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE 3" 2" 1 ¹ /2 1" 3/4" 7/2 3/4" 7/4 No. 4 No. 8	
PERCENT PASSING	90 80 70 60 50 40			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE 3" 2" 1½ 1½ 1½ 3/4 7/2 3/6 7/4 No. 4 No. 8 No. 16	
PERCENT PASSING	90 80 70 60 50 40 30			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE 3" 2" 1½ 1½ 1" 3/4 7/2 3/6" 7/4 No. 4 No. 8 No. 16 No. 30	
PERCENT PASSING	90 80 70 50 40 30 20 10			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE 3" 2" 1 ¹ /2" 1 ¹ /2" 1 ¹ /2" 3 ¹ /4" 7 ¹ /2" 3 ¹ /4" 7 ¹ /2" 3 ¹ /4" 7 ¹ /2" 3 ¹ /4" 7 ¹ /2" 3 ¹ /4" 7 ¹ /2" 3 ¹ /4" 7 ¹ /2" 3 ¹ /4" 7 ¹ /2" 3 ¹ /4" 7 ¹ /2" 3 ¹ /4" 7 ¹ /2" 3 ¹ /4" 7 ¹ /2" 3 ¹ /4" 7 ¹ /2" 3 ¹ /4" 7 ¹ /2" 3 ¹ /4" 7 ¹ /2" 3 ¹ /4" 7 ¹ /2" 7	
PERCENT PASSING	90 80 70 60 50 40 30 20			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.		%	SIZE 3" 2" 1 ¹ /2 1" 3/4" 1/2 3/4" 7/2 3/6" 7/4 No. 4 No. 8 No. 16 No. 30 No. 50 No. 100	
PERCENT PASSING	90 80 70 60 50 40 30 20 10			ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.	No 325	%	SIZE 3" 2" 1 ¹ /2 1" 3/4" 1/2 3/4" 7/2 3/6" 7/4 No. 4 No. 8 No. 16 No. 30 No. 50 No. 100	
PERCENT PASSING	90 80 70 60 50 40 30 20 10		3" 2"	ARSE	%		FINE		COA	RSE	No.	DIUM	%	f	No		/o No.	No 325	%	SIZE 3" 2" 1 ¹ /2 1" 3/4" 7/2 3/4" 7/2 3/4" 7/4 No. 4 No. 8 No. 16 No. 30 No. 50 No. 100 No. 200	PASSING
PERCENT PASSING	90 80 70 60 50 40 30 20 10		3" 2"		·/~					RSE No 8		DIUM	%		No		/o No.		%	SIZE 3" 2" 1 ¹ /2 1" 3/4" ¹ /2 ³ /4" ¹ /4 ¹ /2 ³ /4" ¹ /2 ³ /4" ¹ /2 ¹ /4 ¹ /2 ¹ /2	PASSING

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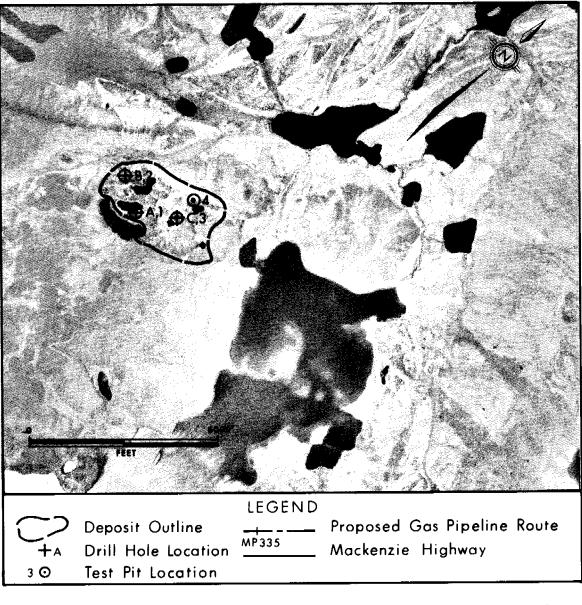
SUMMART	OF LABORATORY TE FOR	EST DATA	
SUITABILITY	OF AGGREGATES IN	I CONCR	ETE
	DATE SAMPLED : August 21, DATE TESTED : March, 197		
SOUNDNESS OF AGGR SULPHATE TEST	EGATE	ORGANI TEST	C IMPURITIES
COARSE AGGREGATE			EMOVED : 5
LOS ANGELES ABRAS PERCENT LOSS ■	10N TEST 21.0 %	REMOVE COAL C	ROOTLETS D : ⁵ ONTENT : Trac CANCE :
SUMMARY OF ROCK TYPE	S, COARSE AGGREGATE. (I	PETROGRAPI	IC ANALYSIS
ROCK TYPE	CLASSIFICATIONS	5	TOTAL
			WEIGHTED COMPONENT 9
Quartzite	Very strong, Good	-	
			COMPONENT 9
Quartzite Sandstone	Very strong, Good		22.20 44.25
Quartzite Sandstone Siltstone Chert	Very strong, Good Medium strong, Good Potentially reactive, Fair		COMPONENT 9 22.20 44.25 7.15 1.95
Quartzite Sandstone Siltstone Chert Flint	Very strong, Good Medium strong, Good Potentially reactive, Fair		22.20 44.25 7.15 1.95 4.74
Quartzite Sandstone Siltstone Chert Flint PN = 118 INTERPRETA	Very strong, Good Medium strong, Good Potentially reactive, Fair	ate OCIATES LTD.	COMPONENT 9 22.20 44.25 7.15 1.95 4.74

	OF LABORATORY TH FOR OF AGGREGATES IN		
	DATE SAMPLED : August 21, DATE TESTED : March, 197		
SOUNDNESS OF AGGI SULPHATE TEST	REGATE	ORGANI TEST	IC IMPURITIES
COARSE AGGREGATE FINE AGGREGATE	-		R : 5 REMOVED : 5
LOS ANGELES ABRAS	21.0 %	REMOV	& ROOTLETS ED : 5 CONTENT : Trace
	PES, <u>FINE</u> AGGREGATE. (PHIC ANALYSIS
ROCK TYPE	CLASSIFICATIONS	5	TOTAL WEIGHTED COMPONENT %
Quartzite	Very strong, Good		9.58
Sandstone Siltstone	Strong, Good		3.13 4.84
Chert Flint	Potentially reactive, Fair		0.87
PN = 118 INTERPRETA	TION : Good quality aggregat	e	19.70
COMMENTS : See also	page 341.		
Engineering Second	CONSULTING ENGINEER		N75_1060_01
Company Limited			PAGE 342

1060 - B2 - A 378230E 7530160N B2 - B 377960E 7530440N B2 - C 378580E 7530440N

- Deposit 1060-B2 is a kame and kettle complex **Lo**cuted Physical Setting: 4 miles northeast of Crossing Creek Lake and 3 miles northeast of the right of way at milepost 137.
- SAND and GRAVEL interbedded well graded sand and gravel. Material:
- 4,500,000 cubic yards. Volume :

Deposit 1060-B2 is a source of good quality granular Assessment: material suitable for general fill, backfill, building pads and possible concrete aggregate. Access presents no serious problems over the 3 miles of rolling upland.



A22935-98 Airphoto No. Approximate Scale: 1" = 3100'

67° 52' Latitude : Longitude: 131° 53'

DEPOSIT 1060-B2

PHYSICAL SETTING

This deposit is a kame and kettle complex 4 miles northeast of Crossing Creek Lake and 3 miles northeast of the pipeline right of way at milepost 137. This deposit corresponds to part of source number 1137 in EBA DIAND Granular Materials Inventory Volume IV (1974) report.

The complex has local relief between 50 and 100 feet with slopes up to 15 degrees. Generally, hills and slopes are well drained, with gentler slopes and depressions imperfectly to poorly drained. Overburden is less than 1 foot, except possibly in depressions.

The active layer varies from 1 to 6 feet or more and below this the deposit is frozen. Ice contents appear to be low, although some excess ice was observed in some strata.

A rolling drift covered upland is typical of the terrain located between the deposit and pipeline right of way.

BIOLOGICAL SETTING

Vegetation at this site consists of a dense stand of black and white spruce up to 30 feet in height. The understory consists of alder and willow and a ground cover of dwarf shrubs, lichen and moss. The area provides winter range for caribou and moderately productive habitat for upland furbearers, black and grizzly bear and moose. Caribou and fox sign were observed at the site. There was no evidence of beaver in the small adjacent lake. No information is available on waterfowl use or fisheries potential of the small lakes and streams in the area. The adjacent lake does not appear to support fish populations.

MATERIAL

Material at this deposit consists of interbedded well graded sand and rounded gravel with varying amounts of sand and silt. Sand beds contain small quantities of silt and fine gravel.

VOLUME

The maximum depth of gravel and sand is probably slightly in excess of the local relief, which for hills and ridges is in the order of 75 feet. Using this depth and an area of 160 acres, the total estimated volume is 4,500,000 cubic yards. The DIAND report indicates there is a similar deposit of somewhat smaller area to the north across a nearby lake.

DEVELOPMENT AND REHABILITATION

Deposit 1060-B2 is a source of good quality granular material suitable for general fill, backfill in pipeline construction, building pads, and possibly concrete aggregate. Location of areas to be exploited would be determined by further exploratory drilling.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the pipeline right of way, over 3 miles of rolling drift covered upland presents no serious problems, although steeper slopes should be avoided to prevent initiation of bimodal flows. In order to minimize environmental damage, snow roads would be built to transport the borrow material from the deposit to haul points on the pipeline right of way. Excavation would be done carefully to minimize siltation in adjacent lakes.

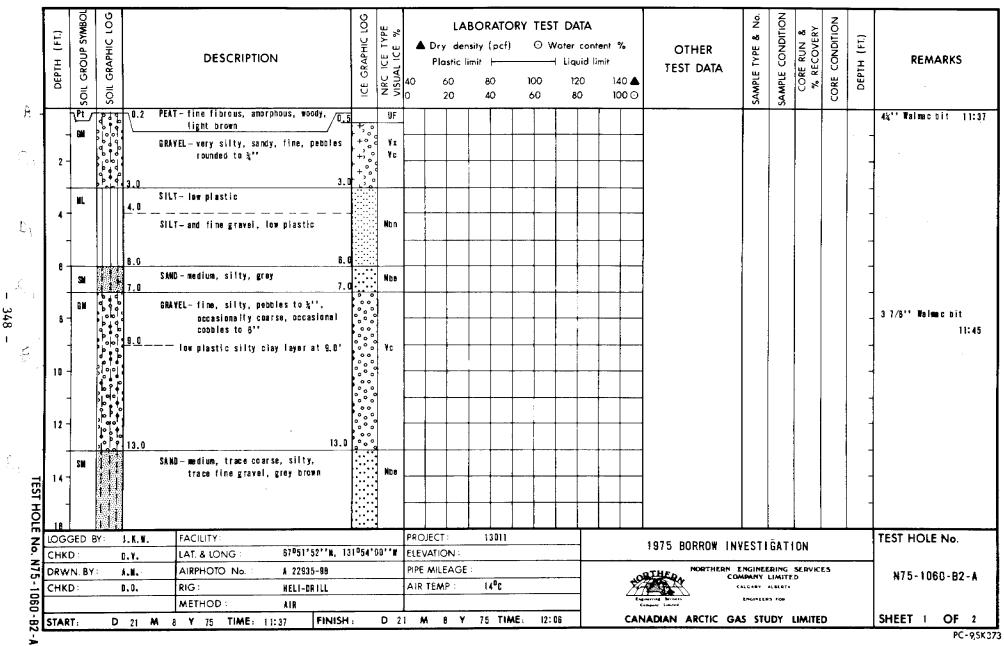
- 346 -

Initially, the tree cover would have to be removed from selected sites and along the haul road right of way and harvested according to land use regulations. Overburden is thin over the deposit necessitating some stripping. Development of this deposit would involve excavating borrow material evenly or in stages from the higher, well drained areas to a level that promotes good drainage over the site. Detailed development plans would be prepared after further exploratory investigations were completed. Conventional earthmoving techniques would be used as ice contents are low. Blasting might be necessary if material with a high degree of ice cementation is encountered. The excavated material may have to be stockpiled, thawed and drained before it is used.

Crushing and/or screening of the material may be required to produce quality construction aggregates. Equipment required for development would be dozers, rippers, end-dump trucks, front-end loaders, as well as screening, crushing and concrete plants if required.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

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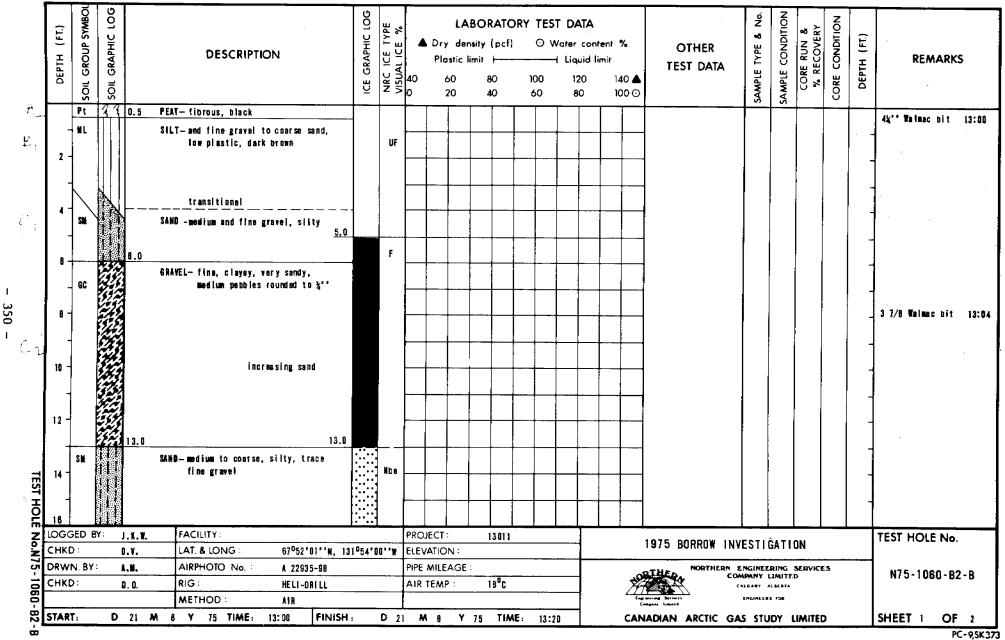


001 SYMBOL GRAPHIC LOG ŝ SAMPLE CONDITION CORE CONDITION NRC ICE TYPE VISUAL ICE % O & LABORATORY TEST DATA CORE RUN & % RECOVERY DEPTH (FL) SAMPLE TYPE & DEPTH (FI.) GRAPHIC GROUP OTHER **DESCRIPTION** REMARKS Plastic limit + - Liquid limit TEST DATA 100 60 80 120 140 🔺 Щ SOIL SOIL 20 40 60 80 100 🖸 SAND (cont'd) 1 + SH + 17.0 + 5 + + + + GM GRAVEL- and silt, sand, medium, coarse Lolo_ + 11:55 18 -++ + +* + + + + + + + + + ¥x 20 + + + 22 + + 24 + + + 4 26.0 Loss of circulation End of hale + 28.0 28 12:06 TEST HOLE FACILITY PROJECT : TEST HOLE No. No. N75-1060-B2 LOGGED BY: J.K.W. 13011 1975 BORROW INVESTIGATION LAT. & LONG 67°51'52''N, 131°54'00''W ELEVATION : CHKD D.¥. A 22935-98 PIPE MILEAGE DRWN. BY: AIRPHOTO No. NORTHERN ENGINEERING SERVICES A.N. THE N75-1060-B2-A COMPANY LIMITED 14⁰C AIR TEMP CHKD: RIG : HELI-DRILL 0.0. CALGARY ALBERTA ENGINEERS FOR METHOD : AIR. Commany Limited FINISH : D 21 M 8 Y 75 TIME: 12:06 CANADIAN ARCTIC GAS STUDY LIMITED SHEET 2 **OF** 2 START: D 21 M 8 Y 75 TIME: 11:37

TEST HOLE LOG

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PC-9,5K373



	DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTIO	N	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	▲ 1 40 0	Dry die	nsity (p	ocf)	⊙w	DATA ater cont Liquid li 120 80	mit 14	% 40 ▲ 20 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FI.)	REMARKS
Ī		3 4		SAN 17.0	D (cont°d)			NDS														-	
	18 -			GR A	YEL-fine, silty, pebo occasional coarsu End of hole	bles to ½'', e to 2''																20.0	Loss of circulation
	20 -							1		-													13:20
	-																						
	-		1						╞──╌╇─	1	+ +	-	+ +									-	
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TEST HOLE No. N75-1060-B2-B	1																						
z	LOGO	GED 6	BY: J	.K.W.	FACILITY				PROJE	CT :	1	30 11					1975 BORROW INV	ESTI	<u><u><u></u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u><u></u></u>	0N		•	TEST HOLE No.
2 Z	снк) :		.Ψ.	LAT. & LONG	67 ⁰ 52'01''N, 131 ⁰	54'00	* * W	ELEVA														
175-	_	N. BY		. N.	AIRPHOTO No.	A 22935-98			ŧ	ILEAG		8 ⁰ C				-0		APANY	LIMITE		ES		N75-1060-B2-B
ā	СНК	D: 	D	.0.	RIG : METHOD :	HELI-DRILL			AIR T	CMP.	1	5-U				2		ALGARY EMGINEL					
Ë	STAR	<u>т.</u>	D	21 M	8 ¥ 75 TIME:	AIR 13:00 FINISH		D 2	1 M	8 1	15	TIME	13:2	D			NADIAN ARCTIC GA	S STI	UDY	LIMITE	D		SHEET 2 OF 2
12 L													•										PC-9,5K37

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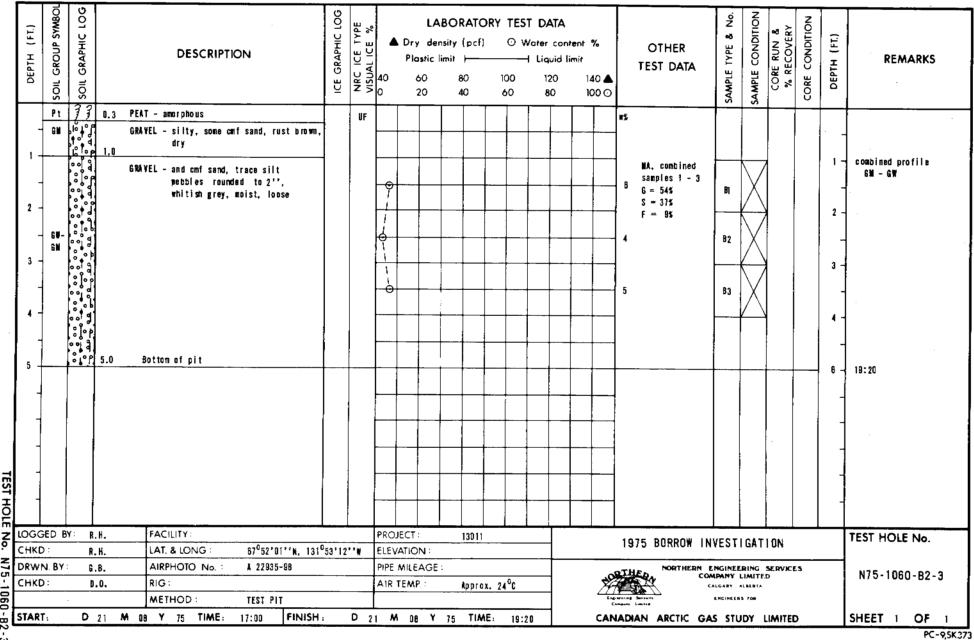
PC-9,5K373

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DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG			DESCRIP	TION			ICE GRAPHIC LOG	NRC ICE TYPE	40	Pla	dens		TORY T (F) C 100 60) Wai i)			OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
	Pt	35	0.4	PEAT - fine	fibrous, bi	rown, ro	ots		Τ	UF															
1-	GN				ty, and sm nded to 3' -graded, wi	', possi	bly als	0											MA, combined samples 1 - 5 6 = 53% S = 40% F ≕ 7%	B1					
3-			4 4 4 3. 4	Îlă	vel to 3'' µlar, ceme															82 83)		3-	
4-	64		•	GRAVEL - fin bro	e to coars wn, cobble															B4)		4- - 5-	
-			<u>ا</u>	Bot	<u>tom of pit</u>															85	X			-	
										7															
	GED	BY :	R.H. D.O.	FACIL	LITY :	A7 ^C	51'44''	N. 131 ⁰	53133		-			130	11				1975 BORROW I	NVES.	TIGA	 TION			TEST HOLE No.
	N.B	(:	5.0. F.B. D.D.	AIRPH RIG :	1010 No.	: A 2	2935-98				PIP	E MILI R TEM	AGE		rox. 21 ⁰ (;	Ź	09 77 1.4		ENGINE MPANY CALGARY LINGINE	LIMIT	F.D	CES		N75-1060-B2-
TAR				M 08 Y				FINISH		D 3	21	M 0.8	Y	75 T	IME:	1:45	 c,		DIAN ARCTIC G	AS ST	UDY	LIMIT	ED		SHEET 1 OF

SAMPLE CONDITION SAMPLE TYPE & No. CORE CONDITION ICE GRAPHIC LOG **GROUP SYMBOI GRAPHIC LOG** CORE RUN & % RECOVERY LABORATORY TEST DATA NRC ICE TYPE VISUAL ICE % 0 & DEPTH (FI.) DEPTH (FT.) O Water content % ▲ Dry density (pcf) OTHER REMARKS DESCRIPTION Plastic limit 🕂 - Liquid limit TEST DATA 100 120 140 📥 60 80 SOIL soil 100 🖸 60 80 20 40 ۳, 3 ÜF PEAT - coarse fibrous, dark brown Pt GM GRAYEL - silty, orange brown MA, combined ____ coarse to fine, some cmf sand 1 samples 1 - 5 6 = 60% 51 15 0 S = 27% cebbles subrounded to 4" F = 13%2 -2ł (81) 2 ⊕ ١. ٦ 3 -3 ٦ 83 Ð 1 4 occasional cobble to 6" 4 1 occasional ironstone 84 5 θ 5 5 ١ 85 Ð boulder, rounded, 12** at 5.8* 6 Bottom of pit 6 TEST HOLE TEST HOLE No. PROJECT : 13011 1975 BORROW INVESTIGATION FACILITY LOGGED BY R.H. No. 57°51'52''N, 131°54'00''W ELEVATION : LAT. & LONG CHKD R. H. NORTHERN ENGINEERING SERVICES PIPE MILEAGE N75-1060-B2-2 N75 AIRPHOTO No. A 22935-98 DRWN. BY: COMPANY LIMITED G. B. CALGARY ALBERTA AIR TEMP Approx. 24⁰C 9.0. RIG: CHKD ENGINEERS FOR 060 L METHOD : JEST PIT OF SHEET 1 1 CANADIAN ARCTIC GAS STUDY LIMITED D 21 M 08 Y 75 TIME: FINISH : D 21 M 08 Y 75 TIME: START: - B2 - 2 PC-9,5K373

TEST HOLE LOG



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HOLE Z o N75-

1060 - B2 - 3

RW HK	N.E D:	BY:		F.B. 1.0.	R		A 22935-98	. <u> </u>		-+	R TEMI			x. 24 ⁰ C			že L		CALGARY	LIMI	FE.D			N75-1060-B2-
нк				R.H.		AT. & LONG	67 ⁰ 51'53''N, 1	31 ⁰ 53'	12''#	-	VATIO					┣		NORTHER				CES		
OG	GED	BY	':	1. A.H.	F	ACILITY				_	DJECT		1301		•			1975 BORROW	INVES	TIG	TION			TEST HOLE No.
-																								
																							.	
_																							.	-
-																							.	
6-		•	•	8.0		Bottom of pit		+ .					<u>_</u>	+	+ +			· · · · · · · · · · · · · · · · · · ·	+	╀	¥		6.0	Kame-like mound
-																-+-			B5	X			-	18:10
5 -												- 1								Ť.	1		5.0 -	
-		6												<u> </u>					B4				-	1
4-												Ì								\mathbb{N}	1			
		8				on gravel, cobi	les rounded to 8"	'											83	\square			4.0 -	
	64	<u>م</u>)		3.2	GRAVEL		brown, cementation				ļ							(GW-GN)		\bigtriangledown	7		3.2	· · · · ·
3 -		9	ີ. ເຈົ້າ	2 9							-							S = 29% F = 9%		\square	4		3.0 _	17:40
_		4												<u>↓ </u>				Oversize 6.2: G = 62%	82	X	1			
2 -		4				rounded to 4'', loose, dirty	cementalion,							┼╴╎				MA, combined samples 1 - 5	81	Ł			2.0 -	
	GM				GRAVE L	- silty, some fm				-		_								+	7		1.5 -	
1-				1.2		to ¾**, slight pl dry	astic, red-brown,					_			++		_						1 -	
4	SM	- E.S.	I	0.4	SAND -	medium grain, sil		1		-					++									
-	ා Pt		-v.v] 5(PEAT -	coarse fibrous, I	ark brown, dry		UF			-							~~~	N I	-	-		18:50
	SOIL G		SOIL G					ICE 0	NRC ICE	40	6 2		80 40	100 60	126 80		140 ▲ 100 ⊙		SAMPLE TYPE	SAMPLE CONDITION	<u></u>	CORE CONDITION	DEI	
- -	GROUP		GRAPHIC			DESCRIPTIC	N	GRAPHIC LOG	U U				nit ⊣		-1 ligu			TEST DATA	TYPI	l D	CORE RUN & % RECOVERY	N N N	DEPTH (FL)	REMARKS
2	SYMBOL		10 100					Ϋ́	TYPE F %		Drv	dens	ity [pcf	0	ST DA Woter		+ %	OTHER	• 0	Į	Z Z Z	Ĩ	ET.)	

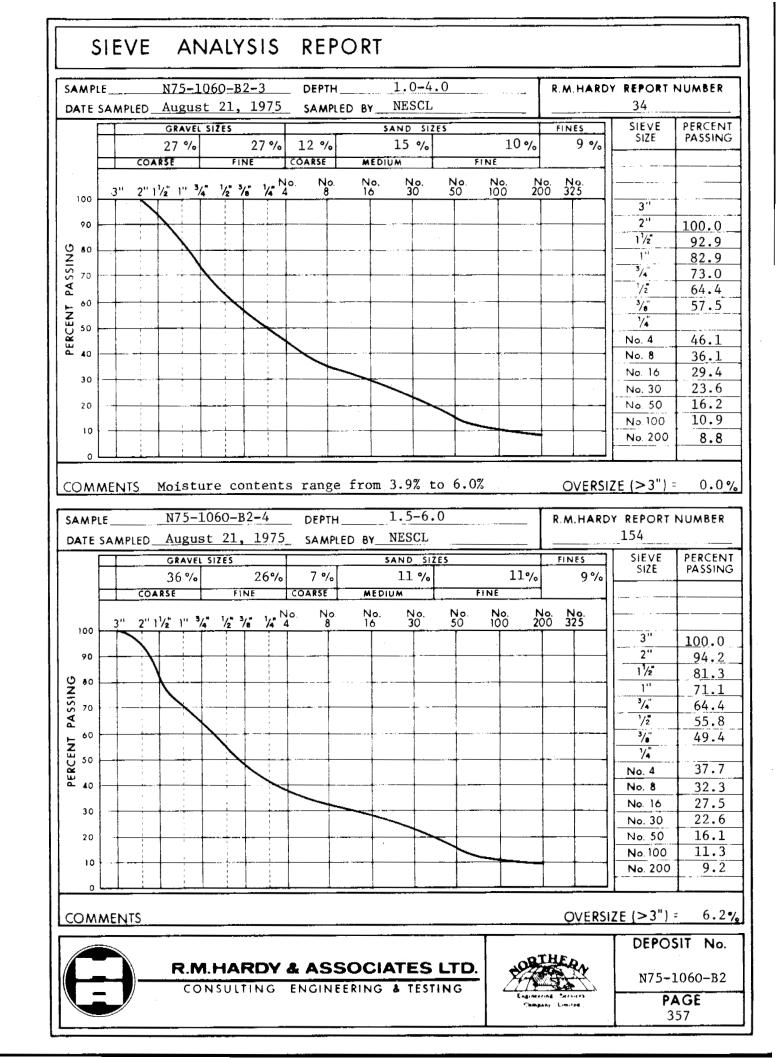
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S	SIEVE A	NALYSIS	REPOI	RT					
	LE N75- SAMPLED Augu	1060-B2-1 st 21, 1975	DEPTH SAMPLED E	1.0-6 NESCL			R.M.HAR	54	NUMBER
	GRAV	EL SIZES		SAND SIZE	ES	I	FINES	SIEVE	PERCENT
	25%	• 28 %	10%	16 %		14 %	7%	SIZE	PASSING
	COARSE	FINE		MEDIUM	Fr		, ,,		
		N			No.		0 N/0		
100	3" 2" 1/2 1"	3/4 1/2 3/2 1/4 N	8 1	No. No. 16 30	50	No. N 100 20	o. No. 0 325		
								3"	100.0
90			<u> </u>			-+		2"	97.8
0 10								1 1/2"	91.9
SNISSA VISSA VISSA								1"	82.0
S 70								3/4"	74.5
. 60								1/2	64.7
I Z								3/8	58.1
1 2 50				<u>├───</u>	-			7.	
			\searrow					No. 4	46.9
								No. 8	38.4
30					_ +			No. 16	31.8
20	_							No. 30	25.3
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10				+				No. 100	8.7
l 。L								No. 200	6.6
1	AMPLED_Augus	<u>1060-В2-2</u> st 21, 1975) 		R.M.HARD	Y REPORT I	NUMBER
		LSIZES		SAND SIZE	5		FINES	SIEVE	PERCENT
	40%		8%	9%		10 %	13 %	SIZE	PASSING
⊦	COARSE	FINE	COARSE M	EDIUM	FI	NÉ			
	3" 2" 1 ¹ /* 1"	1/4 1/2 3/6 1/4 A	D. NO. N	o. No.	No.	No. No. 100 200	No. 325		
100	NIT			, <u> </u>		<u>100 200</u>	325		100.0
90	+ $+$ $+$ $+$ $+$							2"	100.0
								11/2	87.6
l 2 ⁰ ∣					-+			1"	65.5
080	+ $+$ $+$	╉┈╡╎┊╍╉						3/4	60.2
4								1/2	53.4
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10-		<mark>┽┈┆╎┉┊┈╎</mark>						No. 100	16.0
l 。L								No. 200	13.4
COMM	ENTS Moist	ure contents	range from	n 3.5% to	8.3%		OVERSIZ	<u>(>3") =</u>	0.0 %
					Γ			DEPOSI	T No.
		HARDY &				NOBTI	E en	N75-10	60-B2
	_/ CO	NSULTING E	NGINEERING	G & TESTIN	IG I				1

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	OF LABORATORY TE FOR OF AGGREGATES IN		
	2 DATE SAMPLED : August 21, DATE TESTED : January, 1		
SOUNDNESS OF AGG SULPHATE TEST	REGATE	ORGANI TEST	C IMPURITIES
	: LOSS = 3.25 % : LOSS = 12.30 %		R : 2+ EMOVED : Nil
LOS ANGELES ABRAS	SION TEST	COAL & REMOVE	ROOTLETS D : Nil
PERCENT LOSS =	21.5 %		CONTENT : Nil CANCE :
SUMMARY OF ROCK TYPE	ES, COARSE AGGREGATE. (P	ETROGRAPI	HIC ANALYSIS)
ROCK TYPE	CLASSIFICATIONS		TOTAL WEIGHTED COMPONENT %
Quartzite			33.75
Granite	Strong to very strong, Good		12.55
Basalt			0.35
Siltstone	Strong, Good	-	1.55
Limestone	berong, oood		4.55
Chert	Potentially reactive, Fair	ļ	0.3
Flint	resolution reactive, rall		1.9
Sandstone	Weak, Friable, Poor	-	4.85
Soft siltstone			0.25
Clay	Soft, Weak, Poor	ŀ	1.35
Ironstone	1	ŀ	1.2
PN = 192 INTERPRETA	ATION : Poor		62.6
COMMENTS : Chert sand	dstone may be source of aggregat	e instabilit	y.
Limited	CONSULTING ENGINEER		DEPOSIT No. N75-1060-B2 PAGE 358

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1060 - B3 - A 392320E 7510420 N B3 - B 392760E 7511240N

< 1 (1 + 1) (2 + 1) (2 + 1) (2 + 1) (2 + 1)

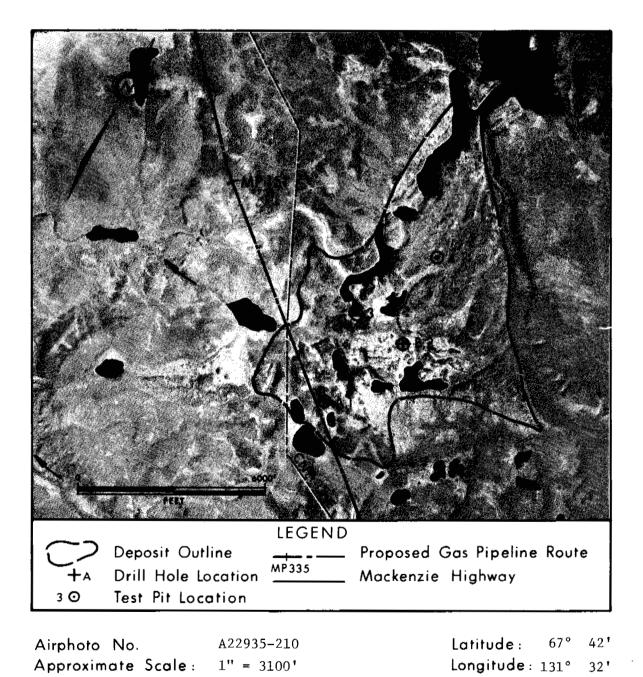
See 1098-1 EBA

Physical Setting: Deposit 1060-B3 is a kame and kettle complex and channeled outwash plain located 3 miles east of Travaillant Lake and crossed by the right of way at milepost 153.

Material: SAND and GRAVEL - interbedded silty sand and gravel.

Volume: 10,000,000 cubic yards.

Assessment: Deposit 1060-B3 is a source of fair to good quality granular material suitable for general fill, backfill, and building pads. Access presents no problem as the right of way crosses the deposit.



DEPOSIT 1060-B3

PHYSICAL SETTING

Deposit 1060-B3 is a kame and kettle complex and channeled outwash plain located 3 miles east of Travaillant Lake. The proposed pipeline right of way crosses the deposit at milepost 153. This deposit corresponds to part of source number 1098 in EBA DIAND Granular Materials Inventory Volume III (1974) report.

The kame and kettle complex at the southern end of the deposit has relief in the order of 100 feet with slopes up to 20 degrees. Relief on the outwash plain is about 15 feet between bars and abandoned channels. Meltwater channels and lakes within the plain are inset about 100 feet below the outwash surface. Except for depressions, the site has very little overburden and drainage is moderately good to good. Peat and silt in excess of 5 feet are found in the depressions which are poorly drained. The active layer ranges from 1 to 8 feet in depth, below this the deposit is frozen with low ice content.

BIOLOGICAL SETTING

The vegetation at the site consists of light to moderately dense tree cover made up of white and black spruce and paper birch, a thick understory of soapberry, willow, alder, ericaceous shrubs and moss. The deposit is located in moose and caribou habitat. It is moderately productive lynx, fox, wolf, and marten habitat. The adjacent lakes appear to offer suitable waterfowl habitat but none were seen during the 1975 survey. Travaillant Lake, approximately 3 miles away, supports several fish species but the small lakes adjacent to the deposit appear to be unsuitable fish habitat. The site is located in an active trapping area.

MATERIAL

Drill hole, test pit logs and the DIAND report indicate that the material in this deposit is interbedded sand and gravel. Both gravel and sand are well graded, but silty. Further drilling would be required to assess material quality in the northern part of the deposit.

VOLUME

A total estimated volume for the kame-kettle complex, based on an area of 500 acres, and an average depth of 30 feet is 5,700,000 cubic yards. A total volume for the outwash plain, based on 600 acres and 10 foot depth over half the area, is 4,300,000 cubic yards. The conservative total volume for the deposit is 10,000,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 1060-B3 is a source of fair to good quality granular materials. Location of areas to be exploited will be dictated by haul distances, overburden thicknesses, insitu material quality, and material requirements. Granular material from this deposit may be used for general fill, backfill in pipeline construction and building pads.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Since the pipeline right of way crosses the southwest corner of the deposit, access is not a problem and haul distances will be short. Snow roads would be constructed to transport the borrow material from the deposit to haul points on the pipeline right of way. Vegetative cover would have to be removed or disposed of in accordance with land use regulations. Overburden is negligible at this site, thus very little stripping and stockpiling will be necessary in the excavation area.

Development of this deposit would involve excavating borrow material evenly from the higher, well drained areas so that good drainage would be maintained over the area. A perched water table exists in flatter areas and will have to be considered in development. Open face excavations could be developed along the steep slopes within the deposit. Smaller areas would be developed by this method and less clearing would be required. Excavations would be kept away from adjacent lakes to minimize siltation. Either type of development could be accomplished by using blasting or conventional earthmoving techniques. The excavated material may have to be stockpiled, thawed, and drained before it is used.

Equipment required for development would be dozers, rippers, end-dump trucks and front-end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

	DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		D	ESCRIPTIC	о		ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	4 0 0	LA Dry de Plastic 60 20	ensity (pcf) D	οw	DATA ater con Liquid 120 80	ntent limit 1.	% 40 ▲ 00 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS	
ſ	_	Pt	AL AN	1.5	PEAT- fine fi inclusi	brous, amor ons, black	phous, wood		×4.	ŬF															4½'' Waimac bit	17:21
	2 -	WL		4.0		fine gravel onal coarse c, pebbles t	gravel, lor	4.0		Yx Yr														-		
	4-	6 M			GRAVEL- COST	se, very sil	ty, sandy			Nb																
	6 -	SM		6.0	SAND - fine to	nedium, ve Fravel	•]																	
е 1 1	- 8 - - 10 -			11.0		avel, trace se, fine pe onally coars	obles,	um																-	37/8** Walmac bit	t 17:43
	12 -	31			GRAYEL - COBT trace to 1/	cosrse, pe																				
TEST HOLE	18			18.0	I sa cupe	·····-						JECT :		130 11										-	TEST HOLE No.	
51-		GED B		<u>).X.W.</u> .Y.	FACILIT		67°41'26	''N, 131	⁰ 32'4	8''#		ATION							1975 BORROW IN	ESTI	ĜATI	ON				
		N. BY	. 4	.W.	AIRPHO RIG : METHO	DTO No. :	A 22935- HEL1-DRI AIR	209			L	MILEAG	E:	18 ⁰ C				20		ENGINE MPANY CALGARY ENGINE	LIMITI	E.D.	ES		N75-1060-B3	8-A
	STAR			21	M 8 Y 7			FINISH		D 2	1 M	1 8 1	Y 75	TIME	: 18:4	5		CAN	ADIAN ARCTIC G	AS ST	JDY	LIMITE	D		SHEET I OF	2

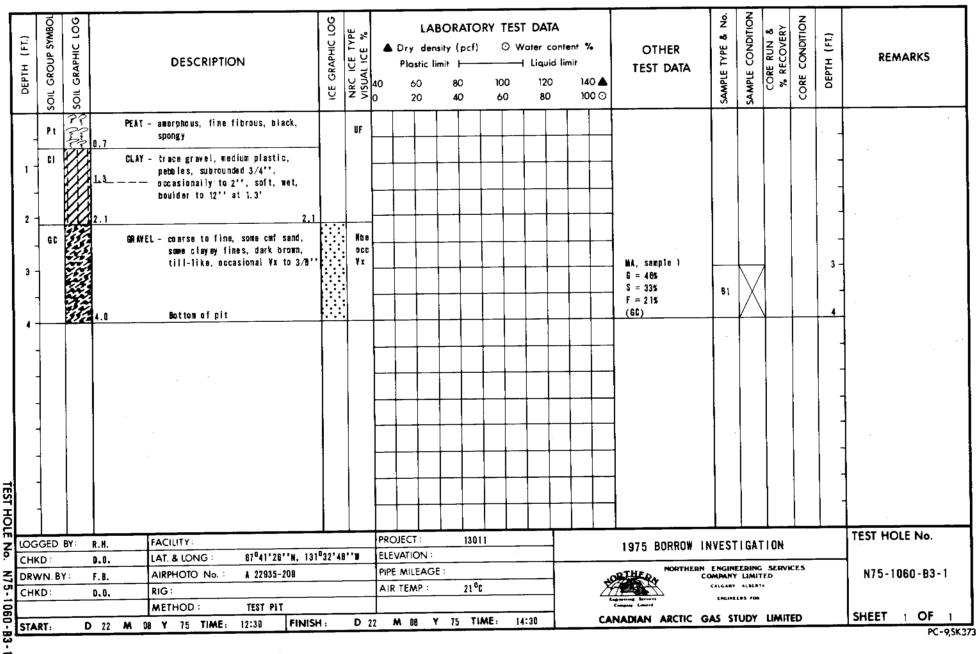
- 364 -

500	DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTIC	N	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	LA Dry der Plastic 60 20	nsity (p	cf}	ΟW	DATA ater cont Liquid li 120 80	mit 144	, 0 ▲ 0 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FI.)	REMARKS
×	16 - 18 -	SC		SAND –	very fine to medium coarse gravel, mois		+ + + + + + + + + + + + + + + +						-									-	3 7/8'' Walmac bit 10:00
	20 -			21 <u>.0</u>			+ + + + + + + + + + 0 + +	₩x														-	3 7/8** Tricone 18:20
	22 -	GM		23.0	L- coarse, and coars angular 		-	F														-	
	24 -	SM 			to 1.5" in upper 3	3.0'					:								-			-	
	26 - - 28 -			28.0 Sut	sandy, fine to med	ium Inwintastic																-	
F. TEST	1			29.0	nd of hole																	29.0	18:45
HOLE	LOGO	GED 1	3Y :	J.K.W.	FACILITY				PRO.	JECT :	13	011					1975 BORROW II		LĒAT			-	TEST HOLE No.
No. N75-106	снк	D : /N. BY	:	D, V. A.M. D. O.	LAT. & LONG : AIRPHOTO No. : RIG : METHOD :	67 ⁰ 41'26''N, 131 ⁰ A 22935-209 Heli-Drill Air	D ³ 2'48	''₩	PIPE	ATION : MILEAGI TEMP :		3 ⁰ C				TO	NORTHERN		ERING LIMITE	SERVIC	ES		N75-1060-B3-A
1060 - B3	STAR	शः	D	21 M 8	Y 75 TIME:		1:	D 2	1 M	1 B Y	75	TIME	1 8: 4	5		CAN	IADIAN ARCTIC G	AS ST	UDY	LIMITE	D		SHEET 2 OF 2 PC-9,5K37

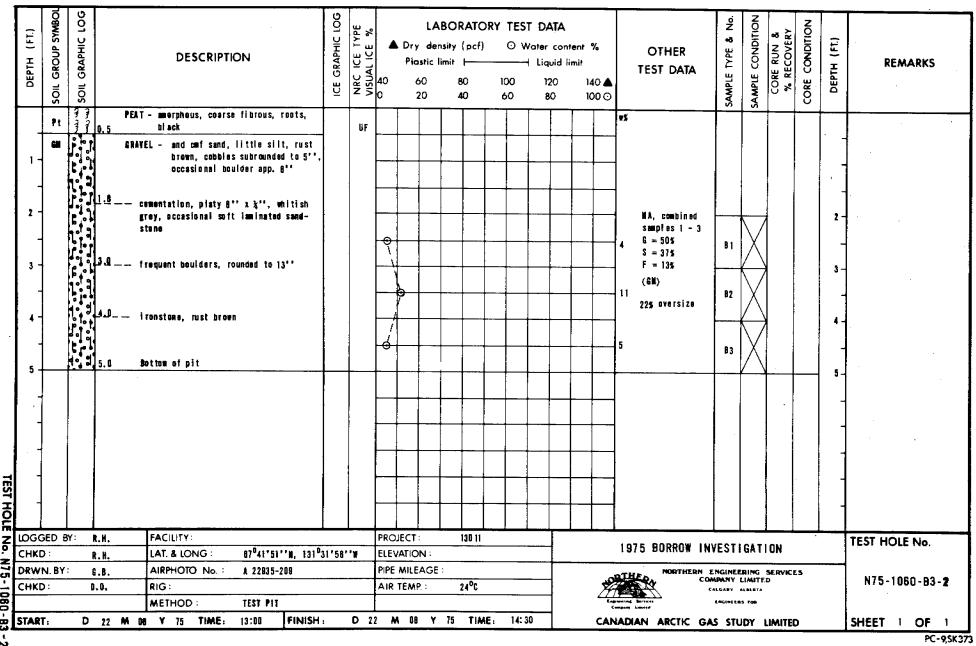
- 365 -

DEPTH (FT)	SOIL GROUP SYMBOI	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	▲ D: P 40 0		ORATO ity (pcf) nit BO 40	Ο \	T DATA Vater co H Liquid 120 80	ntent % limit 140		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
		ို့ရစ္ဦ		fety thin peat cover		UF									1					4¼'' Walmac bit
2-	GNi		GRAVEL	L-fine to coarse, some fine to coarse sand, little silt, light brown, cobbles to 4°1.								•								removed 8° cobble cobbles and large pebbles falling into 1 hole.
4				large cobble or small boulders End of hole															4	to 4%" rock bit. Hol going askem.
5				drilf rig positienad en top of sambi mound, possibly kame. Cobbles, boulders exposed at surface.																At 5.0' depth hole is approx. 12'' diameter with subsequent loss fallure of air circulation.
	GED E	BY: p	¥.¥	FACILITY			PROJEC	.T: 1	13011					1975 BORROW		TIÈ		<u> </u>	1	TEST HOLE No.
СНК		0,		LAT. & LONG : 67º41'51''H, 131º31'5	6''¥		ELEVAT													
DRW CHK	(N. BY D :	: A. D.		AIRPHOTO No: A 22935-209 RIG: HEL1-DRILL			PIPE MI AIR TE	LEAGE : MP. :	lpprox. 1	9 ⁰ C			<u>an</u>		ENGINE MPANY CALGARY ENGINEE	LIMIT	F.D	25		N75-1060-B3-B
				METHOD : AIR									c	ompany Limited						SHEET I OF I

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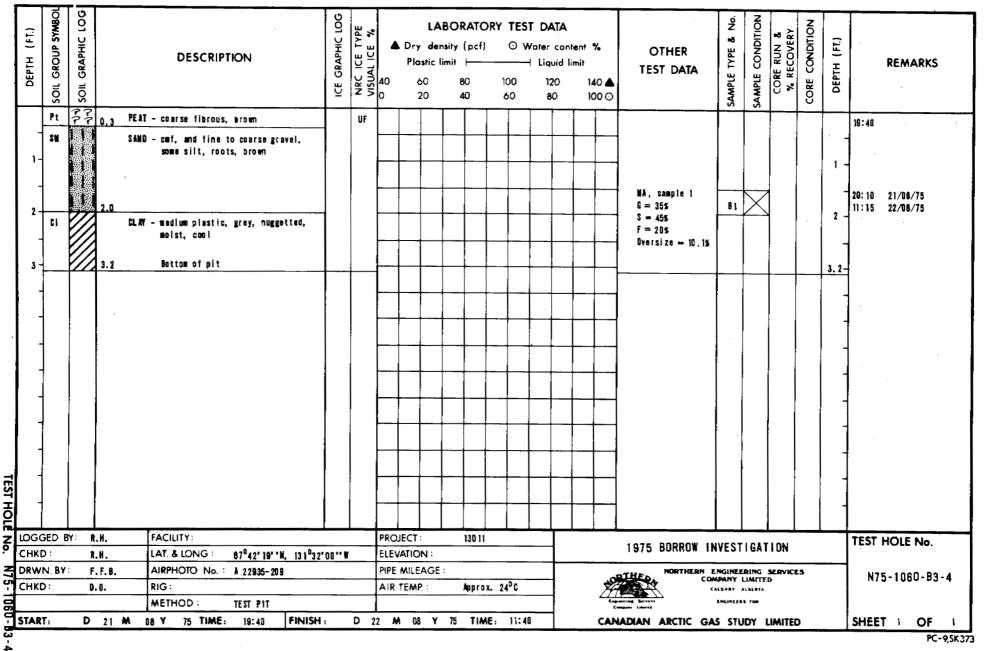
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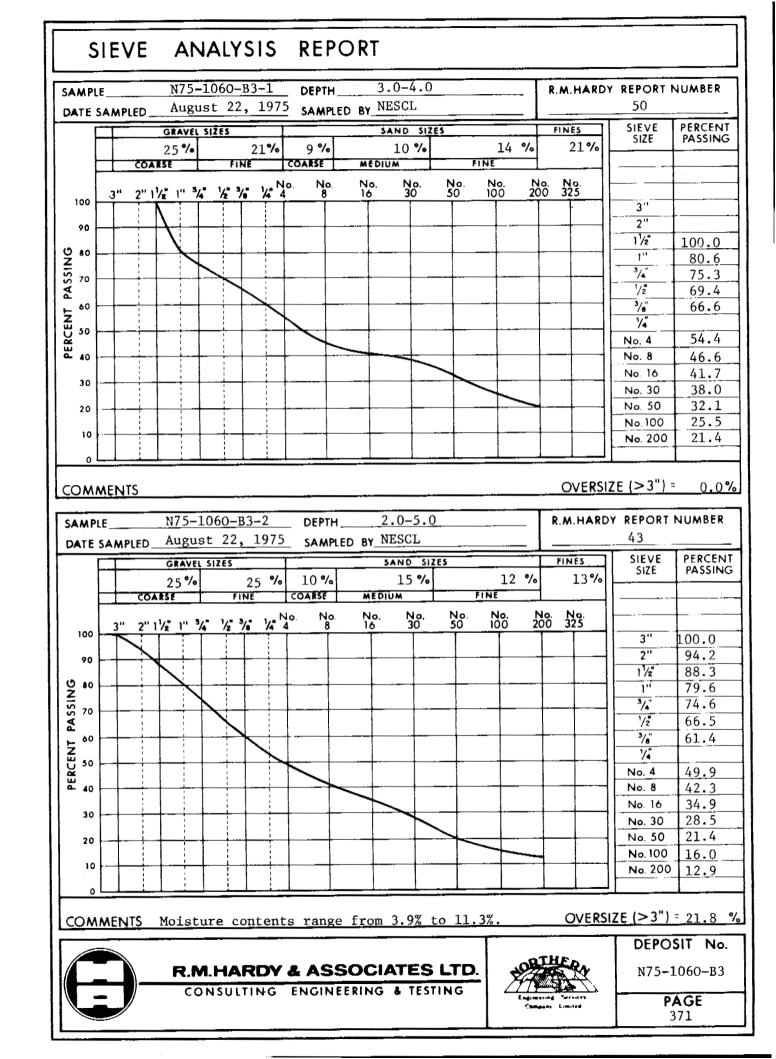
DEPTH (FT)		SOIL GROUP SYMBOL	SOIL GRAPHIC LOG	<u></u>	DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Dry	densi tic lin 0		cf)		Wate - Li		ent % mit 140		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
	_	Pt	37777	0. B	amorphous, fine fibrous, dark brown		UF					-												Ho samples taken
		+	N- N- N-	PEAT-	with silt (organic)non-plastic, 1.0 black, occasional organic inclusion to depth of 1.5°, then numerous,1.5	4::	NDB OCC. YX																-	
	2 +-		77	<u>2.0</u> I CE -	inclusions clear ice to ¼'' 2.0 clear (85%) with S1LT (organic), black	+ +	25			-					-				-				-	
	3 			3.0	Bottom of pit	1.1.1. 1.1.1.1. 1.1.1.1.1.1.1.1.1.1.1.1					-								1				3.0	Abandon ed
	_													+							-		-	
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				. '								_			-	-		•					-	
	-																	-						
TEST							-																	4
5	4			!													•							· · · · · · · · · · · · · · · · · · ·
		ED (BY:	R. H.	FACILITY			PR	OJECT	[: [:	1	3011						1975 BORROW IN	IVEST				_	TEST HOLE No.
	HKC			D.O.	LAT. & LONG : 67º 41' 55' 'N. 13	1 ⁰ 32'4	1'''		EVATIO									NORTHERN						
~		N. BY	1:	A.M.	AIRPHOTO No. A 22935-209			_	PE MIL						_			C C	OMPAN	Y LIMI	TE.D			N75-1060-B3-3
-1060	нк): 		D.O.	RIG				RTEN	1P.:		upp ro	x. 10 ⁰	և			4	ingineering Services		LENS FOR				
	TAR				METHOD : TEST PIT 08 Y 75 TIME: 11:45 FINIS		D	22	M	08 Y	75	TIA	Ne:	12:15			CA	NADIAN ARCTIC G	AS S	TUDY	LIMI	TED		SHEET 1 OF 1 PC-9.5K3

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				A	ugu	st		L,_		-		TH_		1.5- NESC		0		•••••		R	. M . F	AR	DY RE 77	POR	NUA	ABER
			(0)	ARSI	8°/	_	51 2 E	S FIP		%	12ª			18 °		5	FIN		5 %	F	1NES 20	%	5	IEVE SIZE		RCENT SSING
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CON SAM DATE	_ PLE_					1 51	ZES			%		PLED		ND S	<u></u>					R./	N.H.		Y REF		NUM	BER
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NT PASSING 00 00 00					1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1								 <u></u>			-							1 1 3/. 1/ 3/.	4 2		
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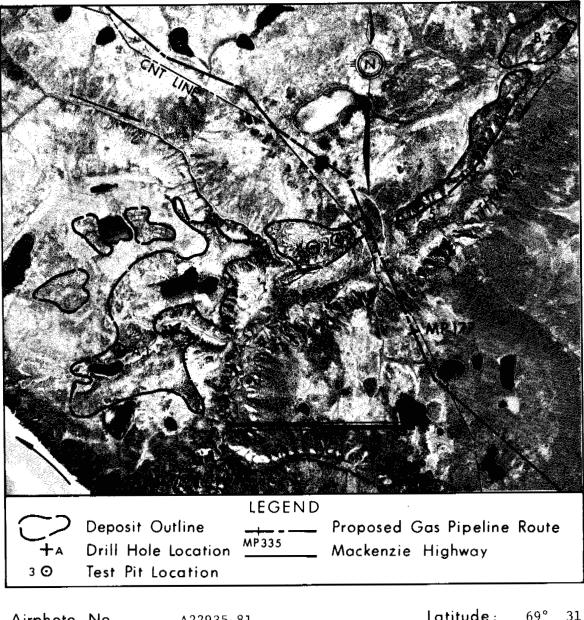
Deposit 1060-B4 consists of an eroded kame terrace, an Physical Setting: outwash plain and a fluvial terrace along the western edge of Thunder River canyon and is crossed by the proposed pipeline at milepost 174. Material :

SAND - fine to medium, with a varying silt content.

Volume : 13,000,000 cubic yards.

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Deposit 1060-B4 is a source of fair quality granular Assessment: material suitable for general fill and backfill. Hau1 distances to the right of way are up to 2 miles.



Airphoto No. A22935-81 Approximate Scale: 1'' = 3050' Latitude : 69° 31' 53' Longitude: 130°

DEPOSIT 1060-B4

PHYSICAL SETTING

Deposit 1060-B4 is a combination of remnants of an eroded kame terrace, an outwash plain and a fluvial terrace. It extends from 1 mile north of the Thunder River and Mackenzie River confluence in a northerly direction along the western edge of the Thunder River canyon. The proposed pipeline right of way crosses the centre of the deposit at milepost 174. This deposit corresponds to source numbers 1084 and part of 1089 in EBA DIAND Granular Materials Inventory Volume III (1974) report.

The southern portion of the deposit consists of fragments of an outwash plain with a flat to gently sloping surface. Channels have been incised into the outwash to depths of 30 feet.

The middle of the deposit consists of fluvial terraces formed during postglacial excavation of the Thunder River valley. These terraces stand 150 to 200 feet above the river valley and 50 to 100 feet below the level of the upland, and are separated by steep scarps. Their upper surfaces slope gently to the east. Some gullies have formed perpendicular to the valley, but are presently inactive.

The northern segment of the deposit is either an esker, or more likely, an eroded kame terrace that parallels the Thunder River canyon. It is defined by a 300 foot scarp on the river side and a 50-foot scarp on the upland side.

All parts of the deposit are moderately to well drained with negligible overburden, except for some of the abandoned channels where peat and silt cover is thicker and drainage is poor. The active layer varies from 1 to 8 feet and is deepest in well drained areas. Generally, ice content is low although a few ice lenses were encountered in drill hole 1060-B4-A. A deep gully separates the southern part of the deposit from the pipeline right of way.

BIOLOGICAL SETTING

Vegetation at this extensive site consists of white spruce, black spruce, paper birch, Labrador tea, lichen, and moss. In the better drained areas, spruce reach heights of 50 feet or more while stunted spruce, shrubs, and sedges are more prevalent in imperfectly to poorly drained areas. Banks of the Thunder River valley provide good denning habitat for bear and other denning species. The general area is used by caribou, marten, lynx, fox, snowshoe hare and wolf. Year-round habitat is available for moose. Several well-used game trails cross the site. Bear, snowshoe hare, and red squirrel sign were observed during the 1975 survey. Nearby lakes and streams provide suitable habitat for aquatic furbearers and waterfowl. Waterfowl are most numerous during the April to May period when they congregate on the Mackenzie River. No raptor sign was observed in the area although potential habitat is available. Grouse and ptarmigan are common in the area. The Thunder River supports populations of grayling, lake trout, round whitefish, broad whitefish, pond smelt, pike and longnose suckers.

MATERIAL

The material in this deposit is mainly fine to medium sand with varying silt content. Occasional thin, poorly graded gravel beds are scattered throughout the section.

VOLUME

In the southern section of the deposit the drill hole log shows 20 feet of sand without excess ice and a further 5 feet of icy sand before encountering silt and clay. A conservative volume estimate of 4,300,000 cubic yards is based on a depth of 15 feet and area of 300 acres. Granular material in the two northern parts of the deposit is probably in excess of 50 feet thick. A very conservative depth of 20 feet and area of 300 acres gives a total estimated volume of 8,700,000 cubic yards.

The combined volume of the whole deposit is conservatively estimated at 13,000,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 1060-B4 is a source of fair quality granular materials. Location of areas to be exploited will be dictated by haul distances, overburden thicknesses, insitu material quality, material requirements, and any required protection of the Thunder River valley environment.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the deposit with equipment may be achieved by barge to Thunder River, and overland via the pipeline right of way, from there to the deposit. In order to minimize environmental damage, snow roads would be built to transport the borrow material from the deposit to haul points on the right of way.

Tree and vegetative cover will have to be removed and harvested or disposed of in accordance with land use regulations. Overburden is negligible, therefore little or no stripping will be required.

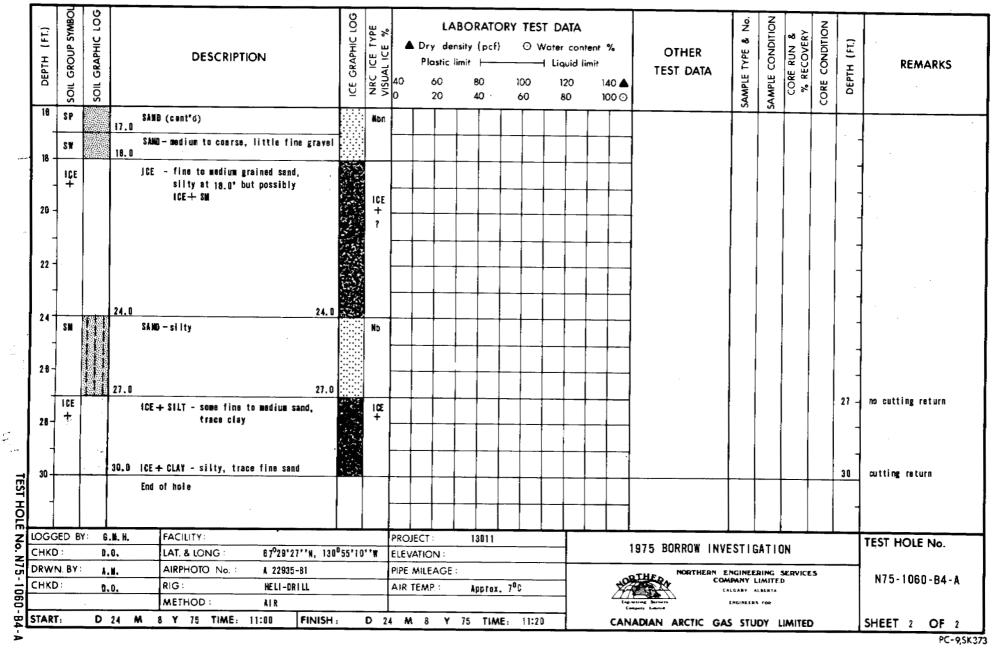
Development of this deposit would involve excavating borrow material evenly from the higher, well drained areas to a grade that would maintain good drainage over the area. Open face pit development could be established on the steep slopes within the deposit. Either type of development could be accomplished by conventional earthmoving techniques since drainage is generally good and ice content low. Excavations will be kept away from lakes and the Thunder River to prevent siltation. Granular material from this deposit may be used for general fill and backfill in pipeline construction. The excavated material may have to be stockpiled, thawed, and drained before it is used.

Equipment required for development would be dozers, rippers, end-dump trucks and front-end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

DEPTH (FT.)		SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0		nsity (p	100			OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FL)	REMARKS
_			रय	0.5 <u>P</u>	EAT cover	1	UF							· · · · ·			1			
2	1	SP			AND - fine to medium, trace silt, light rust brown, moist	t													-	
	-				grey brown, less silt3.5	0.00	Hbo.												-	. Nearby test pit froze at depth 4,6"
4	-			6.0	damp when thawed		Nbn 												-	
8	-	211			AND -silty, grey														-	
10	-	SP		<u>10.0</u> s	AND-fine to medium, fairly clean		· · · · · · · · · · · · · · · · · · ·												-	
12	-			12.0	trace silt														-	
14 _16																				
ιo	GG	ED E	BY :	6.1L H.	FACILITY			+	JECT :		301 1			1975 BORROW IN	VESTI	GAT	ON			TEST HOLE No.
-		1: N. BY		<u>D.C.</u> A.W.	LAT. & LONG 87 ⁰ 29'27''N, 1 AIRPHOTO No. A 22935-81	30°55'	<u>10''₩</u>	+ …	MILEAC					OTHES NORTHERN	ENGINE	ERING	SERVI	CES		N75-1060-B4-A
	HKD		•	D.O.	RIG: HELI-DRILL			+	TEMP		pprox. 7 ⁰ C		<u>to</u>		CALGARY					
ST/					METHOD: AIR 8 Y 75 TIME: 11:00 FINISI	 H .		24	M a	Y 15	TIME: 11	:20	לי האר	NADIAN ARCTIC G			LIMIT	ED		SHEET 1 OF 2

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	DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG	~	DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40		densit tic lim	ty (pcf)		ST DA Water - Liqu 12 8	conte uid lir 20			SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FL)	REMARKS
-			11	pe	eat cover 0,1° thick on surface												1				a	4%'' Walmac bit
i.	-			SAND - f	ine, silty, light brown		UF	-								- ·					· -	-
	2 -	SM		2.0					$\left \right $		_					4			1		-	
					edium-grained,clean, trace fine <u>3.0</u> sand, light groy brown			 			_											ļ
					aun, ittir Riet ninni		Nb			ĺ											ļ	
	4	SP																			_	
	-							<u> </u>								-					-	
	8				stratified visible			ļ		_						-					-	-
				7.0	ice layerin one																	
		SC 7		8.0	coopie piece of clay return		¥s														- 1	Te new 3 7/8'' Weimac bit.
ж. Д. н.	• •	CL		CLAY-s	ilty, and fine to coarse gravel, ebbles average %''		Nb									•					-	
	10		(22	<u>. 10,0</u> Sand M	edium, trace silt.																-	
17		-																				
	12 -	SP																			-	
	-								\vdash				+	-+							_	
_	14 -			14.0																		drill ababbar 15,95
TEST HOLE	19	6P		GRAVEL-	-coarse, some medium sand, trace clay]					14 -	drill chatter 15:35
- 7	-		ີເຈິ	GRAVEL-	to 14,9° - fine, fairly clean									\rightarrow		1					-	
	16		<u>,</u> ^ ^ _					0.0.0									L					
Ş		GED B	-	1. M. H). Y.	FACILITY LAT. & LONG 67°32'32''N, 130°50'	13''¥		<u> </u>	JECT : /ATION		13011			{		1975 BORROW	INVE	STIC	GATIO	N		TEST HOLE No.
N75		N. BY		L.N.	AIRPHOTO No. : A 22835-81	. ч т		+	MILEA							NORTHERN E	MGINE	RING	SERVIC			
	снк):).0.	RIG: HELI-DRILL			AIR	TEMP	:	Approx.	21 ⁰ C			₩ ¥		APANY Algary		D			N75-1060-B4-B
8					METHOD AIR]		genering Services Company Landed	ENGINELI	15 FOR				
Ē	STAR	T:	D	22 M 08	Y 75 TIME: 15:15 FINISH	:	D	22 N	A 08	Y 7	5 TI M	E: 18	i:30		CAI	NADIAN ARCTIC GA	s stu	IDY	LIMITE	D		SHEET 1 OF 3 PC-9,5K3

PC-9,5K373

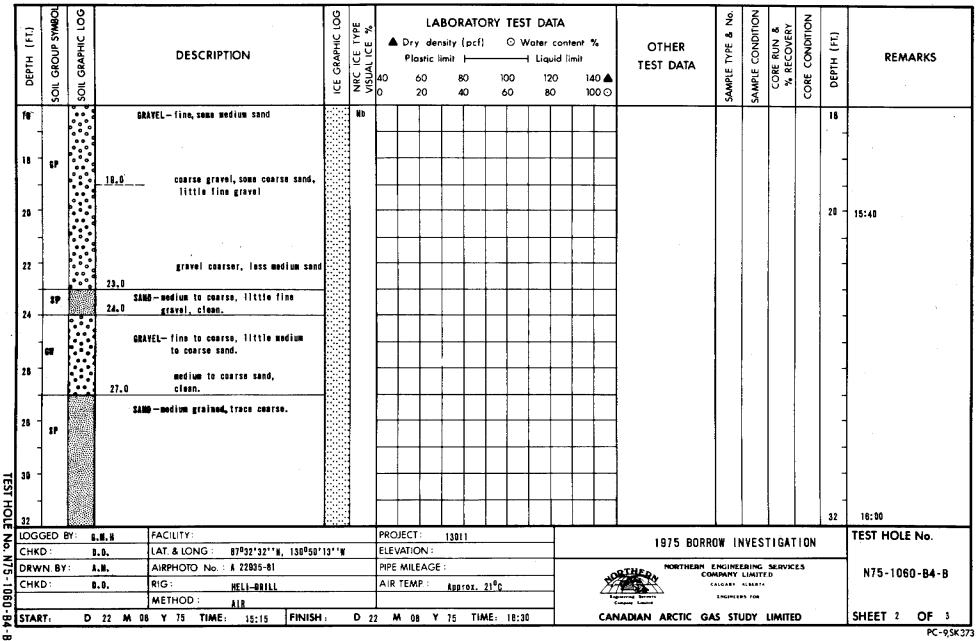
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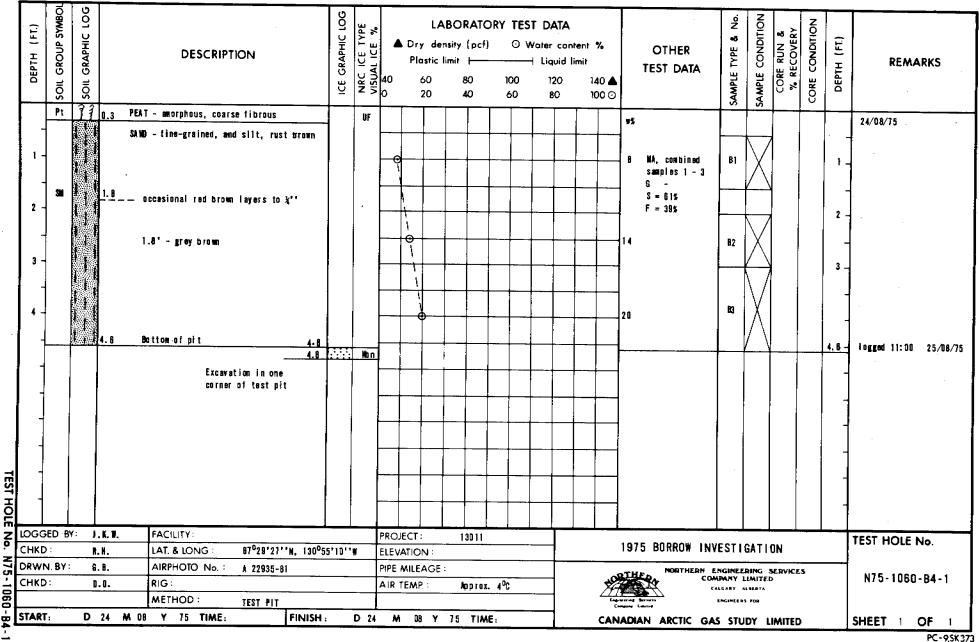
106 ŝ SAMPLE CONDITION **GROUP SYMBOI** ICE GRAPHIC LOG CONDITION NRC ICE TYPE VISUAL ICE % LABORATORY TEST DATA CORE RUN & % RECOVERY (FT.) -8 DEPTH (FL) GRAPHIC ▲ Dry density (pcf) ○ Water content % SAMPLE TYPE OTHER DESCRIPTION REMARKS DEPTH Plastic limit |---- Liquid limit TEST DATA CORE 60 80 100 120 140 📥 SOIL SOIL 20 40 80 100 🔿 60 32 SAND 32 N b SP 34 medium grained, little course 38 grained. New 3 7/8'' Walmac, 38 -38 approx. 3' of leose sand in the hole. 40 42 End of hole 44.0 44 18:30 44 Stem difficult to withdraw, end of hole. TEST HOLE TEST HOLE No. FACILITY PROJECT : LOGGED BY 13011 No. G.N.H 1975 BORROW INVESTIGATION ELEVATION : CHKD : D.9. LAT. & LONG : 87°32'32''N, 130°50'13''W N75 -AIRPHOTO No. : PIPE MILEAGE : NORTHERN ENGINEERING SERVICES DRWN. BY: A.N. A 22935-81 N75-1060-84-8 COMPANY LIMITED CHKD D.O. RIG : HELI ORILL AIR TEMP : Approx, 24°C CALGARY ALBERTA 1060 EMGENEERS FOR METHOD : AIR SHEET 3 OF 3 CANADIAN ARCTIC GAS STUDY LIMITED D 22 M 08 Y 75 TIME: 15:15 FINISH : D 22 M 08 Y 75 TIME: START: 16;30 84

TEST HOLE LOG

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PC-9,5K373



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001 SAMPLE CONDITION ŝ ICE GRAPHIC LOG **GROUP SYMBO** CONDITION NRC ICE TYPE VISUAL ICE % 0 b CORE RUN & % RECOVERY LABORATORY TEST DATA (FT.) (FT) -8 GRAPHIC ▲ Dry density (pcf) 🛛 🏵 Water content 🐐 SAMPLE TYPE OTHER REMARKS DESCRIPTION DEPTH DEPTH Plastic limit |-- Liquid limit TEST DATA CORE 60 80 100 120 140 📥 SOIL SOIL 100 🖸 20 40 60 80 33 UF Pt 0.3 PEAT No samples taken SM SAND - fine-grained, trace clayey silt —— trace gravel to 3'', dilatant 2 -3 -GRAVEL - some sand, fine-grained, peoples to 1"', subrounded 4.2 4.5 Possibly a pocket of GP ີ່ຈັ 4.5 Bottom of pit gravel Fine sand TEST HOLE TEST HOLE No. PROJECT : 13011 Z_o FACILITY LOGGED BY: ¥. ¥. 1975 BORROW INVESTIGATION ELEVATION : LAT. & LONG : 67⁰30'21''N, 130⁰53'10''W CHKD R. H. NORTHERN ENGINEERING SERVICES N75-PIPE MILEAGE : A. K. AIRPHOTO No. : A 22835-01 DRWN. BY : N75-1060-B4-2 COMPANY LIMITED AIR TEMP. : Approx. 21⁰C * CALGARY ALBERTA CHKD: RIG : D.O. ENGINEERS FOR 060-B4 METHOD : TEST PIT CANADIAN ARCTIC GAS STUDY LIMITED SHEET 1 OF FINISH : D 22 M 08 Y 75 TIME: 08 Y 75 TIME: START: D 22 M PC-9,5K373

TEST HOLE LOG

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วี่	Vay SOIL GRAPHIC	P	DESCRIPTION EAT - amotphous, fine fibreus, woody	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Dry der Plastic I 60 20	nsity {pol limit) © 100 60	(i)	er contr iquid lir 120 80	nit 14(OTHER TEST DATA	SAMPLE TYPE &	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FL)	REMARKS
	~		inclusions, dark brown AMD - medium to fine, silty, rust brown		UF Non									MA, samapie 1 G = 2.45 S = 835 F = 135	B1					probable iron exides
		1.2	ND - medium grain, trace coarse, non- plastic, brown, clean " 1½" leyer with organic silt at 3.2" Bettem of pit											11 A, combined samples 2 & 3 G = 9% S = 95% F = 6%	B2 B3	X			3	Difficult to excavate from 1.5°
			Rofor elso ta drillhalo 175-1888-84-8 approximatoly 25' N.W. of test pit																	•
BY:			FACILITY: LAT. & LONG : 87 ⁸ 32'32''#, 130 ⁰	50'13'	'₩	ļ		130 1 1						1975 BORROW IN	IVEST	I GAT	1 ON		_	TEST HOLE No.
3Y :	F.	.9.	AIRPHOTO No. : A 22835-81 RIG : METHOD : TEST PIT			PIPE M	ILEAGE	24 ⁹ C			-			co co	MPANY I	LIMITE.	SERVICI D	E S		N75-1060-B4-3
	BY	PAR BY: R. R. Y: F.	P 0.5 0.5 2 1.5 2 2.5 3 3.2 3 4.0 4 BY: R.M. R.M. R.M. Y: F.B. 0.0. 0	PEAT - amorphous, fine fibrous, woody 0.5 inclusions, dark brown SAMD - medium to fine, silty, rust brown 1.5	PEAT - amergahous, fine fibrous, woody 0.5 inclusions, dark brown SAMD - medium to fine, silty, rust brown 1.5 medium to fine grained, some fine, 1.5 gravel (ta ½*')little silt, gray, well banded by ice 2.5 SAMD - medium grain, trace coarse, non-plastic, brown, clean 1.2	PEAT - amorphous, fine fibrous, woody inclusions, dark brown UF SAMD - medium to fine, silty, rust brown 1.5	PEAT - amorphous, fine fibrous, woody UF 0.5 inclusions, dark brown SAMD - medium to fine, silty, rust brown 1.5	PEAT - amerphous, fine fibrous, woody inclusions, dark brown UF SAMD - medium to fine, silty, rust brown UF 1.5	PEAT - amorphous, fine fibrous, soudy inclusions, dark brown UF SAMD - medium to fine, silty, rust brown UF 1.5	PEAT - amorphous, fine fibrous, soody inclusions, dark brown UF SAMD - medium to fine, silty, rust brown UF 1.5	PEAT - amorphous, tine fibrous, woody inclusions, dark brown UF UF SAMB - medium to fine, silty, rust brown UF UF 1.5	PET - am randous, time fibreus, woody inclusions, dark bram UF UF SAMD - medium to fine, silty, rust bram UF UF 1.5	PEXT - amorphous, tine fibrous, soody inclusions, dark brown UF UF SAMD - medium to fine, silty, rust brown inclusions, dark brown UF UF 1.5 medium to fine, silty, rust brown grawi (ta %")little silt, groy, will banéed by ice Wn UF 2.5 SAMD - medium grain, trace coarse, non- plastic, brown, clean Wn UF UF 3.2	PEXT - amorphous, tine fibrous, woody inclusions, dark prown UF UF SAMD - medium to fins, grained, some fine, J.S. grawi (ta 3*')little slit, grey, well banded by ice WF WF J.S	PEXT - sam rabeus, fine fibrous, sondy inclusions, dark brown UF M., sample i SMB - medium to fine, silty, rust brown UF M., sample i 1.5	PEAT - amonbast, fine fibrous, wordy B.5. UF Mail among and the set of the	F617 - am synbacs, fine fibrois, seedy inclusions, dark bram UF Image: Constraint of Constraint	F617 - am yrhos, fife fibrus, wedy inclusion, dark prom UF Image: Constraint of the provided and promised and pro	PEXT - marphotos. files filteres, seedy inclusions, dark brow UF Image: Construction of the period of the per	PET - marganos. The fibres, sondy inclusions, fack brain SAMD - medium to fine, silty, rust brown UF UF M., sepin 1 1.1

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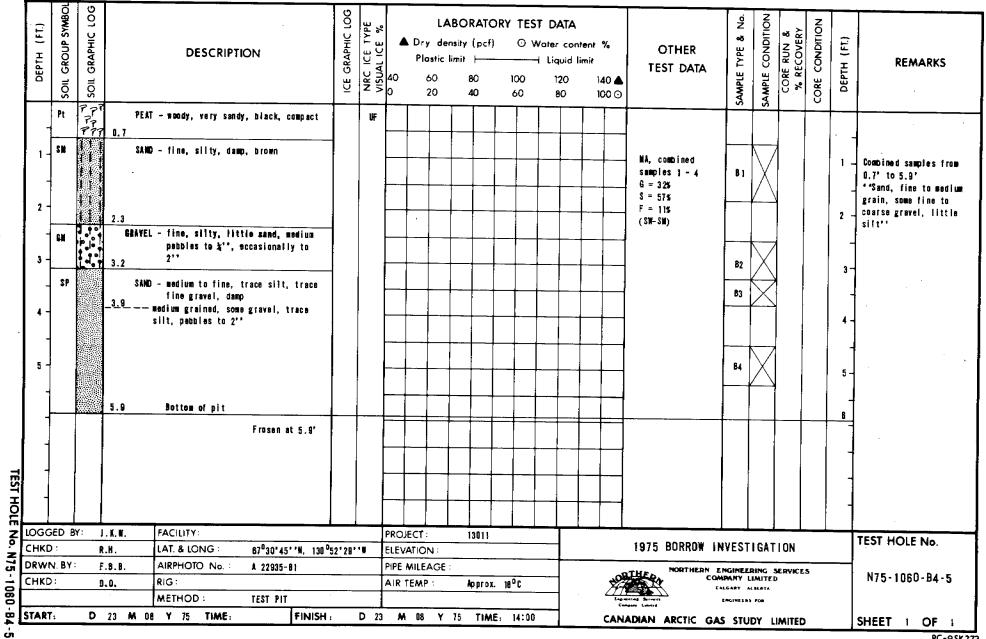
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DEPTH (FT)			SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0		dens tic lir D	SORAT(sity (pcf nit — 80 40		Water — Lia	r cont		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FI.)	REMARKS
┢─	P		77	0.2 PEAT -	coarse, fibrous, roots		ÜF		Ī													
1				GRAVEL	- and sand, medium, silty, rust brown, dry, cobbles to 5", rounded																· -	
			ູ້ໃຈໃ	2.0										_		MIA, samaple 1		<u> </u>			2 -	combined horizons
2	n.	6₩		GRAVEL	- little sand, medium grain, peobles to 1½", transition to medium, coarse, fine, little											ши, semple t G = 30% S = 64% F = 6%	B1	\mathbb{X}			-	SAND, mcf, some gravel
3			١,	34ND -	gravel			-						+		(SW)		╟	X		3 -	combined SAND, cmf, some grave!
				3.5			1									MIA, complined samples 2 - 4	82	V			-	
	s	SW			medium grain, some gravel to 1½'',					ĺ						6 = 23%		$ \rangle$			4 -	
1					clean, moist, 100se											S = 72% F = 5% (SW)	B3				-	
5	i -			<u>5.5</u>	d amp												B4	\mathbb{N}	K		5 -	
	1				Bottom of pit								i					V	\backslash		6	
6	8+-			<u> </u>	Frozen at 6.0'		F														-	
	1]
,	-		ļ						†					1	+							
				1				-	+		+-+				╁╌╂┈╼						-	1
2																						
10	GGE	ED	BY :	R. H.	FACILITY:			_	OJECT		1 30	<u>111</u>				1975 BORROW I	NVEST	F I GA	TION			TEST HOLE No.
	IKD			R. H.	LAT. & LONG : 67°30'14"'N, 130	⁰ 53'21	<u>1''W</u>	-+	EVATIC							NORTHERN	ENGIN	EERIN	SERV	KES		N75 1000 04 4
~		N. BY		F.B	AIRPHOTO No. : A 22935-81	. <u> </u>		-			21	00		-	Ŕ	CTHE OA	CALGARY	r LIMI	TED			N75-1060-B4-4
는	IKD			D.O.	RIG: METHOD: TEST PIT										<u>[]</u>	deserved Servers Company Limited	E MGI MI	LERS FOR				
<u>i</u>	ART				8 Y 75 TIME: 20:15 FINIS	H :	D	22	M 0	8 Y	75 1	IME:	21:20	-	CAI	NADIAN ARCTIC C	AS S	TUDY	LIMI	FED		SHEET I OF I PC-9,5K

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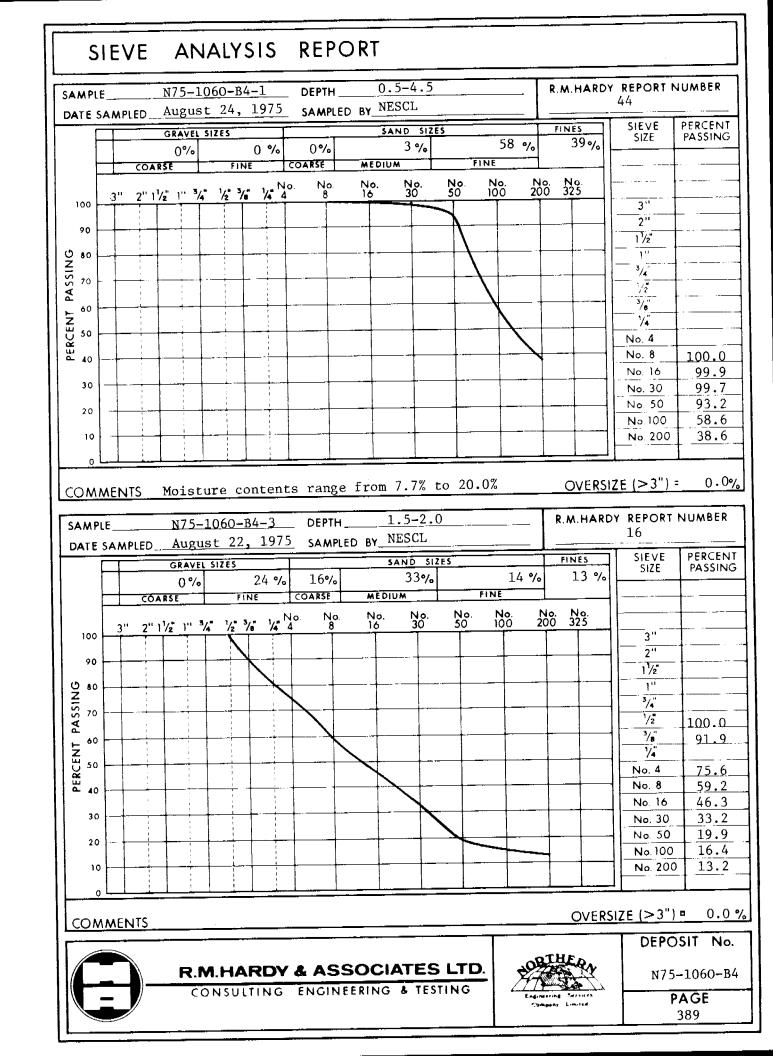


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PC-9,5K373

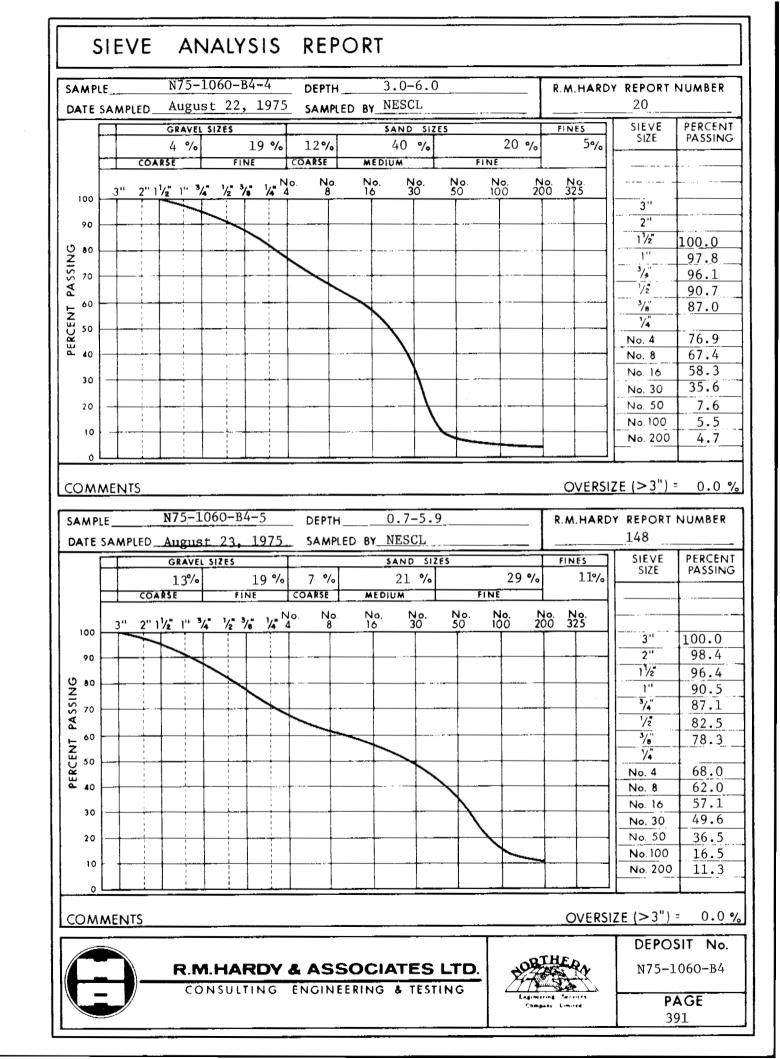


S	SIEVE	ANAL	YSIS	REPOR	T					
		175-1060- August_22		DEPTH	2.0-4.0 NESCL	η _{ε/}		R.M.HARD	Y REPORT I	NUMBER
	COARS	GRAVEL SIZES	8 %	9%	SAND SIZE		27 %	FINES 6 %	SIEVE SIZE	PERCENT PASSING
100 90	3" 2" 1/2	1" 3/4 1/2	3/6 1/4 4	No. No 8 16	5. No. 30	No. 50	No. No. 100 200	2 No. 325	3"	
DA SSING					$\overline{\mathbf{X}}$				$\frac{\frac{1^{1}/2^{a}}{1^{\prime\prime}}}{\frac{1^{\prime\prime}}{\frac{3/4^{\prime\prime}}{1/2^{a}}}}$	100.0 98.6
PERCENT									3/8 7/4 No. 4	97.5 95.8 90.7
- 40 30 20									No. 8 No. 16 No. 30 No. 50	84.9 77.5 55.5 12.4
10									No. 100 No. 200	7.4
SAMPL	SAMPLED	175-1060- Nugust 22	B4-4 , 1975	DEPTH				R.M.HARD	ZE (>3") = Y REPORT 1 21	NUMBER
	COARS		INE CO		43 %	FI	9 % ne	FINES 6 %	SIEVE SIZE	PERCENT PASSING
100 90	3" 2" 1/2	1" 3/4 1/2	3/6 1/4 4	No. No 8 16	0. No. 30	50	No. No. 100 200) <u>No.</u> 325	3"	
PASSING									$\frac{\frac{1}{2}}{\frac{1}{2}}$	100.0 94.9 91.8 87.0
PERCENT									3/8 7/4 No. 4 No. 8	81.8 70.0 59.7
30 20					\mathbf{X}				No. 16 No. 30 No. 50	51.4 22.1 9.1
10 0									No.100 No.200	<u>6.9</u> <u>5.8</u>
COMM	MENTS								<u>2E (>3") =</u> DEPOS	
	9			GINEERING			La contraction			060-в4 GE 0

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	OF LABORATORY TE FOR OF AGGREGATES IN		
	DATE SAMPLED : August 23, DATE TESTED : January, 19		
SOUNDNESS OF AGGE SULPHATE TEST	REGATE	ORGANI TEST	C IMPURITIES
COARSE AGGREGATE FINE AGGREGATE	5.71		R : 2 EMOVED : Nil
LOS ANGELES ABRAS	ION TEST	REMOVE	ROOTLETS D : Nil
PERCENT LOSS =	17.9 %		CONTENT : Nil
SUMMARY OF ROCK TYPE	S, COARSE AGGREGATE. (P	r	TOTAL WEIGHTED COMPONENT %
Quartzite Granite	Strong to very strong, Ver	ry good	22.8 1.15
Gneiss			0.05
Sandstone			1.1
Siltstone	Medium strong, Good		2.8 2.15
Chert Flint	Potentially reactive, Fair	: -	0.4
Ironstone	Soft, Friable, Poor		0.35
PN = 135 INTERPRETA	TION : Fair quality		32.0
to very strong, with no tend	of rock types present in sample dency to split or to flake. Al 4 expansion after 3 months = 0.	kali Aggregat	e Reaction
	R.M.HARDY & ASSO		DEPOSIT No. N75-1060-B4
Company Limited			PAGE 392

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1060 - B5 - A 422130E 7485900 N B5 - B 421960E 7486240N B5 - C 421170E 7485260N

DEPOSIT 1060-B5

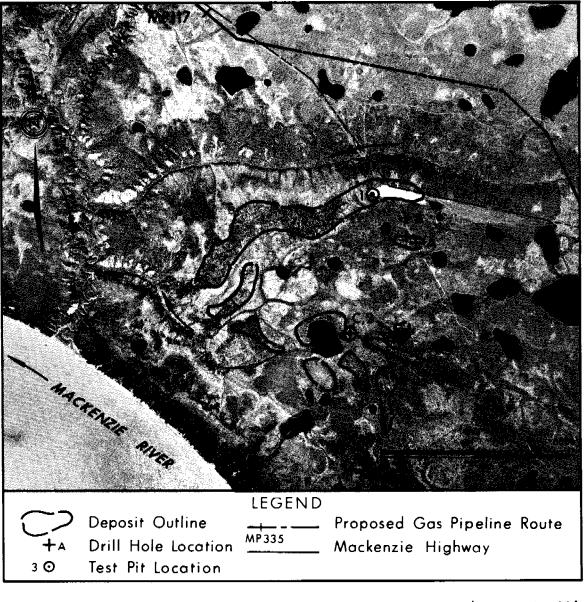
Jee 1085-1 EBA

Physical Setting: Deposit 1060-B5 consists of a number of kames located 1.5 miles east of the Thunder River mouth and 2 miles south of the right of way at milepost 177.

Material: SAND - poorly graded, silty, and some fine gravel.

Volume: 1,000,000 cubic yards.

Assessment: Deposit 1060-B5 is a source of fair quality granular material suitable for general fill and backfill. Access to the right of way is fairly good but a gully would have to be skirted.



Airphoto No.A22935-80Approximate Scale :1" = 3100'

Latitude: 67° 31' Longitude: 130° 50'

DEPOSIT 1060-B5

PHYSICAL SETTING

This deposit consists of a number of kames located 1.5 miles east of the mouth of Thunder River, near the site of an existing airstrip. It is 2 miles south of milepost 177 on the present pipeline alignment. A proposed airstrip lies directly on the larger part of the deposit and a proposed compressor station is 2 miles away. This deposit corresponds to source number 1085 in EBA DIAND Granular Materials Inventory Volume III (1974) report.

The irregularly shaped flat-topped kames stand 5 to 10 feet above the surrounding terrain. Most of their surfaces have thin covers of peat and fine grained material but locally it may thicken to 5 feet. The kames stand slightly above the surrounding terrain, and therefore are well to moderately well drained. Drainage in the intervening areas is poorer. The active layer varies from 2 to 7 feet depending on the depth of overburden. Granular material in this deposit has low ice contents.

BIOLOGICAL SETTING

The vegetation in this area is composed of black spruce, white spruce, and paper birch, with an understory of alder, willow, Labrador tea, soapberry, rose, dillberry, lichens and grasses. The general area provides habitat for caribou, moose, marten, lynx, fox, wolf, and black bear. Caribou, moose and bear sign were observed in the area during the 1975 survey. The area provides good denning potential for bear and other denning species. Waterbodies in the area provide suitable habitat for aquatic furbearers including muskrat, mink and beaver. Marten tracks were also observed in the area in 1975. Waterfowl are most numerous during the April to May migration period when they utilize open-water leads on the Mackenzie River. Ptarmigan and falcons have been reported from the area. The Thunder River supports populations of grayling, lake trout, round whitefish, broad whitefish, pond smelts, pike and long-nosed suckers. Other small ponds and lakes in the vicinity of the site do not appear to support fish populations.

MATERIAL

NESCL drill hole and test pit logs and the DIAND report shows this deposit is mainly poorly graded, silty sand with some fine, rounded gravel. The granular material is underlain at shallow depths by fine grained sediments. Several drill holes encountered only fine grained material.

VOLUME

The total estimated volume, based on an area of 260 acres and a 4 foot depth is 1,000,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 1060-B5 is a source of fair quality granular materials. Location of areas to be exploited would be dictated by haul distances, overburden thicknesses, insitu material quality, and material requirements. Granular material from this deposit may be used for general fill and backfill in pipeline construction.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the deposit with equipment may be achieved by barge to Thunder River and overland from there to the deposit, a distance of 1.5 miles.

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This route crosses very hilly terrain. Access to the pipeline right of way from the deposit involves skirting a gully to avoid initiating bimodal flows. In order to minimize environmental damage, snow roads would be built to transport the borrow material from the deposit to haul points on the right of way, a distance of at least 1 mile.

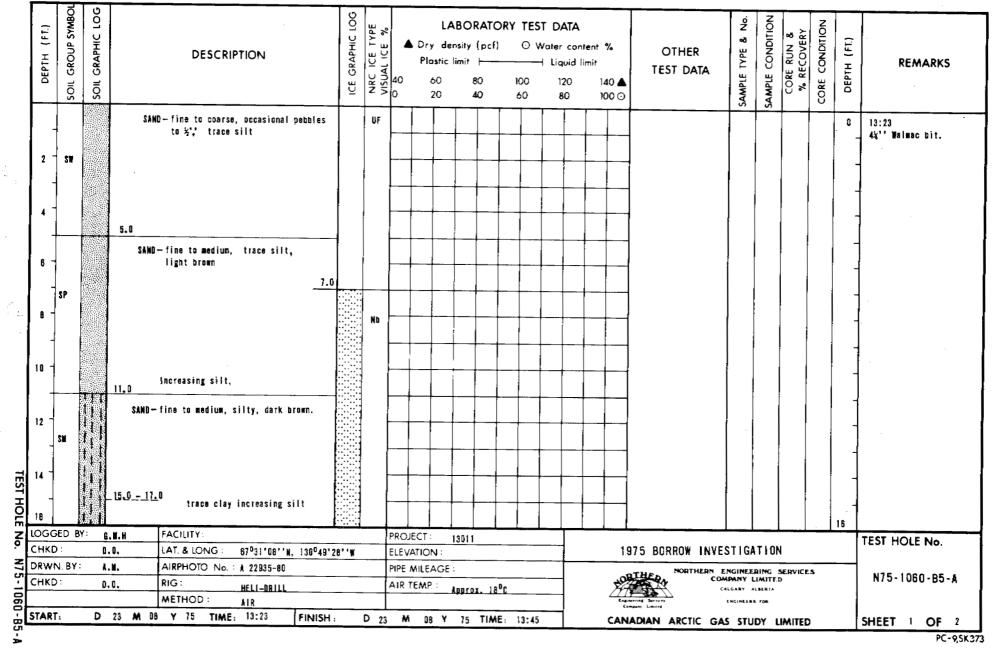
Tree and vegetative cover would have to be removed and harvested or disposed of in accordance with land use regulations. The peat cover and overburden would then be stripped from the area to be excavated, and stockpiled around the edge of the site.

Development of this deposit would involve excavating borrow material evenly from the higher, well drained areas. Excavations would be kept away from nearby lakes to protect them from siltation.

Development could be accomplished by using conventional earthmoving techniques as ice contents are low. The excavated material may have to be stockpiled, thawed, and drained before it is used.

Equipment required for development would be dozers, rippers, end-dump trucks and front-end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.



GROUP SYMBOI **GRAPHIC LOG** ICE GRAPHIC LOG ź SAMPLE CONDITION CONDITION NRC ICE TYPE VISUAL ICE % LABORATORY TEST DATA CORE RUN & % RECOVERY DEPTH (FT.) SAMPLE TYPE & DEPTH (FL) ▲ Dry density (pcf) O Water content % OTHER REMARKS DESCRIPTION Plastic limit -Liquid limit 4 TEST DATA CORE 60 80 100 120 140 📥 SOIL SOIL 20 40 60 80 100 🖸 16 SAND (cont'd) Nb 18 SNI 12" of slough in hele. 18 1 18 19.0 fine-grained, silty, medium brown 20 22 23.0 SILT - clayey, little fine sand, dark brown 24 HL. 28.0 28 SAND - fine to medium, fittle silt, Sì trace clay 27.5 less clay, trace silt helow 27.5' 21 28.0 End of hole 28 TEST HOLE TEST HOLE No. LOGGED BY FACILITY: PROJECT : Z o 8.1.9 13011 1975 BORROW INVESTIGATION LAT. & LONG 67⁰31'08''N, 130⁰49'48''W ELEVATION CHKD : 0.0. N AIRPHOTO No. : 1 22935-80 PIPE MILEAGE : NORTHERN ENGINEERING SERVICES A.M. N75-1060-85-A DRWN. BY: COMPANY LIMITED Ģ AIR TEMP. RIG : Approx. 18⁰C CALGARY ALBERTA CHKD: D.O. HELI-DRILL ENGINEERS FOR 060-85-A METHOD : AIR 1-----SHEET 2 OF 2 D 23 M 08 Y 75 TIME: 13:45 CANADIAN ARCTIC GAS STUDY LIMITED 08 ¥ 75 TIME: 13:23 FINISH : START: D 23 M

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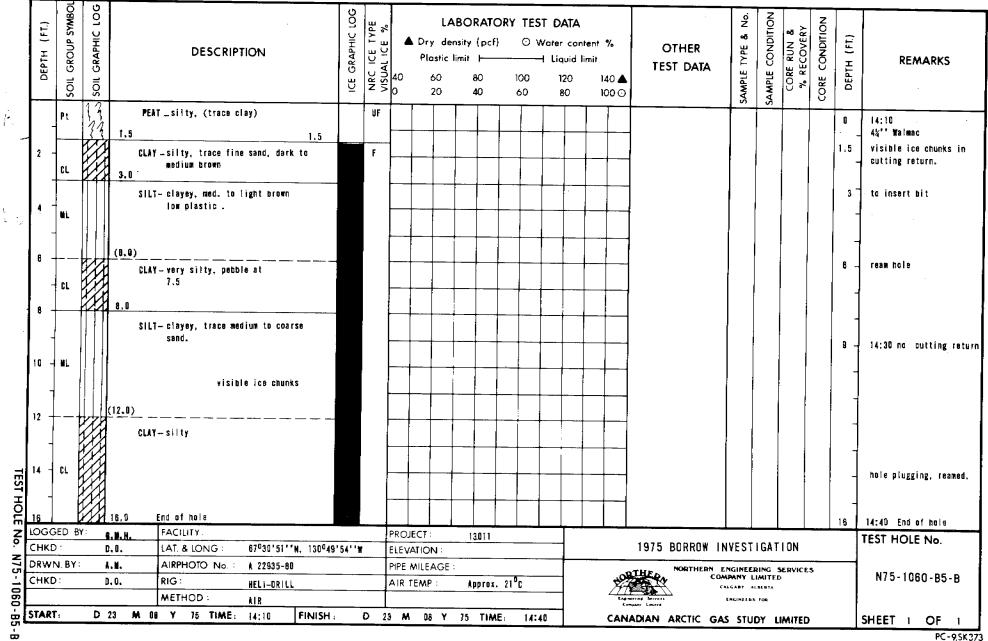
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TEST HOLE LOG

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PC-9,5K373

SAMPLE TYPE & No. SAMPLE CONDITION ICE GRAPHIC LOG CONDITION GROUP SYMBOI GRAPHIC LOG NRC ICE TYPE VISUAL ICE % O & CORE RUN & LABORATORY TEST DATA DEPTH (FT.) DEPTH (FT.) ▲ Dry density (pcf) ① Water content % OTHER REMARKS DESCRIPTION - Liquid limit Plastic limit -TEST DATA CORE 120 140 📥 80 100 60 SOIL SOIL 80 100 🖸 20 40 60 ?? PEAT-fibrous, woody, brown UF 33 1.0 Pt 74 F ice visible in peat 2 -22 Nb GRAVEL-fine, some med. to coarse sand, little silt 4 -PL • B.B..... trace clay, increasing silt 5 Ĩ 7.0___coarse gravel . 8.5 SILT-very sandy, trace coarse sand, occasional pebble 10 11.0 __ pebble clay adhering to drill-12 stem during trip out 16:00 13.0 13 no cutting return, hard CLAY-silty, trace fine to med. sand, layer or object at 15' CL low plastic, dark grey 14 TEST HOLE TEST HOLE No. PROJECT : 13011 FACILITY LOGGED BY: G.M.H. Š 1975 BORROW INVESTIGATION ELEVATION : 67°31'35''N, 130°50'33''W LAT & LONG CHKD 0.0. N75 WORTHERN ENGINEERING SERVICES PIPE MILEAGE A 22935-80 AIRPHOTO No. : N75-1060-B5-C DRWN. BY: 1.1 COMPANY LIMITED Approx. 24°C CALGARY ALBERTA AIR TEMP :: RIG: HELI-9RILL CHKD: D.O. 1060-ENGINEERS FOR METHOD : AIR SHEET 1 OF 2 CANADIAN ARCTIC GAS STUDY LIMITED FINISH : D 23 M 8 Y 75 TIME: 16:15 D 23 M 8 Y 75 TIME: 15:45 START 8 PC-9.5K373

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TEST HOLE LOG



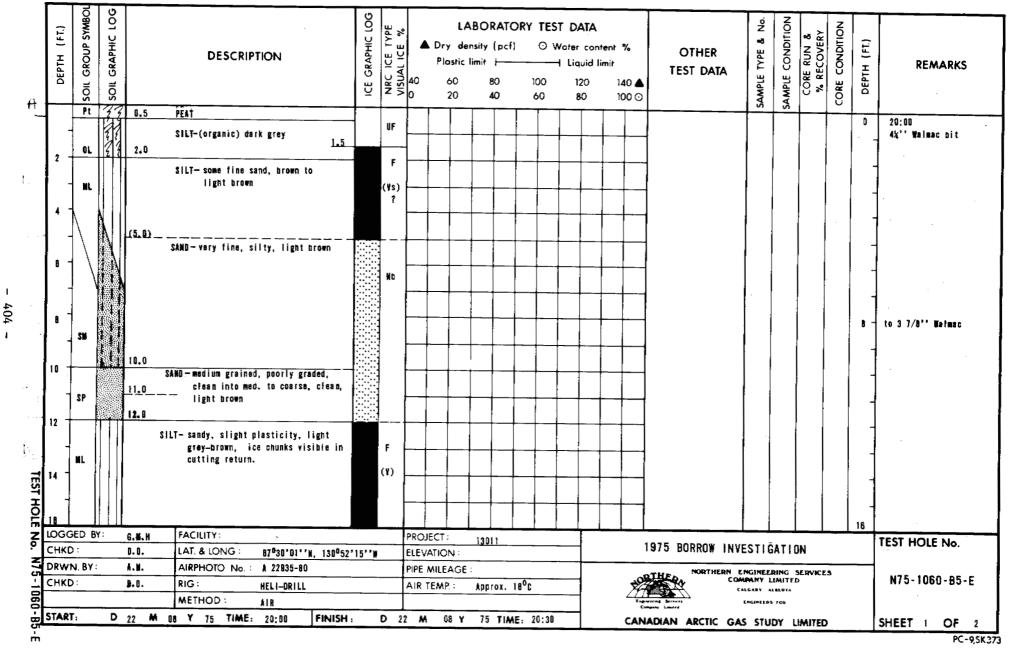
DEPTH (FT.)	SOIL GROUP SYMBOI	SOIL GRAPHIC LOG		DESCRIPTION		ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	LA Dry de Plastic 60 20	nsity (pcf)	0 w	T DATA later con Liquid 120 80	ntent limit 1	% 40 ▲ 00 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
18	CL			¥ (cont'd)			ND															
18 -			17'	trace gravel (occasiona	il pebble) ice chunks in										L						.	
					cutting return																	
																		ĺ			-	'No cutting return at 21°, drilistem bindi
20-			21.0	End of hole																	-	in hole
		278	41.0				+		-+-												21	
-									_					+	+							
_									_	$\left \right $		-		-							-	
-																						
1	i			,										\uparrow								
-										+		+										
4										+				+	-						_	
-												_										
														\square							1	
-						-						+	- -		+	2					-	
+										+				+								
	ED B	<u> </u>	.W.H.	FACILITY			<u> </u>	PROJ	ECT:		011		<u> </u>									TEET HOLES
HKC			0.		67 ⁰ 31'35''K, 130	°50'3	3''#									1975 BORROW IN	VESTI	GATI	ON		ļ	TEST HOLE No.
	N. BY	: 1 .	U .		A 22935-80				MILEAGE	:						ATHEN NORTHERN	ENGINE	RING	SERVIC	ES		N75-1060-85-0
HKC):	D	0.		HELI-DRILL			AIR 1	EMP.	Ap	prox. 2	4 ⁰ C			Ž		CALGARY	AL BERTA			I	
TAR			23 M 8	METHOD: Y 75 TIME: 15:	45 FINISH				8 Y			16:1			5 C	ADIAN ARCTIC G	ENGINEES				l	SHEET 2 OF 2

- 402 -

CHKD	D.Q.	RIG: HELI-DRILL METHOD: AIR M 58 Y 75 TIME: 18:20			22			101. 24 ⁰ C	1:45			ENGINE	as roa		FD		SHEET 1 OF
DRWN BY:		AIRPHOTO No. : A 22935-80			+	MILEAC				÷			LIMIT	F.D	~~~		N75-1060-B5-D
CHKD :	D.C.	LAT. & LONG : 67 ⁰ 30'06''N, 13	0 <mark>"51'2</mark>	9''W	+						NORTHERN	FNGINE	FRING	SERVE	CES		-
OGGED B	(: G.N. H.	FACILITY				JECT :	130	11			1975 BORROW IN	VEST	IĞAT	I ON			I IESI HULE NO.
28		End of hole				<u> </u>			<u> </u>				<u> </u>	<u> </u>	<u> </u>	28	18:45 TEST HOLE No.
1 F		trace sand															
		- -												1		_	
28 -		the cutting roturn			-		<u> </u>	- - -				1	1			-	1
1 1	1 A	less ice visible in		//	1							Ί				"	
										<i>,</i>							¥
					\vdash	\vdash			++	-++		1				-	1
18 -		sand, fine to coarse										1	1				
	118.0	—— decreasing plasticity, increasing														-	
+	XA .				\vdash		-+ +-		-+								•
"1					1						/	1				"	
16	XX -								- ↓ - ↓		/					7	/
1 4		infrequent peoble from depth 13' to 16'					1 1					1					
							1					1					
12 -										+						-	
11	XX -	outtings		1	1							1				/	
		ice in cuttings									//						//
		chunks of			\vdash		+ +		+ +							-	
		CLAY-silty, trace fine sand, low plastic, grey															
	1/2 5				$\left - \right $			++	+ +	+						-	
2 -																	
				F													Possibly ¥s ice
- m	<u> </u>	SiLT - clayey, trace fine sand <u>1.</u>			+			-+	+	+ $+$ -1						-	Be to the runner
Pt	77 0.5	PEAT - fibrous, woody, dark brown	-	UF													18:20 Walmac bit Change to 4%*** insert
	soit		Ĕ	2 >	0	20	40	60	80	100 🖸 .		Å	Ş		Ŭ		
DEPTH IL GROU	ຍ 		U U	1SU.	40	60	80	100	120	140 🔺		SAMPLE TYPE	MPL	8 %	CORE	DE	
E Q	RAP	DESCRIPTION	5RAI	F CI		Plastic	limit ⊢		- Liquid		TEST DATA	Ц Ш	Ŭ щ	RE O	U	РТН	REMARKS
DEPTH (FT.) SOIL GROUP SYMBO	GRAPHIC	DESCRIPTION	GRAPHIC LOG	NRC ICE TY VISUAL ICE	▲		ensity (pc	-	Woter co		OTHER	H H	SAMPLE CONDITION	CORE RUN & % RECOVERY	CONDITION	DEPTH (FT.)	REMARKS
() Å	200		12	Т УРЕ Е %		L	ABORAT	ORY TE	SI DAIA			So. No.	JI N	∞ <u>~</u>	E	2	

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ŝ SAMPLE CONDITION ICE GRAPHIC LOG CONDITION SOIL GROUP SYMBOL SOIL GRAPHIC LOG CORE RUN & % RECOVERY NRC ICE TYPE VISUAL ICE % O & LABORATORY TEST DATA SAMPLE TYPE & DEPTH (F1.) DEPTH (FL) ▲ Dry density (pcf) 👘 🏵 Water content % OTHER REMARKS DESCRIPTION - Liquid limit Plastic limit |-TEST DATA CORE 80 100 120 140 📥 60 100 🖸 60 80 20 40 16 SILT (cont'd) 18 F UIL. 18 20 22 24.5" - 25.0" occasional people 24 20:20, hole plugged -25.0 25 CLAY-silty, trace fine sand, low reamed 20:30 problems of poor 28.0 26 plastic, grey. C۱ circulation because of 26 End of hole clay. TEST HOLE TEST HOLE No. PROJECT FACILITY 13011 1975 BORROW INVESTIGATION LOGGED BY: 6.**0.**H z ō ELEVATION : LAT. & LONG 67°30'01''N, 130°52'15''W CHKD : 8.0. NORTHERN ENGINEERING SERVICES 8 L N PIPE MILEAGE A 22935-80 N75-1060-85-E AIRPHOTO No. A. M. DRWN.BY: COMPANY LIMITED AIR TEMP : Approx. 18⁰C CALGARY ALBERTA HELI-DRILL CHKD D.O. RIG ENGINEERS FOR \square METHOD : AIR 60-SHEET 2 OF CANADIAN ARCTIC GAS STUDY LIMITED - 2 D 22 M 08 Y 75 TIME: D 22 M 08 Y 75 TIME: 20:00 FINISH : 20:30 START: œΙ

TEST HOLE LOG

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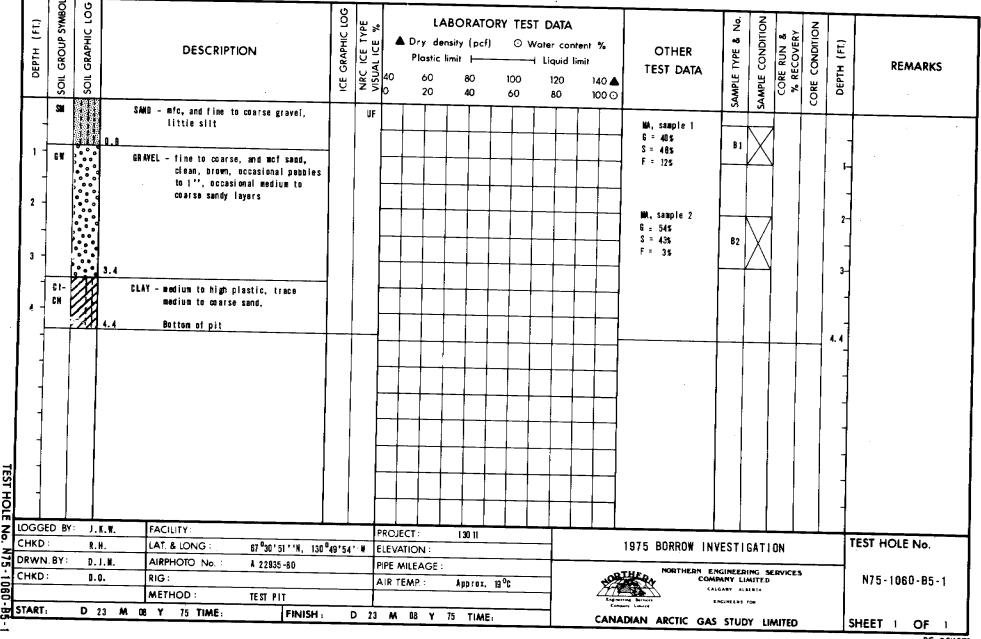
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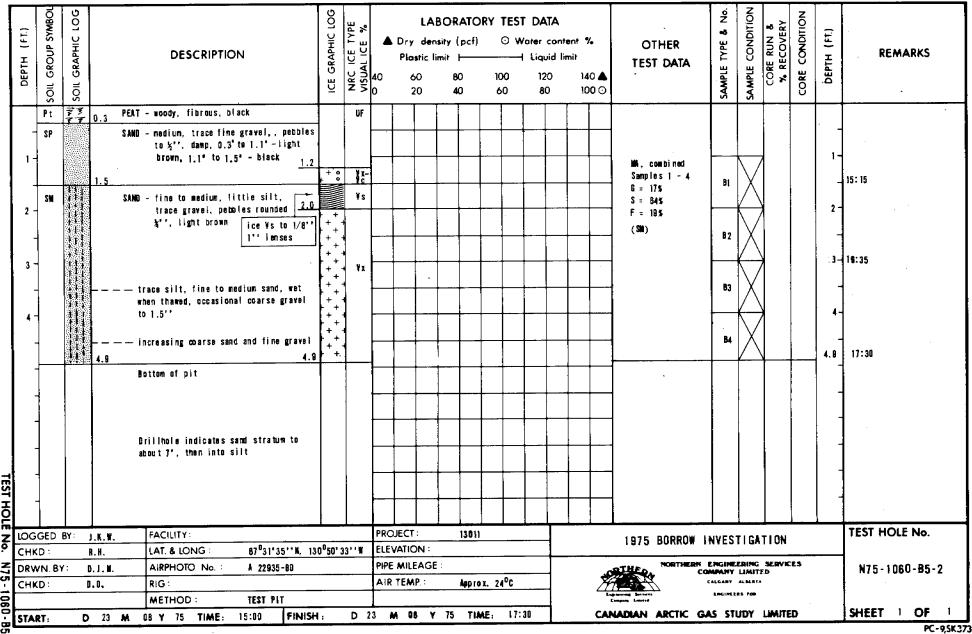
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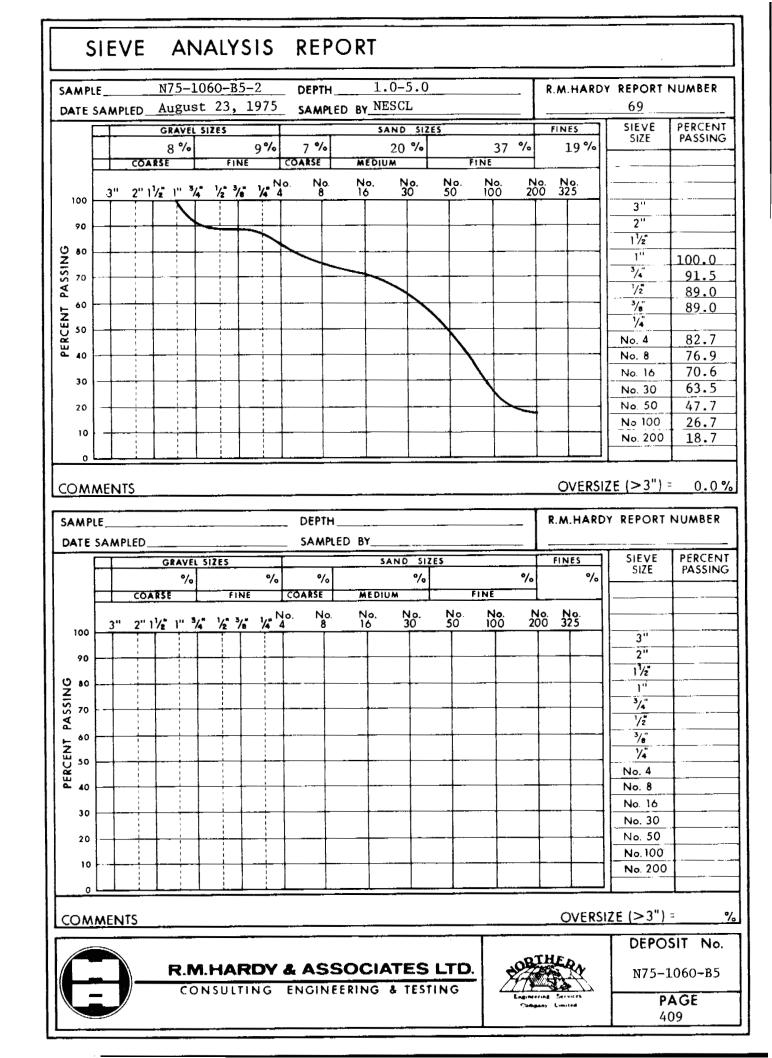
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SAM	PLE	MPLED	N75	-100	60-В 23	197	D	EPTH.		0.0-				<u> </u>	R.M.HARD	Y REPORT	NUMBER
DAT	E SA	MPLED					<u> </u>	AMPLE	D BY_							72	
		1	GRAV					<u> </u>			SIZE	5			FINES	SIEVE	PERCENT
			10 %	•		30 %	, 1	2%		18	3%		18	%	12%	SIZE	PASSING
		co/	ARSE	1	FIN	IE] COA	RSE	MEC	NUM	1		FINE				
		<u></u>	1/*	3/-	1/* 3/	- 1/-	No.	No.	No.	N	No.	No.	No.	No 200	No. 325		
100	> i	3" 2"	1/2 1"	74	/2 /0	<u> </u>	4	8	<u>16</u>		30		100	200	325		·
													[3"	Ĺ
90				K							†					2"	100.0
0 00	,	ļ			\mathbf{X}		_				İ					1 1/2	98.0
ON ISS 70					N											1"	94.2
S 70					+											3/4	89.7
1 2 60				_												/2	80.3
l z °						1	N									3/8	73.0
00 20	-	<u> </u>	+ +	+	-		\rightarrow	\leftarrow			+	_				1/4	
PERCENT PA																No. 4	59.9
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30	-		+ +	+	- 											No. 16	42.1
						ł										No. 30	36.1
20					; †		†									No. 50	24.1
10	,				\downarrow									<u> </u>		No.100	15.2
1						ĺ										No. 200	11.5
		<u> </u>	1 :	1	<u> </u>		1				i .						
CON	ME	NTS 1	Moist	ure	con	tent	of	5.3%							OVERSI	<u>ZE (>3") =</u>	0.0%
SAM	DIF		N75	-106	50 - B	5-1		EPTH_		2.0-	-3.0						
														-	K.M.HAKU	REPORT	NUMBER
DATE	: SA	MPLED_				197	<u> </u>	AMPLE	D BY	NES	<u>ىل</u> ى					73	
			GRAVI	1				· · · · ·			SIZE	5			FINES	SIEVE SIZE	PERCENT PASSING
			25%	Þ		29 %		2•/。		19	%		12	%	3 %	5121	PASSING
		COA	RSE	Ι	FIN		COA	RSE	MED	IUM		1	INE				
	.	3" 2"1	¹ /z" 1"	3/* '	1/= 3/-	5 '4"	No.	No.	No.	Ņ	lo. 0	No.	No.	No. 200	No. 325		
100	·		/2	14	/2 /8	<u>) /4</u>	4	-	16	و		50	100		325	3"	
			ΝE														100.0
90																	100.0
U 00				_	+ +		-	_								1 1/2	94.7
1 S		1		X	{	1			{							1"	83.9
S 70						1 1	1					+				3/4	75.4
PERCENT PASSING			ļ	_	Ň					·····		_				1/2	66.6
1 z																3/8	59.8
so يَرْ	-	;	+ +	1	$\frac{1}{1}$		<u> </u>									74	
1 H 40	L						N									No. 4	46.3
- *0		3			T	1										No. 8	35.7
30	\vdash		<u> </u>	+	;	+					• • • •	_				No. 16	27.2
_					1	1						1	1			No. 30	19.6
20	1			1	;		1	1				-+	-		-+	No. 50	10.2
10					<u> </u>	<u>.</u>	 						.			No. 100	4.2
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COM	ME	NTS	Mois	ture	e co	nten	t of	2.82	~						OVERSI	ZE (>3") =	0.0 %
							• •							LT Q		DEPOS	IT No.
	-							INEE					Ž	H		N75-10	
		/									<u>.</u>			ngi nga king Mangga ki	uervites Limited	PA 40	GE 8

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1060 - B6 - A	444310 E	7465380 N
B6 - B	444120E	7465350N
B6 - C	444480E	7468270N
B6 - D	444150E	7467810N

UTH - ZON 9

Longitude : 130°

18'

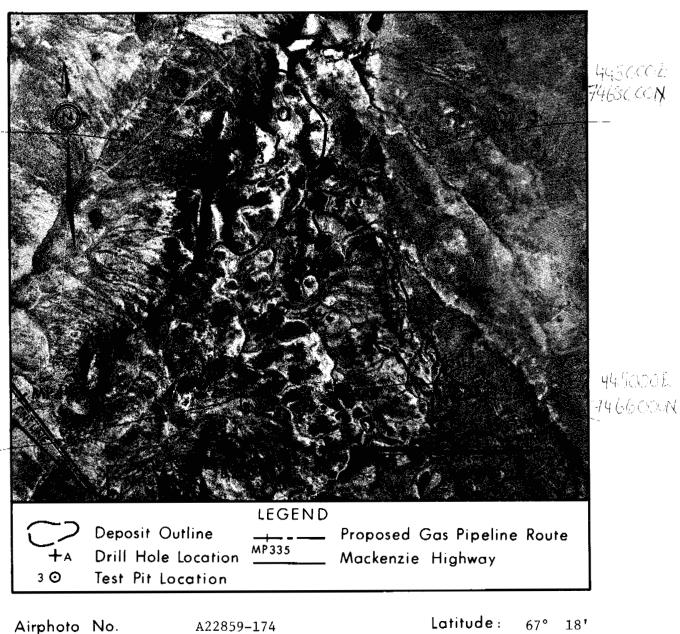
DEPOSIT 1060-B6

Physical Setting: Deposit 1060-B6 consists of hummocky morain with kames located 9 miles north of Little Chicago and 2 miles northeast of right of way milepost 197.

Moterial: GRAVEL - segment "a", gravel and till. TILL - segments "b" and "c", till with minor gravel.

Volume: Segment "a" contains an estimated 5,000,000 cubic yards of granular material.

Assessment: Deposit 1060-B6 is not recommended for development. Further investigation of segment "a" should be done before a final assessment is made. Access may be difficult.



444.0008 7468000N

444.000.12 7466.0000

1'' = 3200'

Approximate Scale:

DEPOSIT 1060-B6

PHYSICAL SETTING

This deposit consists of hummocky moraine with numerous kames located 9 miles north of Little Chicago and 2 miles northeast of milepost 197 of the proposed pipeline right of way.

Parts "a" and "b" of this deposit are mainly clusters of kames with isolated morainic hills, whereas part "c" appears to be mainly hummocky moraine. In section "a" steep sided hills of 50 to 150 feet in height are present. Relief in the other two sections is generally less than 50 feet.

Overburden on most hills and ridges is negligible, although it may thicken to 2 or 3 feet on gentle north-facing slopes, and up to 10 feet in depressions. South-facing slopes, hills and ridges are all well to moderately well drained and depressions poorly drained. The active layer varies between 5 and 10 feet in the better drained areas. Ice content of the granular material is low, although icy zones may be present in the ablation till.

There is a 350 foot moderate to steep descent from the bench on which the deposits are situated to the lowland that the pipeline crosses.

BIOLOGICAL SETTING

Vegetation on the better drained areas of this site consists of spruce up to 40 feet or more in height, aspen, a light shrub understory and ground cover of herbs, lichen, and mosses. The more poorly drained areas support stunted spruce, shrubs, and a ground cover of moss and lichen. The area provides low to moderately productive habitat for marten, snowshoe hare, red squirrel, fox, lynx, caribou, black bear and moose. Waterfowl are most numerous during the April to May migration period when they utilize open-water leads on the Mackenzie River. Raptors may nest in the area but no other important bird habitat has been identified. No suitable fish habitat occurs in the vicinity of the site.

MATERIAL

Material in segment "a" consists of either well graded, silty, subrounded gravel, with frequent cobbles or ablation till. Segment "b" was not tested but is probably gravel, sand and ablation till. Ablation till with interbedded coarse gravel was found in segment "c".

VOLUME

Material volumes were not calculated for segments "b" and "c" since the material is of very poor quality. Segment "a" contains an estimated 5,000,000 cubic yards based on an area of 400 acres and a 25 foot thickness (x $\frac{1}{3}$ for topography).

DEVELOPMENT AND REHABILITATION

Since a large portion of this deposit consists of ablation till, it is not recommended for development unless there is insufficient borrow in nearby sources to meet construction requirements. Further testing of segment "a", to delineate areas underlain by good quality granular material, should be undertaken if such material is required. Access to the pipeline right of way involves crossing hilly terrain with moderate to steep slopes which could also cause difficult problems.

LOG **GROUP SYMBOI** ICE GRAPHIC LOG ŝ SAMPLE CONDITION CONDITION NRC ICE TYPE VISUAL ICE % 0 & LABORATORY TEST DATA CORE RUN & % RECOVERY (FT.) -5 (FT.) GRAPHIC ▲ Dry density (pcf) ① Water content % OTHER SAMPLE TYPE DESCRIPTION DEPTH REMARKS — Liquid limit DEPTH Plastic limit 🕂 TEST DATA CORE 60 80 100 120 140 📥 SOIL SOIL 20 40 60 80 100 🖸 27 19:20 ₽t PEAT - fibrous, woody, dark brown ŬF 1.0 1.0 CLAY - silty, trace fine to coarse sand, F grey, occasional peobles to %'', 2 (pessibly till), cobbles to 8" at surface 4 visible ice chunks CL. in cutting return 6 19:30 B unfrozen soil at surface plugging hole to insert bit . hole plugging 9,0 -- slightly more silt 10 -10 - cemple, increase in coarse sand and 20 20 fine gravel 22 TEST HOLE 23 19:50 cobbie End of hole 23.0 LOGGED BY: FACILITY PROJECT : TEST HOLE No. G. M. H. 13011 <mark>Z</mark> 1975 BORROW INVESTIGATION 87⁰18'03''N, 130⁰17'53''W ELEVATION : CHKD 0.0. LAT. & LONG : Z PIPE MILEAGE : DRWN, BY : **A. N.** AIRPHOTO No. 1 A22859-174 NORTHERN ENGINEERING SERVICES N75-1060-86-A COMPANY LIMITED õ CHKD: 0.0. RIG : HELI-DRILL AIR TEMP. : Approx. 7⁰C CALGARY ALBERTA 1060-86 ENGINEERS FOR METHOD : AIR CANADIAN ARCTIC GAS STUDY LIMITED SHEET 1 OF FINISH : D 24 M 8 Y 75 TIME: START: D 24 M 6 Y 75 TIME: 19:20 19:50 *

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TEST HOLE LOG

PC-9,5K373

	DEPTH (FI.)	GROUP SYMBOL	GRAPHIC LOG			DES	CRIPTIC) N		ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %		≜ Dry ₽k		isity (pcf)		GT DAT Nater a ⊣ Liqui	onten		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CONDITION	DEPTH (FI.)	REMARKS
	DE	SOIL G	SOILG							С.	NRC	40		60 20	80 40		100 60	120 80		140 ▲ 100 ⊙		SAMPL	SAMPLI	Ö,⊀	CORE	DEI	•
		₽t		1	PEAT .0	- flbrous,	brown, r	meist	-		ŬF	ľ															New Weimac bit, 3 7/8**
	2	SM-			24 MD	- fine, ve send) h	ery silty prown, moi		C9#F58 2.0																		
	4	M.			1.0						Nb															4	
	4 -	CL				- silty, t (till ?)	race coa , cobble	erse sand, approx.	8., Eleà'																	1	
	8 -	ML			SILT	- littie f																				8 -	20:30 te reck bit
	8 -					- eccasiona pessibly	ti I	, (CODDIe	at 8.9')																	-	
	10 -	67	• • • •) <u>.</u> 0 + Grav		e, freque	ional bou																		-	 No fines in cutting: coarse gravel or ver graveliy till layer
~ ₁	12-	7				(20221	u i <u>y</u> (() (1	
TEST HOLE	14 -																									14 -	Yory wet at 18.0° due thewing of permatrost
	16	GED			I.K.	FACILITY						PP	OJECT	 r:		13011											TEST HOLE No.
~ F	CHK			8.1		LAT. & LON	IG :	87 ⁹ 17	'5 9'' N, 1:	30 ⁰ 17'	54"'W	-	EVATIO								1975 BORROW IN	VEST	GAT	ION			
	DRW CHK		:	A, I D. 1		AIRPHOTO RIG :	No.	A 228 #EL1-1					PE MIL Ir ten			in rev	. 10°C			20	NORTHERN C	ENGINE DAPANY CALGARY	LIMIT	F.D	E5		N75-1060-86-8
8				0.1		METHOD :	:	AIR												211 Engi	werned Serveres many Lawred	ENGINE					
	STAR	T:	(> 2	24 M 8	Y 75	TIME:	20: 15	FINIS	1:	D	24	M I	Y	75	TIM	E: 21:	25		CAN	ADIAN ARCTIC G	AS ST	UDY	LIMITE	D		SHEET 1 OF 2 PC-95

GROUP SYMBOI GRAPHIC LOG ICE GRAPHIC LOG SAMPLE TYPE & No. SAMPLE CONDITION CORE CONDITION CORE RUN & % RECOVERY LABORATORY TEST DATA ТҮРЕ Е % DEPTH (FI.) DEPTH (FI.) OTHER NRC ICE 1 VISUAL ICE 0 05 REMARKS DESCRIPTION Plastic limit |--------- Liquid limit TEST DATA 100 120 140 📥 60 80 SOIL SOIL 20 40 60 80 100 🖸 <u>____</u> GRAVEL (cont'd) Nb GP 17 hole plugging 00 17 ° ° ° 17.5 SILT - sandy 18 End of hole HL. ! (he.c 18-**TEST HOLE** TEST HOLE No. FACILITY PROJECT : 13011 LOGGED BY: 6.M.H. 1975 BORROW INVESTIGATIONS Z₀ 67°17'59''N, 130°17'54''W ELEVATION : CHKD LAT. & LONG : D.O. NORTHERN ENGINEERING SERVICES N75-PIPE MILEAGE AIRPHOTO No. DRWN. BY: A.W. A 22859-174 N75-1060-B6-B COMMANY LIMITED Approx. 10⁰C AIR TEMP. CHKD D.O. RIG : KELI-DA ILL CALGARY ALBERTA ENGINELES FOR 90 METHOD : ALR SHEET 1 0 CANADIAN ARCTIC GAS STUDY LIMITED OF 2 FINISH a D 24 M 8 Y 75 TIME: 21:25 M 8 Y 75 TIME: 20:15 START: D 24

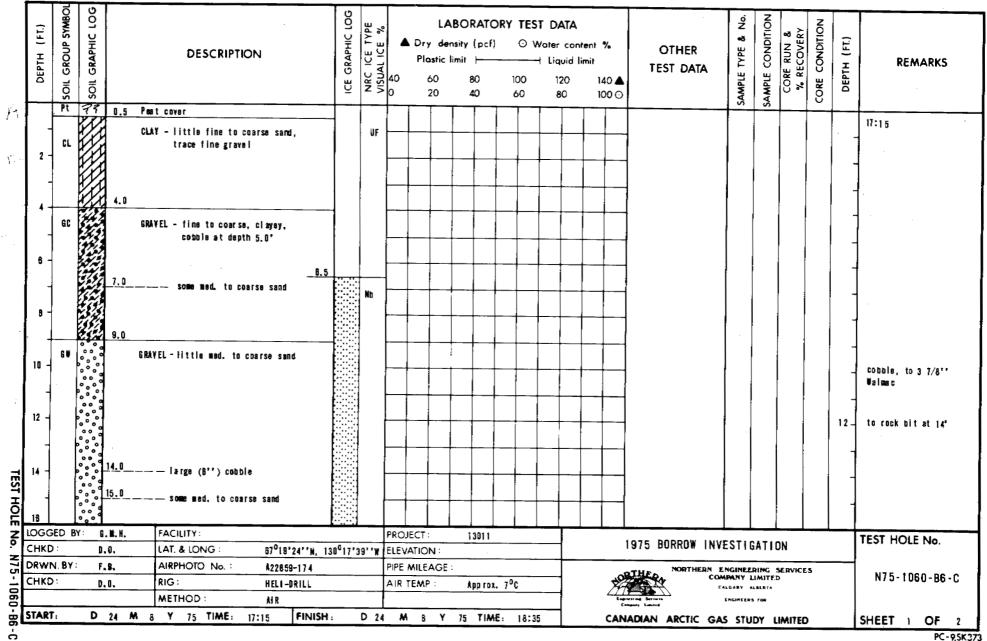
TEST HOLE LOG

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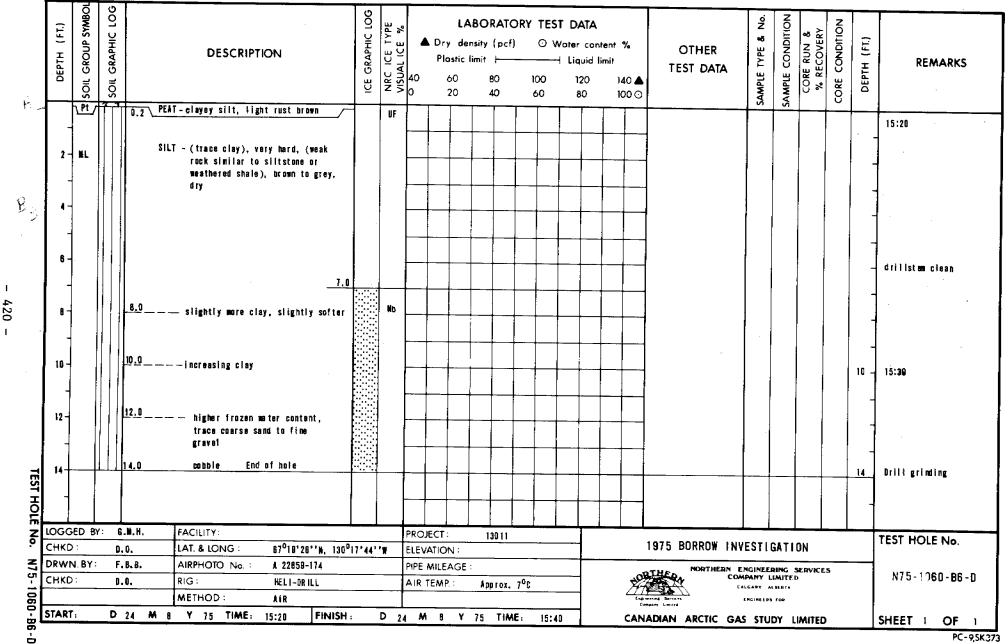
PC-9,5K373

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DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPT	ION	ICE GRAPHIC LOG	NRC ICE TYPE	40 04	▲ Dr) Pla	y den		pcf))	ΟV	T DATA Vater co Liquid 120 80	ntent limit 1	% 40 ▲ 00 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
16	GW		GRAY	/EL (cont'd)			Nb	· †										+	- v ,	<u> </u>			· · · · · · · · · · · · · · · · · · ·
-								\vdash	+													· -	
18 -							3			ļ			_									-	
		0.0	9 19.0	- — cobble																			
20 -										1			- -		+							20 -	Hole plugging at 18° cuttings, caving
-		le e	21.0	End of hole		:::	<u>:</u>	+		-		_	_		-	+		_			1	21	-
-			E											++-		+ 1						-	
-									_	<u> </u>			·	<u> </u>	_							-	-
-											i												· ·
-								\vdash			<u> </u>			++	+	+						-	
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-																						-	
-								-	+													-	
060	GED	BY:	G.M.H.	FACILITY:				PR		·;	<u>نا ا</u> 1	3011					1000 D00000 ···				1	1	TEST HOLE No.
СНК	D :		D.O.	LAT. & LONG :	67 ⁰ 19'24''N,	130 ⁰ 17'	39''W	٤L	EVATIO	DN :							1975 BORROW IN	IVE211	GAI	UNS			1
	N. BY	¥:	F.8.	AIRPHOTO No. :	A22859-174			_	PE MIL							204	NORTHERN C	OMPANY	LIMIT	F.D	CES		N75-1060-B6-C
снк	D:		9.0.	RIG:	HELI-DRILL AIR				ir te <i>n</i>	iP.		pprox.	7°C			Ž	A Servert	CALGARY ENGINEE		•			
	t:			METHOD : 8 Y 75 TIME:		IISH :		1	M	0 V	75	TIME	. 16	:35		CAN	IADIAN ARCTIC G			1.564171	50		SHEET 2 OF

- 419 -

TEST HOLE LOG



DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Dry	den: itic lir 0	sity (pc	f) 1	0 w	T DATA /ater contre Liquid lin 120 80			SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FI.)	REMARKS
-	Pt	22	PE AT	– moss cover, dark brown		UF									<u> </u>	<u> </u>		†			No samples taken
0.5		- ~~ ~~ ~~ ~~ ~~ ~~ ~~ ~~ ~~ ~~ ~~ ~~ ~~		amorphous, black, damp																	
1.0	CL	KXX	1.1 CLAY	- silty, trace sand, fine, grey																	
				brown, damp											-					-	
1.5	-						<u> </u>	++							-					-	
		K/X	1.8	1.8	1014	I CE +	<u> </u>								4					-	
2.0		777	2.0 TILL		ni ⊨±	Yx 25]					-					<u> </u>		ļ	2,0	Ab ando ned
2.0				'- trace gravel, pebbles subangular / to 3/8"', pockets of sandstone /																	
	1			to 3/8°°, carbon specks											1						
	1			Bottom of pit					•						-					-	•
	-						<u> </u>								-					_	
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	-							┼╌┨				+			4					-	
÷L				r															<u> </u>		
	GED		J. K. W. R. H.	FACILITY: LAT. & LONG : 61 ⁰ 18'03' 'N, 130 ⁰	17'53			VATIO		13	01 1	-			1975 BORROW IN	VEST	IGAT	I ON			TEST HOLE No.
╸┝──	NN. B		<u>к. п.</u> А. N.	AIRPHOTO No. : A 22859-174	11 00		+	MILE		:					ATHED NORTHERN	ENGINE			ES		N75-1060-B6-1
л 🗕 —	KD :		D. C.	RIG			AIR	TEMP	> _:	Ap.	p rox.	16 ⁰ C		Ž		CALGARY	AL BERTA				
				METHOD : TEST PIT			<u> </u>							-	Ingenerating Services Company Limited	ENGINES					SHEET 1 OF 1
STA	RT:	D	24 M I	08 Y 75 TIME: 16:15 FINISH	:	D 2	4 1	M 58	Y	75 T	IME:	16:	3U	CA	NADIAN ARCTIC G	AS 51	UUT		:0		PC-9,5K37

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TEST HOLE LOG

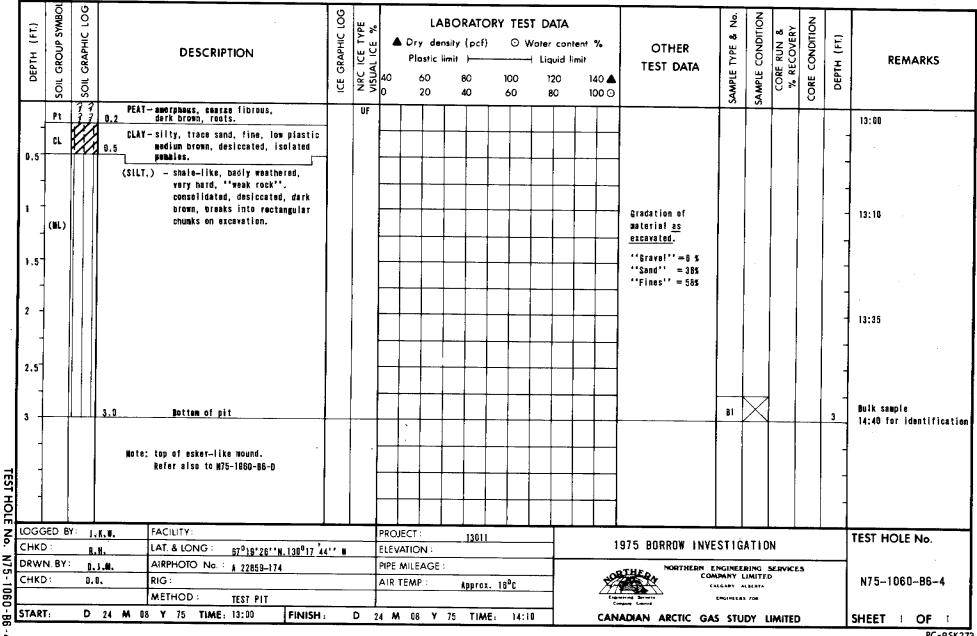
DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Dry	densi tic lim	ty (pc		• Wa	DATA ter conte Liquid lin 120 80	nit 14(0 ▲ 0 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FL)	REMARKS
	Pt	77	0.2 PEAT	– amorphous, coarse fibrous, black,	1	UF									- 1							16:00
	CL		CL AY	roots										_					-			No samples taken
	- - 2-		CLAY	f - trace gravel, trace sand, cmf, medium plastic, peobles rounded, mainly fine, occasional to 2'', (tili-like), grey, slight mottled, grey orange, carbonaceous plant material, rust spots, fine sand pockets to ½'', shale fragments															-		-	16:25
	3-			nstone concretion, and granitic cobble 5'', damp Bottom of pit													1				-	16:39
																					-	
										-		_										
																			1 1		-	
TES																						
B	1				1																	
19 0	l GGED	BY:	J. K. W.	FACILITY			-	DJECT		131	011	-				1975 BORROW IN	VEST	IGAT	ION			TEST HOLE No.
	KD :		R.H.	LAT. & LONG : 87 ⁰ 17'59''N, 130	0 ⁰ 17'5	4' '₩	<u> </u>	VATIO								NORTHERN	ENGINE	ERING	SERVI	CES		
	WN.E	Y:	<u>A.W.</u>	AIRPHOTO No. : A 22859-174 RIG :				TEM			i ro <u>x.</u> 13 ⁰	C			P O	co co	CALGARY	LIMIT	F.D			N75-1060-B6-2
				METHOD : TEST PIT												Indering Services Company Limited	ENGINE			-		
1060-B6-2	ART:	D	24 M	08 Y 75 TIME: 16:00 FINIS	H:	Ð	24	M 08	<u> </u>	75 1	IME:	16:5			CAN	ADIAN ARCTIC G	AS 57	UDY	LIMIT	50		SHEET 1 OF 1 PC-9,5K37

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				METHOD: TEST PIT								<u> </u>	generating Serverts Company Limited	ENGINEE					
DRW CHK	(N. B)	(:	F.B. D.O.	AIRPHOTO No. : A 22859-174 RIG :			PIPE MIL			. 16 ⁰ C		₹¢	OTHED CO	ENGINE DALPANY CALGARY	LIMIT	F.D	ES		N75-1060-86-
снк			R. H.	LAT. & LONG : 67 ⁰ 19'24''N, 130	917'39''	W	ELEVATIO						1975 BORROW I	NVES	T I GA	TION			
OG	GED	j BY: R	 H J.K.W.	FACILITY:	_ <u></u>		PROJECT	<u> </u> :	13011	<u> </u>					<u> </u>		1	<u> </u>	TEST HOLE No.
-	1					1						<u> </u>	1					-	1
-	1										•								
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-	-							$\left \right $										-	
-		1.10	5.7	damp Bottom of pit									·	BS	[X]			5.1	}
5 -			P					$\left - \right $	-+-+						\mathbb{K}	×		5-	
-	-	۴.۴.	A	content fines				$\left \cdot \cdot \cdot \right $						B4	IX			L 1	
4 -	1	ີເ	4.0	 pocket to 2'' of micaceous medium grain sand, moist, less 											K,	1		4-	
-	1			— ironstone pocket										83	Ň				
3 -				·											\mathbb{N}	1			
n –			3.0	irenstone pocket											\square			3_	
_										•			(GM)	B2	\mathbb{N}			-	
2 -			e	subrounded to 7'', rootlets									a - 345 F = 18%		()	×		2 -	
-				little fines, grey brown, pebbles rounded to 3", cobbles						_			G = 48% S = 34%	B1	IX			-	
1 -	6W		10.9 GRAV	EL - fine to coarse, some cmf sand,									MA, combined samples 1 - 4			7		1-	
-	CL	V		- silty, little sand, fine, burnt orange						_								-	
_	Pt	34	PEAT 0.3	- coarse fibrous, black, woody inclusions		UF									0			+	
DEF	SOIL G	SOIL G			ICE O	NRC ICE VISUAL ICE	40 (0 (50 20	80 40	100 60	120 80	140 ▲ 100 ⊙		SAMPLE TYPE	SAMPLE	0.%	CORE	DEF	
DEPTH (GROUP SYMBO	GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	L CE	Pic		nit				OTHER TEST DATA	TΥΡΙ	CONDITION	CORE RUN & % RECOVERY	CONDITION	DEPTH (FT.)	REMARKS
(FT.)	SY	<u></u>			Ϋ́	TYPE E %	A Dry	dens	ity (pcf)	οw	oter cont	ent %	OTUER	•5	Į	Z N Z N	Ĩ	Ē	

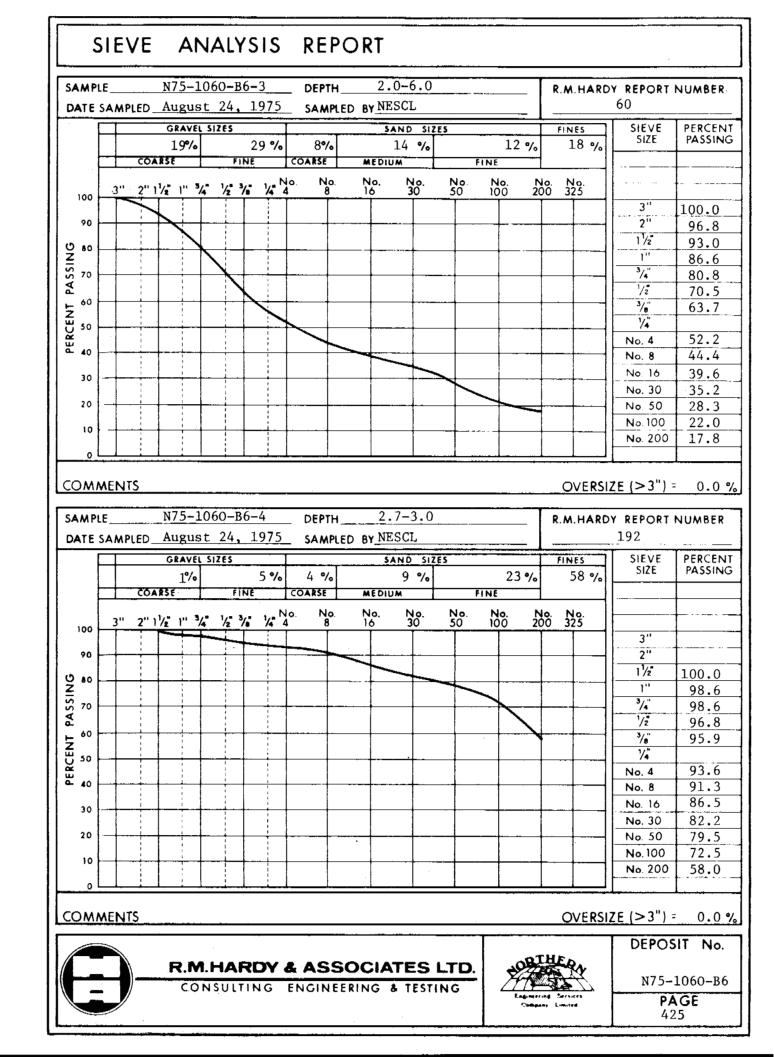
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PC-9,5K373



	Y OF LABORATORY TE FOR Y OF AGGREGATES IN		ETE
SAMPLE No. N75-1060-B6 DEPTH (FT.): 2-6			ED BY : NESCL D BY : RMHA
SOUNDNESS OF AGO SULPHATE TEST COARSE AGGREGAT	E: LOSS = 10.51%	TEST	IMPURITIES
FINE AGGREGATE		COAL RE COAL & REMOVED	MOVED : Nil ROOTLETS D : Nil DNTENT : Nil
SUMMARY OF ROCK TYP	PES, COARSE AGGREGATE. (PI		ANCE : IC ANALYSIS)
ROCK TYPE	CLASSIFICATIONS		WEIGHTED COMPONENT %
Quartzite Granite	Very strong, Good		21.4 2.95
Sandstone Siltstone	Very strong		6.15 2.7
LimestoneChert	Medium strong, Fair		0.1
Flint	Potentially reactive, Fair		0.6
Soft Sandstone	Friable, Weak, Poor		0.7
Clay Ironstone	Soft, Deleterious		1.45
PN = 190 INTERPRE	TATION : Poor		47.8
COMMENTS: Indicat:	ion of unstable aggregate, cautior	advised	
OBTHER	R.M.HARDY & ASSO		DEPOSIT No. N75-1060-B6
Engineering Service Company Limited			PAGE 426

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DEPOSIT 1060-B7

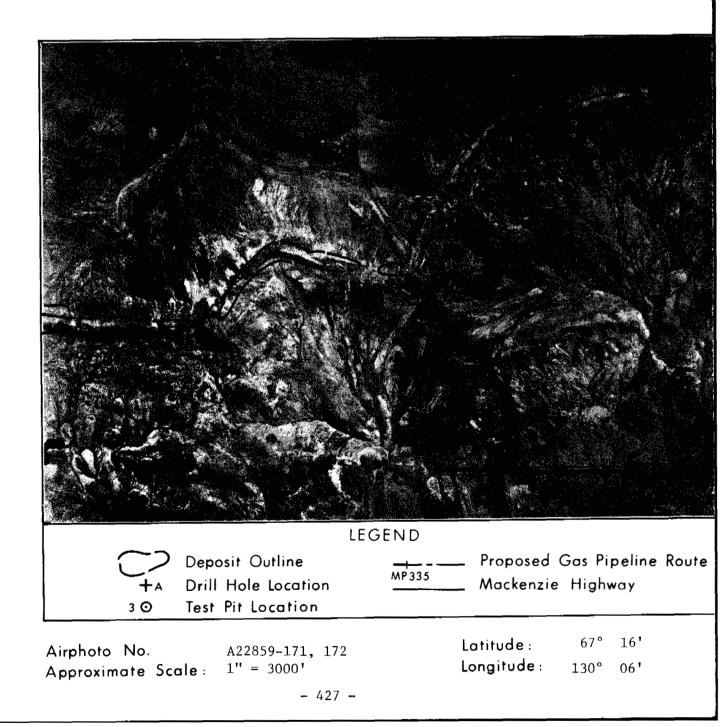
1057-1 EBA

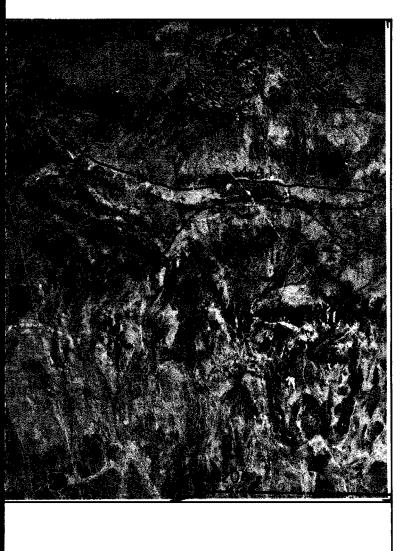
Physical Setting: Deposit 1060-B7 consists of coalescing kame deltas along the crest of a broad bedrock ridge, located 7 miles north of Little Chicago and 2.5 miles from the right of way.

Moterial: GRAVEL - well graded, rounded, with variable silt and sand.

Volume: 12,000,000 cubic yards.

Assessment: Deposit 1060-B7 is a source of good to excellent quality granular material suitable for general fill, backfill, building pads and possible concrete and asphalt aggregate.





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PHYSICAL SETTING

Deposit 1060-B7 is a moraine ridge consisting largely of coalescing kame deltas positioned along the crest of a broad bedrock ridge. It is located 7 miles north of Little Chicago and is 2.5 miles northeast of milepost 211 of the pipeline alignment. This deposit corresponds to source number 1057 in EBA DIAND Granular Materials Inventory Volume II (1974) report.

The moraine ridge is rounded with a crest 30 to 100 feet across and has steep side slopes. It is generally free of overburden although the gentle north-facing slopes may have a peat cover of 1 or 2 feet. The site is well drained due to its form and topographic position, and has an active layer in excess of 20 feet; possibly the entire deposit is free of permafrost.

Access to the pipeline right of way involves a drop in elevation of 800 feet. In places the descent is marked by cliffs, but in other areas "ramps" with more moderate slopes are present. These slopes are covered by till and colluvium.

BIOLOGICAL SETTING

Much of this site has been recently burned and is now covered with a thick growth of shrubs and young trees. On the unburned sections a dense stand of spruce and aspen up to 40 feet in height occurs, with an understory of small shrubs and herbs. The area provides moderate to good habitat for marten, fox, and lynx. Caribou and moose sign were observed at the site during the 1975 survey. Lakes, streams, and associated areas provide moderate to good habitat for aquatic furbearers, black bear, and moose. Grouse and ptarmigan are common in the area. There is no raptor, waterfowl, or fish habitat in the immediate vicinity of the site. Waterfowl are most numerous in the area during the April-May migration period when they use open-water leads on the Mackenzie River.

MATERIAL

Drill hole and test pit logs and the DIAND report indicate material within the moraine ridge is predominately well graded, rounded gravel with variable silt and sand content, and zones of abundant cobbles and boulders. Occasional beds of well graded sand with variable silt are also present.

VOLUME

The maximum depth under the ridge crests is probably 50 feet. A total estimated volume based on an average depth of 25 feet and an area of 550 acres is 12,000,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 1060-B7 is a source of good to excellent quality granular materials. Location of areas to be exploited will be determined by further exploratory drilling. Granular material from this deposit may be used for general fill, backfill in pipeline construction, building pads, and possibly concrete and asphalt aggregate. The gravel will require further testing prior to use in concrete.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

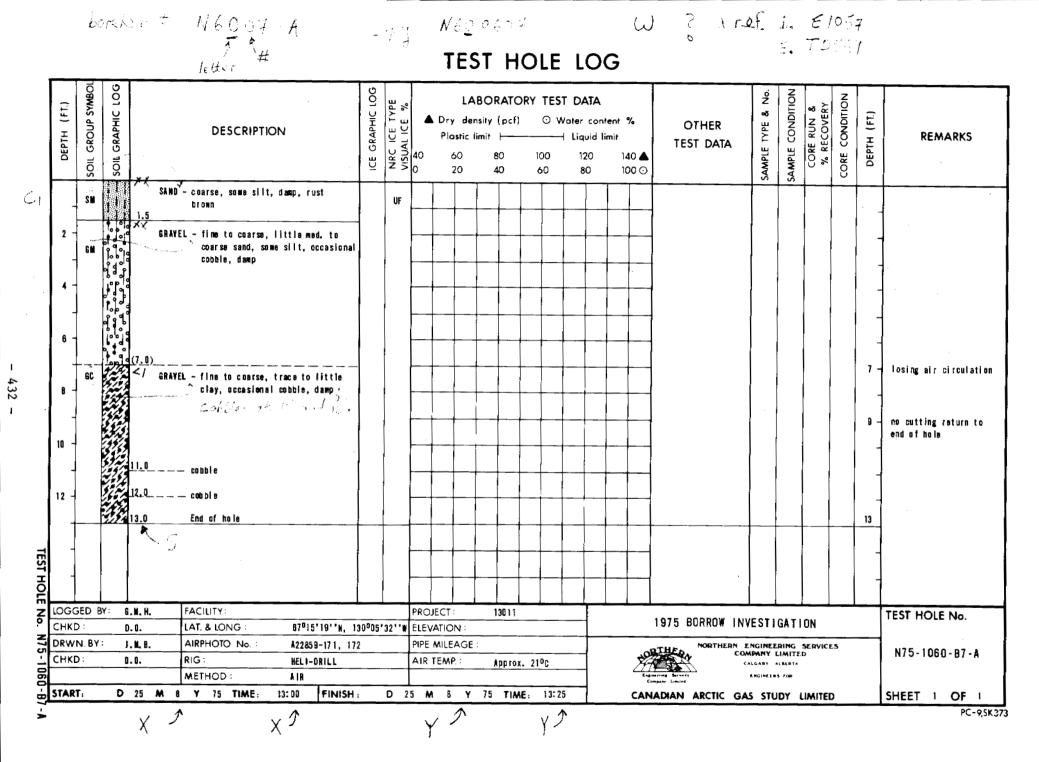
Access to the deposit with equipment may be achieved by barge to Little Chicago and overland from there to the deposit, a distance in excess of 5 miles. Access to the pipeline right of way from the deposit involves a descent of 800 feet over drift covered slopes. No cliffs need be crossed. Some seismic lines could also be used for access. In order to minimize environmental damage, snow roads would be built to transport the borrow material from the deposit to haul points on the right of way, a distance of at least 2 miles.

Vegetative cover would have to be removed from the haul road right of way and excavation areas and disposed of in accordance with land use regulations. The peat cover and overburden would then be stripped from the area to be excavated, and stockpiled around the edge of the excavation.

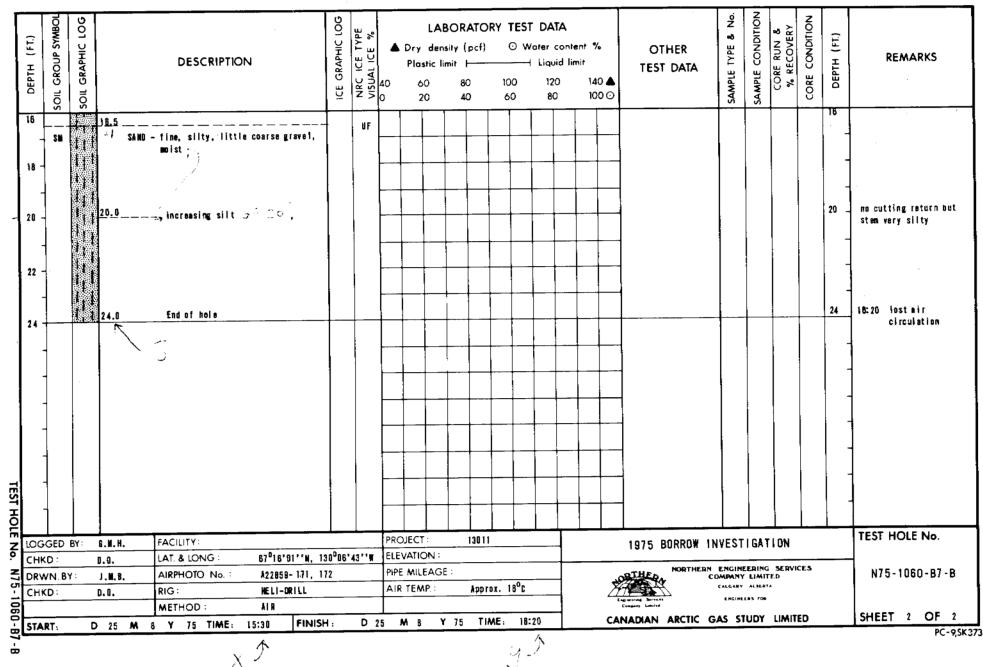
Development of this deposit would involve excavating borrow material evenly or in stages from the higher, well drained areas so that good drainage would be maintained over the area. Open face pit development could be established on the steeper slopes of the deposit. Conventional earthmoving techniques would be used as the deposit is well drained and thawed. Crushing and/or screening of the material may be required to produce quality construction aggregates.

Equipment required for development would be dozers, rippers, end-dump trucks, front-end loaders, as well as screening, crushing, concrete and asphalt plants if required.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.



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DEPTH (FT.)	SOIL GROUP SYMBOI	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE	40 0		BORATO nsity (pcf) imit H 80 40	0	Noter co H Liquid 120 80	ntent limit 14	% 40 ▲ 00 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
+	SM		- ҚҚ Б	PEAT SAND - fine to coarse, silty, rust		UF						<u> </u>			°/	s		_	0	15:30
2 -				brown, damp																
+	_		3.0																-	
4 -	6M	׀ <u>ָ</u>		GRAVEL - fine to coarse, very silty, Fittle fine to medium sand,				_											_	
	ľ			brown, damp, occasional cobb and fine to med, sand	e														-	
6 -												1							5.5	cobble
-			7.0					ł												
8			74	SAND - fine to coarse, very silty, li coarse gravel, occasional cobb				- -											1-	cobble, losing cir- culation in grave!
•	SML			(cobble at 9.5')															-	stratum
]									-+-+	_ -									-	
10 -	5155 F2000					İ													-	
1			< 1	SANGS			\vdash					+							-	
12 -	· F		12.0	— gravelly ·			┢╼╍╴╃╴	-				+							12-	drill vibration and
+	SP-		13.0		um	 Ì	┡┼-			_									-	grinding
14 -	SP-			sand, less silt , - /2'.																
			15.0										Í						7	
16				little gravel, occasional cobble								+							-	
· · · ·	ED BY	: c	. H. H.	FACILITY		L	PROJE												16	
HKD			0,	LAT. & LONG : 67º18'01''	. 130°D8'	43''W			13011				1	975 BORROW INV	ESTI	GATI	ON			TEST HOLE No.
RWN	BY:	J	M. B.	AIRPHOTO No. : A22859-171				ILEAGE		·				THE NORTHERN E		_				
HKD	:	D	0.	RIG: HELI-DAILL			AIR TE		Approx.	16 ⁰ C			200	сом сом	PANY L	IMITEI)			N75-1060-B7-1
				METHOD : AIR									2		L#GI#EE#5					
TART	:	D	25 M	8 Y 75 TIME: 15:30 FIN	SH :	D 21	j M	8 Y	75 TIME	: 18:20	_			DIAN ARCTIC GAS						SHEET 1 OF 2

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OVER:

in the negative

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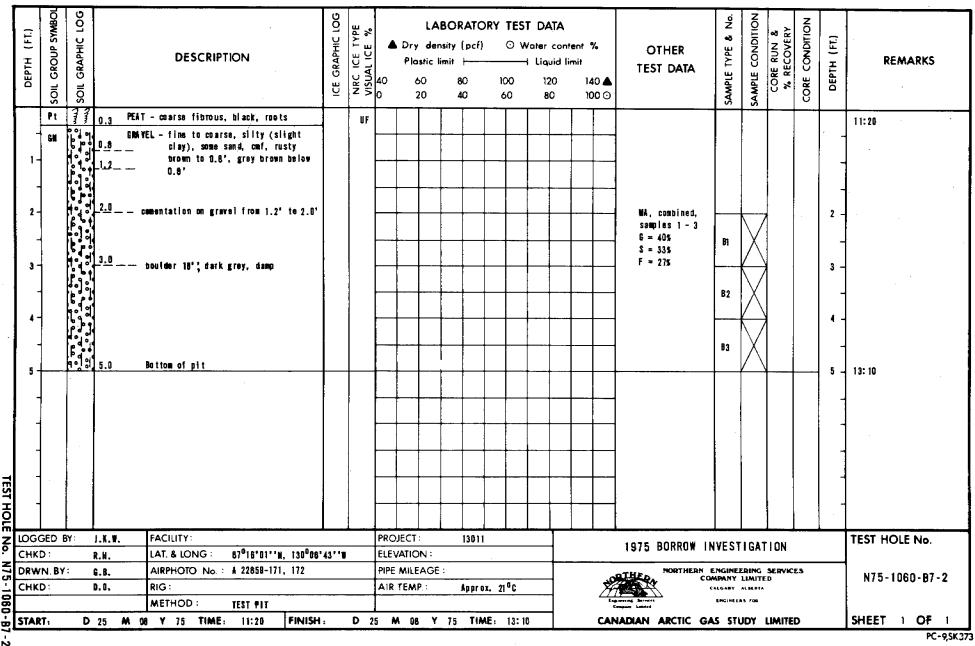
SAMPLE CONDITION 100 ICE GRAPHIC LOG ź GROUP SYMBOI CONDITION CORE RUN & % RECOVERY ТҮРЕ Е % LABORATORY TEST DATA (FT.) ۰ð (FT.) GRAPHIC SAMPLE TYPE OTHER NRC ICE VISUAL ICE 0 05 REMARKS DEPTH DESCRIPTION — Liquid limit DEPTH Plastic limit |-TEST DATA CORE 100 120 140 📥 60 80 SOIL SOIL 60 80 100 🖸 20 40 17:55 PEAT - coarse fibrous, black, roots UF 0.1 GRAVEL - fine to coarse, silty, and GN fine to medium sand, rust brown to 0.6", grey from 0.6" 1-18:15 1 NA, combined samples 1 - 3 **†** 4 1.5___ occasional ironstone, trace coarse sand 81 ы° 16 6 = 49% S = 28% 2.0 boulder, 12"', rounded 2 - 18:35 2 F = 23% (GM-6C) t٩ B2 2 GRAVEL - clayey, isolated pockets of GC 3 - 18:55 clay, cream-coloured 3 83 4 19:30 4.0 boulders (2) 18''+ Occasional boulder to 24" 4.1 Bottom of pit exposed on surface TEST HOLE TEST HOLE No. 13011 PROJECT : FACILITY: LOGGED BY: J.K.W. No. 1975 BORROW INVESTIGATION 67⁰15'19''N, 130⁰05'32''W ELEVATION : CHKD R.H. LAT. & LONG NORTHERN ENGINEERING SERVICES A 22859 - 171, 172 PIPE MILEAGE N75 -AIRPHOTO No. : DRWN. BY F.B.S. N75-1060-B7-1 COMPANY LIMITED Approx. 16⁰C AIR TEMP. CALGARY ALBERTA RIG : CHKD: D.C. ENGINEERS FOR 1060-TEST PIT • METHOD : SHEET I OF 1 CANADIAN ARCTIC GAS STUDY LIMITED D 24 M 08 Y 75 TIME: FINISH : 19: 30 START: D 24 M 08 Y 75 TIME: 17:55 œ PC-9,5K373

TEST HOLE LOG

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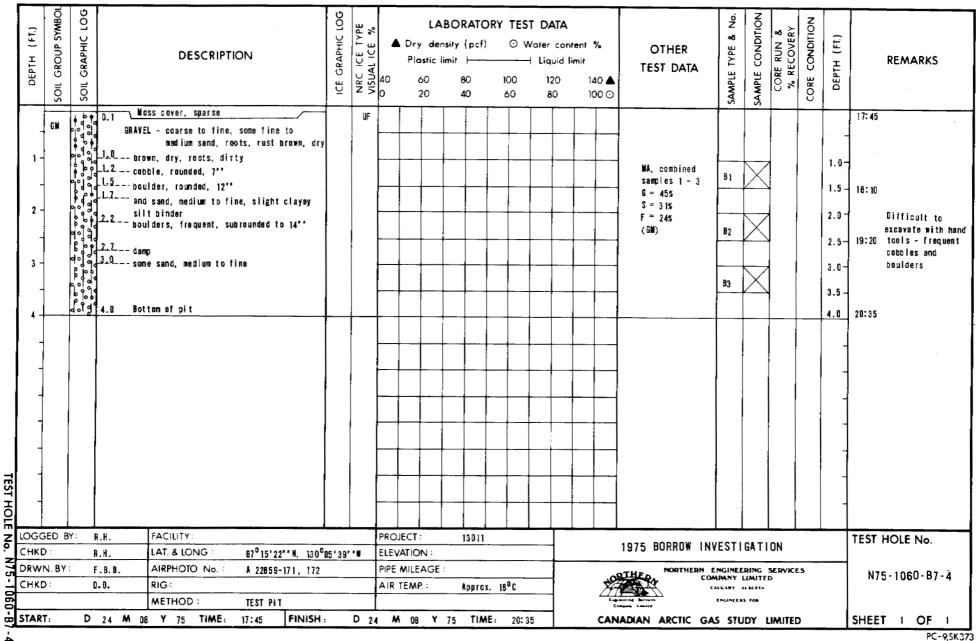


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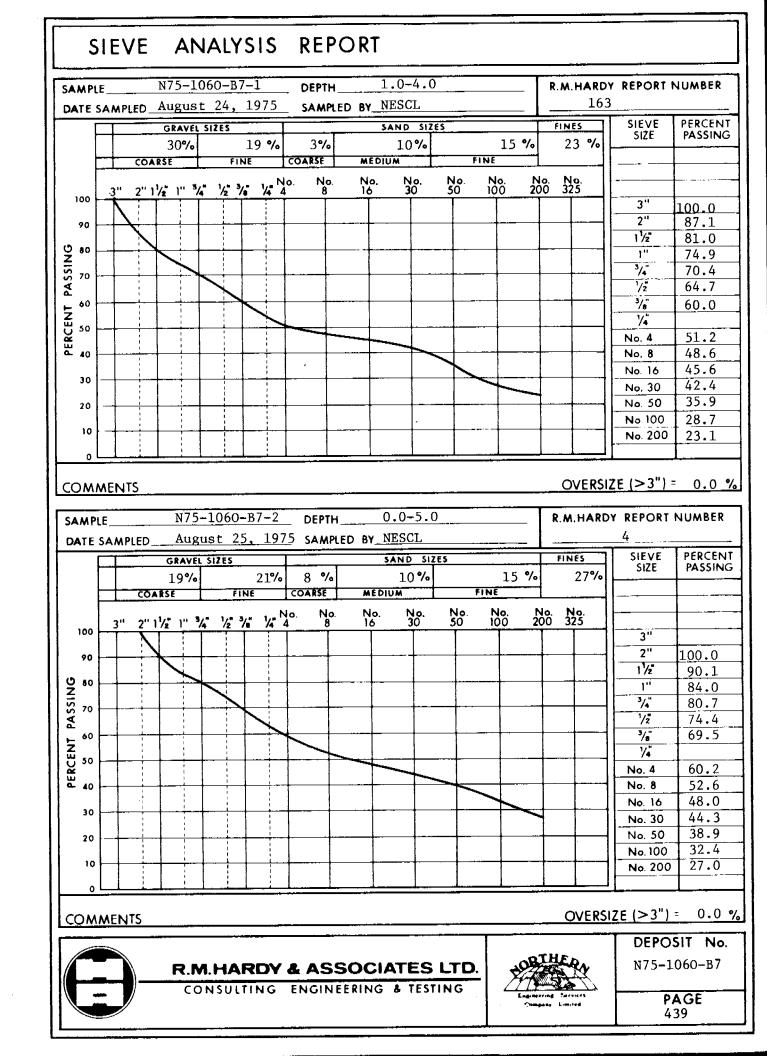
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DEPTH (FT.) SOIL GROUP SYMBOL		SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	L Dry d Plastic 60 20	ensity : limit	(pcf)	0	ST DAT Water c Liqui 120 80	ontent * Limit 14	% 10 ▲ 00 ⊙		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT)	-	REMARKS
2 - 3 - 6W 4 - 5 - 6 -			2.7 5.0	 fine fibrous, black,rootlets trace gravel, coarse, trace sand, fine to medium, orange brown, roots FEL - fine to coarse, silty, slight clay, and sand, cmf, grey brown, cobbles rounded and subangular to 6'', isolated boulder to 10" WEL - fine, little sand, cmf, dark brown, damp, occasional pebble to 1.5'' NY - low plastic, brown, wet Bottom of pit 		UF									#% - 8 - 5 - 4 - 8	MA, combined Samples 1 - 4 G = 53% S = 36% F = 11% (GP-GM)	B1 B2 B3 B4				- 1 2 - 3 3 5 - 5 - 6	12:50	Bug into one corner of test pit
LOGGEI CHKD : DRWN CHKD : START :	: I. BY :	(:	J.K.W. R.H. F.B. D.O.	FACILITY: LAT. & LONG : 67 ⁰ 15'58''N, 130' AIRPHOTO No. : & 22859-171, 172 RIG : METHOD : TEST PIT DB Y 75 TIME: 11:20 FINIS			ELI PIP	DJECT : VATION E MILE/ R TEMP	AGE)X.]6 ⁰ (14:05		2		1975 BORROW	ENGIN OMPAN CALGAR ENGIN	EERIN Y LIMI Y ALBER EERS FO	G SERV ITED	VICES		-1	HOLE No. 5-1060-B7-3 ET <u>1 OF 1</u> PC-959



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DAT	re s/	AMPLED	Aug	ust	25,	, 1	<u>975</u>	SA	MPL	ED BY	NES	CL				-		19	
	Ē	L	GRAV									D 512	/ F S				FINES		PERCENT
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90			GRAVE 25 % RSE		ES FIN	20 1e	%	5	°% E	ME	SANI 10 DIUM	> siz %		FINE		%	24 %	SIEVE SIZE 3" 2" 1½ 1½ 1" 3/4	PERCENT PASSING 100.0 97.9 89.8 83.8 74.8
90 90 90 90 90 90 90 90 90 90 90 90 90 9			GRAVE 25 % RSE		ES FIN	20 1e	%	5	°% E	ME	SANI 10 DIUM	> siz %		FINE		%	24 %	SIEVE SIZE 3" 2" 1½ 1½ 1'' 3/4" 1/2	PERCENT PASSING 100.0 97.9 89.8 83.8 74.8 68.7
90 90 90 90 90 90 90 90 90 90 90 90 90 9			GRAVE 25 % RSE		ES FIN	20 1e	%	5	°% E	ME	SANI 10 DIUM	> siz %		FINE		%	24 %	SIEVE SIZE 3" 2" 1½ 1½ 1' 3/4 1/2 3/6	PERCENT PASSING 100.0 97.9 89.8 83.8 74.8
90 90 90 90 90 90 90 90 90 90 90 90 90 9			GRAVE 25 % RSE		ES FIN	20 1e	%	5	°% E	ME	SANI 10 DIUM	> siz %		FINE		%	24 %	SIEVE SIZE 3" 2" 1½ 1½ 1 ["] 3/4 1½ 3/6 1/2	PERCENT PASSING 100.0 97.9 89.8 83.8 74.8 68.7 63.4
90 90 70 50 90 90 90 90 90 90 90 90 90 90 90 90 90			GRAVE 25 % RSE		ES FIN	20 1e	%	5	°% E	ME	SANI 10 DIUM	> siz %		FINE		%	24 %	SIEVE SIZE 3'' 2'' 1\/z 1'' 3/4 '/2 3/6 '/4 No. 4	PERCENT PASSING 100.0 97.9 89.8 83.8 74.8 68.7 63.4 54.8
PERCENT PASSING			GRAVE 25 % RSE		ES FIN	20 1e	%	5	°% E	ME	SANI 10 DIUM	> siz %		FINE		%	24 %	SIEVE SIZE 3" 2" 1½ 1½ 1½ 1 ¹¹ 3/4 1½ 3/6 1/2 3/6 1/4 No. 4 No. 8	PERCENT PASSING 100.0 97.9 89.8 83.8 74.8 68.7 63.4 54.8 50.8
90 90 70 50 90 90 90 90 90 90 90 90 90 90 90 90 90			GRAVE 25 % RSE		ES FIN	20 1e	%	5	°% E	ME	SANI 10 DIUM	> siz %		FINE		%	24 %	SIEVE SIZE 3" 2" 1½ 1½ 1½ 3/4 1/2 3/6 1/4 1/2 3/6 1/4 No. 4 No. 8 No. 16	PERCENT PASSING 100.0 97.9 89.8 83.8 74.8 68.7 63.4 54.8 50.8 50.8 46.9
PERCENT PASSING 0 0 0 0 0 0 0 0 0 0 0			GRAVE 25 % RSE		ES FIN	20 1e	%	5	°% E	ME	SANI 10 DIUM	> siz %		FINE		%	24 %	SIEVE SIZE 3" 2" 1½ 1½ 1" 3/4 1/2 3/6 1/4 No. 4 No. 4 No. 8 No. 16 No. 30	PERCENT PASSING 100.0 97.9 89.8 83.8 74.8 68.7 63.4 54.8 50.8 46.9 43.0
PERCENT PASSING			GRAVE 25 % RSE		ES FIN	20 1e	%	5	°% E	ME	SANI 10 DIUM	> siz %		FINE		%	24 %	SIEVE SIZE 3" 2" 1½ 1½ 1" 3/4 1½ 1/2 3/6 1/2 3/6 1/2 3/6 1/2 3/6 1/2 3/6 1/2 0 0.0 8 No. 16 No. 30 No. 50	PERCENT PASSING 100.0 97.9 89.8 83.8 74.8 68.7 63.4 54.8 50.8 46.9 43.0 36.2
PERCENT PASSING 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			GRAVE 25 % RSE		ES FIN	20 1e	%	5	°% E	ME	SANI 10 DIUM	> siz %		FINE		%	24 %	SIEVE SIZE 3" 2" 1 ¹ /2 1 ¹ /2 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/6 1 ² 0 1 ³ 0 1 ⁴ 0 1 4</sup> 0 1 ⁴ 0 1 ⁴ 0 1 ⁴ 0 1 ⁴ 0 1 ⁴ 0 1 ⁴ 0 1 ⁴ 1 ⁴ 1 ⁴ 1 ⁴ 1 ⁴ 1 ⁴ 1 ⁴ 1 ⁴	PERCENT PASSING 100.0 97.9 89.8 83.8 74.8 68.7 63.4 54.8 50.8 46.9 43.0 36.2 28.8
00 00 00 00 00 00 00 00 00 00 00 00 00			GRAVE 25 % RSE		ES FIN	20 1e	%	5	°% E	ME	SANI 10 DIUM	> siz %		FINE		%	24 %	SIEVE SIZE 3" 2" 1½ 1½ 1" 3/4 1½ 1/2 3/6 1/2 3/6 1/2 3/6 1/2 3/6 1/2 3/6 1/2 0 0.0 8 No. 16 No. 30 No. 50	PERCENT PASSING 100.0 97.9 89.8 83.8 74.8 68.7 63.4 54.8 50.8 46.9 43.0 36.2
00 00 00 00 00 00 00 00 00 00 00 00 00		3" 2" 1	GRAVE 25 % RSE		ES FIN	20 1e	%	5	°% E	ME	SANI 10 DIUM	> siz %		FINE		No. 200	24 %	SIEVE SIZE 3" 2" 1 ¹ /2 1 ¹ /2 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/4 1 ² 3/6 1 ² 0 1 ³ 0 1 ⁴ 0 1 4</sup> 0 1 ⁴ 0 1 ⁴ 0 1 ⁴ 0 1 ⁴ 0 1 ⁴ 0 1 ⁴ 0 1 ⁴ 1 ⁴ 1 ⁴ 1 ⁴ 1 ⁴ 1 ⁴ 1 ⁴ 1 ⁴	PERCENT PASSING 100.0 97.9 89.8 83.8 74.8 68.7 63.4 54.8 50.8 46.9 43.0 36.2 28.8 23.7
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90 00 00 00 00 00 00 00 00 00 00		3" 2" 1	GRAVE 25 % RSE 1/2* 11"	1. SIZ			%		% FE No. 8				No. 50	FINE	o. 0	No. 200	24 %	SIEVE SIZE 3" 2" 1½ 1½ 1½ 3/4 ½ ½ 1/2 3/6 ½ 1/2 3/6 1/2 3/6 1/2 3/6 1/2 3/6 1/2 3/6 1/2 2 3/6 1/2 2 3/6 1/2 2 2 2 2 2 2 2 2 2 2 2 2 2	PERCENT PASSING 100.0 97.9 89.8 83.8 74.8 68.7 63.4 54.8 50.8 46.9 43.0 36.2 28.8 23.7 0.0 % IT No.

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SUMMARY OF LABORATORY TEST DATA FOR SUITABILITY OF AGGREGATES IN CONCRETE

SAMPLE No. N75-1060-B7-3 DATE SAMPLED : August 25, 1975SAMPLED BY : NESCLDEPTH (FT.):1-5DATE TESTED : February, 1976TESTED BY : RMHA

SOUNDNESS OF AGGREGATE SULPHATE TEST

COARSE AGGREGATE : LOSS = 8.1 % FINE AGGREGATE : LOSS = 13.7 %

LOS ANGELES ABRASION TEST

PERCENT LOSS =

26.1 **%**

ORGANIC IMPURITIES

NUMBER : 2 COAL REMOVED : Nil COAL & ROOTLETS REMOVED : Nil COAL CONTENT : Nil SIGNIFICANCE :

SUMMARY OF ROCK TYPES, COARSE AGGREGATE. (PETROGRAPHIC ANALYSIS)

ROCK	TYPE	CLASSIFICATIONS	TOTAL WEIGHTED COMPONENT %
Quartzite			6.40
Granite		Strong to very strong, Good	2.58
Sandstone			1.92
Siltstone		Medium strong, Good	3.85
Limestone			31.55
Finegrained s altered rocks	silicate	Soft, Medium strong, Good	3.5
Schist			0.45
Flint		Potentially reactive, Fair	0.32
Clay			0.25
Ironstone		Weak, Friable, Deleterious	0.18
PN = 109	INTERPRETA	TION : Excellent	51.0
COMMENTS	: Satisfacto	ry	



R.M.HARDY & ASSOCIATES LTD.

CONSULTING ENGINEERING & TESTING

DEPOSIT No.

N75-1060-B7

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106P - BI-A 458280E 7449470N

X ref EBA 1049 Tech BD6-2

Vie 1049-1 6BA

DEPOSIT 106P-B1

Physical Setting: Deposit 106P-Bl consists of 2 small eskers and a series of kames located 8 miles southeast of Little Chicago and crossed by the right of way.

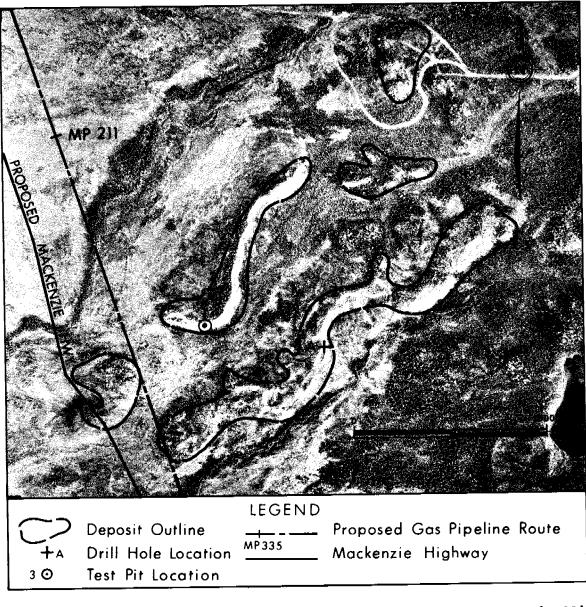
Material: SAND - well to poorly graded with a trace of gravel.

Volume: 1,400,000 cubic yards.

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Assessment: Deposit 106P-Bl is a source of fair quality granular material suitable for general fill and backfill. The deposit is crossed by the right of way facilitating access.



Airphoto No.NW84872-118Approximate Scale :1" = 1000'

Latitude: 67° 09' Longitude: 129° 57'

DEPOSIT 106P-B1

PHYSICAL SETTING

Deposit 106P-Bl consists of 2 small eskers and a series of kames located 8 miles east southeast of Little Chicago. The proposed pipeline right of way crosses the western end of these ridges. This deposit corresponds to source number 1049 in EBA DIAND Granular Materials Inventory Volume II (1974) report.

The eskers and kames range between 30 and 80 feet in height. Crests are generally rounded and about 30 feet across. Side slopes are steep, ranging up to 30 degrees.

This deposit is free from overburden and the eskers and kames are well drained with intervening poorly drained flat areas. Water draining the uplands to the east of the deposit crosses the low lying areas by surface seepage and in poorly defined drainage courses. The active layer is 12 to 15 feet deep in this area. Below this depth the deposit is frozen with very low ice content.

BIOLOGICAL SETTING

Vegetation on the eskers consists of a discontinuous ground cover of grasses and herbs with occasional clumps of white birch and aspen. The kames are generally covered by spruce with willow, rose and fireweed. Much of the area has been burned within approximately the last 20 years. Burned areas provide good habitat for moose. Marten, fox, lynx, caribou, and black bear also occur in the area. Moose tracks were observed along a small lake and an inactive fox den was found at the site during the 1975 survey. Arctic loons and scotters were also observed on the lake. Waterbodies in the area provide good beaver habitat but do not appear to support fish populations.

MATERIAL

Material in this deposit is mainly well graded to poorly graded sand with a trace to little silt and trace of fine gravel. The DIAND drill hole encountered sandy silt and silty, sandy clay. Therefore, quality is not consistent throughout the deposit.

VOLUME

The total estimated volume based on an area of 70 acres and depth of 12 feet is 1,400,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 106P-Bl is a source of fair quality granular material and would be suitable for general fill and backfill in pipeline construction. This source is conveniently located directly on the pipeline route and is free of overburden. The varied quality of material indicates further drilling would be required in order to locate the most promising areas for development.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Snow roads would be built to transport borrow the short distance from borrow areas to haul points on the right of way. This would eliminate any serious environmental damage. Trees and vegetative cover, though not extensive at this site, would be removed and harvested or disposed of in accordance with land use regulations. Overburden at this site consists only of top soil which would be stripped and stockpiled around the perimeter of the borrow pit areas.

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Development would probably involve excavating borrow material in stages from the eskers and kames to a level which would retain the natural drainage over the area. Since drainage of the eskers and kames is good and ice contents very low, conventional earthmoving techniques would be used.

Equipment required for development would be dozers, rippers, end dump trucks, and front-end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

	BOL	00	t NGPOI-A copy								<u> </u>		X (्र .े च	\mathcal{T}_{1}	0.007 0.60 E T	2	······
DEPTH (FT.)	GROUP S		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE	40 0	Dry den	sity (pcf	ORY TES) ⊙ v 100 60	Vater con	imit 14	% 0▲ 0⊙	OTHER TEST DATA	SAMPLE TYPE & No.	AMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FL)	REMARKS
2 -	SM		SAND - fine to coarse, silty, trace fine gravel, light brown, dry, dusty		UF									0,	<u> </u>			0	20:31 4%** Walmac
4 -															ĺ			-	fosing air through dr sand
6 		1 7.0	→ damp, brown, trace silt > 7															1	
	SP	- XX	SAMD - fine to medium, (trace coarse), clean, brown, damp :															8 -	te 3 7/8°° Walmac
2 -		(12:0	very slight silt at (2)		Nbn													12 -	20:37
														"	1				,
I GGEI	D BY:	6. H . H	. FACILITY			PROJE												24	
IKD :		Ð.Q.	LAT. & LONG : 87 ⁰ 09'35''K, 129 ⁰ 57	'37'	'W		TION	13011				19	175 BORROW INVE	STIĞ		N		·	TEST HOLE No.
WN. IKD :	BY:	J. N. B J. K. W.				PIPE N	MLEAGE : EMP. :	Appro	. 21 ⁰ C			LORT F		GINEER MNY LI	MITED	ERVICES			N75-106P-B1-A

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PC-9,5K373

GROUP SYMBOL ICE GRAPHIC LOG SAMPLE TYPE & No. SAMPLE CONDITION GRAPHIC LOG CONDITION LABORATORY TEST DATA NRC ICE TYPE VISUAL ICE % CORE RUN & % RECOVERY DEPTH (FL) DEPTH (FT.) ▲ Dry density (pcf) ○ Water content % OTHER REMARKS DESCRIPTION ---- Liquid limit Plastic limit |-TEST DATA CORE 60 80 100 120 140 🔺 SOIL SOIL 100 🖸 20 40 60 80 24 24 Nbn ---SAMD (cont'd) SP 28.0 _____ fine to medium, trace silt, moist 26 when thawed, grey brown c = 25 . 28 29.0 29,0 F SAND - coarse, trace fine, little silt, SI trace fine gravel 30 🐟 visible ice chunks in returns 🔪 32.0 32.0 32 SAND - fine to medium, trace silt, (poorly graded) Nb SP 34 -38 -38 21:10 End of hole 38.0 38 TEST HOLE . 5 TEST HOLE No. PROJECT : FACILITY 13011 LOGGED BY: 6. M. H. 1975 BORROW INVESTIGATION ELEVATION LAT. & LONG 87°08'35''N, 129°57'37''W CHKD 0.0. NORTHERN ENGINEERING SERVICES PIPE MILEAGE NW 84872-118 J. M. B. AIRPHOTO No. N75-106P-81-A DRWN.BY: COMPANY LIMITED HELL-BRILL AIR TEMP. Approx. 21⁰C CALGARY ALBERTA RIG: CHKD: 1.8.8. ENGINEERS FOR AIR METHOD : SHEET 2 OF 2 D 25 M 8 Y 75 TIME: CANADIAN ARCTIC GAS STUDY LIMITED FINISH : 21:10 D 25 M 8 Y 75 TIME: 20:30 START: PC-9.5K373 -)^{*} \mathbf{N}

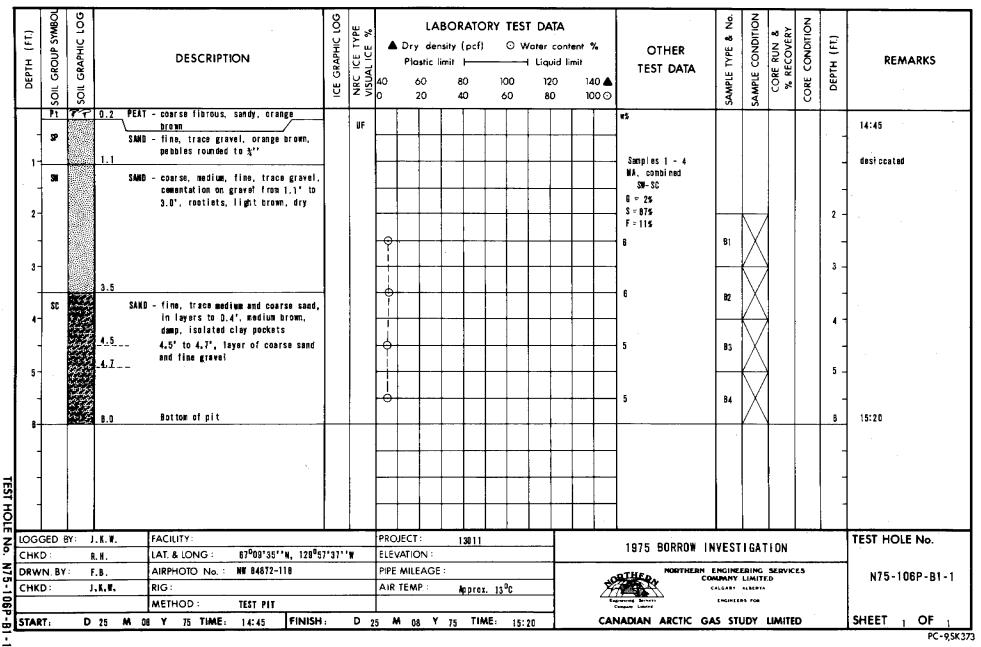
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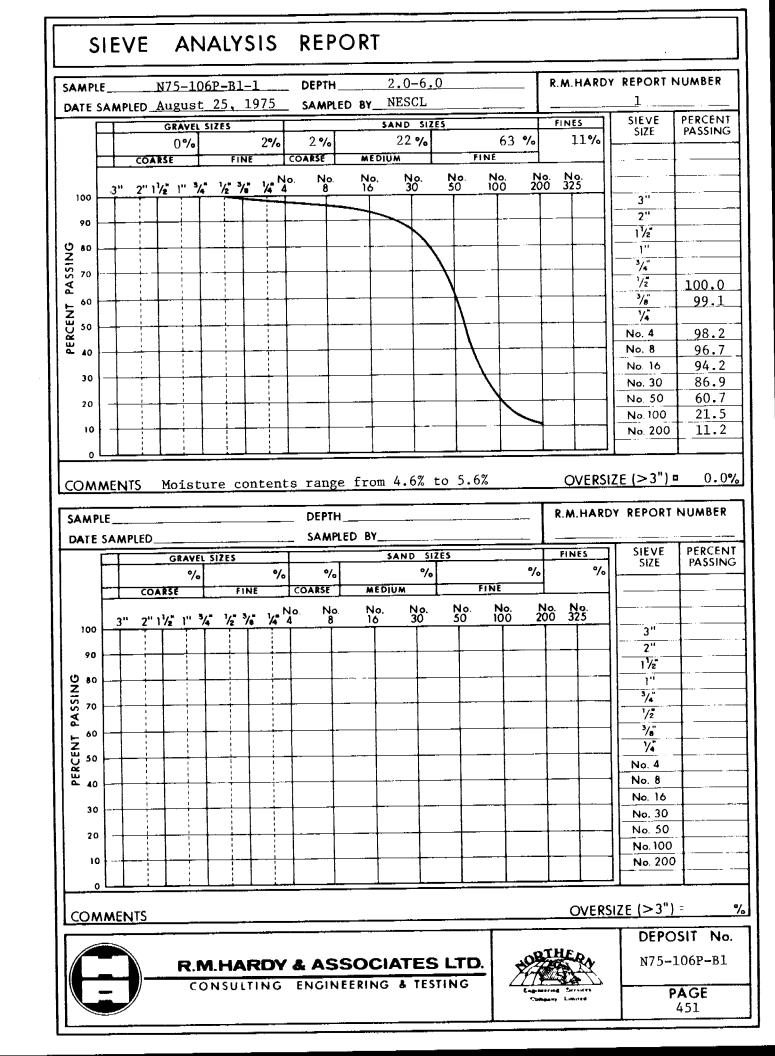
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TEST HOLE LOG

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106P-B2-A 460850E 7447830N (C) correction

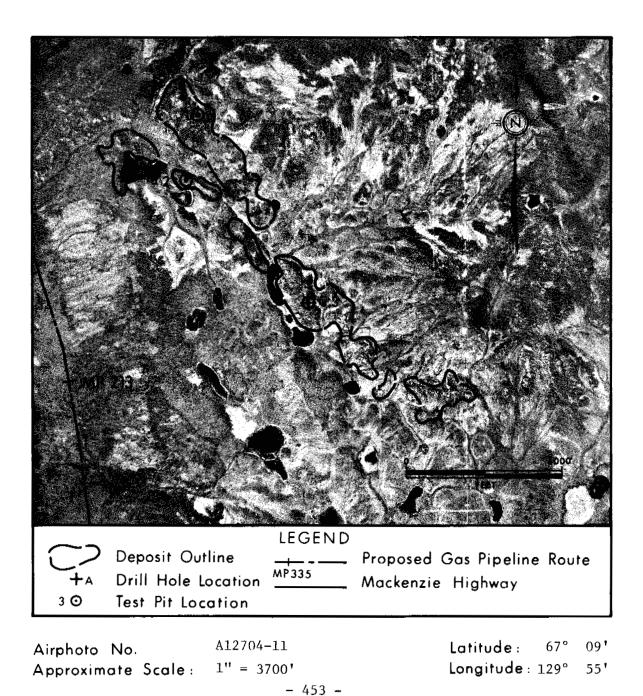
120 1050-1 (BA

Physical Setting: Deposit 106P-B2 is a kame complex located 9.5 miles ESE of Little Chicago and less than 2 miles northeast of milepost 212 on the right of way.

Material: SAND and CRAVEL - interbedded.

Volume: 5,500,000 cubic yards.

Assessment: Deposit 106P-B2 is a source of fair quality granular material suitable for general fill and backfill.



DEPOSIT 106P-B2

PHYSICAL SETTING

This deposit is a kame complex located about 9.5 miles east-southeast of Little Chicago and less than 2 miles northeast of milepost 212 on the proposed pipeline right of way. This deposit corresponds to source number 1050 in EBA DIAND Granular Materials Inventory Volume II (1974).

The kame complex has local relief of about 50 feet. In the northeastern part of the deposit a creek has incised 100 feet or more below the general level of the surrounding terrain. The complex has less than 1 foot of overburden and is well drained. Drill hole 106P-B2-C indicates an active layer of at least 15 feet and low ice content.

A moderately steep escarpment lies between the pipeline alignment and the deposit. However, the creek valley that dissects the deposit provides good access to the pipeline route.

BIOLOGICAL SETTING

Most of this site has been burned and, except for scattered groves of spruce, now supports a thick growth of shrubs with a grass-herb ground cover. The area provides low to moderately productive habitat for marten, fox, lynx, black bear and moose. Limited areas of caribou habitat also occur. Lakes and streams provide low to moderately productive habitat for aquatic furbearers and are used throughout the openwater season by migratory and resident waterfowl. It is unlikely that any of these lakes support fish populations.

MATERIAL

Material in this deposit consists of interbedded sand and gravel. Sands are well graded with variable silt and gravel content. Gravel is poorly graded, fine and rounded with a high percentage of sand and a trace of silt.

VOLUME

Total estimated volume, based on a maximum depth of 30 feet under hill crests and an area of 370 acres is 5,500,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 106P-B2 is a source of fair quality granular material and is suitable for general fill, and backfill in pipeline construction. Initially, extensive drilling would be required on the deposit to locate areas of better quality material.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigations. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

In order to minimize environmental damage, snow roads would be built for transporting the material a distance of 1.8 miles from the deposit to haul points on the right of way. This road would probably follow the creek valley in order to avoid crossing the escarpment that lies west of the deposit.

The thick brush cover would be removed and disposed of in accordance with land use regulations followed by a minimal amount of stripping to remove the thin peat and silt overburden. This material would be stockpiled around the edge of the selected sites. Borrow material could be excavated evenly from the higher, well drained areas so that good drainage would be established. Open face pit development could also be accomplished on some of the steep slopes of the deposit. This site has fairly low ice contents so that conventional earth moving techniques would be used. However, any areas of high ice cementation might require blasting. The excavated material may have to be stockpiled, thawed and drained before it is used.

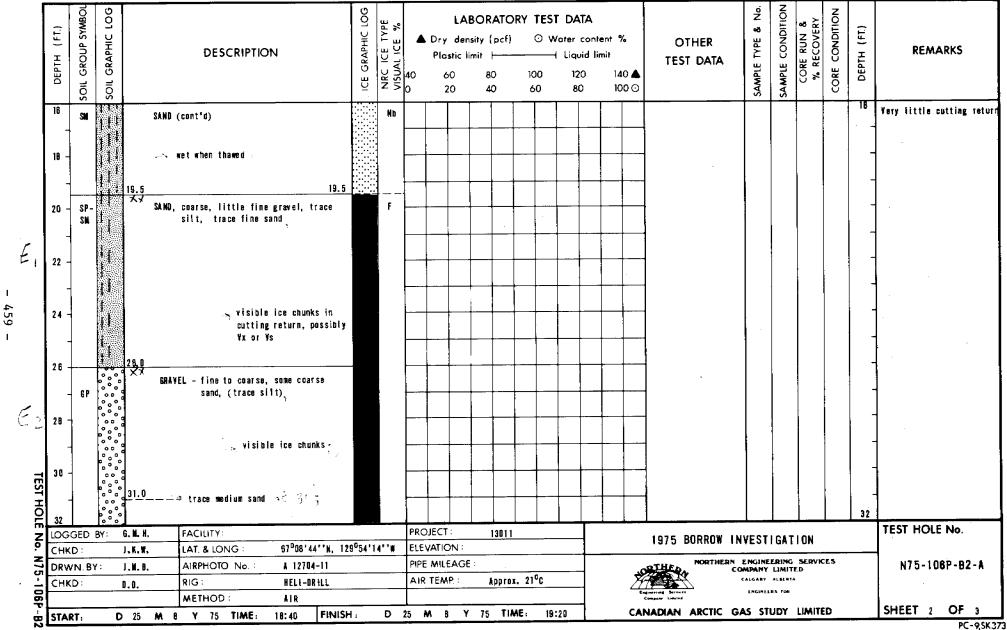
Equipment required for development would be dozers, rippers, end-dump trucks and front-end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

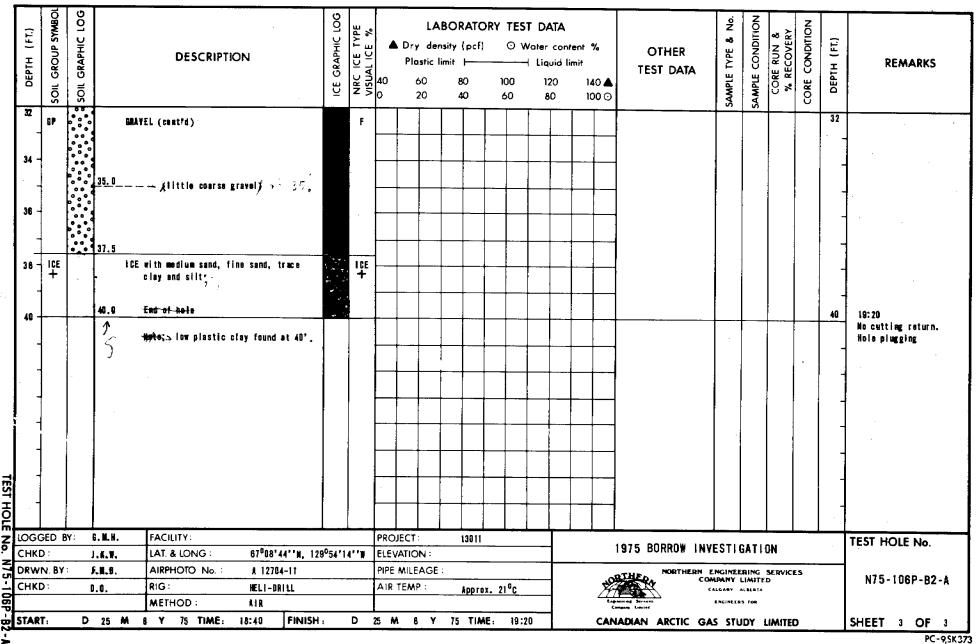
= 11- Friend supp 112 Friend W. 1 7747256 460850 Xref D. Ens TEST HOLE LOG S. 10.35-00 **GROUP SYMBO** GRAPHIC LOG SAMPLE CONDITION ź CONDITION LABORATORY TEST DATA TYPE E % CORE RUN & % RECOVERY DEPTH (FT.) GRAPHIC •ð (FT) ▲ Dry density (pcf) O Water content % OTHER SAMPLE TYPE NRC ICE VISUAL ICE 0 05 DESCRIPTION Plastic limit |-REMARKS - Liquid limit DEPTH TEST DATA CORE 100 140 📥 60 80 120 ۳ sol SOIL 20 40 100 🖸 60 80 ι, GRAVEL-fine (trace coarse), very silty, UF 4%'' Walmac 🔿 light brown, damp Gr Ĩ 2 -51 SAMD - fine to cearse, silty, little fine gravel, damp, brewn 6-1 losing air circulation 8 XХ SAMD - (less silty) SP. 10 -10 -18:48 11.0 --- moist, less coarse sand at 1. Frank 12. <u>12.0</u> → → more coarse gravel to approx. depth 12 -14.8' TEST HOLE γ_{A} 2 10 8 - fine to medium, silty, trace gravel, -71 molst, dark brown, infrequent * hole plugging slit cebble . sticking to stem 18.0 18 ş LOGGED BY: >> G.N.H. FACILITY PROJECT : 1301 1 TEST HOLE No. **1975 BORROW INVESTIGATION** CHKD : う しまれ LAT. & LONG : 67⁰08*44***N, 129⁰54*14*** ELEVATION : DRWN. BY: AIRPHOTO No. : 4901-51 A 12704-11 J.N.B. PIPE MILEAGE : NORTHERN ENGINEERING SERVICES N75-106P-B2-A COMMANY LIMITED CHKD: J. S. RIG : AIR TEMP : Approx. 21°C HELI-DRILL CALGARY ALBERTA METHOD : ALB ENGINEERS FOR 82 START: D 25 M 8 Y 75 TIME: 18:40 FINISH: D 25 M 8 Y 75 TIME: 19:20 CANADIAN ARCTIC GAS STUDY LIMITED SHEET 1 OF 3. PC-9,5K373 хŶ

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000 GRAPHIC LOG SAMPLE CONDITION CONDITION NRC ICE TYPE VISUAL ICE % 0 & CORE RUN & % RECOVERY ۰ð (FT.) GRAPHIC ▲ Dry density (pcf) 🛈 Water content % OTHER SAMPLE TYPE DESCRIPTION REMARKS DEPTH Plastic limit + - Liquid limit TEST DATA CORE 100 120 140 📥 60 80 ۳ soil 100 🖸 20 40 60 80 **?**? ?? UF PEAT - coarse fibrous, crange brown SiLT and gravel, fine, trace sand, coarse, 0 7 peoples rounded to %'' MA. combined. isolated iron stains CLAY - low plastic, some sand, trace fine samples 1 - 4 gravel, dry, light brown, white G = 10% B1 | calcifled layers at 1.2" and 1.8" S = 38\$ F = 5452 . CLAY - low plastic, grey, friable B2 SAND - fine, some fine gravel, trace siit, 3 medium brown, damp 83 3.7SMD - very fine, clean, brown 84 4.8 5 SAMB - cmf, trace fine gravel, brown G = 9% S = 80% - some silt, trace gravel, brown, SI NO 85 F = 31% damp. 8 Bottom of pit 6.4

PROJECT

67009'48''N, 128055'51''W

FINISH :

A 12704-11

TEST PIT

ELEVATION :

AIR TEMP.

PIPE MILEAGE :

D 25 M 08 Y 75 TIME:

130 11

Approx. 13⁰C

TEST HOLE LOG

LABORATORY TEST DATA

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1975 BORROW INVESTIGATION

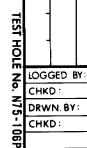
CANADIAN ARCTIC GAS STUDY LIMITED

NORTHERN ENGINEERING SERVICES

COMPANY LIMITED

CALGARY ALBERTA

ENGINEERS FOR



-82

START

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GROUP SYMBOI

SOIL

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SP-3 -

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SP

SN

FACILITY

RIG :

D 25 M 08 Y 75 TIME:

LAT. & LONG :

METHOD :

AIRPHOTO No. 1

1.8.0.

R.H.

F.B.

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8 -SW

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(FT.)

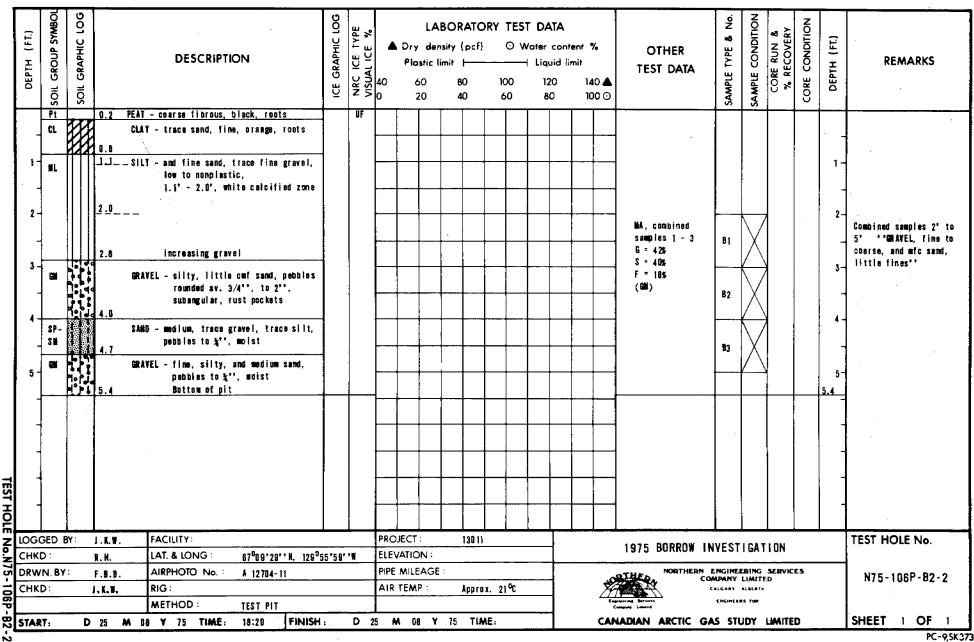
DEPTH

PC-9.5K373

TEST HOLE No.

SHEET 1 OF

N75-106P-B2-1



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DEPTH (FI.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	▲ D⊤ Pl 40		sity (pcf)	0	Nater cor Liquid 120 80	ntent 🍫		SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FT.)	REMARKS
	ў Рt	3	PEN	T - coarse fibrous, sandy, dark brown,	+									+ <u>"</u>	5	1			14:45
-	SM		0.3 SAN	dry D - very fine, silty, trace gravel, diy to desiccated	-	UF			-				-					· -	
1 -			1.3 1.0	- 1.5' calcified zone	1								- MA, combined samples 1 - 5		$\overline{\Lambda}$	1		1-	14:55
_	Gill-			YEL - fine, and fine sand, trace silt. pebbles av. %'' to 3''.									G = 20% S = 80% F = 12%	B1	M				
2 -	SM												(SW-SW)	B2	M			2 -	15:00 Basy to excavate
3 -				cleaner	:								-		$\left \right\rangle$	*		3 -	
-		• °]		D - medium to coarse, trace fine grave				-		┼┟╴			-	B3	X			-	
4 -	SP		un n	clean	.,								-	B4	Ń	X	1	4 -	: 15:20 +3" = 6.3% of tota samples
5 ~	6P		f GRJ	WEL – little sand, medium to coarse, pebbles to ≵", occasionally to									_	B5	K			5 -	
6 -			<u>8.0</u>	2** Bottom of pit				-			+ +				<u>/ '</u>	\		6 -	15:30
-													-					-	
-								-			+		-					-	
-													-					-	
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	.D : /N. BY		<u>R.H.</u>	LAT. & LONG : 87 ⁰ 08'44''N, AIRPHOTO No. : 1 A 12704-11	129*54	14'''	ELEVAT PIPE M		:				NORTHERN				CES		N75-106P-82
			G.B. J.K.W.	RIG:			AIR TE		····	ox. 21 ⁰ C		Ź	°	CALGARY					[[#10-100C-82
				METHOD : TEST PIT			36 M	09 V	75 TI	ME. 19	: 30	C.	Engenerate Service Company Constant			LIMIT	ΈD		SHEET 1 OF
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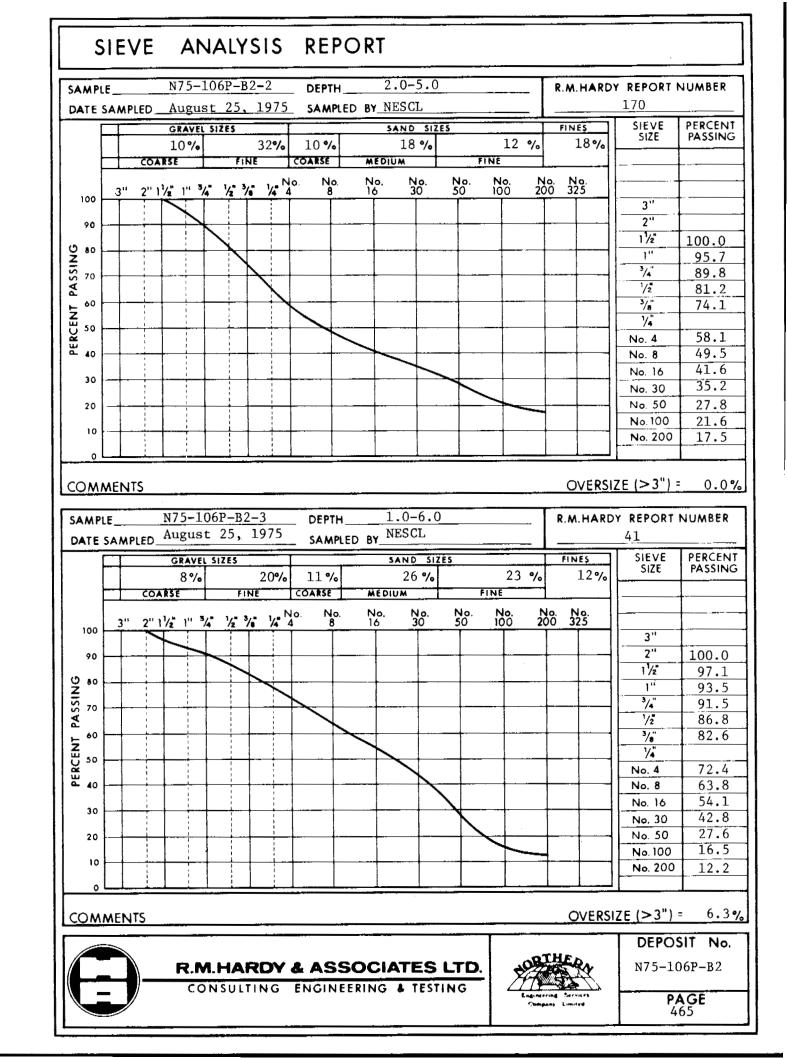
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106 P - B3 - A 456420E 7436140N B3 - B 456570E 7433810N

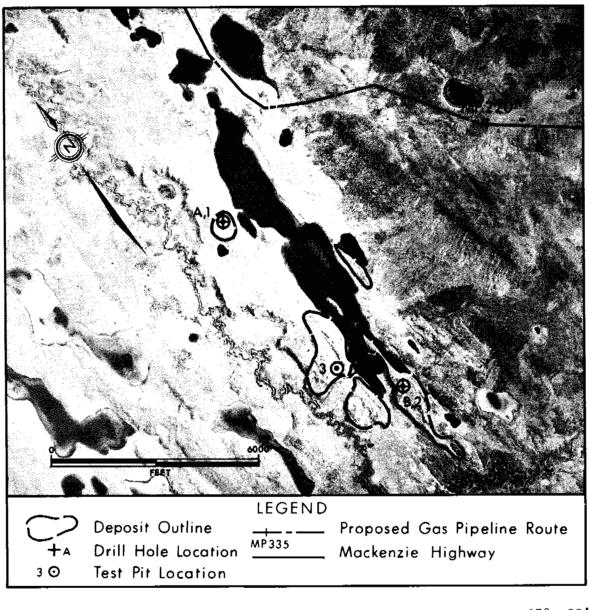
1200 1047-1 EBA

Physical Setting: Deposit 106P-B3 is an esker and kame complex located 13 miles southeast of Little Chicago and about 2 miles west of milepost 220 on the right of way.

Material: SAND and GRAVEL - variable throughout the deposit.

Volume: 4,200,000 cubic yards.

Assessment: Deposit 106P-B3 is a source of fair quality granular material suitable for general fill and backfill. Access to the deposit is good overland from the right of way.



Airphoto No. A22890-85 Approximate Scale : 1" = 2750' Latitude : 67° 02' Longitude : 130° 00'

DEPOSIT 106P-B3

PHYSICAL SETTING

This deposit is an esker and kame complex located 13 miles southeast of Little Chicago and about 2 miles west of milepost 220 of the proposed pipeline right of way. The deposit corresponds to a portion of source number 1047 in EBA DIAND Granular Materials Inventory Volume II (1974) report.

The complex has local relief to about 50 feet with steep slopes flanking the hills and ridges. The small northern part of the deposit is a flat topped kame with sides defined by 10 foot scarps. Overburden is negligible except in depressions where it may exceed 5 feet. Kames and eskers are all well drained; intervening low lying areas are less perfectly drained. The active layer is about 5 feet deep in the north and 10 to 15 feet deep in other parts of the deposit.

East of the deposit, a lacustrine plain with high ice contents is present.

BIOLOGICAL SETTING

Much of this site has been recently burned, although scattered clumps of spruce and birch up to 40 feet high are present. The understory consists largely of alder, rose, and willow with a ground cover of grasses and sedges in low lying areas. The area provides habitat for caribou, lynx, fox, marten, black bear, moose, and caribou. Moose may migrate through this area in late fall and early spring enroute to or from islands in the Mackenzie River. An unidentified eagle and an occupied beaver lodge were observed at the site in 1975. The small lakes in the area do not appear to provide suitable fish habitat.

MATERIAL

Material in this deposit appears to be quite variable. Sand is predominant and is generally medium grained and clean with occasional

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fine gravel. Two test pits encountered interbedded sand and gravel. The gravel in this case is rounded, and either fine grained or well graded with considerable sand. Traces of silt and thin lenses of clay occur periodically. Low moisture contents were found at all test sites.

VOLUME

Maximum depths of granular material at this deposit are in excess of 50 feet. Total estimated volume based on this depth and an area of 210 acres is 4,200,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 106P-B3 is a source of fair quality granular material which is suitable for general fill and backfill in pipeline construction. Extensive drilling and test pitting would be required to locate areas of better quality material prior to any excavation.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the deposit from the pipeline right of way would be 2 miles overland to the deposit. In order to minimize environmental damage, snow roads would be built to transport the borrow material from the deposit to haul points on the right of way after the right of way has been cleared of trees and scrub brush.

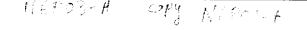
At selected sites, the tree and vegetative cover, although minimal, would be removed and disposed of in accordance with land use regulations. The kames and eskers are essentially free of overburden, therefore, little or no stripping will be required.

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Excavation would involve removing the borrow material evenly from higher, well drained areas so that good drainage would be established over the site. Open face pit development could also be carried out at steeper slopes on eskers and kames. Conventional earthmoving techniques would probably be all that is required for excavation at this site as ice contents are low. However, blasting would be used if areas of high ice cementation were encountered.

Equipment required for development would be dozers, rippers, end-dump trucks and front-end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.



	DEPTH (FT)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0		BORATC hisity (pcf) imit	Οw			OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
\mathcal{B}_{ℓ}					SAND-fine grained, clean light rust brown to brown,										\square				Û	13:15 insert bit
- Su	-	1			damp, poorly graded		UF								ĺ				· _	-
	2 -	SP											$ \begin{bmatrix} - & - & - & - & - & - & - & - & - & -$						-	
R	· -			3.5									$\left[- \right] $						-	
B:	4 -	CL	R		CLAY — trace fine sand, grey, damp.								┝╌┼╌╢						-	· · ·
	-		W/A	5.0		-							<u>├</u> ─┼─-┫						-	
01	6 -	SP			SAND-medium,trace coarse, clean _s (<u>B.D</u>		<u> </u>												6 -	new 3 7/8'' Walmac
	-	4					Nb												_	
472	8 -			8.0	Solittle coarse of the															
21	10 ⁻	SW			SAND-cmf. little fine gravel clean											-			1	
	12			14-0															-	
TES	14 -			14.0	SAND-medium,trace coarse, clean														-	
	-				poorly graded.														-	
Ē	16 1060	L GED	BY :	G.N.H	FACILITY:	•••		PROJ	ECT :	13011		<u> </u>					[16	TEST HOLE No.
ē.	СНК			J.K.W.	LAT. & LONG : 67002'33''N, 13000	05' ' W								1975 BORROW	I NY	ESTI	GATI	ON		
N75	DRW		1:	J. M. B	AIRPHOTO No. : 1 22890-85				MILEAGE					THED NORTHERN E			SERVIC	ES		N75-106P-B3-A
- 10	СНК	D:		0.0.	RIG: KELI-DRILL			AIR	EMP. :	Approx.	18 ⁰ C		ŽA		ALGARY EMGIMEER	AL BERTA				
06P -	STAR		D	28 M	METHOD: AIR 08 Y 75 TIME: 13:15 FINISH		D 1	6 M	DR Y	75 TIM	E: 13:3		CAN	ADIAN ARCTIC GA			LIMITE	D		SHEET 1 OF 2
B3-A		•••					- 1	<u> </u>	1		1	I								PC-9,5K373

DEPTH (FT.)	·	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE	40 0	Pla	y den:		ORY T (f) G 100 60) w)		imit 14	¢ 0 ▲ 0 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FI.)	REMARKS
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18	3]																		:				
	-							\vdash		++					+							-	
				20.0																			
20	1	SW		611	D-medium to coarse, little fine to	1::::																	
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23	2 -						:																
	-								<u> </u>			+ +			+						1	-	
	1			24.0			3		1					1									
2	4-				-— trace fine gravel		3															-	
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3	0+			30.0					+						1.							-	
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TEST HOLE	1				Pud of bala		-																19.90
Fi 36	_			38.0	End of hole		·1	-	OJECT						J	.		1			1	38	13:38 TEST HOLE No.
	GG HKD	ED	BI	G.N.H	FACILITY: LAT. & LONG : 67 ⁰ 02'33''N, 130 ⁰ 0	0'05''	' 1	_	EVATIO		13011						1975 BORROW	NVES	TIG	TION	I		TEGT TICLE NO.
z⊢		N. BY	v ·	J.K.W.	AIRPHOTO No. : 1 22890-85					EAGE	:			<u> </u> -			NORTHERN	ENGINE	ERING	SERVE	CES		N75 1000 03 4
ິ 🗕	HKD	_	• •	<u> </u>					RTEN			x. 18 ⁰ C				202	co co	MPANY	LIMIT	F.D			N75-106P-B3-A
ᇙᆣ				J.U.	RIG: HELI-BRILL METHOD: AIR											<u></u>	awarand Berrents	[MG) M [2	RS FOR				
⊸⊢	ARI	r .		26 M	08 Y 75 TIME: 13:15 FINIS	 1 :	D	26	M 0	8 Y	75 1	IME:	13:3	8		CAN	IADIAN ARCTIC GA	s sti	UDY	LIMIT	ED		SHEET 2 OF 2
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YEST HOLE LOG

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	TH (FT.)	GROUP SYMBOL			•••	DESCRIPTION		ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %		L. Dry de Plastic	ensity	(pcf)	۰ ن	T DATA Vater co H Liquid	ntent	%	OTHER TEST DATA	TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CONDITION	DEPTH (FL)	REMARKS
	DEPTH	SOIL	ŝ	รี				ICE G	NRC	40 0	60 20		ici ici	100 60	120 80		40 ▲ 00 ⊙		SAMPLE TYPE	SAMPLE	COR R &	CORE	DEP1	
- 1			纖		.5	SAND-silty to 0.5'					I		T										0	
	2	SW				SAND — fine to coarse, little fine gravel, trace silt, brown, damp to 4.5°			UF														-	
	4 -			_	<u>4.5</u>	— — moist													5 6 7				-	
	6 - 6 -				8.0																			
	10 -	SP				SAND—fine to medium, moist	<u>10,0</u>		ND							-							-	
2	12 -																							some caving due to thawing.
TEST HOLE	14 ⁻ -																							
듥		GED	_ <u>K⊗</u> BY∶	9993	6. N .H	FACILITY:		·····,	1	PRO	 JECT :		13011		1 1 1				<u> </u>	1	<u>i</u>	l	110	TEST HOLE No.
- -	СНК				J.K.W.	LAT. & LONG : 87001*18**N, 1	29 ⁰ 59'	50''¥		+	ATION		iaari					1975 BORROV	1 NV	ESTI	GATI	ON		1.501 110LE 110.
N75-1	DRWI	N. B	(:		J. H. 8 D.O.	AIRPHOTO No. : A 22890-85 RIG : HELI-BRILL					MILEAC		Appro:	x. 18 ⁰ C			200	ZARA TRY	ENGINE MPANY CALGARY ENGINEE	LIMETE	SERVIC ED	ES		N75-106P-B3
융	STAR	τ.		D	26 M		FINISH		D 🤉	1	1 08	Y 75	TIM	E: 15:	15		CAN	ADIAN ARCTIC GA			LIMITE	D		SHEET 1 OF 3

	DEPIH (FI.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Pla ć		sity (p	cf)	100 60	Nater	conte id li n 0	nit 140		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
1	6				SAND (cont'd)		Nb																16	······································
	-			17.5	— fine to medium grained																		-	
1	6 -																_						18 -	no cutting return
	-	SP												$\left \right $	-							ļ	-	,
2	0 -														-	-							-	· ·
	-																						-	¢
2	2 -			1	some coarse sand to fine gravel			-	$\left \cdot \right $						\rightarrow	+							-	
	-				- trace fine gravel																		-	
2	4 -			24.0	trace coarse sand (very little			-	$\left \right $					$\left \right $	\rightarrow								-	
	-				gravel) trace fine gravel							-											-	
2	16 -		0.0	26.0				┢──				+				_							28 -	14:55
		GP			GRAYEL- fine, and med. to coarse sand.		F									_		•					_	
,	8			28-0			L									_							28 -	approx. 18'' of stou
Ι.					SAND-medium to coarse, little fine gravel, trace silt.		F																	in the hole
],		SP			ice visible in cutting return		(٧)																	
1																		:						
	12																						-	-
zιc	GG	GED E	3Y :	G. N. H	FACILITY			-	DJECT		1301)			· · ·				1975 BORRO		VEST	TADI			TEST HOLE No.
<u> </u>		D : N. BY	:	J.K.W.	LAT. & LONG : 87 ⁰ 01'18"'N, 129 ⁰ AIRPHOTO No. : & 22890-85	59'5D'	1	+	VATIO									NORTHERN E						
C	нк				RIG : KEL1-ORILL			<u> </u>	TEMP		pprox.	16 ⁰ (2				XQ		LGART	LIMITE		_		N75-106P-B3-
		-	-		METHOD : AIR												E-401	empany Lumited	ENGINE LI			_		
ت ا	AR	1:		26 M	08 Y 75 TIME: 14:30 FINISH		U	26 /	vn ()8	T	75 1	I IME:	: 15:	15			CAN	IADIAN ARCTIC GA	5 511	JDY	LIMITE	D		SHEET 2 OF 3

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	DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	4 0 0		density	(pcf)	0RY TI 0 100 60	Woter Lic	conte		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT)	REMARKS
	32	SP		12 0	ND - (cont*d) bble, some fine gravel		F (¥)														32	
52	34 -	GP		GA.	AYEL - fine, some medium to coarse sand																1	
Es	38 -	SP		38.5 SA	ND - medium grained, clean d of hole																38	
- 476	38 -																					
۱ ۲	-																			1	-	
	-																				-	
	-																					
TEST HOLE	-																				-	
Z Z		GED I		<u>a.w.H</u> J. X.W.	FACILITY: LAT. & LONG : 87 ⁰ 01*18''N, 129 ⁰ 59'5				ECT : ATION		1011			-		1975 BORROW	INVE	STIG	ATIO	N		TEST HOLE No.
N75		N. BY	:	J.A.W. 	AIRPHOTO No. : A 22880-85 RIG : HELI-DRILL METHOD : AIR	U. ' T		PIPE	MILEAC	GE :	prox.	16 ⁰ C		+	20	NORTHERN E		RING :	SERVICE			N75-106P-83-8
	STAR	T:	D	28 M	88 Y 75 TIME: 14:30 FINISH	1	D 2	6 M	08	Y 78	5 TIM	iE: 15	:15	1	CAN	IADIAN ARCTIC GA	s stu	DY L	IMITE	>		SHEET 3 OF 3 PC-9,5K37

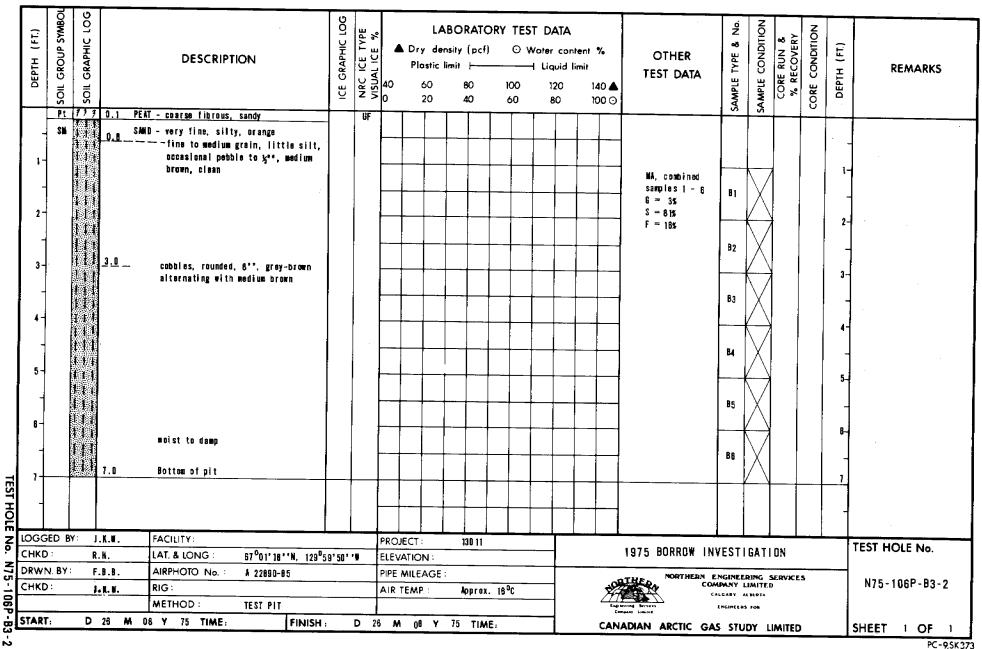
LOG GROUP SYMBOL ICE GRAPHIC LOG SAMPLE CONDITION SAMPLE TYPE & No. CONDITION LABORATORY TEST DATA CORE RUN & түрЕ Е % (FT.) (FT) GRAPHIC ▲ Dry density {pcf} O Water content % OTHER NRC ICE 1 VISUAL ICE 0 05 DESCRIPTION DEPTH REMARKS DEPTH - Liquid limit Plastic limit + TEST DATA CORE 100 120 140 📥 60 80 sol Sol 100 🖸 20 40 60 80 Pt 😨 🕄 0.2 PEAT - coarse fibrous, sandy, black, burnt, 85 12:55 ŮF roots SP SAND - medium, trace siit, orange brown, moist 1 - 13:00 MA, combined. 1 samples 1 & 2 6 = 6% 81 1.8 CLAY-med. plastic, grey, damp, thickness S = 425 varies from 0.2' to 0.5' 10 F = 58% 2 -2 (SC-CL) 2.0 Alternate layers of SAND, medium to fine, ١ SC clayey, with CLAY, tan brown to grey 82 ŝ, CL 3 _ 13:15 3 1 3.8 Ð 1 4 \$**#**-SAND - and gravel, cmf, trace to little MA, combined, SC fines sampies 3 🛔 4 B3 6 = 38\$ \$ = 52\$ 5 5 F = 10% (SW-SC) 3 Θ 84 13:30 Bettom of pit ß 6.D 8 TEST HOLE TEST HOLE No. FACILITY PROJECT : 13011 <u>Z</u> LOGGED BY: J.K.W. 1975 BORROW INVESTIGATION 67⁰02'33''N, 130⁰00'05''W ELEVATION : CHKD : LAT. & LONG R.H. PIPE MILEAGE : NORTHERN ENGINEERING SERVICES AIRPHOTO No. : A 22090-05 DRWN, BY: F. 8. N75-106P-B3-1 COMPANY LIMITED CHKD RIG : AIR TEMP Approx. 13⁰C J.K.W. CALGARY ALBERTA ENGINEERS FOR 8 METHOD : HAND TOOLS SHEET I OF FINISH : D 28 M 08 Y 75 TIME: CANADIAN ARCTIC GAS STUDY LIMITED 13:30 D 28 M 08 Y 75 TIME: 12:55 START: PC-9,5K373

TEST HOLE LOG

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001 GROUP SYMBOI ICE GRAPHIC LOG SAMPLE TYPE & No. SAMPLE CONDITION CONDITION NRC ICE TYPE VISUAL ICE % LABORATORY TEST DATA CORE RUN & % RECOVERY DEPTH (FT.) DEPTH (FI.) GRAPHIC A Dry density (pcf) O Water content % OTHER DESCRIPTION REMARKS - Liquid limit Plastic limit + TEST DATA CORE CORE 100 120 140 🔺 80 40 60 SOIL SOIL 80 100 🖸 20 40 60 ZŻ PEAT-coarse fibrous, black, roots UF Pt 0.2 ML SILT - trace sand, fine, low to nonplastic, orange brown, roots 0.9 1 MA, combined, S₩-SAND - fine to coarse, silty, and some samples 1 - 5 SN gravel, grey brown, dry, pubbles 81 6 = 385rounded 3", occasional to 1.5" S = 58% 2 2 F = K 1.8' to 2.4', pocket medium sand 1.3' to 3.5', white, cementation (SW-SH) **B**2 <u>3.0</u> fine gravel, coarse sand З. 3 83 4 - walls caving slightly GRAVEL - coarse to fine, little sand, 4 - GW 00 peobles to 2", rounded 0.0 84 4.1 5.0 SAND - modium, slight coarse, clean 52 5 5 GRAVEL - and cmf sand, light brown, QP. 00 occasional cobble to 6", dry 85 to moist Bottom of pit 5.8 5.8 TEST HOLE TEST HOLE No. FACILITY PROJECT : Ş 13011 LOGGED BY: J.K.W. 1975 BORROW INVESTIGATION 87⁰01'34''N, 130⁰00'20''W ELEVATION : LAT. & LONG CHKD R.H. N75 PIPE MILEAGE NORTHERN ENGINEERING SERVICES AIRPHOTO No. DRWN, BY: F. B. A 22890-85 N75-106P-B3-3 COMPANY LIMITED AIR TEMP. Approx. 17⁰C CHKD: RIG : CALGARY ALBERTA J.K.W. 106P -----METHOD : TEST PIT SHEET 1 OF FINISH : D 28 M 08 Y 75 TIME: CANADIAN ARCTIC GAS STUDY LIMITED B START: D 26 M 08 Y 75 TIME:

TEST HOLE LOG

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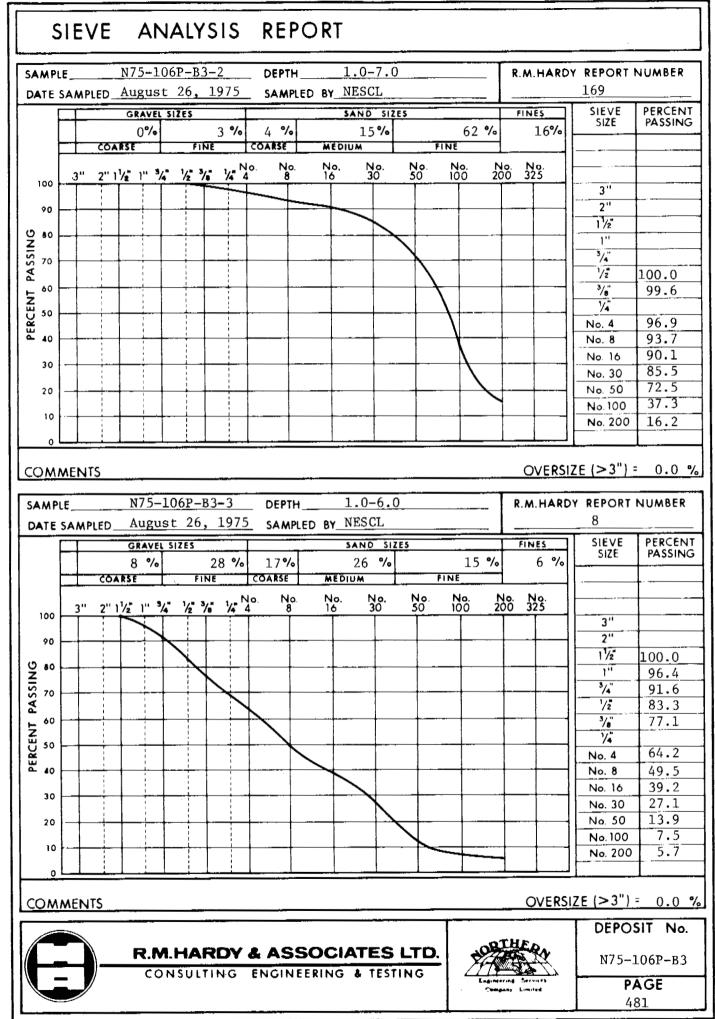
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PC-9,5K373

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					DEPTH_					R.M.HAR	DY REPORT	NUMBER
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10 -								-+	+		No. 200	57.9
٥ Ĺ		1										
		Augus	st 26,		DEPTH	BY NES	SCL			K.M.HAKD	25	
	-	GRAVEL		259/	7		ND SIZES	·		FINES	SIEVE SIZE	PERCENT
	COAL			25%	COARSE	MEDIUM	23 %	FIN	14%	10 %		
								· · · ·	_		·····	
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60 50 40 30											'/z" 3/e" '/4" No. 4 No. 8 No. 16 No. 30 No. 50 No. 100	77.4 71.8 61.5 49.7 39.5 28.9 19.5 13.7
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106P-B4-C 468560E 7436830N (Drill Hole Az BP)

· See 1045-1 EBA

Physical Setting: Deposit 106P-B4 consists of 2 kame complexes located 11 miles southeast of Little Chicago and 5 miles east of milepost 220 on the right of way.

Moterial: SAND and GRAVEL - interbedded.

Volume: 9,300,000 cubic yards.

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Assessment: Deposit 106P-B4 is a source of good to excellent quality granular material suitable for general fill, backfill, building pads and possibly concrete and asphalt aggregate.



Airphoto No. Approximate Scale :

A13402-131 1" = 3200' Latitude: 67° 02' Longitude: 129° 44'

DEPOSIT 106P-B4

PHYSICAL SETTING

This deposit consists of 2 kame complexes located 11 miles southeast of Little Chicago and 5 miles east of the pipeline alignment milepost 220. This deposit corresponds to source number 1045 in EBA DIAND Granular Materials Inventory Volume II (1974) report.

The kame complexes are separated by a moraine plain and each complex contains hills and ridges with maximum local relief of 50 feet. Overburden is slight except in depressions and the deposit is well drained. The deposit was unfrozen to a depth of 8 feet.

A till covered upland with moderate slopes lies between the deposit and proposed pipeline right of way.

BIOLOGICAL SETTING

This site is covered by spruce up to 40 feet in height with an understory of shrubs including ericaceous species. Parts of the area show evidence of an old burn. The area provides productive habitat for beaver, lynx, fox, marten, black bear, moose and caribou. The small lakes in the area do not appear to provide suitable fish habitat.

MATERIAL

This deposit is a source of good quality granular material. Interbedded sand and gravel were found at all test pit and drill hole locations. Sand is mainly well graded, with a variable amount of gravel. Some silt is present near the surface, but the sand beds become cleaner with depth. The largest percentage of material is well graded, rounded gravel with fairly high sand content and a trace of silt. Occasional boulders to 10 inches were encountered.

VOLUME

Total estimated volume, based on an area of 440 acres and a maximum depth of 30 feet under hill and ridge crests is 9,300,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 106P-B4 is a source of fair to excellent quality granular material and would be suitable for general fill, backfill in pipeline construction, building pads, and possibly concrete and asphalt aggregate. The gravel will require further testing before use in concrete production. Further drilling would be required to locate areas of the best quality material.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the deposit with equipment would probably be via the pipeline right of way and overland from there to the deposit, a distance of 5 miles. In order to minimize environmental damage, snow roads would be built to transport the borrow material across the till covered upland from the deposit to haul points on the right of way. The access right of way would have to be cleared of the tree cover. Trees and vegetation would be removed in accordance with land use regulations. The thin layer of peat and silt would then be stripped from the area to be excavated, and stockpiled around the edge of the site.

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Development of this deposit would involve excavating borrow material evenly from the higher, well drained areas so that good drainage would be maintained over the deposit. Conventional earthmoving techniques would probably be used at this site, however, if areas of high ice cementation are encountered, blasting may be necessary. The excavated material may have to be stockpiled, thawed, and drained before it is used. Crushing and/or screening of the material may be required to produce quality construction aggregates.

Equipment required for development would be dozers, rippers, end-dump trucks, front-end loaders, as well as screening, crushing, washing, concrete and asphalt plants if required.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

1.28-1.4 M6703-A

DEPTH (FT.)	GROUP SYMBOI	GRAPHIC LOG		DESCRIPTION	-	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	•	Dry de			0 w	DATA ater con Liquid	ntent	%	OTHER TEST DATA	E TYPE & No.		CORE RUN & % RECOVERY	CONDITION	DEPTH (FL)	REMARKS
DEF	SOILG	solt				ICE O	NRC	40 0	60 20	80 40		00 60	120 80		40 ▲ 00 ⊙		SAMPLE TYPE	SAMPLE	CORE % Re	CORE	DEP	
	Pt.	37	0.5	PEAT_fibrous, woody, da moist	ark brown,		UF			Π								1			Q.5	19:00 4%** Walmac
2 -				QRAYEL- fine to coarse, little fine to damp brown, fre frequent boulde	coarse sand, quent cobbles,																-	40'' boulder
4		11	5.8																- - - - - -		4 ⁻ 4.5 _	Using shovel, foose material. Beulder Te rock bit, bit ''walked'' off beuld
8 -	<u>ew</u>			GRAVEL - some fine to co trace silt, fre and boulders. End of hole										-							-	causing incline of drill rig. Caved in at depth 5.0 after removal of bit. 8.0' large diameter b
1-		[* .*'										╞┈╴┠					-		+	<u></u>	6	and air roturn too lo roturn cuttings.
-				Nete: large beulders exp surface	esed at the																-	
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bool	GED	BY :	144.	FACILITY				PRO	JECT :	130	11					1975 BORRO	W 101			NN		TEST HOLE No.
снкі	D:		J.K.W.	LAT. & LONG : 67 ⁰ 02	2 '22''W , 128 ⁰ 4	5'00'	•₩	ELEV	ATION :							19/3 BUKKU	1 1 1 1 1			UNE		
	IN. BY	t:	J. W. B		102-131				MILEAG						.ol	THEDA CO	E NGINE			ES		N75-106P-B4-
СНК	D:		0.0.		-98 LL			AIR	TEMP. :	App	10x. 13 ⁰ 0				Zh	A STATE	CALGABY					
				METHOD : ALR											5.00 (1	merne Bernitt meane Lonited	ENGINEE	n 1 FOR				
STAR	IT 1	D	26 M	10 Y 75 TIME: 18:0	6 FINISH	1	D	28 A	A 68 '	¥ 75	TIME:	19:50			CAN	ADIAN ARCTIC G	AS ST	UDY	LIMITE	D		SHEET 1 OF

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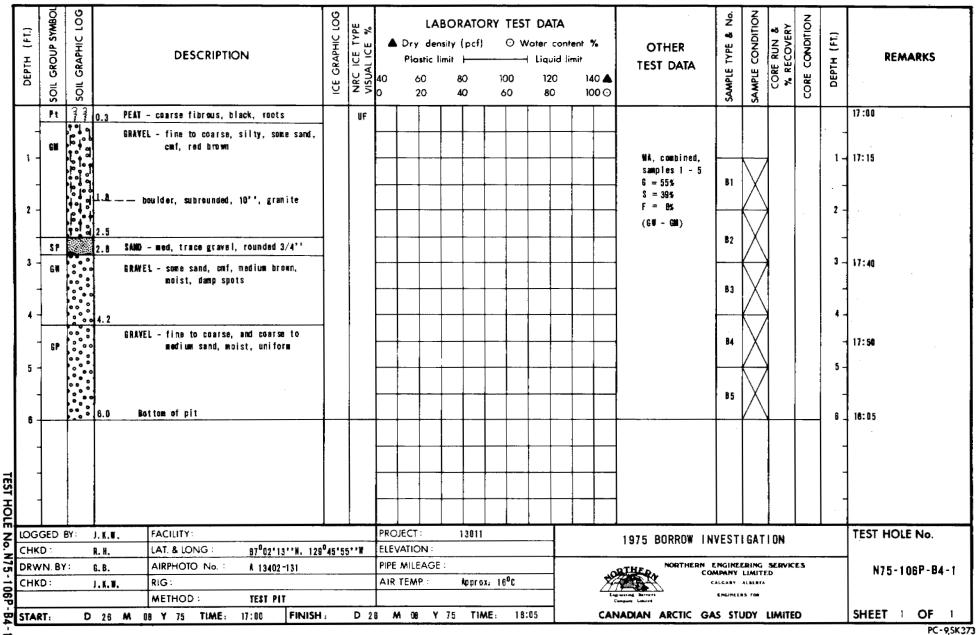
TEST HOLE LOG

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DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Dry	densit ic limi		G	⊙ wa 0	DATA Ster conte Liquid lir 120 80	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
2	SN GN		GRAV 4.0 /SAND 4.5	 fine to coarse, silty, some fine gravel fine to coarse, and coarse, medium, fine sand, silty, brown, damp, occasional cobble fine to coarse, silty, some fine gravel, damp, brown, cobble at 4.5' fine to coarse, very silty, some fine to med. sand End of hole 		UF										3			3	17:10 4%** Walmac to rock bit 17:25 no air circulation, therefore no cuttings, hole caving
~ —	GGED	BY:	<u>6. N. H.</u> J. K. W.	FACILITY: LAT. & LONG : 87 ⁰ 02*55**N, 12	904314	42''W	-		N :	1301	1			1975 BORROW IN	VEST	I GAT			-	TEST HOLE No.
	WN.B KD:		J.M.B. D.G.	AIRPHOTO No. : A 13402-131 RIG : HELI-DRILL METHOD : A IR B Y 75 TIME: 17:10 FINISH			AIR	E MILEA R TEMP. M 8	:		0X. 13	⁰ Ċ 17:2	5	20.05.101	MPANY CALGARY ENGINE	LIMIT ALBERT	F.D			N75-106P-B4-B SHEET 1 OF 1 PC-95K37

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- **B**4 - B



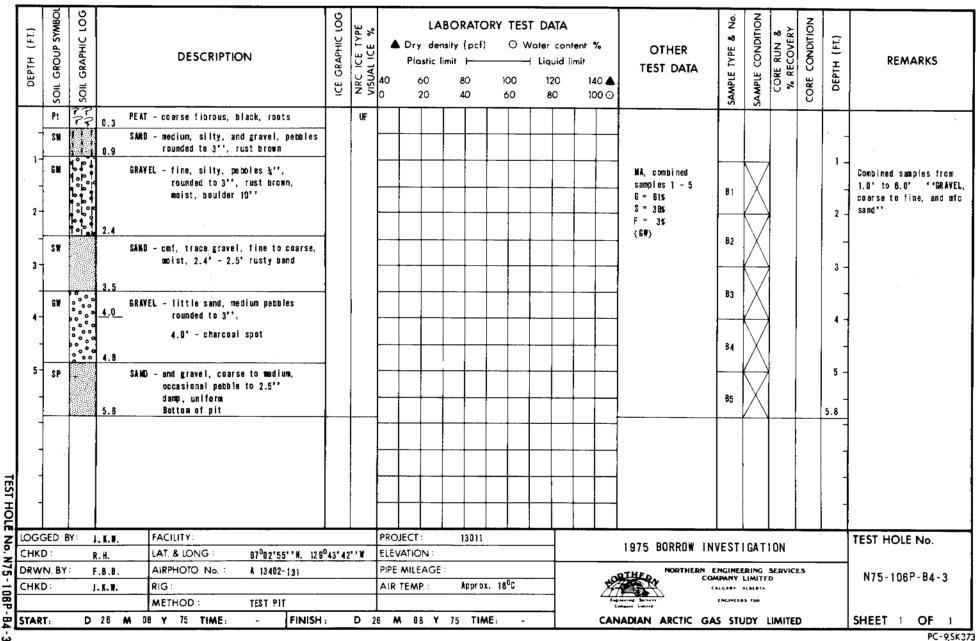
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DEPTH (FL)		SOIL GROUP SYMBOU	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Pla: 6	den	sity (pcf) D		Wot L	tent % imit 140 ▲ 100 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
			23 22	PEAT 0.4	- fine fibrous, amorphous, black		UF															No samples taken
1			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		(organic) with COBBLES, BOULDERS to 24" (oversize material with silt filler)													-			-	difficult to excavate
	1	_	33	1.7	Bottem of excavation															<u> </u>	1.7	20:00
TECT LO				No te:	Refer also to #75-106P-B4-A, drillhole at lower elevation																	
1.01	GGE	ED B	Y:	J. K. W.	FACILITY:			PRC	JECT	:	1	3011				1975 BORROW INV	IESTU	CATI	กง			TEST HOLE No.
DR CH	KD WN KD	I. BY		R.H. A.M. J.K.W.	LAT. & LONG : 67 ⁰ 02'22''N, 12 AIRPHOTO No. : À 13402-131 RIG :	9 ⁰ 45'0	0''W	PIPE	VATIC MILE TEMI	AGE		lpp rox	t. 16 ⁰	C	Ž	NORTHERN CO		ERING LIMIT	SERVK F.D	CES		N75-106P-B4-2
ST/	ART	:	D	26 M 0	METHOD: TEST PIT 8 Y 75 TIME: - FINISH	l :	D 2	6	V 08	Y	75	TIM	E: :	20:00	 CA	NADIAN ARCTIC G			LIMIT	ED		SHEET 1 OF 1 PC-9,5K3

TEST HOLE No. N75-106P-B4-2

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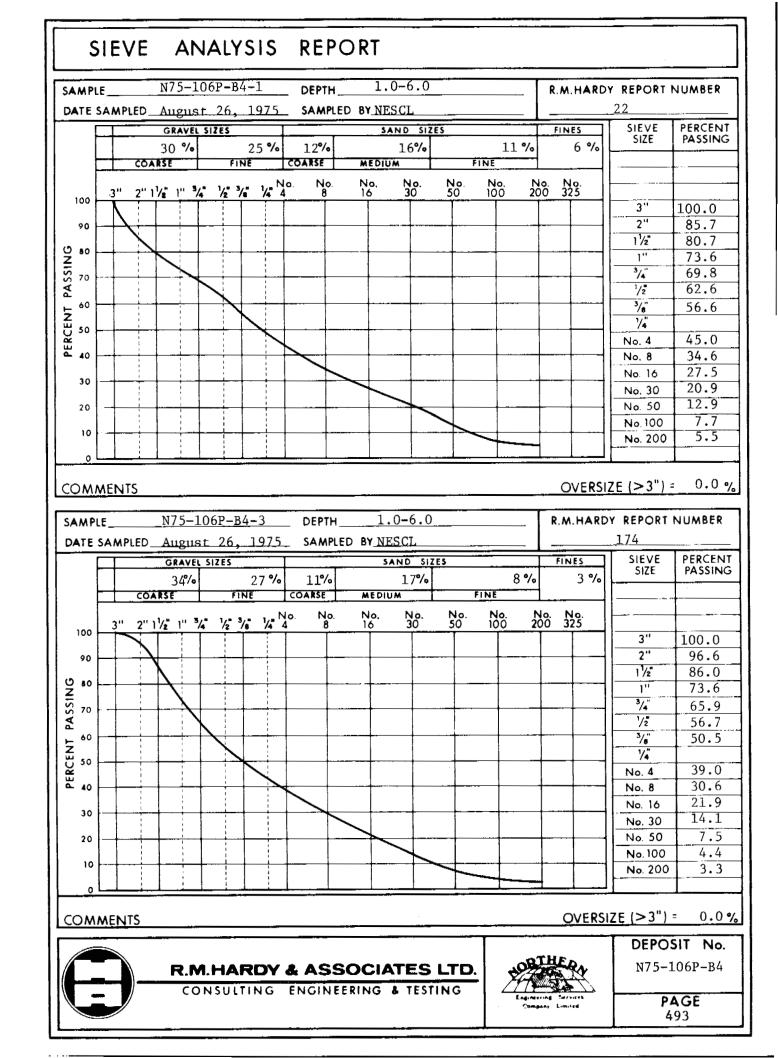


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> No. N75 106P

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	OF LABORATORY TE FOR OF AGGREGATES IN		
	³ DATE SAMPLED : August 26, DATE TESTED : January, 1		
SOUNDNESS OF AGG SULPHATE TEST	REGATE	ORGANI TEST	C IMPURITIES
COARSE AGGREGATE FINE AGGREGATE	: LOSS = 6.97 % : LOSS = 16.72 %		: 4+ MOVED : 4
LOS ANGELES ABRAS	ION TEST	COAL & REMOVE	ROOTLETS D : 4
PERCENT LOSS ₪	20.1 %		ONTENT :Trace
SUMMARY OF ROCK TYPE	S, COARSE AGGREGATE. (P	ETROGRAPH	IC ANALYSIS)
ROCK TYPE	CLASSIFICATIONS		TOTAL WEIGHTED COMPONENT %
Quartzite			20.8
Granite	Strong to very strong, Very	good	3.6
Basalt			1.3
Sandstone			12.75
Siltstone	Medium strong, Good		1.9
Limestone			13.0
Impure Limestone			6.0
Chert	Potentially reactive, Fair		0.3
Flint			0.45
Ironstone	Weak, Friable, Deleterious		0.65
Clay		-	0.25
PN = 116 INTERPRETA	L Good quality		61.0
	tely 10% of the pebble surfaces coating. Strength tests requir		with a
TOBTHERS	R.M.HARDY & ASSO		DEPOSIT No. N75-106P-B4
Engineering Services Company Limited			PAGE 494

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DEPSOIT 106P-B5(R)

100 1052-1 EBA

Physical Setting:Deposit 106P-B5(R) consists of several small esker
ridges and a kame delta located 1 mile south of
Tutsieta Lake and 3 miles northeast of milepost
208 on the right of way.Material:GRAVEL - silty, and sand.

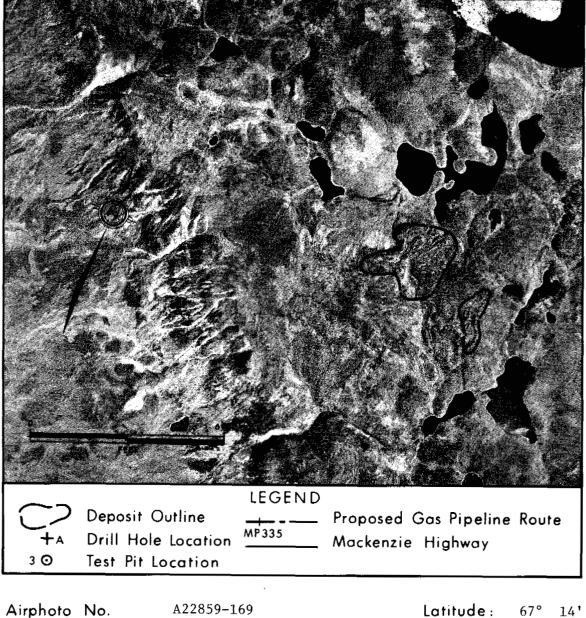
Volume: 120,000 cubic yards.

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Assessment: Deposit 106P-B5(R) is a source of fair quality granular material suitable for general fill and possible backfill. Access would involve crossing an escarpment. Because of low quality, quantity, and access, this source would probably not be developed.



Approximate Scale: 1" = 3000'

Latitude: 67° 14' Longitude: 130° 00'

106P - B5(R)

PHYSICAL SETTING

Several small esker ridges and a kame delta make up this deposit. They are located 1 mile south of Tutsieta Lake and 3 miles northeast of milepost 208 on the proposed pipeline right of way. Deposit 106P-B5(R) forms part of source 1052 in the EBA DIAND Granular Materials Inventory Volume II (1974) report.

Relief within the deposit varies locally from 15 to 30 feet. Ridges are well-drained and intervening depressions are imperfectly to poorly drained. The site has a general northeast slope and surface drainage is toward lakes to the northeast.

Peat and silt cover is less than 1 foot except in depressions where it may be as much as 10 feet thick. Thaw depths of 12 feet can be expected during summer months.

Terrain between the deposit and pipeline right of way consists of three types; rolling moraine, a colluvium covered escarpment characterized by skin flows, and gently sloping alluvial fans.

BIOLOGICAL SETTING

Portions of this site have been recently burned. The dominant vegetation consists of spruce, with scattered birch. Ground cover consists of willow, grasses and herbs with sedges in isolated depressions. The area provides low to moderately productive habitat for marten, fox, lynx, beaver, muskrat, black bear, moose, and caribou. An unidentified active eagle nest was located at the site in 1975. Nearby lakes are used by waterfowl but do not appear to provide suitable fish habitat. Tutsieta Lake, approximately 1 mile north of the site, supports several fish species including whitefish, grayling, pike and lake trout.

MATERIAL

No drilling or test pitting was carried out at this deposit, however, the DIAND (1974) Granular Materials Inventory Report, Vol. II shows this deposit consists of silty gravel and sand. This site was checked by an NESCL geologist during the field reconnaissance.

VOLUME

The DIAND report estimated a volume of 120,000 cubic yards. This volume could probably be increased by including the adjacent deposits of similar material.

DEVELOPMENT AND REHABILITATION

Deposit 106P-B5(R) is a source of fair quality granular material according to previous investigations. This material would be suitable for general fill and possibly backfill in pipeline construction. Further drilling and test pitting would be required to accurately assess the quality and quantity of aggregate in this deposit.

Access to the deposit from the pipeline right of way would involve crossing an escarpment, and care would have to be taken not to initiate skin flows over this area.

Because of the low quality, volume, and possibly difficult access, this deposit would probably not be developed unless sources 1060-B7, 106P-B1 and 106P-B2 were not adequate to meet local requirements for borrow material.

106I - BI - A 456710E 7421790N BI - B 456870E 7418230N

DEPOSIT 106I-B1

PHYSICAL SETTING

This deposit consists of remnants of an outwash plain located 5 to 10 miles north of the mouth of Payne Creek and 4.5 miles west of milepost 230 on the proposed pipeline right of way. This deposit corresponds to source numbers 1035 and 1036 in EBA DIAND Granular Materials Inventory Volume II (1974) report.

The outwash remnants stand 20 to 50 feet above the surrounding terrain. Their surfaces are flat to gently undulating and the scarps marking the edges are steep, with slopes up to 20 degrees or more.

Most of the deposit appears to be relatively free of overburden, although some flat central areas could have a cover of 1 foot of peat and silt. The remnants are well drained around the edges and well to moderately well drained in the centre. Many of the intervening areas have very poor drainage, although the gravelly alluvial fan separating the two main sections of the deposit has moderately good drainage. The active layer was not determined but is probably in excess of 15 feet.

Moderately sloping till plain with local marshy areas lies between the deposit and pipeline alignment.

BIOLOGICAL SETTING

A wide range of vegetation communities is found on this extensive site. Vegetation consists of dense stands of white spruce, black spruce, white birch, and scattered aspen with individual trees up to 50 ft. in height. Scattered shrubs make up the understory and ground cover consists of isolated patched of herbs, grasses and lichen. Low lying areas support sedges, mosses and scattered, stunted black spruce. The area provides productive habitat for beaver, wolf, lynx, fox, marten, black bear, moose, and caribou. An abandoned trapper's cabin was located at the site during the 1975 survey. Numerous ungulate tracks suggest the possible existance of a mineral lick in the vicinity. Waterfowl are most numerous in the area in the April-June period when they congregate on the Mackenzie River. Waterfowl occur in lesser numbers on waterbodies adjacent to the site throughout the open-water season. Some of the larger lakes in the vicinity support fish populations including whitefish, pike, lake trout and suckers.

MATERIAL

Shallow drill holes and test pits indicate that the deposit is predominately well graded sandy gravel with variable silt and occasional cobbles. Interbedded sand and gravel was encountered in 3 test holes with the sand beds being clean and well graded. Moisture content at shallow depths is very low.

VOLUME

The geomorphology of the deposit and the drill hole described in the DIAND report for Site 1035, indicate that these outwash remnants are at least 20 feet thick. Total estimated volume, based on this depth and an area of 1,140 acres is 35,000,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 106I-Bl is a source of good to excellent quality granular material which is suitable for general fill, backfill in pipeline construction, building pads, and concrete and asphalt aggregate production. The gravel will require further testing before use in concrete. A detailed drilling program would be necessary to accurately determine the best areas for borrow pit development. DEPOSIT 106I-B1

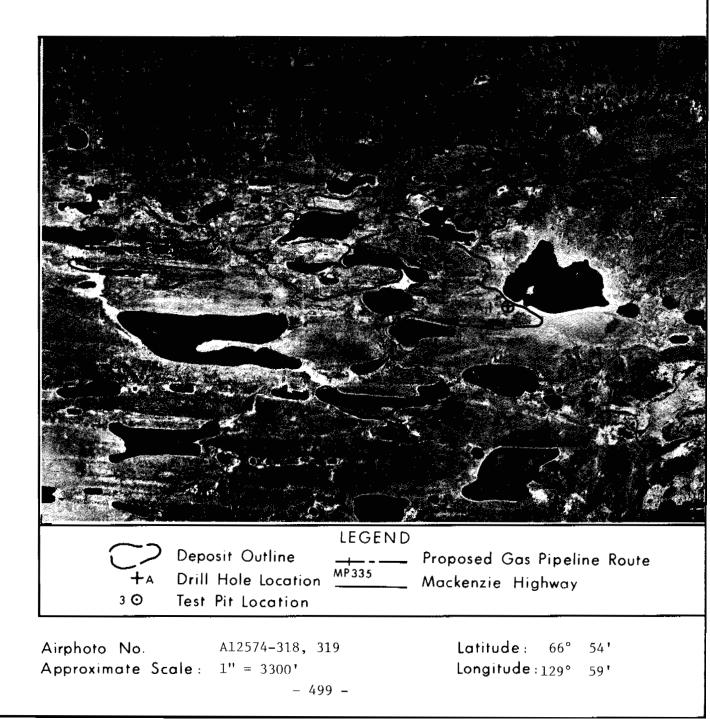
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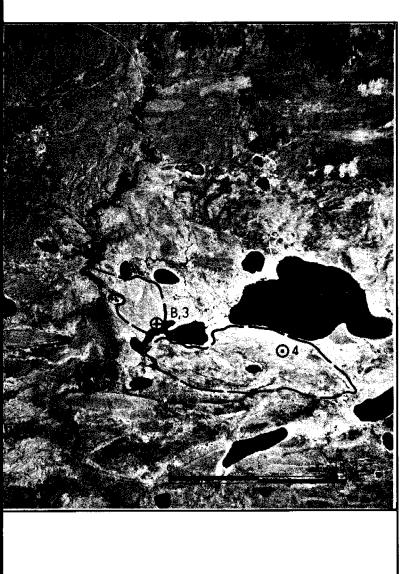
See EBA

- Physical Setting: Deposit 106I-B1 consists of remnants of an outwash plain located 5 miles north of the mouth of Payne Creek and 4.5 miles from the right of way.
- Moterial: GRAVEL well graded, sandy, with variable silt content.

Volume: 35,000,000 cubic yards.

Assessment: Deposit 106I-B1 is a source of good to excellent quality granular material suitable for general fill, backfill, building pads and concrete and asphalt aggregate.





No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the deposit would probably be achieved via the pipeline right of way and then overland about 4.5 miles west to the deposit crossing a moderately sloping till plain and some local marshy areas. In order to minimize environmental damage care would be taken to provide adequate siltation and drainage controls and snow roads would be built to transport borrow material to haul points on the right of way.

Initially, trees and other vegetation would be removed from the selected sites and access right of ways and harvested or disposed of in accordance with land use regulations. Most of the deposit is free of overburden, therefore, little stripping will be required.

Development of this deposit would involve excavating borrow material evenly from higher well drained areas so that good drainage would be established over the area. Conventional earthmoving techniques would be used as the deposit has low moisture content and is unfrozen to a depth of over 15 feet. If ice was encountered blasting could be used. Crushing and/or screening of the material may be required to produce quality construction aggregates.

Equipment required for development would be dozers, rippers, end-dump trucks, front-end loaders, as well as screening, crushing, concrete and asphalt plants if required. A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs. A Sector Francisco Martin Francisco

TEST HOLE LOG

DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Pla: 6	den	BORAT sity (pc mit ⊢ 80 40	:f) 	οw	Vater (conter id limi D		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FI.)	REMARKS
	GP- GM			EL - fine to coarse, (trace silt), occasional cobbles		UF															0	4%** Waimac
2 · 4 · 6 ·	SP	<u>, </u>	2.0 Sand	- fine to medium, trace coarse sand, light brown to grey, clean, moist																	ء 	lesing air circulation in sand, no cutting return, hole caving
8 ·			8.0	End of wols																		Át 0.0°, difficult to extract stom due to sand in hole
-																					1	
	GED E		G. W. H.	FACILITY:			PROJ			130	11					1975 BORROW INV	ECTI	CAT	01			TEST HOLE No.
СНК	D :		J.K.W.	LAT. & LONG : 87 ⁰ 52'15''N, 132 ⁰	01°02		ELEV															
DRW CHK	(N. BY D :		J.N.B.).0.	AIRPHOTO No. : A12574-318, 319 RIG : NELL-DRILL METHOD : AIR				MILE# TEMP			rox. 2	°C					NGINEE PANY I LGARY A	LIMETE.	SERVICE D	:5		N75-106 -81-A
STAP	≀⊺ ∶	D	28 M 8	Y 75 TIME: 09;25 FINISH:	:	D 28	M	8	Y	75 T	ME	09:4	0		CAN	ADIAN ARCTIC GAS	STU	DY I	.IMITEC	>		SHEET I OF 1
							~	:				1	- <u></u>								. <u> </u>	PC-9,5K373

- 505 -

TEST HOLE No. N75-1061-B1-A

VOID - B copy NOIS + P

TEST HOLE LOG

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DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE	40	▲ Dry Pla	/ den:		TORY T cf) © 100 60) Wai)	DATA ter contr Liquid lir 120 80				SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FT.)	REMARKS
-			GRA	YEL - fine to coarse, silty, some		UF	ľ	-		~		,	<u> </u>				8	S.			0	10: 15
-	GM			fine to coarse sand, occasional cobble		Ur					•	+			-						· -	4¼'* Walmac
2 -							-					_			-						-	
-		ן יין אין אין אין אין אין אין אין אין אי						_		-+					_				:		-	
		l e b	(4.0)]																	
	6 W- 6C		GRA	YEL-fine to coarse, trace clay, (trace silt)			1														4.5	lost air circulation.
	96	É.		(trace sive)			-	-		+-	++				1				1		-	Difficulty in with- drawing drill stem
8 -			0.5	End of hole				+	┥┥						-						6.5	no cutting return, or
-							-						<u> </u>		- _						-	dust
																					_	
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				FACILITY			00	ROJECT	·.		011				<u> </u>	_						TEST HOLE No.
HKI	GED D		6. N. H. D. C.	LAT. & LONG : 88 ⁰ 52'45"'N,	129 ⁰ 58'	55''W	-	EVATIO							1975 BO	RROW IN	IVEST	IGAT	10N			
	'N. BY		J.W.B.	AIRPHOTO No. 412574-318, 3			PIF	pe Mil	EAGE						ATHER.	KORTHERN CC	ENGINE		SERV)	CES		N75-1061-81-
нк	D:		J. K. W.	RIG: HELI-DRILL			A	IR TEM	P:	Ap	prox. 2 ⁰ (:		Ž	AAK		CALGART	AL BERTA				
				METHOD: AIR 08 Y 75 TIME: 10:15 FINIS				M 08		75	TIME: 1	0.40		<i>.</i>		DCTIC C				50		SHEET 1 OF

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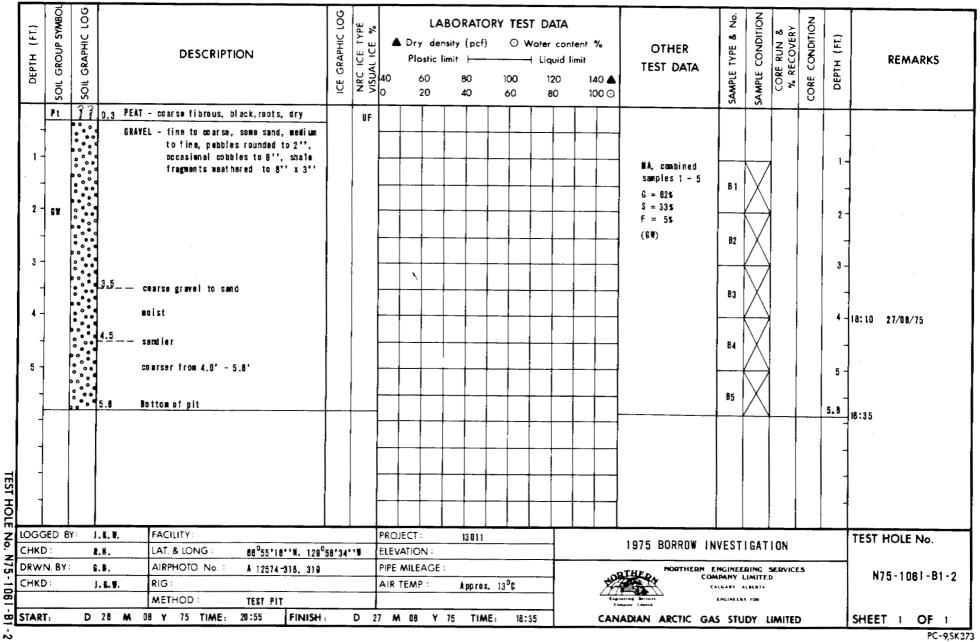
100 **GROUP SYMBOI** ICE GRAPHIC LOG ŝ SAMPLE CONDITION CONDITION NRC ICE TYPE VISUAL ICE % 0 & LABORATORY TEST DATA CORE RUN & % RECOVERY (FT.) GRAPHIC I SAMPLE TYPE & DEPTH (FI.) ▲ Dry density (pcf) ○ Water content % OTHER DESCRIPTION DEPTH REMARKS Plastic limit + - Liquid limit TEST DATA CORE 60 80 100 120 140 🔺 SOIL SOIL 20 40 60 80 100 🖸 27 Pt PEAT - coarse fibrous, black, roots UF 20:55 5 1 SAND - medium fine, and silt, some gravel, coarse to fine, peobles rounded to 3", rust brown 21:15 1-1 00 WA, combined GW GRAVEL - coarse to fine, some sand, trace samples 1 - 5 silt, occasional cobbles to B", B1 6 - 51% shale fragments 0.0 \$ * 45% 2 2 -F = 4% . (6#) **B**2 21:25 3 3. 83 00 3.8 4-SP SAND - medium to coarse, trace gravel, fine, 21:35 medium brown, clean, molst 84 61 GRAVEL - fine, and sand, curf, pubbles rounded to %"*, damp 5 -00 5 - coarser from 5.2', gravel to 3'' 85 °. • . Bottom of pit 8.0 6 21:45 8 TEST HOLE No. LOGGED BY: J.K.W. FACILITY PROJECT : 13011 TEST HOLE No. 1975 BORROW INVESTIGATION CHKD LAT. & LONG 66⁰55'18''W, 129⁹58'34''W ELEVATION : R. H. N75 DRWN, BY: F.B.B. AIRPHOTO No. A 12574-319, 318 PIPE MILEAGE : NORTHERN ENGINEERING SERVICES THE N75-106|-B1-1 COMPANY LIMITED CHKD: RIG: AIR TEMP. Approx. 16⁰C 1.8.8. CALGARY ALBERTA - 1901 -----TEST PIT METHOD : START D 28 M 08 Y 75 TIME: 20:55 FINISH : D 26 M 08 Y 75 TIME: 21:45 CANADIAN ARCTIC GAS STUDY LIMITED SHEET I OF I ÷

TEST HOLE LOG

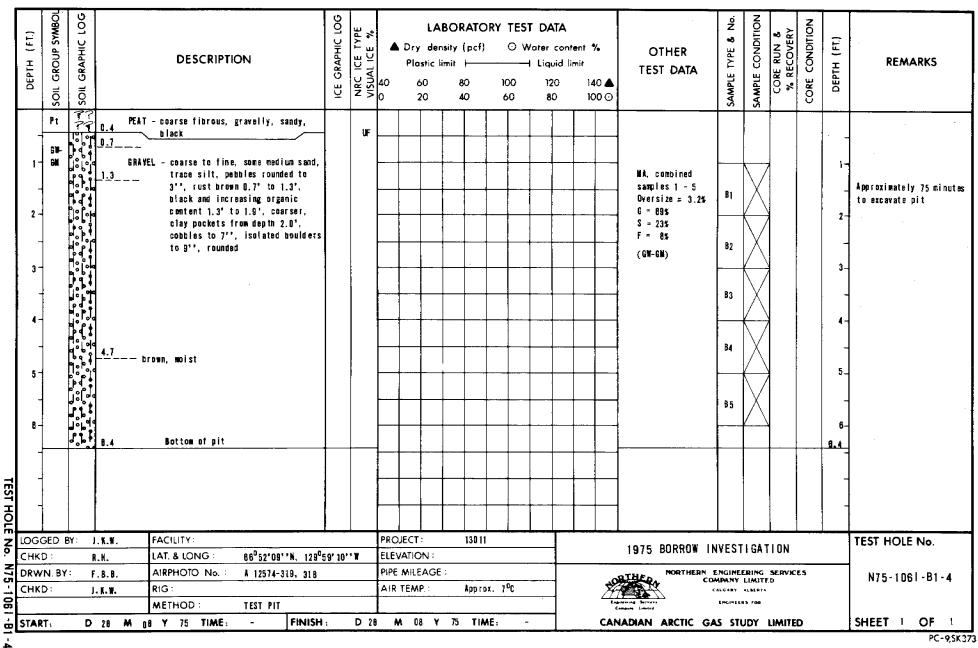
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PC-9,5K373



DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG		ÐESCRIPTK		ICE GRAPHIC LOG	NRC ICE TYPE	40	Dry de	ABORAT ensity (pcf limit +	i) () v	Noter cont H Liquid li 120 80		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FI.)	REMARKS
	Pt	33	0.3 PEAT	- coarse fibrous,	black, rootlets		UF													12:25
- 1-	GM	。。。。。。。。。。。 。。。。。。。。。 。。。。。。。。。。。。。		EL - and sand, silty to 3'', rusty t shale blocks to sulphur stains, from 0.7'	brown to 0.7',									Combined MA, Sample 1 - 3, 6 48% S 30%	B1		7		1 -	1 2: 50
2-	GC	44.67.44 46.64 46.		EL - clayey at 2.0°, isolat (till?)	ted bouiders to 9""	-								F 22% (GC)	B2				2 -	- 13 : 10
3-					stone, cobbles to										B3		K		3 -	13:20
4-			- <mark>4.5</mark>	ay layer 1°° thick, '	isolated layers to									-					4 -	13: 35
			Br	sttom of pit															-	
-																				· · · · · · · · · · · · · · · · · · ·
		BY :		FACILITY					DJECT:	1301	1			1975 BORROW	INVES	TIGA	TION			TEST HOLE No.
		~ .	R.H.	LAT. & LONG	85 ⁰ 52*45**N. 129 ⁰ 5	8'55'	<u>'₩</u>	-	VATION :					NORTHERN	ENGIN	ERING	SERVI	CES		
CHK	N. BY D :		i.B. I.K.W.	RIG:	A 12574-318, 319			-	TEMP:		ox. 3 ⁰ C		ž	Con C	CALGARY	LIMIT	'ED			N75-106 -B1-
				METHOD: DB Y 75 TIME:	TEST PIT 12:25 FINISH					Y 75 TI	<u> </u>	1:00		Company Second Company Limited NADIAN ARCTIC Q		ERS 704				SHEET I OF I

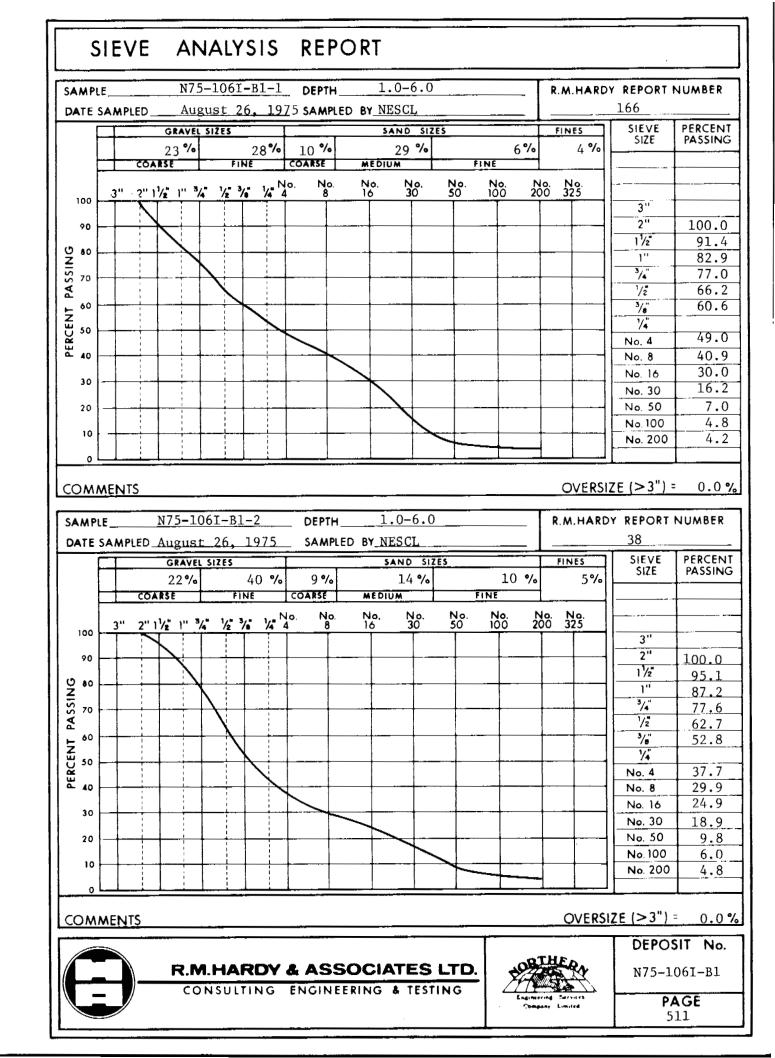


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			2	6	%			22	%		9	%			10 %			1	1%		22	%	SIZE	PASSING
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	-						-B1 28,					TH_		N	.0-6 NESCL	TOTAL AND ADDRESS OF TAXABLE			-	R ./	N.HA		REPORT	NUMBER
SAMP DATE	-		D_4	Aug GR/	us i	t 2	28,	19	75	-	SAN		D BY	541	IESCI						NES		164 SIEVE	PERCENT
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	-	MPLE	D_4	Aug GR/ 48	us i	t 2	ES FI	19 21 NE	75 %		5A A 4 °	APLEI	D BY	SAN J	IESCL	ES	FIN	IE .		Fi	NES 8ª		164 SIEVE	PERCENT
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100 90 90 80 70	SAI	MPLE		GR/ 48	vel %	t 2	ES FI	19 21 NE	75 %		5A A 4 °	APLEI	D BY	SAN J	IESCL	ES		IE .		Fi	NES 8ª		164 SIEVE SIZE 3'' 1'/2 1'' 3'4" 1/2 3'4" 1/2 3'4" 1/2 3'4" 1/2 3'4" 1/2 3'4"	PERCENT PASSING 100.0 84.4 71.5 58.7 52.4 44.8 39.0
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DATE 100 90 00 00 00 00 00 00 00 00 00 00 00 0	SAI	MPLE		Aug GR/ 48	vel %	t 2	ES FI	19 21 NE	75 %		5A A 4 °	APLEI	D BY	SAN J	IESCL	ES		IE .		Fi	NES 8ª		164 SIEVE SIZE 3'' 2'' 1'/2 1'' 3/4" 1/2 3/6" 7/4 No. 4 No. 8 No. 16 No. 30 No. 50	PERCENT PASSING 100.0 84.4 71.5 58.7 52.4 44.8 39.0 30.7 26.2 21.5 15.1 10.1
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DATE 100 90 06 06 06 00 100 00 00 00 00 00 00 00 0				Aug GR/ 48	vel %	t 2	ES FI	19 21 NE	75 %		5A A 4 °	APLEI	D BY	SAN J	IESCL	ES		IE .		• • •	Ne. 325		164 SIEVE SIZE 3" 2" 1½ 1½ 3/4" Ŋo. 4 No. 8 No. 16 No. 50 No. 50 No. 100 No. 50 No. 100 No. 50 No. 100 No. 50 No. 100 No. 100 No. 100 No. 50 No. 100	PERCENT PASSING 100.0 84.4 71.5 58.7 52.4 44.8 39.0 30.7 26.2 21.5 15.1 10.1 8.4
DATE 100 90 06 06 00 20 10 0 0 0				Aug GR/ 48	vel %	t 2	ES FI	19 21 NE	75 %		5A A 4 °	APLEI	D BY	SAN J	IESCL	ES		IE .		• • •	Ne. 325		164 SIEVE SIZE 3" 2" 1½ 1½ 1½ 3/4" ½ 1½ 3/4" ½ No. 4 No. 8 No. 16 No. 30 No. 50 No. 100 No. 200 E (>3") =	PERCENT PASSING 100.0 84.4 71.5 58.7 52.4 44.8 39.0 30.7 26.2 21.5 15.1 10.1 8.4 7.5 3.2%
DATE 100 90 06 06 00 20 10 0 0 0				Aug GR/ 48 13E 12 1	AVEL %	siz	ES	19 21 /*	75 %									IE .		• • •	Ne. 325		164 SIEVE SIZE 3" 2" 1½ 1" 3/4" ½ 3/6" ½ 3/6" ½ 3/6" ½ 1% No. 4 No. 8 No. 16 No. 30 No. 50 No. 50 No. 200 E (>3") = DEPOSI	PERCENT PASSING 100.0 84.4 71.5 58.7 52.4 44.8 39.0 30.7 26.2 21.5 15.1 10.1 8.4 7.5 3.2% T No.
DATE 100 90 06 06 00 20 10 0 0 0				Aug GR/ 48 (3) (2) (2) (2) (2) (2) (3) (3) (4) (3) (4) (4) (4) (4) (4) (4) (4) (4) (4) (4	.M	sız	ES	19 21 NE	75 %						IESCL			No. 100					164 SIEVE SIZE 3" 2" 1½ 1½ 1½ 3/4" ½ 1½ 3/4" ½ No. 4 No. 8 No. 16 No. 30 No. 50 No. 100 No. 200 E (>3") =	PERCENT PASSING 100.0 84.4 71.5 58.7 52.4 44.8 39.0 30.7 26.2 21.5 15.1 10.1 8.4 7.5 3.2% T No. 61-B1

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SUMMARY	OF LABORATORY TES	T DATA	
SUITABILITY	OF AGGREGATES IN	CONCRI	ETE
SAMPLE No. N75-106I-B1-2 DEPTH (FT.): 1-6	2 DATE SAMPLED : August 26, 1 DATE TESTED : February, 19		
SOUNDNESS OF AGGE SULPHATE TEST		ORGANIC TEST	IMPURITI
COARSE AGGREGATE FINE AGGREGATE	\$1 , 8		: 3 MOVED : 3
LOS ANGELES ABRAS	ION TEST	REMOVE	ROOTLETS D : 3 ONTENT : Tr
PERCENT LOSS =	21.6 %		ANCE :
SUMMARY OF ROCK TYPE	S, COARSE AGGREGATE. (PET	[ROGRAPH	
ROCK TYPE	CLASSIFICATIONS		TOTAL WEIGHTEE COMPONENT
Quartzite			34.75
Granite	Strong to very strong, Good	-	5.55
Sandstone Siltstone			1.9 8.0
T. f	1	-	0.65
Limestone	Medium strong, Fair		8.65
Limestone	Medium strong, Fair		
Chert			0.85
	Medium strong, Fair Potentially reactive, Fair		
Chert			0.85
Chert Flint Ironstone	Potentially reactive, Fair	gregate	0.85
Chert Flint Ironstone PN = 142 INTERPRETA	Potentially reactive, Fair Weak, Poor	gregate	0.85 2.3 0.3
Chert Flint Ironstone PN = 142 INTERPRETA	Potentially reactive, Fair Weak, Poor ATION : Poor quality coarse agg	IATES LTD.	0.85 2.3 0.3

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WTM Flore 9

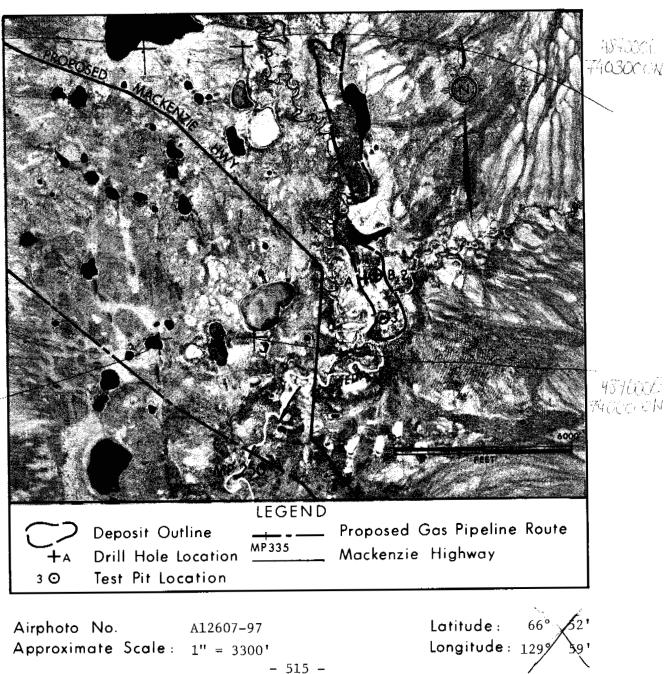
DEPOSIT 1061-B2

Physical Setting:Deposit 106I-B2 consists of terraced kames on the
east side of the Tieda River, about 3 miles south
of Yeltea Lake, and 2.5 miles northeast of milepost
250 of the proposed pipeline right of way.
SAND - poorly graded, fine, with variable silt and
gravel content. Underlain by till.

Volume: 2,500,000 cubic yards.

Assessment: Deposit 106I-B2 is a source of poor quality granular material marginally suitable for general fill. Access is not considered to be a problem over the 2.5 miles from the deposit to the pipeline right of way. Development is unlikely to take place unless extreme shortages of material exist in the area.

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DEPOSIT 1061-B2

PHYSICAL SETTING

This deposit consists of terraced kames located on the east side of the Tieda River about 3 miles south of Yeltea Lake. It is 2.5 miles northeast of milepost 250 on the proposed pipeline right of way.

Kame crests stand about 50 feet above the surrounding terrain. The western flank of the southern section is marked by flat benches separated by scarps 5 to 15 feet high. Other slopes are generally moderate. Overburden is negligible along the crests of the kames, but may be up to 5 feet thick on the back edges of some of the benches. The site is well drained except for flat areas on the benches which have imperfect drainage. The active layer varies from 1 to 6 feet depending on vegetation cover. Although one ice lense was encountered, the material generally has a low ice content.

A small creek and a gently rolling morainic plain lie between the deposit and the pipeline route.

BIOLOGICAL SETTING

Vegetation on the better drained portions of this deposit consists of a dense stand of white spruce up to 40 ft. in height and a mixed ground cover dominated by dwarf shrubs, mosses and lichens. On poorer drained areas stunted spruce and tamarack are also present. The area provides productive habitat for lynx, mink, fox, wolf, black bear, moose, and occasional grizzly bear. Caribou are present in the area during the summer period. Moose migrate through the area in the November-December and March-April periods. No information is available on waterfowl use of the area. During the summer period grayling, long-nose suckers, round whitefish, pike, slimy sculpin, and lake chub are present in the Tieda River. There is no reported winter flow in this river. Spawning runs of grayling and whitefish move through the river enroute to Yeltea Lake.

MATERIAL

Drilling and test pit investigations were carried out only in the southern portion of the deposit. Results of this work indicate the deposit is a source of very poor quality granular material. Poorly graded fine sand with variable silt and gravel content was found to a depth of 25 feet. Locally however, the sand was only 1 to 4 feet thick and underlain by till.

VOLUME

Total estimated volume, based on a depth of 10 feet and an area of 370 acres is 2,500,000 cubic yards. Recoverable volumes may be lower depending on overburden thicknesses.

DEVELOPMENT AND REHABILITATION

Deposit 106I-B2 is a source of poor quality granular material which is marginally suitable for general fill. Although there is a lack of good quality material at this site, the scarcity of borrow in this area could necessitate its development.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain period of the year.

Access to the deposit along the east side of the Tieda River from the pipeline right of way presents no major problems. In order to prevent environmental damage, care would be taken to avoid siltation of the Tieda River and snow roads would be built to transport borrow material to haul points on the right of way. A detailed drilling program would be required to delineate areas of the best quality material. Development of the better areas would involve excavating borrow material evenly from the higher well drained kame crests, or from the scarps on the western flank of the deposit. Blasting or conventional earthmoving techniques would be used, depending on the degree of ice cementation. The tree growth will require clearing and harvesting before the selected borrow areas are stripped of overburden and topsoil. The overburden will be stockpiled along the perimeter of the borrow excavation.

Equipment required for development would be dozers, ripperd, end-dump trucks and front-end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs. NOID AND NOID - A

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TEST HOLE LOG

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SAMPLE CONDITION SAMPLE TYPE & No. CONDITION SOIL GROUP SYMBOL **GRAPHIC LOG** ICE GRAPHIC LOG NRC ICE TYPE VISUAL ICE % O & LABORATORY TEST DATA CORE RUN & % RECOVERY DEPTH (FL) DEPTH (FT.) ▲ Dry density (pcf) ⊙ Water content % OTHER REMARKS DESCRIPTION Plastic limit |------ Liquid limit TEST DATA CORE 100 120 140 📥 60 80 SOIL 80 100 🖸 20 40 60 16 18 SILT (cont'd) ¥s ? ML 18 -28.0 _____ clayey, trace to no coarse gravel 20-15:20 20 -22-24sand, occasional peobles 26 28 -15:28 _2<u>8.0 _</u>______ clayey 28-29.0 ____ cobble at 32.0" - trace fine to coarse gravel, TEST HOLE at 35.0' - cobble 37 End of hole 37.0 37 TEST HOLE No. PROJECT : 13011 LOGGED BY: FACILITY G. M. H. **Z**0. 1975 BORROW INVESTIGATION 86⁰43'30''N, 129⁰18'13''W ELEVATION : LAT. & LONG CHKD D.O. NORTHERN ENGINEERING SERVICES PIPE MILEAGE AIRPHOTO No. A12607-97 N75-1061-B2-A J. M. B. DRWN. BY: OTHE COMPANY LIMITED Ģ AIR TEMP. Approx. 2⁰C CALGARY ALBERTA HELI-DRILL RIG : CHKD: J.K.W. INCINELRS FOR 8 METHOD : ALR SHEET 2 OF CANADIAN ARCTIC GAS STUDY LIMITED 2 15:40 M 8 Y 75 TIME: 14:55 FINISH : D 28 D 28 M 8 Y 75 TIME: START: 82

TEST HOLE LOG

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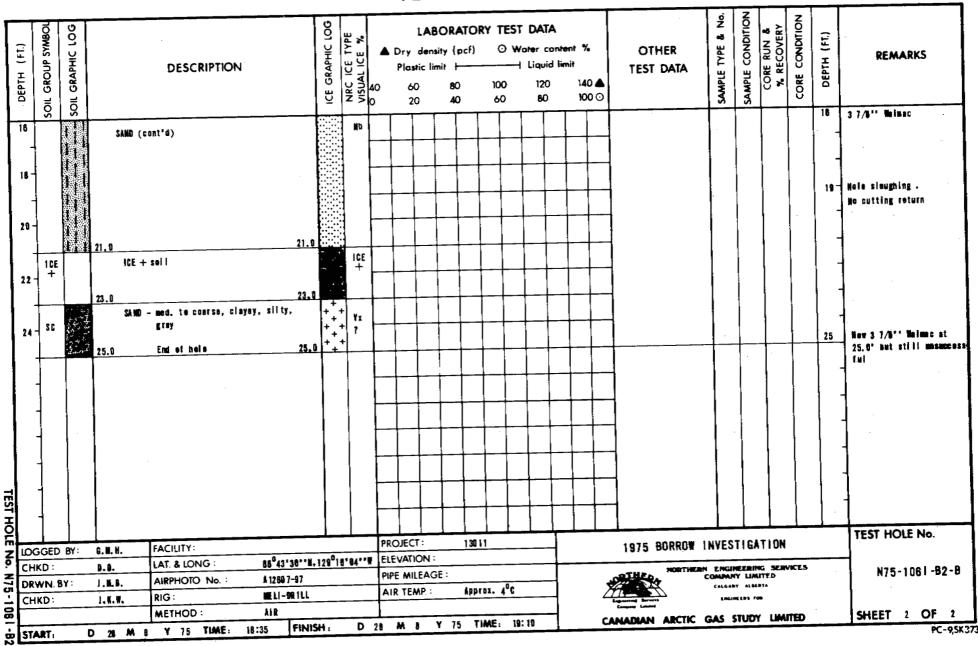
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TEST HOLE LOG

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ź SAMPLE CONDITION CONDITION ICE GRAPHIC LOG 200 CORÉ RUN & % RECOVERY SOIL GROUP SYMBOL NRC ICE TYPE VISUAL ICE % O & LABORATORY TEST DATA SAMPLE TYPE & (FT.) DEPTH (FT.) ▲ Dry density (pcf) O Water content % SOIL GRAPHIC OTHER REMARKS DEPTH DESCRIPTION Liquid limit Plastic limit + TEST DATA CORE 140 📥 100 120 60 80 100 🖸 80 20 40 60 09:00 nç. 弜 ÜF PEAT - coarse fibrous, black, roots Pt 0.3 111 SAND - fine to medium, (slight coarse), SPrust brown, rootlets 11 SH 0 9: 10 1 ~ 111 MA, combined 1 samples 1 - 3 12.2 B 1 G = 2%S = 90% 2 medium, trace coarse sand, some easy to excavate F = 8% 2 gravel rounded to 3**, brown 111 82 4.3 1121_ 3 111 3 -111 B3 **M** 4.3 \odot 3.8 clean, fine, rusty brown pockets, **B** 69:20 4 grey brown, occasional peobles to 4 1 **%**'' 11 5 09:30 6 Bottom of plt 8.0 8 . TEST HOLE TEST HOLE No. PROJECT : 130 11 1975 BORROW INVESTIGATION FACILITY: LOGGED BY: J.K.W. No. 86⁰43'18''N, 129⁰16'00''W ELEVATION : LAT, & LONG : CHKD R.N. . N75 NORTHERN ENGINEERING SERVICES N75-1061-B2-2 PIPE MILEAGE : o THE AIRPHOTO No. A 12807-97 COMPANY LIMITED DRWN. BY: F.B.B. Approx. 7⁰C CALGARY ALBERTA AIR TEMP. -1061-82 RIG CHKD 1.1.1. ENGINELRS FOR TEST PIT METHOD : SHEET 1 OF CANADIAN ARCTIC GAS STUDY LIMITED D 28 M 08 Y 75 TIME: 09: 30 FINISH : D 28 M 68 Y 75 TIME: 09:00 START: PC-9,5K373

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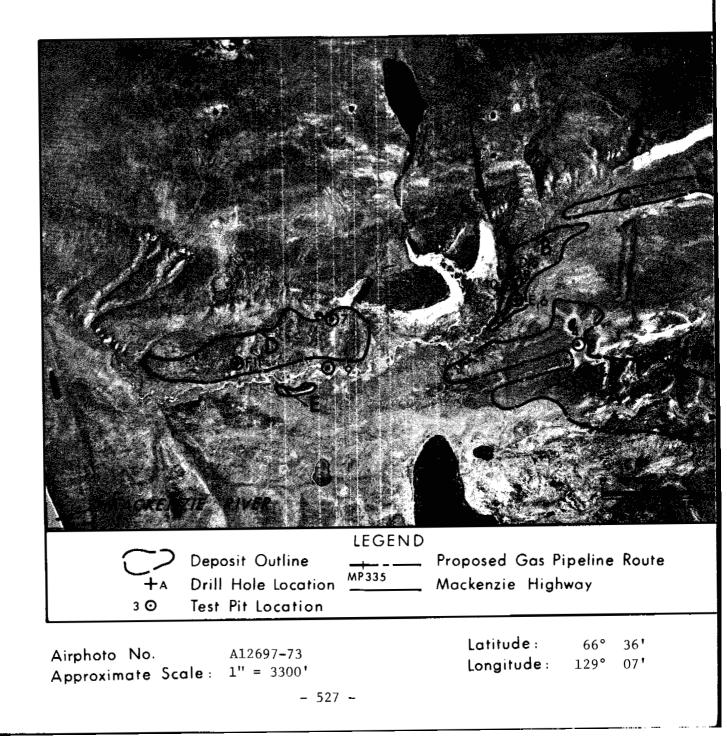
DEPOSIT 1061-B3

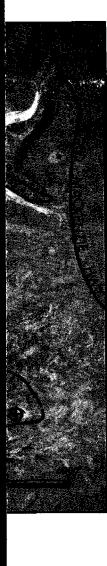
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Physical Setting:Deposit 106I-B3 consists of broad kame terraces and
a small esker located on the south flank of the
Ramparts Plateau 1 mile west of milepost 260 on
the right of way.Material:SAND - fine to medium, with variable silt, clay and
gravel content.

Volume: 6,200,000 cubic yards.

Assessment: Deposit 106I-B3 is a source of fair to good quality granular material suitable for general fill, backfill and possible building pads. Access would involve crossing steep to moderate slopes.





DEPOSIT 1061-B3

PHYSICAL SETTING

This deposit consists of broad kame terraces and a small esker situated on the south flank of the Ramparts Plateau. It is 5 miles east-southeast of the mouth of the Tieda River and 1 mile west of milepost 260 on the proposed pipeline alignment. This deposit corresponds to source number 1022 in EBA DIAND Granular Materials Inventory Volume II (1974) report.

Segment "A" of this deposit is a large kame terrace with meltwater channels cut 20 to 40 feet into its upper flat to gently rolling surface.

Segments "B" and "C" are similar but have linear shapes and a small creek has incised a channel through the centre of part B.

Segment "D" is a broad kame terrace that has been channeled and terraced. Its flat upper surface stands about 150 feet above the creek to the south. Channels and terraces are inset 20 to 100 feet below the main surface.

Segment "E" is a small esker whose rounded crest stands about 50 feet above the surrounding terrain. Slopes up to 30 degrees are common along its edge.

All segments of the deposit have a thin cover of peat and silt which may thicken to 3 feet on some of the broader flat surfaces. Drainage over most of deposit is moderately good to good. Section "E" and scarps along Section "D" are rapidly drained. Within the incised channels drainage is imperfect to poor.

Although the active layer may be deep in the esker and on south facing scarps, it appears to vary between 2 and 10 feet over most of the deposit.

Cliffs to the north and east of the deposit separate it from the pipeline right of way. To the southeast, the terrain appears to be a gently rolling moraine plain with some steep to moderate slopes closer to the pipeline alignment.

BIOLOGICAL SETTING

A wide range of vegetation communities are found on this extensive site. Vegetation on the terraces consists of spruce, 50 ft. or more in height, with clumps of birch scattered throughout. A shrub understory is present with a ground cover of herbs and mosses. Stunted spruce with sedges are found in the poorly drained areas, while rapidly drained sloeps are characterized by scattered aspen with juniper and bearberry.

The area provides moderate to good habitat for a wide range of small and large mammals. Portions of the area may be used for denning. Red squirrel, grouse and Arctic loon sign were observed in the area in 1975. Nearby cliffs provide potential raptor nesting sites. The area is adjacent to the Mackenzie River where large numbers of waterfowl congregate during May and June. Migrating moose may move through the area in November-December, and April-May, enroute to and from islands in the Mackenzie River. The area also provides fair to good moose summer range. The adjacent small ponds and lakes do not appear to support fish populations.

MATERIAL

Material in this deposit is predominately fine to medium sand with a variable silt, clay and gravel content. Beds of coarse and well graded gravel with varying amounts of silt, sand and cobbles are interbedded with the sand in several drill holes and test pits. Drill hole 106I-B3-B encountered 9 feet of sand then 25' of gravel indicating that areas of fairly good quality borrow are available in this deposit.

VOLUME

Total estimated volume for all segments of the deposit, based on an area of 860 acreas and an average depth of 10 feet is 6,200,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 106I-B3 is a source of fair to good quality granular material which is suitable for general fill, backfill in pipeline construction and possibly building pads. Further drilling would be required to locate areas of the best quality borrow.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the deposit from the pipeline right of way would involve crossing steep to moderate slopes. Terrain to the southeast presents the least problems and would probably provide the best though longest route. In order to minimize environmental damage, snow roads would be built to transport the borrow material from the deposit to haul points on the right of way.

Development of the selected sites would initially require the tree and vegetative cover to be removed and disposed of, or harvested in accordance with land use regulations. The thin cover of peat and silt would then be stripped from the site and stockpiled around the edge. Excavation of borrow material would be carried out according to development plans for upland borrow sources, when further information is available for all sections of the deposit. The borrow pit would involve excavating borrow material evenly from higher well drained areas to a grade such that good drainage is maintained. Steep slopes may be opened up and the face of the scarps excavated. Blasting or conventional earthmoving techniques would be used depending on the degree of ice cementation.

The excavated material may have to be stockpiled, thawed, and drained before it is used. Natural mixing during excavation should be adequate to obtain good gradations. Equipment required for development would be dozers, rippers, end-dump trucks, and front-end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs. Marine Karaka Stars

GRAPHIC LOG SOIL GROUP SYMBOI ICE GRAPHIC LOG Ŝ SAMPLE CONDITION NRC ICE TYPE VISUAL ICE % O & CORE CONDITION LABORATORY TEST DATA CORE RUN & % RECOVERY DEPTH (FI.) SAMPLE TYPE & DEPTH (FI.) ⊙ Water content % ▲ Dry density (pcf) OTHER DESCRIPTION Plastic limit -I Liquid limit REMARKS TEST DATA 60 80 ю 120 140 🔺 SOIL 20 40 60 80 юо 🖸 Pt 3 D.4 PEAT cover 4 0 3 7/8" Waimac GRAYEL - fime to coarse, silty, some fine UF î. to coarse sand, brown, moist, frequent cobbies, occasional 2 boulders 4 6,0 6.0 6 SAMD - fine to medium, trace silt (< 5%) SP No 7.0 7 losing some air but GM GRAVEL - fine to coarse, silty, some fine outtings returning to coarse sand, brown, frequent 8 cobbles, occasional boulder 15:50, hole sloughing 9 10.0 10 10 inferred by action of SAND - little coarse gravel (inferred) drili SP no cutting return 12 -End of hole 13.0 13 hole plugging TEST HOLE No. LOGGED BY: G.M.H. FACILITY PROJECT: TEST HOLE No. 13011 1975 BORROW INVESTIGATION CHKD 88°35'57''N. 129°05'13''W D.O. LAT. & LONG ELEVATION : DRWN. BY: AIRPHOTO No. PIPE MILEAGE J.M.B. A12897-73 NORTHERN ENGINEERING SERVICES THE N75-1061-B3-A COMPANY LIMITED CHKD: RIG 1. 6. 8. HEL1-DRILL AIR TEMP : Approx. 21°C CALGARY ALMENTA METHOD : ALR. ENGINEERS FOR START FINISH D 29 M 8 Y 75 TIME: 15:45 D 29 M 8 Y 75 TIME: 18:05 CANADIAN ARCTIC GAS STUDY LIMITED SHEET I OF I PC-9,5K373 <u>e</u>

TEST HOLE LOG

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NGEOS-S TY NGIOS-P TEST HOLE LOG

DEPTH (FT.)	SOIL GROUP SYMBOL	SOIL GRAPHIC LOG	DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	▲ 40 0		BORATC nsity (pcf) imit 80 40	0 1	-	ntent limit	% 140 ▲ 100 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FI.)	REMARKS
2 -	SP		SAND—fine to medium, trace fine to coarse gravel, brown, damp.		UF													0 	17:20 new 3 7/8** Walmac
4 - - 6 -																		-	
- 8 - -	-		9.0	_														-	
10- - 12-	GN		GRAYEL→fine to coarse, silty, some fine to coarse sand, brown, damp.															-	
14-		• • • • • • • • • • • • • • • • • • •																-	
	GED B	Y: 6.0	LH FACILITY:	<u>i</u>		PROJ		13011				<u> </u>	1975 BOR			I Stiga			TEST HOLE No.
CHKE DRWI CHKE	N. BY	D.(j.M. j.K.	B. AIRPHOTO No. : A 12697-73)*04*39'	••₩		ATION : AILEAGE EMP. :		. 21 ⁰ C			10	NORTHERN CO		ERING LIMETI ALBURTA	SERVIC D			N75-1061-B3
STAR	T۰	D	28 M 08 Y 75 TIME: 17:20 FINIS	Н.	D 2	M	08 Y	75 TIA	AE: 11	; 80		CAN	IADIAN ARCTIC G	us sti	UDY	LIMITE	D		SHEET 1 OF

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SOIL GROUP SYMBOI **GRAPHIC LOG** GRAPHIC LOG Ŝ SAMPLE CONDITION CORE CONDITION NRC ICE TYPE VISUAL ICE % O & LABORATORY TEST DATA CORE RUN & % RECOVERY (FT.) ٥ð (ET.) A Dry density (pcf) O Water content % OTHER SAMPLE TYPE DESCRIPTION DEPTH DEPTH REMARKS Plastic limit -- Liquid limit TEST DATA 60 80 100 120 140 📥 Щ SOIL 20 40 60 80 100 🖸 GN UF 18 18 -18.5 water gushes out of hole 20 21 flow of water slows down 22 some slough in hole. 22 24 26 ┸ 28 "at 28.0' free water. "" Very wet from 28.0° to end of hole at 34' TEST HOLE End of hole 34 34 34.0 LOGGED BY: FACILITY PROJECT : 13011 TEST HOLE No. 6.M.H 1975 BORROW INVESTIGATION CHKD : LAT. & LONG : 86⁰35'40""N. 128⁰04"39""W ELEVATION : 6.0. DRWN.BY: AIRPHOTO No. : A 12697-73 PIPE MILEAGE : NORTHERN ENGINEERING SERVICES J. M. B N75-1061-B3-B COMPANY LIMITED CHKD: AIR TEMP : Approx. 21⁰C RIG : J.K.W. MELI-DRILL CALGARY ALBERTA 8 ENGINEERS FOR METHOD : A1R START: D 29 M 08 Y 75 TIME: 17:20 FINISH : D 29 M 08 Y 75 TIME: 18:00 CANADIAN ARCTIC GAS STUDY LIMITED SHEET 2 OF 2 ÷.

TEST HOLE LOG

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TEST HOLE LOG

DEPTH (FT.)	SOIL GROUP SYMBOI	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	▲ D F 40 0		SORATC sity (pcf) mit <u> </u> 80 40	0		conte id lim 0			SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
0			511	LT- trace fine sand, brown, damp		ÜF													0	14:20
2 -	ML			piecas of wood															-	
•																			-	
4 -			4.0																-	
			SAN	D-fine to medium, trace coarse, silty, trace fine gravel, <u>5-</u> 0																
6 -	SM		6,0	brown to rust brown, damp		ND													-	
-			SAN	D-fine to medium, light brown,								_							_	
8 -				clæar. _ <u></u> 8.0		<u> </u>													-	
-			9.0	occasional p e bbles	+++++++++++++++++++++++++++++++++++++++	¥x														
18 -	SP				+++ +++															
-					++++								_							
12 -					+ + + + +	ļ														
					++ +++															
14 -					+ + + +	1										2				
					++++++++++++++++++++++++++++++++++++++															
18				· · · · · · · · · · · · · · · · · · ·	+ + +															
	GED B	<u>Y:</u> D.		CILITY: T. & LONG : 88°35"57""N, 129°C	g+2=++		PROJEC		13011					1975 BORROV	(INVE	ESTI	GATIO	N		TEST HOLE No.
	N. BY		··	RPHOTO No. : A 12697-73	<u>v vv '</u>			LEAGE						DTHED NORTHERN	ENGINE		SERVIC	ES		N75-1061-B3-
СНКС): 	1,1		G: HELI-DRILL			AIR TEI	MP.	Approx. <u>2</u>	1 ⁰ C			Ž	24.05	ENGINELS	AL BL R FA	-			1001-03" 1001-03"
STAR	τ.	D	I .	Y 75 TIME: 14:20 FINISH		D 7	1 19 M (18 Y	75 TIM	E: 14	43		C.84	NADIAN ARCTIC G		เกง		n		SHEET 1 OF

SOIL GROUP SYMBOL SOIL GRAPHIC LOG ICE GRAPHIC LOG Ż SAMPLE CONDITION CONDITION NRC ICE TYPE VISUAL ICE % 0 b LABORATORY TEST DATA CORE RUN & % RECOVERY DEPTH (FT.) SAMPLE TYPE & DEPTH (FT.) ▲ Dry density (pcf) O Water content % OTHER DESCRIPTION REMARKS Plastic limit |-- Liquid limit TEST DATA CORE 60 80 100 120 140 📥 20 40 60 80 100 🖸 16 18 SAND (contid) ¥X + ⊦`+ + SP + + + 18 + 19,0 + cobble + 20 22 24.0 cobble 24 26.0 26 trace fine to coarse gravel + + 28 + 29.0 ÷ 29,0 28 14:34 Nb SAND -fine to medium, silty, 30 - SM TEST HOLE trace gravel, grey, loose. -W2) (W2 less selt 32 32.0 Z_o LOGGED BY: FACILITY PROJECT 13011 TEST HOLE No. 1975 BORROW INVESTIGATION G. M. H 88⁰35'57''N, 128⁰08'35''W CHKD : LAT. & LONG ELEVATION : 0.0. N75-DRWN. BY: AIRPHOTO No. 1 PIPE MILEAGE NORTHERN ENGINEERING SERVICES A 12697-73 1.0.8 N75-1061-B3-C COMPANY LIMITED Approx. 21⁰C CHKD AIR TEMP. J.K.W. RIG : CALGARY ALBERTA HELI-DRILL 106 ENGINEERS FOR METHOD : ALR. -83 START: FINISH : D 29 M 08 Y 75 TIME: CANADIAN ARCTIC GAS STUDY LIMITED SHEET 2 OF 3 D 29 M 08 Y 75 TIME: 14;20 14:43

TEST HOLE LOG

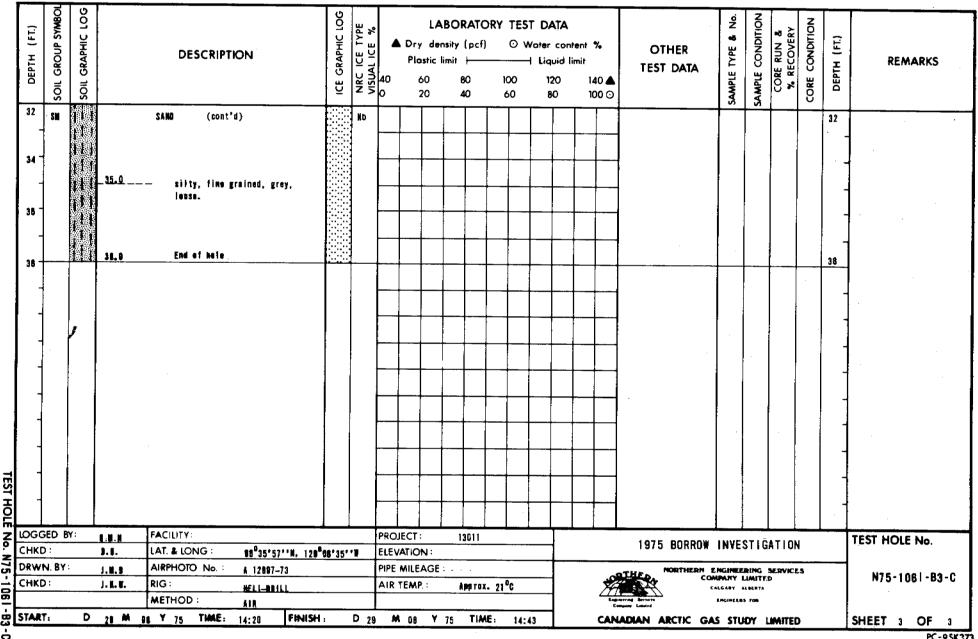
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TEST HOLE LOG

DEPTH (FT.)	SOIL GROUP SYMBOI	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	PI		ORATO ity (pcf) nit —— 80 40	ΟV	T DATA Vater co Liquid 120 80	ntent limit 1.	% 40 ▲ 00 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FT.)	REMARKS
	₽t_	33	0.5	PEAT - brown, woody, damp		UF								·······	1				0	3 7/8" Walmac
2 -				SiLT – trace fine sand, slightly organic, brown to black, damp. _2.0	··														-	Sampies taken at intervals for possibl laboratory verificati
-	ML					•			_				+						_	
4 -			4.0	· • • • • • • • • • • • • • • • • • • •		:		-				_								
·		•••		GRAVEL_fine to coarse, little coarse sand, occasional cobbles, clean.		ND											·			
-	GP					:						1-							-	
8 -		••••]					++				+							-	
-		Î.	7.0	7.0 SAND.— fine to medium.		·	<u></u>	++	-+-+			+	+						-	
e -	SP – SM			trace gravel, trace silt		F													8 -	11:00
	3	1																		new 3 7/6'' Walmac
10		8 8	9.5																	1
10 -	GP	ိုိိ		GRAYEL- fine to coarse, trace fine sand, brown, occasional cobbles															10 -	To rock bit
-			d 					++				+	+		İ				_	
12 -	•		<u>12.0</u>	. mostly course gravel, occasional cobbles				+ +				+							-	
-			å					+ +				-							-	
14 -																			14 -	11:20
				SAND - fine to medium,silty, brown.																3 7/8'' Waimac
18	\$M		16.0																16	hole wet,stem stickin
	GED B	SY :	6.N.H	FACILITY:			PROJEC		13011					1975 BORROW		2710				TEST HOLE No.
CHK	D: N.BY		0.0.	LAT. & LONG : 55 ⁰ 38*29**N, 129 ⁰ (17"41"	1	ELEVATI PIPE MIL							NORTHERN E						
CHK			J . N. B J. K. W.	RIG: HELL-DRILL			AIR TEN		Approx.	10 ⁰ C			t o	CO CO		LIMITE		2.3		N75-1061-B3-
				METHOD : AIR									<u>2.71</u> Engr Co	nering Services many Limited	ENCINELI	S FOR				
STAR	RL:	D	28	M BL Y 75 TIME: 18850 FINISH	:	D 2	9 M	08 Y	75 TIM	E: 12:0	5		CAN	ADIAN ARCTIC GA	S STU	DY I	IMITE	D		SHEET I OF

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DEPTH (FT.)	SOIL GROUP SYMBOI	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE VISUAL ICE %	40 0	Dry de	ABORAT ensity (pc limit — 80 40		ST DATA Water co Liquid 120 80	ntent limit	% 40 ▲ 00 ⊙	OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN & % RECOVERY	CORE CONDITION	DEPTH (FL)	REMARKS
16	(6P)			GRAVEL fine to coarse,		F						Τ				1	1		18	
1		00		occasional cobbles (possib little coarse sand -	16				╉╌╄		+ +	+							17 -	cobble
18 -		ໍໍໍ່	18.0	inferred by action of dri	11												I		18	no cutting return
				End of hole															_	approx. 12'' of slo in the hole.
_							<u> </u>	<u> </u>				_		•					-	•
-								<u> </u>		+									-	
-									+										-	
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_									+-+-		+ +-	-	+						-	
-												-	+						-	1
-	GED B	Y:	G.M.X	FACILITY				JECT	13011					1975 BORROW		FSTI	CAT 10	N.	L	TEST HOLE No.
СНК			D.O.	LAT. & LONG : 85038'28''N, 1280	07'41''	W	<u> </u>	VATION :												4
	N. BY: Di:		J.N.B F.K.W.	AIRPHOTO No. : A 12887-73 RIG : HELI-DRILL				MILEAG	E : Approx.	1000			÷2		ENGINEJ MPANY CALGARY	LIMITE	SERVIC D	E.S		N75-1061-B3-
	-			METHOD: AIR									<u></u>	Barring Bernert	ENGINCE					
TAR	T:	D	28 M	08 Y 75 TIME: 10:50 FINIS	н,	D	29 N	A 08 Y	75 T	ME: 12	85		CAN	NADIAN ARCTIC G	IS STI	UDY	LIMITE	D		SHEET 2 OF

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100 **GROUP SYMBOI** ICE GRAPHIC LOG ź SAMPLE CONDITION CONDITION NRC ICE TYPE VISUAL ICE % LABORATORY TEST DATA CORE RUN & % RECOVERY (FT.) SAMPLE TYPE & (FT) GRAPHIC OTHER DESCRIPTION DEPTH DEPTH REMARKS Plastic limit ⊢ TEST DATA CORE 60 80 100 120 140 🛦 SOIL sol 20 40 100 🖸 60 80 0 12:37 SAND - fine to coarse, silty, little fine - SM to coarse gravel, moist, brown υF 2 -3.0 00 GRAVEL - some fine to coarse sand, trace 0 GW-silt, brown, damp, occasional lost air circulation 4 -4 -GM cobbles hole sloughing ß 0 0 ° 8.0 8 SAND - fine to medium, trace coarse, 9,0 silty, brown, damp 12:45 regained circulation Nb 10 -SH 12 -13.0____ trace coarse grave 13 - hole fairly clean now 14 -TEST HOLE 16 PROJECT : FACILITY: TEST HOLE No. LOGGED BY: 130 11 <u>Z</u> 6. N. H. 1975 BORROW INVESTIGATION CHKD LAT. & LONG : 66⁰36'21''N, 129⁰07'36''W ELEVATION : 0.0. N75 DRWN. BY: PIPE MILEAGE 1. M.B. AIRPHOTO No. A12697-73 NORTHERN ENGINEERING SERVICES TH N75-1061-B3-E COMPANY LIMITED CHKD: RIG : HELI-DRILL AIR TEMP Approx. 18⁰C 1.8.9. CALGARY ALBERTA 8 AIR. ENGINEERS FOR METHOD : START: D 29 M 08 Y 75 TIME: 12:35 FINISH : D 29 M 08 Y 75 TIME: 13:20 CANADIAN ARCTIC GAS STUDY LIMITED SHEET 1 OF 2

TEST HOLE LOG

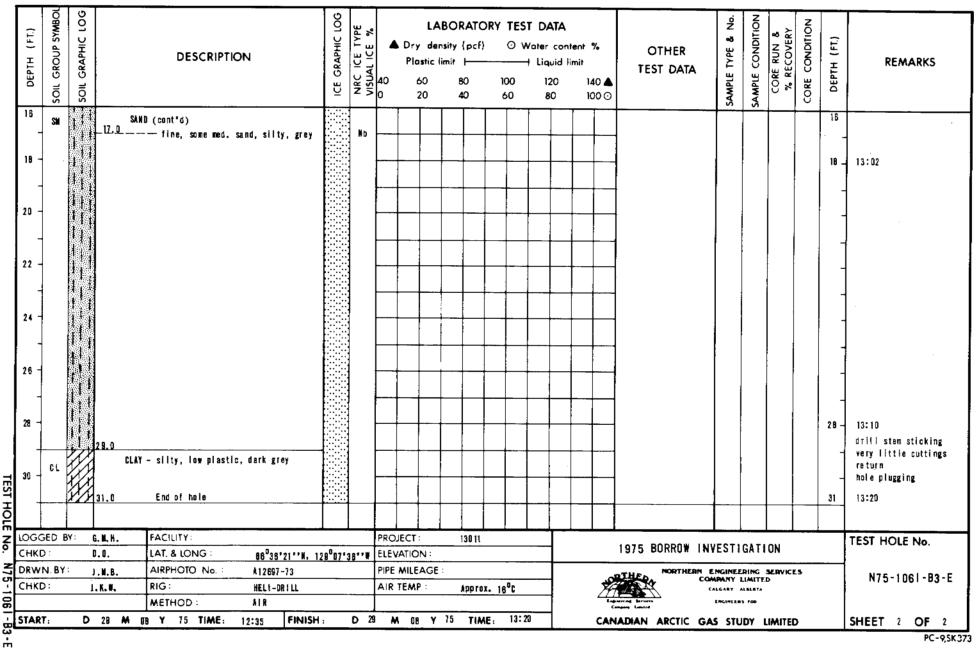
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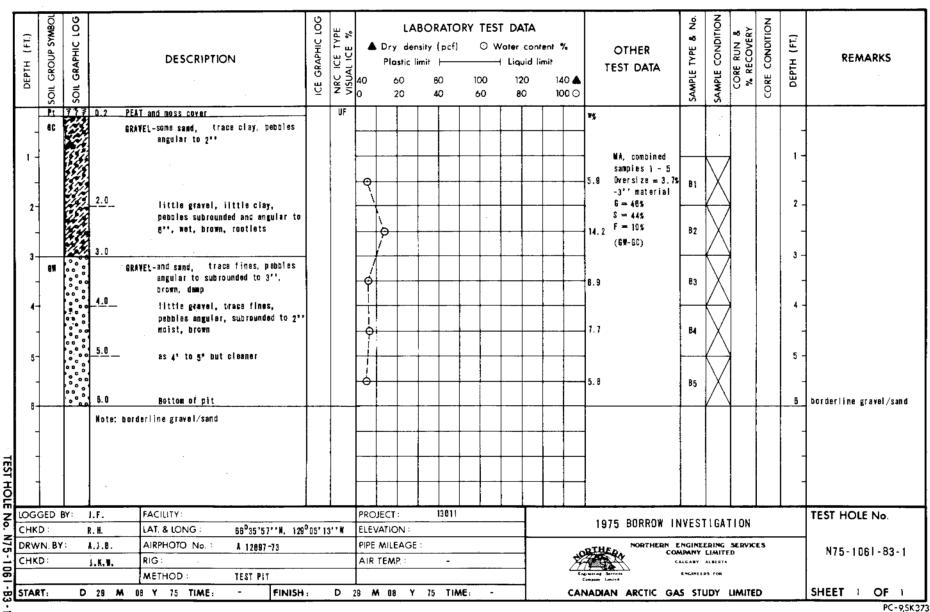
PC-9,5K373



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SOIL GRAPHIC LOG SAMPLE CONDITION SOIL GROUP SYMBO ICE GRAPHIC LOG SAMPLE TYPE & No. CORE CONDITION NRC ICE TYPE VISUAL ICE % 0 & LABORATORY TEST DATA CORE RUN & % RECOVERY DEPTH (FL) DEPTH (FL) ▲ Dry density (pcf) ○ Water content % OTHER REMARKS DESCRIPTION Plastic limit |-- Liquid limit TEST DATA 120 140 🛦 60 80 100 20 100 🖸 40 80 60 3 7/8" Walmac GRAVEL - silty, some fine to coarse Û UF GN sand, brown, moist, frequent cobbles to 8" 2 3 lost air circulation. 3 large hole End of hole á. N . TEST HOLE No. N75-1061-B3-F LOGGED BY FACILITY: PROJECT : TEST HOLE No. 13011 G.M.H **1975 BORROW INVESTIGATION** CHKD LAT. & LONG : 66⁰35'00''N, 129⁰11'00''W ELEVATION : D.O. DRWN BY: AIRPHOTO No. : PIPE MILEAGE NORTHERN ENGINEERING SERVICES COMPANY LIMITED J. M. B A 12697-73 N75-1061-B3-F CHKD: RIG : AIR TEMP J. K. W. Approx. 7⁰C HELI-DRILL CALGARY ALBERTA METHOD : ENGINEERS FOR ALR START: D 29 M 08 Y 75 TIME: FINISH : D 20 M 08 Y 75 TIME: 10:13 CANADIAN ARCTIC GAS STUDY LIMITED SHEET 1 09:45 OF

TEST HOLE LOG



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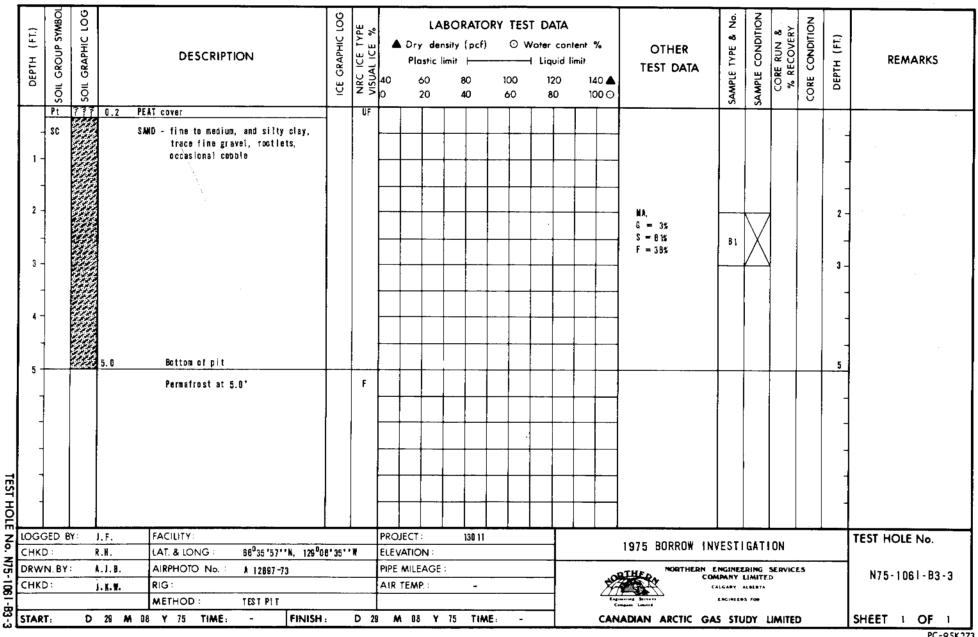
å No. SAMPLE CONDITION SOIL GROUP SYMBOL ICE GRAPHIC LOG GRAPHIC LOG CONDITION NRC ICE TYPE VISUAL ICE % LABORATORY TEST DATA CORE RUN & % RECOVERY DEPTH (FI.) DEPTH (FI.) ▲ Dry density (pcf) O Water content % SAMPLE TYPE OTHER REMARKS DESCRIPTION Plastic limit + TEST DATA CORE 140 📥 60 80 100 120 SOIL 100 🖸 40 60 80 20 777 PEAT cover Pt 0.2 UF 111 SAND - fine to coarse, silty, brown, SM occasional peobles subrounded to angular to ½", damp, occasional 1 11, 1roots, organics, MA, combined Combined 1' - 5' = 11 "SAND, fine to medium, samples 1 - 4 **B**1 6 = 10% and silt, trace fine 11 gravel''. S = 53% 2 -2.0 — 1°' gravel seams, light brown, damp 2 . F = 37% to moist (SM) 82 1 3.0 3 --- occasional cobbles 3 B3 4 4 -84 5 5 6 6.0 Bottom of pit 6 TEST HOLE TEST HOLE No. 13011 PROJECT FACILITY LOGGED BY J.F. No. 1975 BORROW INVESTIGATION 86⁰35'40"N, 129⁰04'39""# ELEVATION LAT. & LONG CHKD R.H. 2 NORTHERN ENGINEERING SERVICES PIPE MILEAGE AIRPHOTO No. N75-1061-B3-2 DRWN. BY: N.L. A 12697-73 σ COMPANY LIMITED AIR TEMP -CALGARY ALBERTA CHKD: RIG : J.K.W. 8 ENGINEERS FOR METHOD : TEST PIT SHEET 1 OF 1 CANADIAN ARCTIC GAS STUDY LIMITED FINISH : D 29 M 08 Y 75 TIME: -START D 29 M 08 Y 75 TIME: -PC-9,5K373

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TEST HOLE No.

PC-9,5K373

ŝ SAMPLE CONDITION 00 ICE GRAPHIC LOG GROUP SYMBOI CONDITION CORE RUN & % RECOVERY LABORATORY TEST DATA ТҮРЕ Е % (FT.) SAMPLE TYPE & (ET.) GRAPHIC ▲ Dry density (pcf) ⊙ Water content % OTHER NRC ICE VISUAL ICE O B REMARKS DESCRIPTION DEPTH DEPTH - Liquid limit Plastic limit |-TEST DATA CORE 60 100 120 140 📥 80 SOIL SOIL 60 80 100 🖸 20 40 UF °°° GRAVEL - some sand fmc, silty, rootlets G M Boulders on surface medium brown. ິ່ ້ ຊຳ. ເ 1 1 MA, combined SAND - fine to medium, silty, little SNsamples 1 - 5 coarse to fine gravel, pebbles Bj ML. Oversize ■ 7.8% subrounded, subangular to 2"", dark 6 = 24\$ Combined samples 1' - 6' brown, dry to damp, rootlets. 2 2 S = 32% = "SAND, fine and silt, F = 44%some coarse to fine 82 Į. gravel". 3.0 ---- cobble to 5°°, fewer coarse rootlets. 3 3 83 4 4 11 4 (4.2) 1 SAND - fine, silty, trace coarse gravel, SN B4 pebbles to 3'', dark brown. 1 5 5 B5 6 EL 146.0 Bottom of pit 6 TEST HOLE TEST HOLE No. PROJECT : 13011 FACILITY LOGGED BY: J.F. Z o 1975 BORROW INVESTIGATION ELEVATION : 66⁰36'05''N, 129⁰06'41''W LAT. & LONG CHKD R.H. **N**35 NORTHERN ENGINEERING SERVICES PIPE MILEAGE AIRPHOTO No. N75-1061-B3-4 DRWN, BY: M.L. A 12897-73 COMPANY LIMITED A1R TEMP. Cool CALGANY ALBERTA RIG : CHKD: 3.K.W. 8 ENGINEERS TOR TEST PIT METHOD : <u>ل</u>ظ SHEET 1 OF 1 M 08 Y 75 TIME: CANADIAN ARCTIC GAS STUDY LIMITED -FINISH : D 29 D 29 M 08 Y 75 TIME: -START:

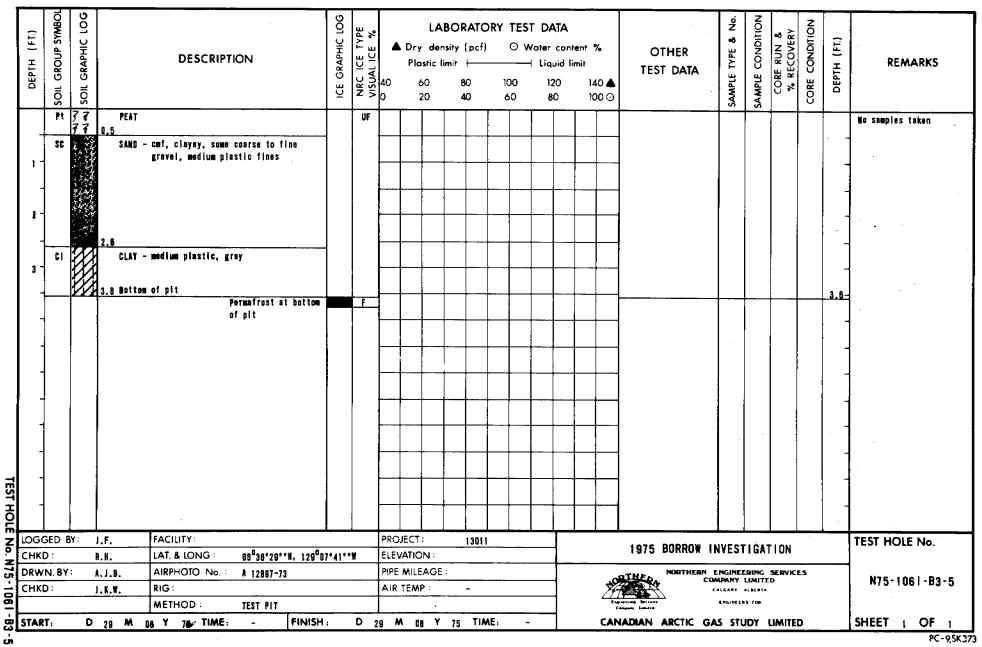
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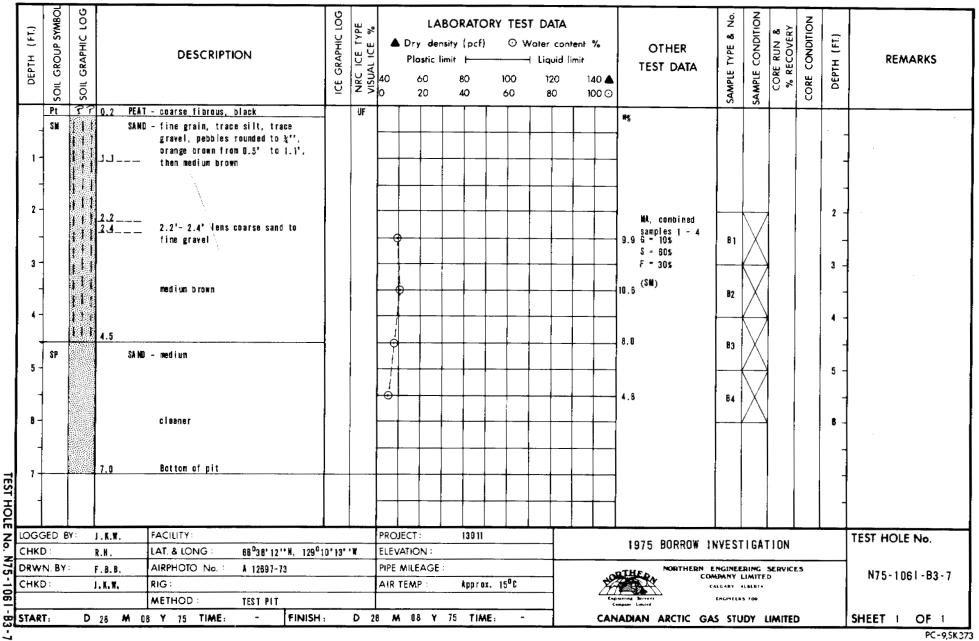
LOG **GROUP SYMBOI** ICE GRAPHIC LOG Š SAMPLE CONDITION CONDITION LABORATORY TEST DATA CORE RUN & % RECOVERY ТҮРЕ Е % (FT.) SAMPLE TYPE & (FT.) GRAPHIC ▲ Dry density (pcf) • Water content % OTHER L ICE DESCRIPTION DEPTH REMARKS - Liquid limit DEPTH Plastic limit |-NRC ICI VISUAL I 0 05 TEST DATA CORE 100 120 140 📥 60 80 SOIL SOIL 20 40 60 80 100 🖸 Pt PEAT - cover 33 *5 UF 6,8% 0.2 GRAVEL- coarse to fine, and sand, trace silty clay, rustcoloured, occasional cobbles, boulders. 1 1 6₩-MA, combined 6,0 Ð B1 GC samples 1 & 2 2 2 G = 55≸ L S = 375 3.4 F = 8% B2 oversize (3.0) 8.9 (GW-GC) 3 3 Ţ MA, combined 5.1 θ B3 transitional samples 3-5 1 A CONTRACTOR OF CONTRACTOR (4.0) 4 Oversize=6.8% 1 -3'' material; *SAND - some gravel, little silty clay, B4 5.5 pebbles to 1.5", wet. G = 445 ٠ 5.0 S = 47% S₩-5 5 F = 9% SC seams of silty clay. Θ 85 7.4 *(SW-SC) 6 Bottom of pit 6.0 6 Would have been preferable to combine • Note: from 3' to 6' borderline sand/ samples as follows: gravel based on -3'' material. 81-83, and 84485. (on basis of total sample: TEST Gravel= 47\$ Sand = 44% HOLE Fines = 9%) FACILITY LOGGED BY: PROJECT : TEST HOLE No. S L.F. 13011 1975 BORROW INVESTIGATION LAT. & LONG : ELEVATION : CHKD 66°36'21''W, 129°07'36'' W R.H. DRWN. BY: AIRPHOTO No. 1 12697-73 PIPE MILEAGE : NORTHERN ENGINEERING SERVICES D.J.W. THE N75-1061-B3-6 COMPANY LIMITED AIR TEMP Approx. 10⁰C CHKD: RIG: CALGARY ALBERTA 1.8.8. 6 ENGINEERS FOR METHOD : TEST PIT SHEET START: D 29 M 08 Y 75 TIME: -FINISH : D 29 M 08 Y 75 TIME: -CANADIAN ARCTIC GAS STUDY LIMITED OF 1 1 PC-9,5K373

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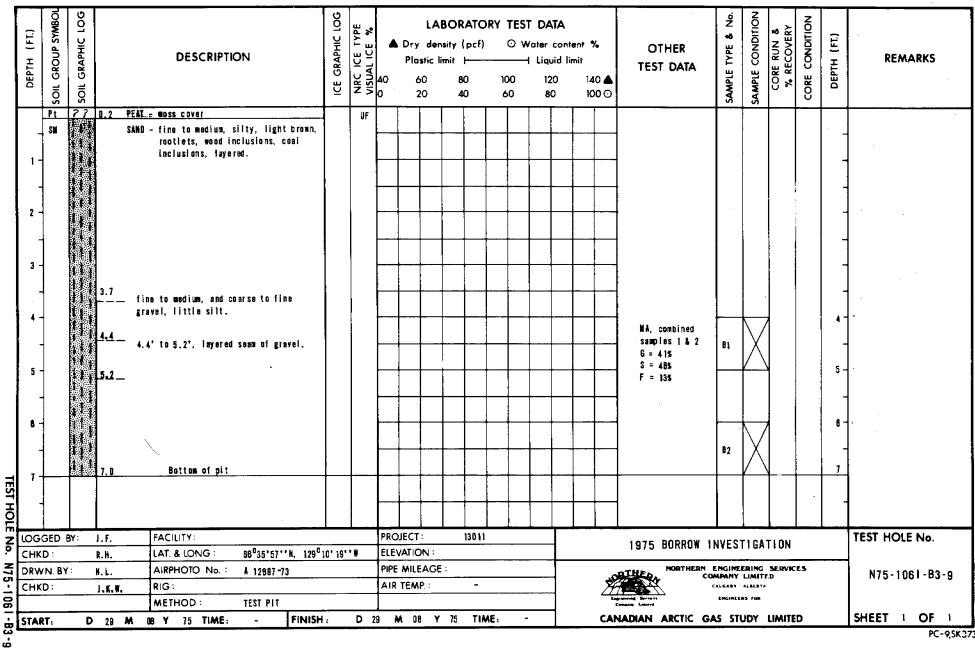
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SAMPLE CONDITION LOG ź ICE GRAPHIC LOG CONDITION GROUP SYMBOI NRC ICE TYPE VISUAL ICE % 0 & CORE RUN & % RECOVERY LABORATORY TEST DATA ٥õ (FT.) (FT.) GRAPHIC ▲ Dry density (pcf) O Water content % OTHER SAMPLE TYPE REMARKS DEPTH DESCRIPTION ---- Liquid limit DEPTH Plastic limit + TEST DATA CORE 120 140 📥 100 60 80 SOIL SOIL 100 🖸 80 20 40 60 No samples taken UF Pt 73 PEAT 77 0.5 SAND - medium, coarse to fine, clayey, SC some fine to coarse gravel, medium 1 plastic fines, medium brown SAND - fine, silty, organic inclusions SM 2 . 2.4 Bottom of pit Permafrost F TEST HOLE TEST HOLE No. PROJECT : 13011 FACILITY Ş 1975 BORROW INVESTIGATION LOGGED BY: 1.F. 66⁰36'27''W, 129⁰07'36''W ELEVATION -LAT. & LONG CHKD R.H. NORTHERN ENGINEERING SERVICES N75-1061-B3-8 PIPE MILEAGE : AIRPHOTO No. 1 OTHE. N75-1061-B3-8 A 12897-73 DRWN. BY : A.J.B. COMPANY LIMITED AIR TEMP. CALGARY ALBERTA -CHKD RIG : J.K.W. ENGINEERS FOR METHOD : TEST PIT SHEET 1 OF CANADIAN ARCTIC GAS STUDY LIMITED D 29 M 08 Y 75 TIME: -FINISH : D 28 M 08 Y 75 TIME: -START:

TEST HOLE LOG

551 ı

PC-9,5K373



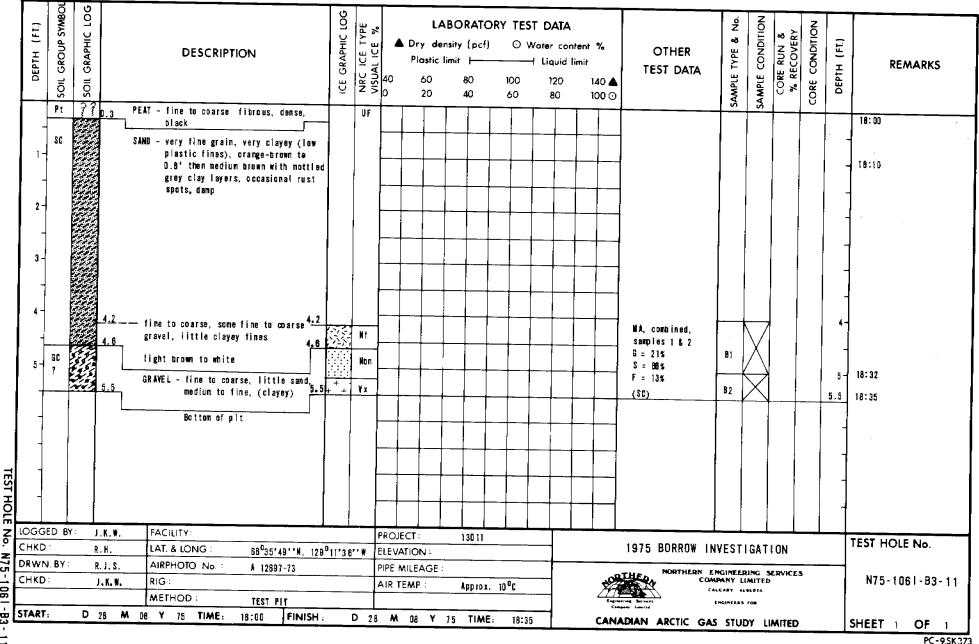
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DEPTH (FT.)	SOIL GROUP SYMBOI	SOIL GRAPHIC LOG		DESCRIPTION	ICE GRAPHIC LOG	NRC ICE TYPE			lensity (c limit BC	pcf)	Οw	T DATA fater control Liquid lir 120 80		OTHER TEST DATA	SAMPLE TYPE & No.	SAMPLE CONDITION	CORE RUN &	CORE CONDITION	DEPTH (FT.)	REMARKS
	Pt	77	P 0.5	EAT		UF														
1-	SM		-	AND - fine to coarse, and silt, trace gravel, subangular to 1°, brown, damp, roots, rootlets.	ŝ			-						NA,combined samples 1 - 5,					1-	
-														Oversize = 8.8% -3'' material:	Bj]
2 -			<u>2.0</u>	silty, little gravel, subrounded to 2".							-			G = 29% S ≈ 53% F = 18%	82				2 -	
3 -			<u>3.0</u> _	occasional inclusions of angular weak sandstone to 1''											B3	\mathbb{N}			3-	
4			4.0	rust pocket, and gravel, angular, rounded to 5'°, damp to moist.											B4				4 -	
5 - -	SC		5.0 S B.0	AND - fine to coarse, clayey, some gravel to 2½°, (medium plastic fines), brown.											85				5- - 8	
- 0				Bottom of pit											ł				-	
-									-										-	
	GED	BY:	J.F.	FACILITY	·		—	ROJECT		3011				1975 BORROW II	NVES.	TIGA	TLON			TEST HOLE No.
	D : N. B)	/:	R.H	LAT. & LONG 68 ⁰ 38'25''N, 129 AIRPHOTO No. A 12697-73	"07 " 4	6''W		EVATION						NORTHERN	ENGINE	ERING	SERVI			N75 100 P2 4
СНК			J. K. W.	RIG:			—	IR TEMP		-			X		MPANY ALGARY					N75-1061-B3-1
				METHOD : TEST PIT									<u> </u>	marring Serenze	EMGINER					
TA	t:	C	29 M	08 Y 75 TIME: - FINISH	:	D	29	M 08	Y 75	TIME	-		CAN	ADIAN ARCTIC GA	LS ST	UDY	LIMIT	ED _		SHEET 1 OF

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PC-9,5K373

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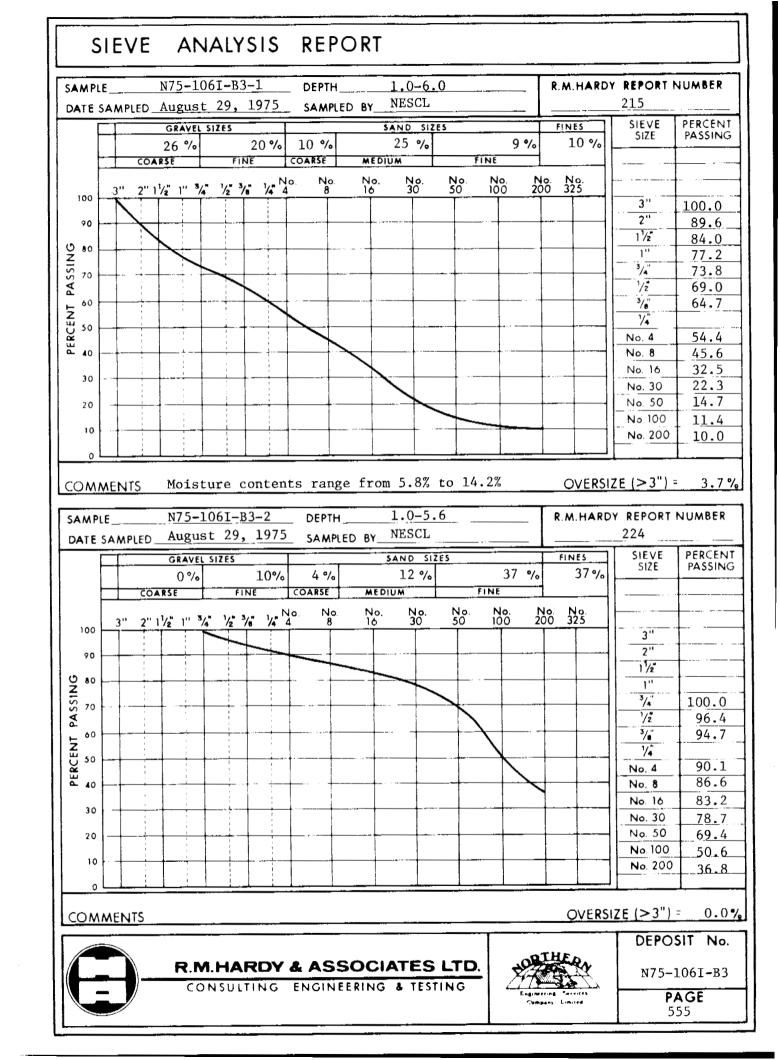
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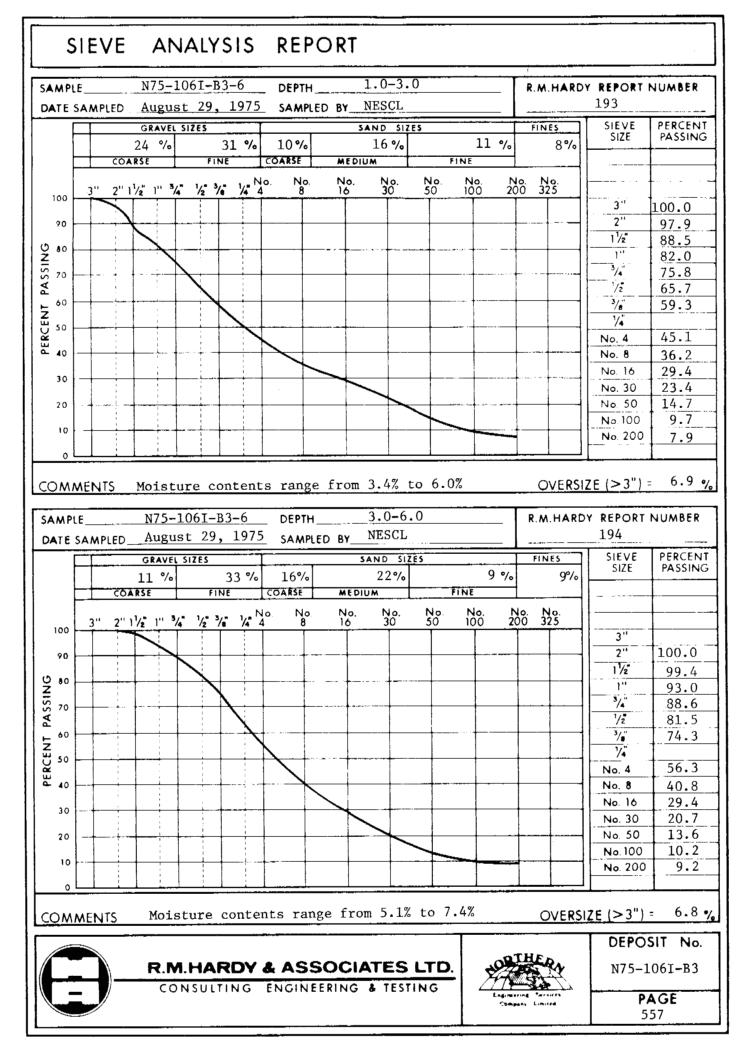
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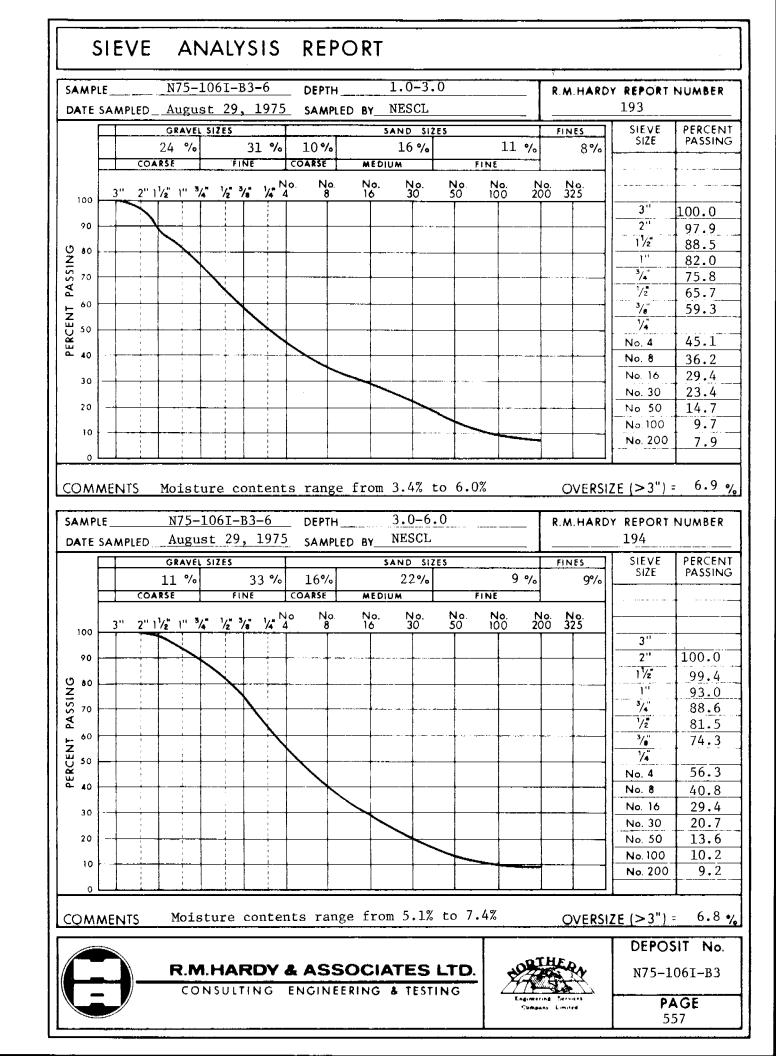
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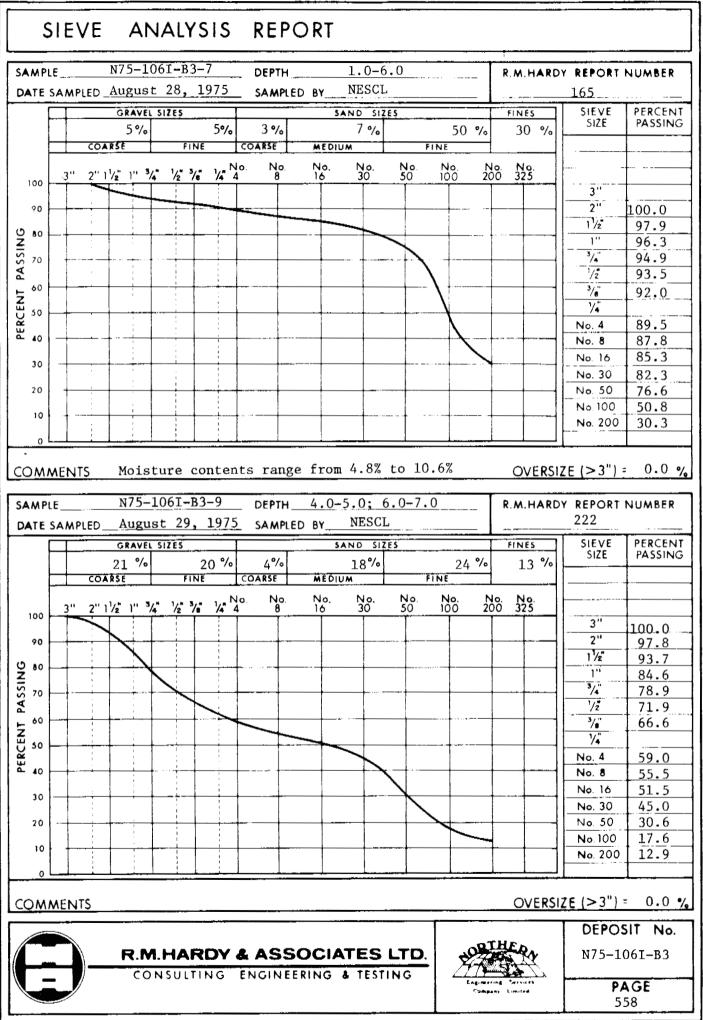
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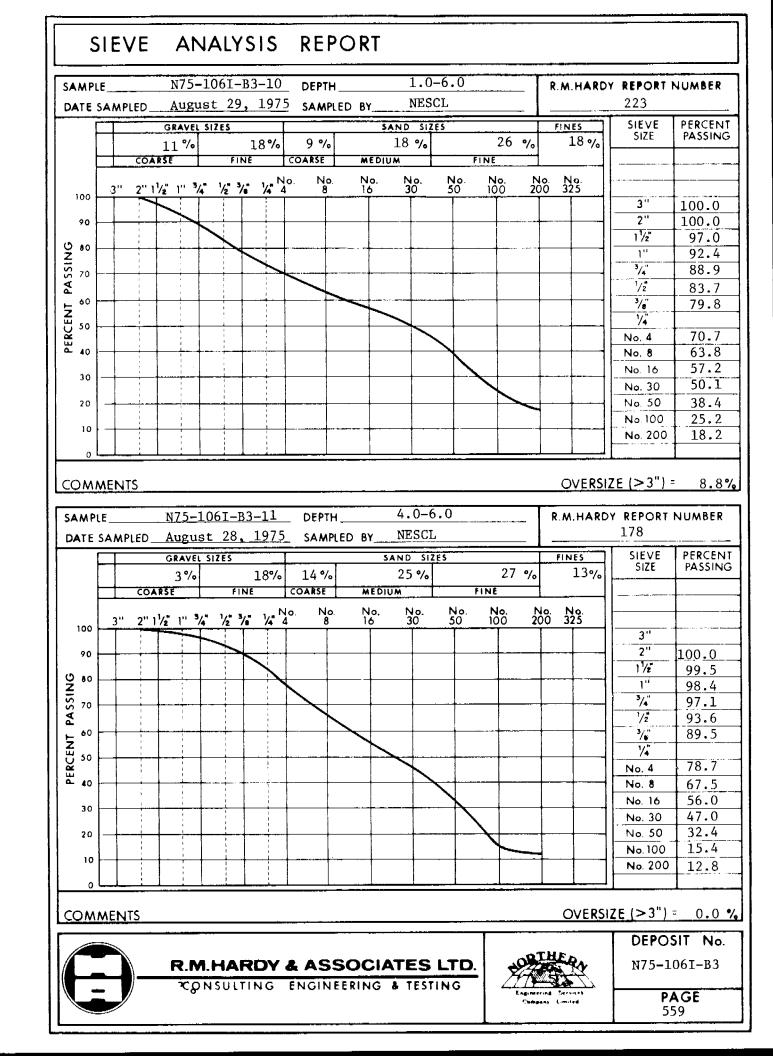


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MPLE_ TE SA	MPLED CO	Aug GRAV 16 % ARSE	gust YEL SIZ	ZES FIN	, 1 8 NE	975	2 COARS	MPLEC %	D BYS	NESCI AND SIZ	5	INE	•⁄。	FINES	DY REPORT 229 SIEVE SIZE 3" 2" 1½"	PERCEN PASSIN 100.0 91.8 87.7
MPLE_ TE SA	MPLED CO	Aug GRAV 16 % ARSE	gust YEL SIZ	ZES FIN	, 1 8 NE	975	2 COARS	MPLEC %	D BYS	NESCI AND SIZ	5	INE	•⁄。	FINES	229 SIEVE SIZE 3" 2" 1½ 1½	PERCEN PASSIN 100.0 91.8 87.7 85.1
MPLE_ TE SA	MPLED CO	Aug GRAV 16 % ARSE	gust YEL SIZ	ZES FIN	, 1 8 NE	975	2 COARS	MPLEC %	D BYS	NESCI AND SIZ	5	INE	•⁄。	FINES	229 SIEVE SIZE 3" 2" 1½" 1½" 3/4	NUMBER PERCEN PASSIN 100.0 91.8 87.7 85.1 83.7
MPLE_ TE SA 00 90 80 70	MPLED CO	Aug GRAV 16 % ARSE	gust YEL SIZ	ZES FIN	, 1 8 NE	.975	2 COARS	MPLEC %	D BYS	NESCI AND SIZ	5	INE	•⁄。	FINES	229 SIEVE SIZE 3'' 1'' 1'' 3'4 '/'	NUMBER PERCEN PASSIN 100.0 91.8 87.7 85.1 83.7 81.5
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MPLE_ TE SA	MPLED CO	Aug GRAV 16 % ARSE	gust YEL SIZ	ZES FIN	, 1 8 NE	.975	2 COARS	MPLEC %	D BYS	NESCI AND SIZ	5	INE	•⁄。	FINES	229 SIEVE SIZE 3'' 1'' 1'' 3'4 '/'	PERCEN PASSIN 100.0 91.8 87.7 85.1 83.7 81.5 79.6
MPLE_ TE SA	MPLED CO	Aug GRAV 16 % ARSE	gust YEL SIZ	ZES FIN	, 1 8 NE	.975	2 COARS	MPLEC %	D BYS	NESCI AND SIZ	5	INE	•⁄。	FINES	229 SIEVE SIZE 3'' 2'' 1'' 1'' 3',4 '/z 3',6	NUMBER PERCEN PASSIN 100.0 91.8 87.7 85.1 83.7 81.5
MPLE_ TE SA 00 90 80 70	MPLED CO	Aug GRAV 16 % ARSE	gust YEL SIZ	ZES FIN	, 1 8 NE	.975	2 COARS	MPLEC %	D BYS	NESCI AND SIZ	5	INE	•⁄。	FINES	DY REPORT 229 SIEVE SIZE 3" 2" 1½ 1½ 1 ¹¹ 3/4 ½ 3/6 ½	PERCEN PASSIN 100.0 91.8 87.7 85.1 83.7 81.5 79.6
MPLE_ ITE SA 00 90 80 70 60 50 40	MPLED CO	Aug GRAV 16 % ARSE	gust YEL SIZ	ZES FIN	, 1 8 NE	.975	2 COARS	MPLEC %	D BYS	NESCI AND SIZ	5	INE	•⁄。	FINES	DY REPORT 229 SIEVE SIZE 3" 2" 1½" 1½" 1½" 3/4 ½" 3/6 ½" 7/4 No. 4	PERCEN PASSIN 100.0 91.8 87.7 85.1 83.7 81.5 79.6 76.0
MPLE_ ITE SA 00 90 80 70 60 50 40 30	MPLED CO	Aug GRAV 16 % ARSE	gust YEL SIZ	ZES FIN	, 1 8 NE	.975 %	2 COARS	MPLEC %	D BYS	NESCI AND SIZ	5	INE	•⁄。	FINES	DY REPORT 229 SIEVE SIZE 3'' 1'' 1'' 3'," '' '' '' '' '' '' '' '' '' '' '' '' ''	PERCEN PASSIN 100.0 91.8 87.7 85.1 83.7 81.5 79.6 76.0 74.1
MPLE_	MPLED CO	Aug GRAV 16 % ARSE	gust YEL SIZ	ZES FIN	, 1 8 NE	.975 %	2 COARS	MPLEC %	D BYS	NESCI AND SIZ	5	INE	•⁄。	FINES	DY REPORT 229 SIEVE SIZE 3'' 1'' 1'' 3'," '/" '/" '/" No. 4 No. 8 No. 16	NUMBER PERCEN PASSIN 100.0 91.8 87.7 85.1 83.7 81.5 79.6 76.0 74.1 72.7
MPLE_ ITE SA 00 90 80 70 60 50 40 30 20	MPLED CO	Aug GRAV 16 % ARSE	gust YEL SIZ	ZES FIN	, 1 8 NE	.975 %	2 COARS	MPLEC %	D BYS	NESCI AND SIZ	5	INE	•⁄。	FINES	DY REPORT 229 SIEVE SIZE 3'' 1'' 1'' 1'' 3'/" '/" 3'/" '/" 3'/" '/" No. 4 No. 8 No. 16 No. 30	PERCEN PASSIN 100.0 91.8 87.7 85.1 83.7 81.5 79.6 76.0 74.1 72.7 71.0
MPLE_ ATE SA 000 90 80 70 60 50 40 30	MPLED CO	Aug GRAV 16 % ARSE	gust YEL SIZ	ZES FIN	, 1 8 NE	.975 %	2 COARS	MPLEC %	D BYS	NESCI AND SIZ	5	INE	•⁄。	FINES	DY REPORT 229 SIEVE SIZE 3" 2" 1½ 1½ 1 ¹¹ 3/4 ½ 7/2 3/6 7/4 No. 4 No. 8 No. 16 No. 30 No. 50	PERCEN PASSIN 100.0 91.8 87.7 85.1 83.7 81.5 79.6 76.0 74.1 72.7 71.0 66.5 54.8
MPLE_ ATE SA 000 90 80 70 60 50 40 30 20	MPLED CO	Aug GRAV 16 % ARSE	gust YEL SIZ	ZES FIN	, 1 8 NE	.975 %	2 COARS	MPLEC %	D BYS	NESCI AND SIZ	5	INE	•⁄。	FINES	DY REPORT 229 SIEVE SIZE 3" 2" 1½ 1½ 1½ 3/4 ½ 3/6 ½ 7/4 No. 4 No. 8 No. 16 No. 30 No. 50 No. 100	PERCEN PASSIN 100.0 91.8 87.7 85.1 83.7 81.5 79.6 76.0 74.1 72.7 71.0 66.5
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UTM - Zone9

Longitude: 129°

48'

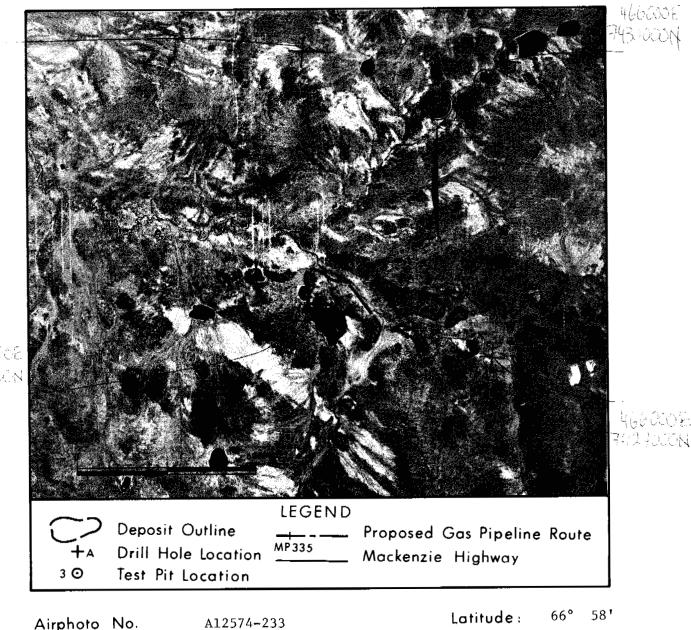
DEPOSIT 1061-B4(R)

Physical Setting: Deposit 106I-B4(R) is a group of kames and a small esker located 10 miles west of Yeltea Lake and about 1 mile east of milepost 226 of the proposed pipeline.

Material: SILT - sandy, with a trace of pebbles.

Volume: 1,800,000 cubic yards.

Assessment: Development of this deposit is not recommended due to its very poor quality material.



4640000E 7427000N

4640000

7430000N

~ 561 -

Approximate Scale: 1" = 3300'

DEPOSIT 106I-B4(R)

PHYSICAL SETTING

This deposit consists of a group of poorly defined kames and a small esker ridge located 10 miles west of Yeltea Lake and 12.5 miles northeast of the mouth of Payne Creek. It is about 1 mile east of milepost 226 on the proposed pipeline right of way.

A small stream dissects the deposit and the kames and esker stand 50 feet above the valley floor. The crests of the kames are flat to gently sloping and the stream-cut banks are moderate to steep. The esker is well drained, but drainage on the kames is imperfect to poor. The stream valley is marshy and very poorly drained. The peat and silt cover is estimated to be 1 to 2 feet thick.

Terrain between this deposit and the pipeline right of way is till covered bedrock with moderate slopes and fairly good drainage.

BIOLOGICAL SETTING

Vegetation on the kames consists of spruce with a moss ground cover. The esker ridge is partly covered with patches of aspen and juniper growing along its crest and south-facing slope. The area provides productive habitat for beaver, lynx, fox, marten, black bear, moose and caribou. Aspen in the area were observed to be heavily browsed by moose in 1975. A game trail is present along the ridge. No dens were observed. A small lake west of the site provides potential waterfowl habitat. None of the nearby lakes or streams appear to support fish populations.

MATERIAL

Drilling and test pit investigations were not carried out at this deposit. However, the field reconnaissance suggests that the deposit consists of sandy silt with a trace of pebbles.

- 563 -

VOLUME

An estimate of the total volume, based on 190 acres and 20 foot depth is 1,800,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Development potential of deposit 106I-B4(R) is low due to the very poor quality material present. However, this deposit should be proven out with test pitting and drilling before a final assessment is made.

UTM Zone 9

DEPOSIT 1061-B5(R)

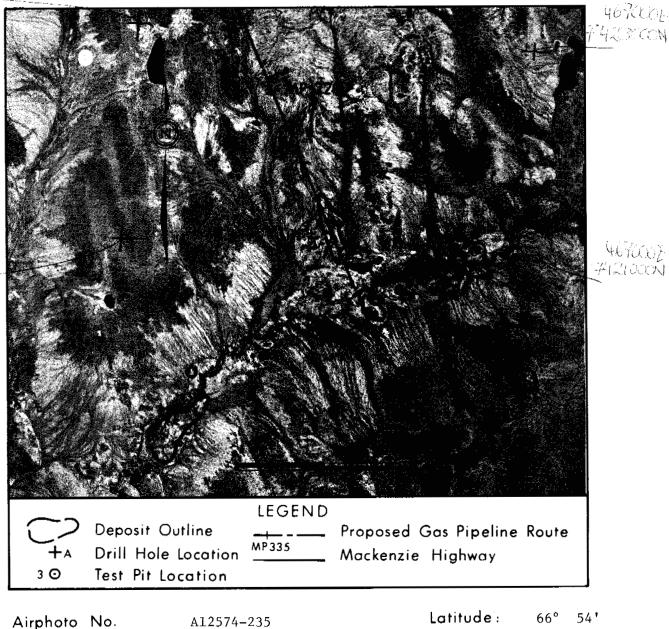
Physical Setting: Deposit 106I-B5(R) is a number of kames located 10 miles west of Yeltea Lake and crossed by the proposed pipeline at milepost 230.

Material: SAND - silty.

Volume: 2,000,000 cubic yards.

Assessment: Deposit 106I-B5(R) is not recommended for development because it contains poor quality material.

4000024 40000247



463000+ -4120012-

Approximate Scale: 1" = 3250'

Longitude: 129°

48'

DEPOSIT 106I-B5(R)

PHYSICAL SETTING

This deposit consists of a number of irregularly shaped kames located 10 miles northeast of the mouth of Payne Creek and 10 miles west of Yeltea Lake. The pipeline right of way crosses the two northern portions of the deposit near milepost 230.

The kames have steep flanks and stand 20 to 80 feet above the surrounding valley floor. There appears to be minimal overburden and good drainage, however, the river valley is marshy and poorly drained.

BIOLOGICAL SETTING

Vegetation on the kames consists of white spruce and aspen up to 25 ft. in height, under which soapberry and moss are common. The area provides productive habitat for beaver, lynx, fox, marten, black bear, moose and caribou. No waterfowl or raptors were observed in the immediate vicinity. It is not known if fish are present in the small adjacent lake.

MATERIALS

Subsurface investigation at this deposit consisted of digging a few very shallow pits which encountered silty sand.

VOLUME

A rough estimate of total volume based on an area of 120 acres and average depth of 15 feet is 2,000,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Reconnaissance investigations indicate deposit 106I-B5(R) is a source of poor quality granular material and is not recommended for development. Drilling and test pitting is recommended to provide an accurate evaluation of quality and quantity of available borrow, since the pipeline right of way crosses the two northern portions of the deposit, and would provide highly accessible borrow material that could be suitable for general fill and possibly backfill.

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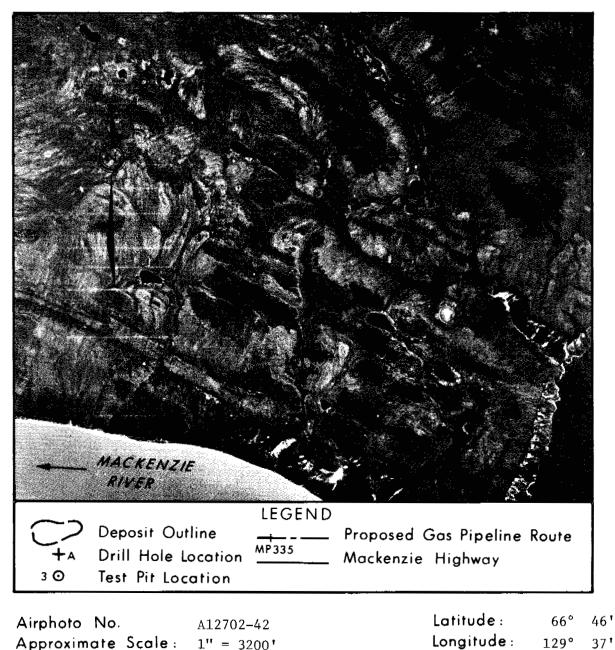
Physical Setting:Deposit 106I-B6(R) is a small esker located 8 miles
west of Yeltea Lake, 2 miles north of the Mackenzie
River and 3 miles southwest of mile 240 of the pro-
posed pipeline right of way.Material:SAND - clean, well graded, little gravel.

Volume: 900,000 cubic yards.

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Assessment: Deposit 106I-B6(R) is a source of fair quality granular material suitable for general fill, backfill, and building pads. Access should present few problems.



DEPOSIT 106I-B6(R)

PHYSCIAL SETTING

This deposit consists of segments of a small esker located 8 miles west of the south end of Yeltea Lake and 2 miles north of the Mackenzie River. It is 3 miles southwest of milepost 240 on the proposed pipeline right of way.

The esker ridge has moderately sloping sides and rises 20 feet above the surrounding terrain. Overburden is negligible and the deposit is well drained. The small valley in which the esker is situated is marshy and poorly drained. Terrain between this deposit and the pipeline right of way is rolling moraine with moderately good drainage and a few wet peat-filled depressions.

BIOLOGICAL SETTING

Vegetation on the esker consists of white spruce and aspen up to 50 ft. in height with a ground cover of dward shrubs and lichens. The area immediately surrounding the esker is a fen with sedges, shrubs and stunted trees. The area provides low quality wildlife habitat. Because of the proximity of the site to the Mackenzie River, large numbers of waterfowl may be present in the vicinity during May and June. None of the small ponds, lakes, or streams in the area appear to provide suitable fish habitat.

MATERIAL

A very shallow pit encountered clean, well graded sand and a little gravel.

VOLUME

An estimated volume, based on an area of 50 acres and an average depth of 15 feet is 900,000 cubic yards.

- 571 -

DEVELOPMENT AND REHABILITATION

Reconnaissance investigations indicate deposit 1061-B6(R) is a source of fair quality granular material, suitable for general fill, backfill in pipeline construction and building pads. Despite the rather low volume, shortages of good quality borrow in this area suggest a drilling and test pitting program should be carried out to properly assess this deposit.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Access to the pipeline right of way is over moderately well drained, rolling moraine and should present few problems. Snow roads would be built to transport the borrow material from the deposit to the pipeline right of way, a distance of 2 miles.

Development of the esker segments would first involve removal of vegetation, which would be disposed of or harvested according to current land use regulations. Overburden is negligible, therefore, minimal stripping and stockpiling of it would be required. Conventional earthmoving techniques should be sufficient for excavation of this unconsolidated, well drained material. Borrow would be removed in stages from higher well drained areas to a grade such that good drainage is maintained.

Equipment required for development would be dozers, rippers, end-dump trucks, and front-end loaders.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

UTM-Zone 9

DEPOSIT 1061-B7(R)

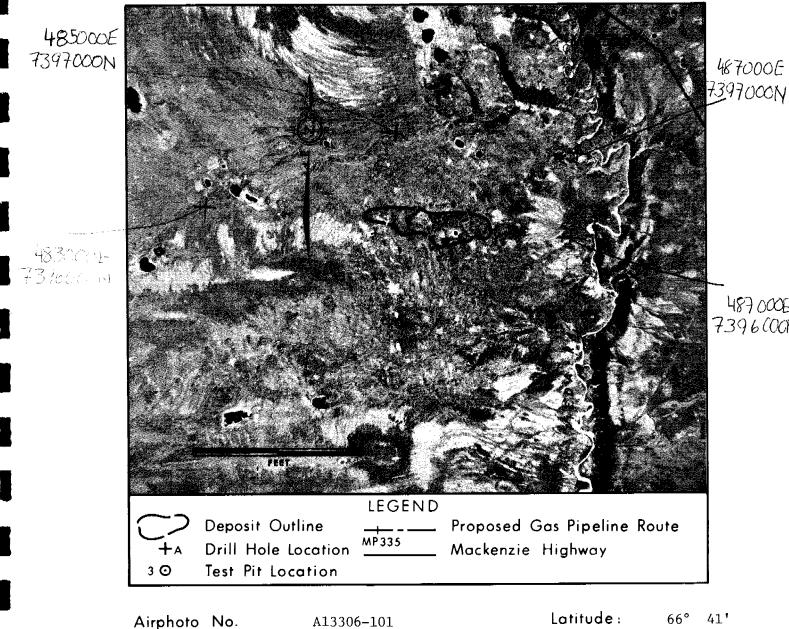
Physical Setting: Deposit 106I-B7(R) is a small kame complex located 1 mile west of Tieda River and 2 miles southwest of milepost 250 on the proposed pipeline.

Material: SAND - silty, with a trace of gravel.

Volume : 1,000,000 cubic yards.

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Deposit 106I-B7(R) is a source of poor quality Assessment: granular material suitable only for marginal fill. Further work is required to determine its suitability for development.



487000E 7396 COCN

129°

Longitude :

20'

1'' = 3400'

Approximate Scale :

DEPOSIT 106I-B7(R)

PHYSICAL SETTING

This deposit is a small kame complex located about 1 mile west of the Tieda River and 2 miles southwest of milepost 250 on the proposed pipeline right of way.

The hills that constitute the kame complex rise 20 to 30 feet above the surrounding terrain. Moderate slopes are well drained, but drainage on the flatter areas is imperfect to moderate. Overburden appears to be negligible on the hills, however it may increase to depths of 10 feet or more in a few poorly drained depressions.

The terrain north toward the pipeline right of way is mainly moderately well drained rolling moraine, although some peat covered areas are present.

BIOLOGICAL SETTING

Vegetation on the kames consists of white spruce and birch up to 60 ft. in height. Soapberry, rose and alder are present in the understory. Surrounding depressional, poorly drained areas are covered with stunted black spruce and sedges. The area provides low quality wildlife habitat. Snowshoe hare sign was observed at the site. The only birds seen in the area were passerines; otherwise this is poor quality habitat for raptors and waterfowl. Nearby streams and ponds do not appear to support fish populations.

MATERIAL

A shallow pit dug at this site encountered silty sand with a trace of gravel. Indications are that the material is of poor quality.

VOLUME

Based on an area of 80 acres and thickness of 10 feet, the volume of granular material in this deposit would be 1,000,000 cubic yards.

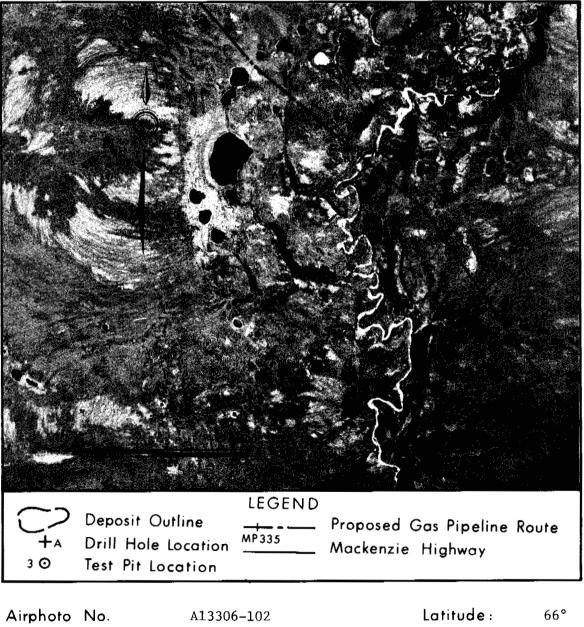
DEVELOPMENT AND REHABILITATION

Reconnaissance observations at deposit 106I-B7(R) indicate it is a source of poor quality granular material suitable only for marginal fill. Additional drilling is recommended in order to accurately assess the suitability of this deposit for development. Physical Setting: Deposit 106I-B8(R) is an esker located on the east side of Tieda River and just 1 mile from the proposed pipeline at milepost 251.

Material: SAND - silty, with a trace of pebbles.

Volume: 700,000 cubic yards.

Assessment: Deposit 106I-B8(R) is a source of poor quality granular material. However, due to its close promixity to the proposed pipeline in an area with a shortage of granular materials, this deposit should be investigated in detail.



Approximate Scale: 1" = 3400'

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A13306-102 1" = 3400' Latitude: 66° 42' Longitude: 129° 17'

DEPOSIT 1061-B8(R)

PHYSICAL SETTING

This deposit is a narrow esker flanking the east side of the Tieda River valley, about 5 miles above its mouth. Milepost 251 on the proposed pipeline right of way is within 1 mile of the northern end of the deposit. This deposit corresponds to source number 1025 in EBA DIAND Granular Materials Inventory Volume II (1974) report.

The crest of the esker stands about 140 feet above river level and 15 feet above the adjacent upland. The esker is well drained, and overburden is nil except on its eastern edge. A narrow, poorly drained peatland is situated directly east of the esker between the deposit and pipeline right of way.

BIOLOGICAL SETTING

Vegetation on the esker consists of white spruce and birch up to 30 ft. in height. Willow, rose, soapberry and juniper are common in the understory and ground cover is mainly moss and lichen. The area provides productive habitat for caribou, lynx, mink, wolf, fox, black bear, moose and occasional grizzly bear. During the period November-December, and March-April, moose migrate through the area enroute to and from islands in the Mackenzie River. Areas of riparian vegetation along the Tieda River provide good moost habitat. A bear or wolf den was observed on the northwest shore of a small lake near the site. Snowshoe hare, squirrel and a wide range of passerine and upland bird species use the area. There is little waterfowl habitat in the vicinity. During the summer period, hrayling, long-nose suckers, round whitefish, pike, slimy sculpin, and lake chub are present in the Tieda River. There is no reported winter flow in this river. Spawning runs of grayling and whitefish move through the river enroute the Yeltea Lake.

MATERIAL

This deposit appears to be silty sand with a trace of pebbles. Trenches on the surface suggest that ice wedges are present. This deposit probably contains poor quality borrow material.

VOLUME

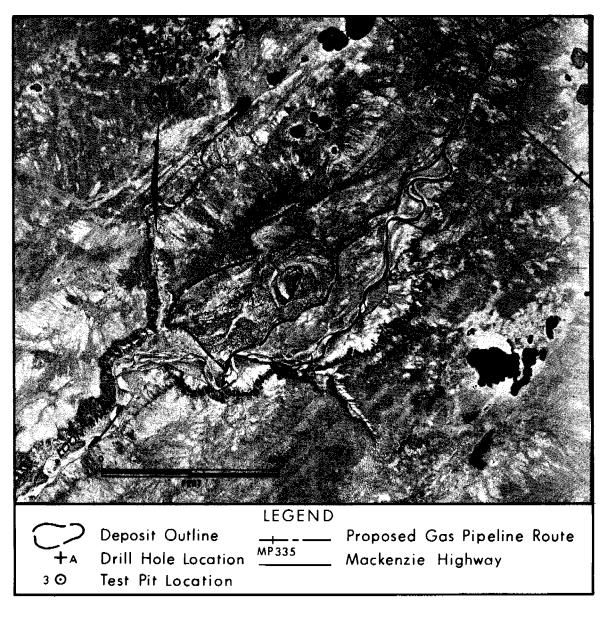
The thickness of the deposit is difficult to assess because of its peculiar position relative to the river valley. An average depth of 10 feet and area of 50 acres were used to estimate a total volume of 700,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Reconnaissance investigations indicate deposit 106I-B8(R) is a source of poor quality granular material. Since this deposit is very close to the pipeline alignment and granular material is scarce in this area, further drilling is recommended to assess material quality and volume before eliminating this deposit as a source of construction materials.

1 Seo 1003-1 (BA

- Physical Setting:Deposit 106I-B9(R) is a series of fluvial terraces
located on the north bank of the Loon River and
skirted on its eastern end by the proposed pipe-
line at milepost 269.Moterial:SAND and GRAVEL interbedded sand and well to
poorly graded gravel.
- Volume: 7,600,000 cubic yards.
- Assessment: Deposit 106I-B9(R) is a source of good quality granular material suitable for general fill, backfill, building pads, and possible concrete and asphalt aggregate. Access presents no problems as the right of way skirts the deposit.



Airphoto No. A12609-19 Approximate Scale: 1" = 3250' Latitude: 66° 29' Longitude: 128° 52'

DEPOSIT 1061-B9(R)

PHYSICAL SETTING

This deposit consists of a series of fluvial terraces located on the north bank of Loon River 3 miles upstream of its confluence with the Mackenzie River. The proposed pipeline alignment skirts its northeastern end at mile 269. This deposit corresponds to a portion of source number 1003 described in EBA DIAND Granular Materials Inventory Volume II (1974) report.

The terraces stand 20 to 70 feet above the level of Loon River floodplain and slope very gently to the west. Scarps separating the terrace levels are steep, and vary from 10 to 40 feet in height.

Drainage on the terraces is good near the scarps, but imperfect to poor on the central and back part of the benches. Overburden is thin near the terrace edges, but probably thickens to 10 feet or more in the poorly drained areas. Thaw depths will be variable, depending on cover conditions.

BIOLOGICAL SETTING

Much of the deposit is covered by white spruce up to 50 ft. in height with an understory of willow, Labrador tea, cinquefoil and blueberry. The poorly drained areas are covered by stunted black spruce and a ground cover of moss and lichens. The general area provides good habitat for upland furbearers, mink, and black bear. The Loon River valley provides excellent winter range for moose and serves as a migration corridor for moose moving to and from islands in the Mackenzie River. The Loon River serves as a spawning and nursery area for long-nose sucker, long-nose dace, pike and grayling, and is a possible spawning area for whitefish, cisco, ninespine stickleback and lake chub. There is a domestic fishery at the mouth of the Loon River and at Loon Lake.

MATERIAL

An exposed terrace and logs from the DIAND report indicates that this deposit is a source of good quality borrow material. Interbedded sand and wellgraded to poorly graded gravel were observed. Some of the gravel beds may contain an abundance of cobbles and boulders.

VOLUME

The estimated volume for this deposit, based on an area of 470 acres and a conservative depth of 20 feet, is 7,600,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 106I-B9(R) is a source of good quality granular material suitable for general fill, backfill in pipeline construction, building pads, and concrete and asphalt aggregate. The gravel would require testing prior to use in concrete aggregate. Extensive drilling would be required to locate suitable areas for development.

No biological factors were identified which would preclude development of this deposit. To minimize biological, environmental and socioeconomic impacts final locations of all facilities including roads, camps, pit boundaries, etc., will be subject to further field investigation. Development and operation of borrow sources may be scheduled and activity restricted to designated areas during certain periods of the year.

Since the pipeline right of way passes near the eastern end of the deposit, access presents no problems. In order to minimize environmental damage, snow roads would be built to transport the borrow material from the pits to haul points on the right of way and excavations would be kept away from the Loon River to prevent siltation. At selected sites, trees and other vegetation would be removed and harvested or disposed of in accordance with land use regulations. The peat and overburden would then be stripped off and stockpiled around the edge of the excavation.

Development would involve excavating borrow material from the face of the scarps or evenly from the higher, better drained areas so that drainage is maintained. Blasting or conventional earthmoving techniques could be used depending on degree of ice cementation. The excavated material may have to be stockpiled, thawed and drained before it is used. Crushing and/or screening of the material may be required to produce quality construction aggregates.

Equipment required for development would be dozers, rippers, end-dump trucks, front-end loaders, as well as screening, crushing, concrete and asphalt plants if required.

A progressive rehabilitation plan will be developed for each deposit. This plan will have the objective of restoring disturbed areas to be compatable with their surroundings, and will outline the sequence of rehabilitation procedures to be used at each stage of development and at the abandonment of the site. This may include procedures such as: selective grading and shaping; selective stripping and replacing of top soil and overburden; installation of physical erosion control structures and material; seeding and mulching; and the planting of trees and shrubs.

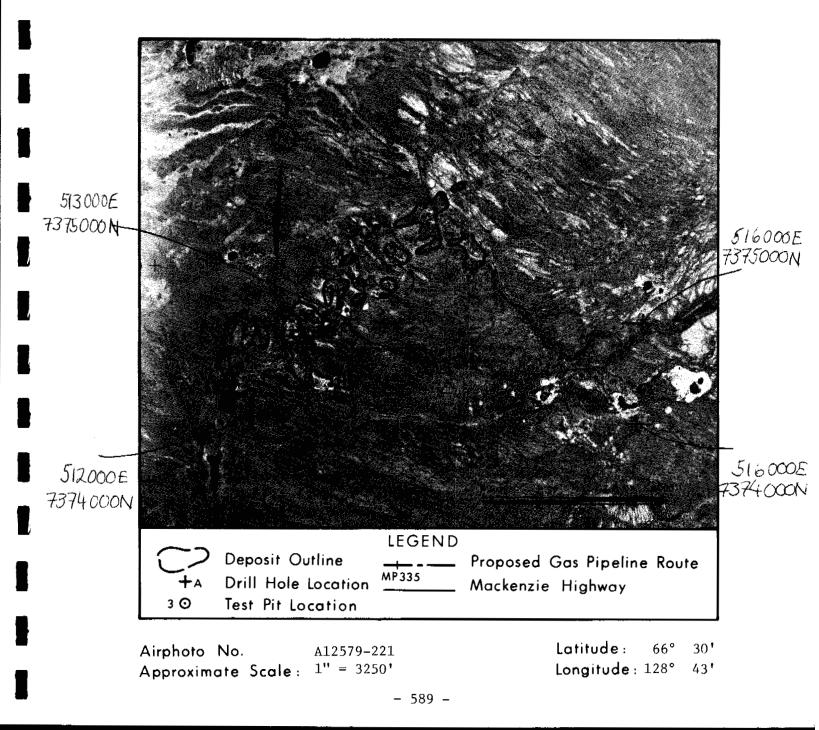
UTM Zone 9

DEPOSIT 1061-B10(R)

Physical Setting:Deposit 106I-B10(R) consists of a number of kames
and small eskers located 6 miles east of the Loon
River mouth and 2 miles east of milepost 272 on
the right of way.Material:SAND - silty.

Volume: 1,000,000 cubic yards.

Assessment: Deposit 106I-B10(R) is a source of fair quality granular material but because other better quality deposits are closer to the right of way it will probably not require development.



DEPOSIT 106I-B10(R)

* PHYSICAL SETTING

This deposit consists of a number of kames and small eskers located 6 miles east of the mouth of the Loon River and 2 miles east of milepost 272 on the proposed pipeline right of way.

The ridges and hills stand 5 to 30 feet, and occasionally 50 feet, above the surrounding terrain. They have gentle to moderate slopes and are well to moderately well drained. Peat cover is generally thin and thaw depths of about 12 feet can be expected.

The surrounding area is a gently sloping till plain covered by black spruce forest with occasional peat bogs and fens.

BIOLOGICAL SETTING

The site is covered by a mixed stand of spruce, aspen and birch up to 30 ft. in height with juniper and soapberry being the most common shrubs. The area provides year-round habitat for upland furbearers, caribou and moose. Potential den sites occur throughout the area. Marten sign was seen during the 1975 survey. The area is hunted and trapped by residents of Fort Good Hope. Ponds and lakes in the vicinity provide limited waterfowl habitat. Streams may support fish populations during the open-water season.

MATERIAL

Surface sampling during the field reconnaissance indicate that this deposit is silty sand, although gravel may be more common at the eastern end.

VOLUME

Based on an area of 200 acres and an average depth of 10 feet, the total estimated volume of borrow is 1,000,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Reconnaissance investigations indicate the material in deposit 106I-B10(R) is of fair quality. However, a detailed drilling program would be required to accurately assess its potential. Deposit 106I-B9(R) is closer to the pipeline right of way and a better source in both quality and volume than 106I-B10(R). It is therefore unlikely that further investigation and development of this site would be necessary. DEPOSIT 106I-B11(R)

JSee FGH 6

- Physical Setting: Deposit 106I-B11(R) is an esker located 10 miles north of Fort Good Hope and about 4 miles east of milepost 279 of the proposed pipeline right of way.
- Moterial: SAND poorly graded, with isolated pockets of gravel.
- Volume: 1,500,000 cubic yards.

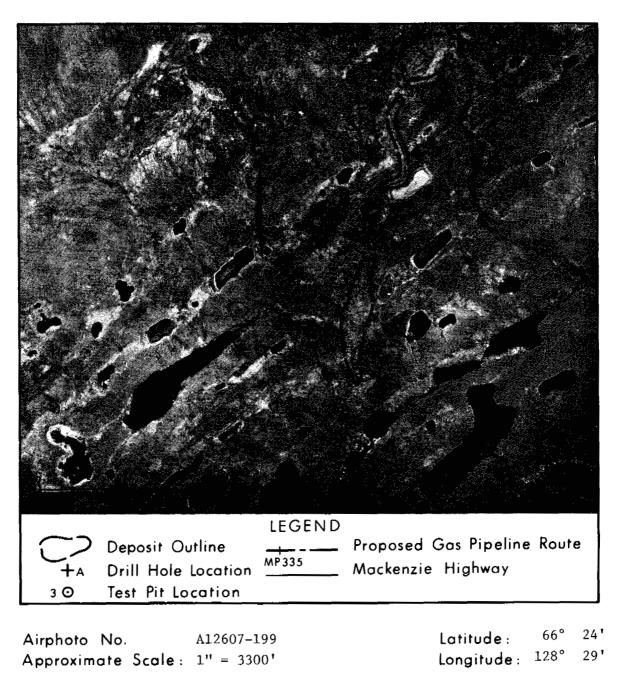
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Assessment: Deposit 106I-B11(R) is a source of fair to poor quality granular material suitable for general fill but not recommended for development.



DEPOSIT 106I-B11(R)

PHYSICAL SETTING

This deposit is an esker located ten miles north of Fort Good Hope and about 4 miles east of milepost 279 on the proposed pipeline right of way. This deposit corresponds to source number 1006a in EBA DIAND Granular Materials Inventory Volume II (1974) report.

The esker has moderate to steep sided slopes and stands 30 to 80 feet above the surrounding terrain. It is a narrow ridge at its northern end, but broadens at its southern end. The deposit is well-drained and overburden is negligible. Thaw depths of 12 feet or more can be expected.

The surrounding terrain is a rolling till plain with many poorly drained, peat filled depressions.

BIOLOGICAL SETTING

This area shows evidence of an old burn. The crest of the esker is now covered by aspen with a dense understory of shrubs, while the slopes are covered by a mixed stand of birch and spruce with scattered alder. This area provides habitat for upland furbearers, moose and caribou. Residents of Fort Good Hope hunt and trap in the area. A pair of Arctic loons was observed nesting on a small adjacent pond. The small ponds and streams near the deposit do not appear to support fish populations.

MATERIAL

The DIAND report shows that the esker consists of poorly graded sand with isolated pockets of gravel. Further drilling and test pitting would be required for an accurate assessment of the deposit.

VOLUME

Volume estimates for this deposit are 1,500,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 106I-B11(R) appears to be a source of fair to poor quality granular material suitable for general fill. Development of this site might be necessary if better quality material is not available closer to the pipeline route, but at this time it is not recommended for development. DEPOSIT 1061-B12(R)

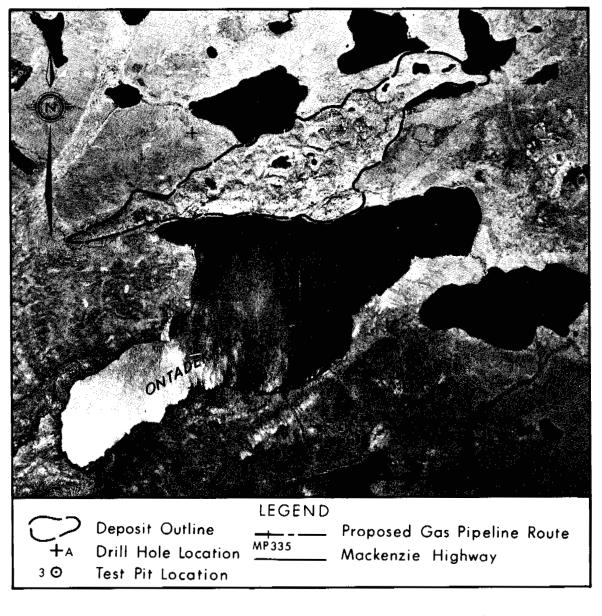
1 See FGH 9

Physical Setting: Deposit 106I-B12(R) is a large kame complex bordering the north edge of Ontadek Lake 9 miles east of Fort Good Hope and 5 miles east of milepost 289 of the proposed pipeline. SAND - poorly graded, fine.

Volume: 12,000,000 cubic yards.

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Assessment: Deposit 106I-B12(R) is a source of fair to poor quality granular material suitable for general fill. Good quality granular material within the deposit may well be located with further exploration. Access presents very few problems.



Airphoto No. A12604-87 Approximate Scale: 1" = 3350' Latitude : 66° 18' Longitude : 128° 23'

DEPOSIT 1061-B12(R)

PHYSICAL SETTING

This deposit is a large kame complex which borders the north edge of Ontadek Lake. It is about 9 miles east of Fort Good Hope and 5 miles east of milepost 286 on the proposed pipeline alignment. This deposit corresponds to source number FGH-9 in Pemcan Services DIAND Granular Materials Inventory (1972) report.

The complex stands 80 to 100 feet above the surrounding terrain and most of its surface is rolling with shallow depressions. Numerous steepsided ridges and kettles are present. Overburden is negligible except in depressions where peat may be 5 feet thick. The site is well drained except for local swales and depressions. Thaw depths of 12 feet can be expected under well drained areas.

Except for a large well drained esker complex near Fort Good Hope, most of the terrain between the deposit and the pipeline right of way is flat to rolling and moderately well to imperfectly drained.

BIOLOGICAL SETTING

Vegetation at this site consists of white spruce with occasional aspen and birch. Poorly drained areas have black spruce and tamarack with a ground cover of sedges, moss, and lichen. Sharp crested ridges have only a partial cover of shrubs and herbs. The area is adjacent to Ontadek Lake which provides good moose habitat. A cow and calf moose and moose tracks were observed during the 1975 survey. A beaver lodge was also seen on the lake. An inactive red fox den was observed as well as snowshoe hare and red squirrel sign. The area provides good marten habitat. Waterfowl utilize the lake during the open-water season. The area is actively hunted and trapped by residents of Fort Good Hope. A one-year-old camp was located in the area. Ontadek Lake is fished from May to September by residents of Fort Good Hope.

MATERIALS

The DIAND report indicates that this deposit consists mainly of poorly graded fine sand. However, many of the sharp-crested ridges superimposed on the kame complex appear to be partly gravel.

VOLUME

Based on an area of 600 acres and a conservative depth of 25 feet, total estimated volume is 12,000,000 cubic yards.

DEVELOPMENT AND REHABILITATION

Deposit 106I-B12(R) appears to be a source of fair to poor quality granular material suitable for general fill. Further drilling might locate areas of good quality gravel. This procedure is recommended so that the better sources near Fort Good Hope may be kept for local use. Access to the deposit over flat to rolling terrain presents few problems. Development could be carried out according to detailed plans to be prepared when more information is available.

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APPENDIX A

Terms and Symbols

APPENDIX A - EXPLANATION OF TERMS AND SYMBOLS

1. <u>General</u>

The terms and symbols used on the test hole logs to summarize the results of the field investigation and of subsequent laboratory testing are described in detail below and are illustrated in the appended exhibit test hole log (Plate 1).

General information, such as test hole number, test hole location, and rig type is noted in the lower portion of the test hole log. Detailed sub-surface information observed at each test hole location and laboratory test data, are presented in columnar form on the test hole log. Each column used is described in detail below using the reference numbers shown on the appended blank test hole log (Plate 2).

It should be noted that the soil type, stratigraphic boundaries, and in situ conditions have been established only at the test hole location and that they are not necessarily representative of subsurface conditions elsewhere across the site.

Columns 1Depth:The depth of test hole below existingand 13:ground surface is shown in these columns.

Column 2: <u>Soil Group Symbol</u>: A soil classification symbol in accordance with a modification of the Unified Soil Classification System¹ is noted in this column. A definition of each Group Symbol is given in Table 1 "Soil Classification System".

Column 3: <u>Soil Graphic Log</u>: Soil strata are depicted graphically in accordance with the "Graphic Symbol" column of Table 1 "Soil Classification System".

(1) References are listed on page A - 21.

Column 4:

Description: A detailed engineering description of each soil stratum encountered is noted in this column. This description is given in accordance with the criteria outlined in Section 2.3 "Soil Description". A description of the ground ice is included in this column according to the NRC procedures² which are explained in Section 2.4 "NRC Ice Type". The depths to ground water level, seepage, and the interface between different soil strata are indicated in this column. The interface between soil strata is shown as a single continuous line. A broken line indicates a change in soil type where the location of the interface between the strata is uncertain or inferred. A double line at the bottom of the test hole log indicates "Refusal" which may be defined as "further penetration was not possible with the equipment used".

- Column 5: <u>Ice Graphic Log</u>: The various types of ground ice are depicted graphically according to Table 2 "Ground Ice Classification".
- Column 6: <u>NRC Ice Type</u>: (Visual Ice %): Abbreviated symbols for the forms of ground ice are noted in this column. A description of the NRC classification² is contained in Section 2.4 "NRC Ice Type", and in Table 2 "Ground Ice Classification". The volume of ground ice is estimated visually and expressed as a percentage of the total volume of soil and ice.
- Column 7: <u>Laboratory Test Data</u>: The results of laboratory determinations of water content, Atterberg limits and density are plotted against depth. These are described in Section 2.5 "Test Data Summary".

A – 2

Column 8: <u>Other Test Data</u>: Test data additional to those represented in Column 7 are noted in this column at the appropriate depth. The symbols used to represent the more common engineering laboratory tests are given in Section 2.5 "Test Data Summary". The results of specialized testing are also indicated in this column using an abbreviated written form.

Column 9: <u>Sample Type and Number</u>: The type and reference number of each sample attempted, whether it was recovered or lost, are recorded at the appropriate depth. The system used is described in Section 2.1 "Soil Sample Data".

Column 10: <u>Sample Condition</u>: The condition of each sample whether it was recovered or lost, is recorded against depth. A description of the graphic representation and abbreviations used is given in Section 2.1 "Soil Sample Data".

- Column 11: <u>Core Run and % Recovery</u>: The length of core recovered is expressed as a percentage of the total length attempted. The depths to the top and bottom of the core run are recorded as described in Section 2.2 "Core Data".
- Column 12: <u>Core Condition</u>: The condition of the core, or segments of the core, is assessed visually and assigned a rating of I to V. The ratings and nomenclature used are given in Section 2.2 "Core Data".
- Column 14: <u>Remarks</u>: Additional pertinent information and comments such as in situ drilling conditions, sampling criteria, and instruments installed are noted in this column.

A – 3

2. <u>Description Details</u>

The various terms, symbols, and abbreviations are discussed in detail to facilitate interpretation and understanding of the data presented on the test hole logs.

2.1 <u>Soil Sample Data</u>

(a) Sample Type and Number (Column 9)

Each sample attempted, whether it is recovered or lost, is assigned a reference number. The series of soil samples from each test hole is numbered in a sequentially increasing numerical order with increasing depth below ground surface.

The type of sample attempted is indicated using one of the following letters:

- A Auger sample
- B Bulk sample
- C Core sample
- D Drive sample (thick-walled tube, unless otherwise noted)
- P Pitcher tube sample
- R Block sample
- S Split spoon standard penetrometer sample
- U Tube sample (thin-walled unless otherwise noted)
- W Wash or Air Return sample
- X Other samples

The sample type and number are recorded at the appropriate depth on the test hole log.

Example: Sample A2: - designates the second sample attempted in the test hole. This sample was taken off an auger.

(b) Sample Condition (Column 10)

The condition of each sample attempted is designated by one of the following symbols at the appropriate depth interval:







undisturbed

disturbed

not recovered

2.2 <u>Core Data</u>

The details relating to length of core attempted and the percentage of core recovered are presented as follows:

(a) Core Run and % Recovery (Column 11)

The length of core attempted is shown by recording the top and bottom depth measurements for each core run. The recovered core length is expressed as a percentage of the total core run attempted.

(b) Core Condition (Column 12)

The condition of each core, or segments of core recovered, together with any unrecovered portions of the core, is recorded. The nomenclature in the following table is used to describe the conditions of the core:

Condition of Soil Cores

Rating	Recovered Condition	Disturbance or Remolding	Suitability for Testing
I	Excellent	Negligible	Representative
II	Good	Slight	Representative
III	Fair	Considerable	Use Judgment
IV	Poor	Complete	Equivalent to
		•	Disturbed Samples
v	No recovery	· – .	-

2.3 Soil Description (Column 4)

Soils are classified and described according to their engineering properties and behaviour.

2.3.1 Soil Description System

The following properties are described for a comprehensive soil classification system:

Grain size distribution or plasticity, colour, moisture, sensitivity, structure, foreign materials, and consistency or strength.

The soil in each stratum is described on the test hole logs using the Unified Soil Classification System¹ modified slightly so that an inorganic clay of "medium plasticity" is recognized. Selected adjectives are used to define the actual or estimated percentage range by weight of the various components. The use of the modifying adjectives is similar to a system developed by D.M. Burmister³.

The identification of soil components and fractions is defined by the Modified Unified Soil Classification System which classifies soils into three major divisions:

Coarse-grained soils - gravel and sand Fine-grained soils - silt and clay Highly organic soils - peat

Classification of soils is based on the grain size distribution of that portion of the soil smaller than the 3-inch U.S. Standard sieve size.

Soils with more than half by weight of the components coarser than the No. 200 U.S. Standard sieve size (0.074 mm) are described as COARSE-GRAINED (or granular) soils. Coarsegrained soils (gravel and sand) are classified by grain size distribution and are subdivided into coarse and fine gravel, and coarse, medium, and fine sand.

Soils with more than half by weight of the components finer than the No. 200 sieve size are described as FINE-GRAINED soils. These may be cohesive or non-cohesive. Note that for visual classification the No. 200 sieve size is about the smallest size of particle that can be distinguished individually by the unaided eye.

Fine-grained soils (silt and clay) are classified by behaviour on the basis of the liquid limit and plasticity index of the fraction finer than the No. 40 U.S. Standard sieve size. The boundaries defining the fine-grained soil groups are shown in the Plasticity Chart in Table 1 "Soil Classification System". The Plasticity Chart is also used to determine the behaviour of the fines content of coarse-grained soils.

Particle size and shape are usually described for coarsegrained soils, and plasticity is usually described for finegrained soils. An exception to this rule applies when describing glacial till; then plasticity, particle size, and shape are all included in the description.

The principal component of the fraction of the soil passing the 3-inch U.S. Standard sieve size is shown capitalized on the test hole logs.

The proportions by weight of the minor components are defined according to the following descriptors:

Descriptor	Proportion
"and"	50 to 35 per cent
"some"	35 to 20 per cent
"little"	20 to 10 per cent
"trace"	10 to 1 per cent

The descriptors used must not contradict the classification by the Modified Unified Soil Classification System.

The terms given above are used to define proportions by weight of granular components, but they may also be used to define the proportion of minor components of fine-grained material, according to the subdivisions of the Plasticity Chart, Table 1 "Soil Classification System". The adjectives are not used to subdivide a principal fine-grained component. The modifier "y" or "ey" (e.g., SILT, clayey) is used when the liquid limit and plasticity index plot close to the "A-line" on the Plasticity Chart.

Peat and other highly organic soils are classified under the Group Symbol "Pt". Peat may be categorized and described using the Radforth Classification System⁴.

The soil is described first by identifying the principal component, followed by the minor components in order of decreasing proportion by weight. This is followed by other significant identifying features such as plasticity, colour, moisture, structure, and strength.

2.3.2 Typical Example of a Complete Soil Description

"CLAY, silty, little medium sand, trace coarse gravel, medium plasticity, yellow-brown", describes a yellow-brown, finegrained, silty clay soil containing 50 per cent or more of components finer than the No. 200 U.S. Standard sieve size with minor components of sand and gravel. The fraction passing the No. 40 U.S. Standard sieve size plots above, and close to the "A-line" on the Plasticity Chart. The soil contains between 10 per cent and 20 per cent of sand particles generally in the size range No. 10 to No. 40 (i.e. finer than the No. 10 Standard sieve size and larger than the No. 40 Standard sieve size) and between 1 per cent and 10 per cent of gravel in the size range 3/4-inch to 3-inch. The identifying feature "medium plasticity" indicates that the liquid limit plots between 30 and 50 on the Plasticity Chart. Such a soil is classified as CI by the Modified Unified Soil Classification System.

2.3.3 Typical Examples of the Use of Modifiers and Descriptors

(a) Fine-grained soil with a minor coarse-grained component:

"CLAY, silty, some fine sand", describes a fine-grained soil having a fines content in excess of 50 per cent (i.e., 50% of material finer than the No. 200 U.S. Standard sieve size), which plots above the "A-line", on the Plasticity Chart, with a liquid limit less than 50 on the Plasticity Chart, and has a minor component of fine sand.

"CLAY, <u>some</u> silt, some fine sand", would not be used as the fines are classified by behaviour (plasticity) and not by particle size. Such a soil would be classified as CI or CL according to the Unified Soil Classification System.

(b) Coarse-grained soil with minor fine-grained component:

"GRAVEL, fine, some silty clay", describes a coarsegrained soil with a minor component of fines, which has a liquid limit and plasticity index that plot above and close to the "A-line" on the Plasticity Chart. Such a soil is classified as GC by the Unified Soil Classification System.

"SAND, some silt", is correct in that "silt" in this case is a minor component of non-plastic fines which plot below the A-line on the Plasticity Chart.

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2.3.4 Glacial Till

The term "glacial till" is in widespread use in present engineering practice, however, because it is a mode of deposition, there is no provision in the Unified Soil Classification System for this term.

The term "till" is used on the test hole logs in its most general form, which has been defined by ASTM Designation D 653 as:

"A material deposited by glaciation, usually composed of a wide range of particle sizes, which has not been subjected to the sorting action of water."⁵

Glacial till is described on the test hole logs as "TILL", followed by the principal soil component also capitalized.

Example: "TILL, CLAY, silty, little fine gravel, low plastic, rust-brown--".

A loose, soft, or slightly stratified deposit believed to be transported or reworked material of glacial deposition, or of uncertain glacial origin, is described as "till-like" at the end of the soil description.

Example: "CLAY, silty, little fine gravel, low plastic, rust-brown, till-like."

2.3.5 Fill

"Fill" is material placed by artificial means, whether or not its placement was controlled.

It is described on the test hole logs as "FILL", followed by the principal soil component also capitalized.

Example: "FILL, SILT, clayey, some fine gravel".

Well-compacted fill, placed some considerable time before the test hole investigation, may be difficult to distinguish from natural material unless the history of the site is known. Such material is indicated as "FILL?" on the test hole logs.

2.4 NRC Ice Type and Estimated Visual Ice (Column 6)

Ground ice is divided by the NRC system on the basis of examination by the unaided eye into the three major categories shown below. A complete description of this system is contained in the NRC "Guide to a Field Description of Permafrost for Engineering Purposes".²

2.4.1 Ground Ice Classification Categories

Non-visible ice	N
Visible ice less than one inch thick	v
Visible ice greater than one inch thick	ICE or ICE + soil type

Table 2, "Ground Ice Classification", shows the various types of ground ice recognized by the NRC Classification System. Graphic symbols for ground ice have been devised to complement the graphic soil log.

Frozen soils in the N group may, on close examination, indicate presence of ice within the voids of the material by crystalline reflections or by a sheen on fractured or trimmed surfaces. The impression received by the unaided eye, however, is that the ice does not occupy space in excess of the original voids in the soil. Excess ice in the N group can be identified by use of a hand magnifying lens, or by placing some frozen soil in a small jar, allowing it to melt and observing the supernatant water. To the unaided eye, ice in frozen soils in the V group appears to occupy space in excess of the original voids in the soils. The volume of ground ice can be described quantitatively in two ways. "Excess ice" is the volume of supernatant water expressed as a percentage of the total volume of the thawed soil and water. This quantity is often referred to as "excess moisture". "Visual ice" is the estimated volume of segregated ice discernible by eye in the frozen sample and is expressed as a percentage of the total volume of the frozen soil. By these definitions the quantity "excess ice" and "visual ice" are not necessarily the same for a given frozen soil. Care is taken when estimating the volume of ice coatings on granular material (Vc). The ice is usually obvious, giving the impression of "excess ice", which may not necessarily be the case.

2.4.2 Ice Description Terminology

The following terminology used in Column 4 "Description" has been generally taken from Table II of the NRC Guide².

"Ice Coatings on Particles" are discernible layers of ice found on or below the larger soil particles in a frozen soil mass. They are associated sometimes with hoarfrost crystals that have grown into voids produced by the freezing action.

"Ice Crystal" is a very small individual ice particle visible in the face of a soil mass. Crystals may be present alone or in combination with other ice formations.

"Clear Ice" is transparent and contains only a moderate number of air bubbles.

"Cloudy Ice" is relatively opaque due to entrained air bubbles or other reasons, but is essentially sound and non-pervious.

"Porous Ice" contains numerous voids, usually interconnected, and generally results from melting at air bubbles or along crystal interfaces, from presence of salt or other materials in the water, or from the freezing of saturated snow; though porous, the mass retains its structural unity.

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"Candled Ice" is ice that has rotted or otherwise formed into long columnar crystals very loosely bonded together.

"Granular Ice" is composed of coarse, more or less equidimensional ice crystals weakly bonded together.

"Ice Lenses" are lenticular ice formations in soil occurring essentially parallel to each other, generally normal to the direction of heat loss and commonly in repeated layers.

"Ice Segregation" is the growth of ice as distinct lenses, layers, veins, and masses in soils, commonly but not always oriented normally to direction of heat loss.

"Well-bonded" signifies that the soil particles are strongly held together by the ice and that the frozen soil possesses relatively high resistance to chipping or breaking.

"Poorly-bonded" signifies that the soil particles are weakly held together by the ice that the frozen soil possesses poor resistance to chipping or breaking.

"Friable" denotes extremely weak bonds between soil particles. The material is easily broken up.

The symbols "UF" or "F" may be used in Column 6. "UF" is added to indicate unfrozen zones in areas of generally frozen ground and also to avoid possible errors of omission. "F" is used in certain cases along with the corresponding graphic representation for "Undifferentiated" permafrost or frozen active layer soils. It may be used:

(1) Where temperature sensors (thermistors) have been installed which indicate that the formation temperature is below 0° C, but the material in the field has the texture of unfrozen material.

- (2) Where temperature sensors have not been installed, but the soil temperature is suspected to be below 0°C. The soil is deformable because of the high unfrozen water content, but is neither "friable" nor "bonded".
- (3) Where the soil is known to be frozen, but due to circumstances beyond field control, the ice type cannot be determined because of grinding or temporary thawing of the material by the drilling operation.
- (4) Where, for reasons of economy or expediency, the hole was neither logged nor sampled, e.g., where instrumentation is installed adjacent to a previous test hole and soil stratigraphy is known to an acceptable degree.

2.5 <u>Test Data Summary</u>

(a) <u>Test Data (Column 7)</u>

The results of laboratory determinations of water content, together with Atterberg limits, and density (unit weight) are plotted symbolically against depth in this column.

Water content is determined in accordance with ASTM Designation D 2216, "Standard Method of Laboratory Determination of Moisture Content of Soil"⁵. The water content of highly organic material is determined by similar procedure, except that the material is oven-dried to constant weight at 85° C instead of $105^{\circ}c^{6}$.

Liquid limit and plastic limit are determined in accordance with ASTM Designations D 423 and D 424, respectively 5 .

In situ density is determined from the weights and volumes of intact samples and is reported as either "dry density" which is the weight of soil solids per unit volume, or as "bulk density" which is the total weight per unit volume.

(b) Other Test Data (Column 8)

Tests and test data other than, or additional to, those shown in Column 7 are indicated in Column 8.

The more common engineering tests are denoted using the following symbols:

D ₁₀	grain size at 10% passing
D ₃₀	grain size at 30% passing
D ₆₀	grain size at 60% passing
С	consolidation
Cc	coefficient of curvature $(D_{30})^2/D_{10} \times D_{60}$
Cu	coefficient of uniformity D ₆₀ /D ₁₀
Gs	specific gravity of soil solids
н	hydrometer analysis
k	permeability
MA	mechanical analysis (sieve analysis)
N	the penetration resistance, i.e., the number of blows required for the second and third 6-inches of penetration during a Standard Penetration Test (SPT) in accordance with ASTM Designation D 1586 (see also SPT)
NP	non-plastic
OC	organic content
рр	pocket penetrometer
P200	per cent passing the No. 200 sieve size
Q	triaxial test
q	unconfined compressive strength
S	shear test
so ₄	water soluble sulphate
SPT	standard penetration test (blow counts for 6-inches, 12-inches, 18-inches penetration are shown sequentially)
TC	thaw consolidation
Ŵ	water content
W_{L}, W_{P}, I_{P}	liquid limit, plastic limit, and plasticity index, respectively

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3. Classification of Construction Materials

3.1 Granular Material Uses

The following is a description of materials that was used within the "Materials" and "Development and Rehabilitation" sections of Individual Site Reports. Material classification has been based on the potential construction usage of the granular material for each deposit.

- Excellent quality material consisting of well-graded, medium-grained gravel suitable for concrete aggregate, with a minimum of processing.
- (2) Good-quality material consisting generally of fine to medium-grained well-graded sandy gravel with varying quantities of silt occurring either as narrow interbeds or dispersed throughout the material. The frequent occurence of deleterious materials such as weathered stones or shale fragments negates its use as concrete aggregate. This material will provide good quality embankment fill for pipeline berms and building pads; base and surface course aggregates; or possible production of concrete aggregate with extensive processing.
- (3) Fair quality material consisting generally of poorly graded, silty, gravelly sand. This material will provide fair quality general fill.
- (4) Poor quality material consisting generally of finegrained, poorly graded sandy silt with minor gravel.
 These deposits usually contain minimal quantities of sand and gravel, are very thin, or are overlain by extensive

thicknesses of overburden. Fine-grained dune sand is included in this category. These materials are considered unsuitable for construction except as marginal fill.

- (5) Bedrock consisting of:
 - (a) Limestone and dolomite which would be suitable for manufacturing various types of construction aggregates.
 - (b) Shale and siltstone with small varying quantities of limestone and dolomite which could be exploited only for fair quality general fill useful primarily in the construction of sub-grades. This category also includes talus slopes containing a mixture of limestone, dolomite and shale blocks and fragments.

Soil Drainage Classes

4.1 Drainage

The Soil Drainage Classes were used in describing the drainage of each deposit that was looked at. The following set of definitions was used to determine the drainage of each site.

The following is extracted from pages 215 and 216 of National Soil Survey Committee, 1970 "The System of Soil Classification for Canada", Canada Department of Agriculture, Ottawa. The system, although devised primarily for agricultural purposes is suitable for engineering purposes and should be employed when describing soil drainage at test hole site locations. The soil drainage classes are defined in terms of:

- (i) actual moisture in excess of field moisture capacity, and
- (ii) the extent of the period during which such excess water is present in the plant-root zone.

Permeability, groundwater levels and seepage affect the moisture status but these are not easily observed in the field and therefore cannot generally be used as criteria for moisture status. The recommended definitions are as follows:

- Rapidly drained The soil moisture content seldom exceeds field capacity in any horizon except immediately after water conditions
- (2) Well drained The soil moisture content does not normally exceed field capacity in any horizon for a significant part of the year. ("significant" - as used in the definitions is considered in relation to plant growth)
- (3) Moderately well drained The soil moisture in excess of field capacity remains for a small but significant period of the year
- (4) Imperfectly drained The soil moisture in excess of field capacity remains in subsurface horizons for moderately long periods during the year
- (5) Poorly drained The soil moisture in excess of field capacity remains in all horizons for a large part of the year
- (6) Very poorly drained Free water remains at or within 12 inches of the surface most of the year

Identification - commonly found morphological features associated with a particular drainage class.

Drainage Class

- (1) free of any evidence of gleying (grey color, reducing conditions) coarse texture steep slopes
- (2) free of mottling in upper 3 feet may be mottled below 3 feet
- (3) commonly mottled in the B and C horizons or below a depth of 2 feet
- (4) commonly mottled in the B and C horizons, matrix generally has lower chroma than in the welldrained soil on similar parent material
- (5) usually strongly gleyed matrix colors of low chroma, faint mottling may occur through out
- usually strongly gleyed,
 subsurface horizons are of low chroma and yellowish to
 blueish hues,
 mottling may be present at depth in the profile

Note:

"Gley" - a soil usually grey or blueish in color, generally oxygen-deficient i.e. reducing conditions prevail. Low chroma are associated with ions of lower valency eg. ferrous iron, Fe⁺⁺, (Fe⁺⁺⁺ is associated with rusty deeper colors)

Just above the zone of contact with excess field moisture and groundwater the soil may be "mottled". This is associated with a fluctuating oxidising and reducing conditions. The soil often appears to have patchy reddish zones or concretions within a blueish grey matrix. -Northern Engineering Services

5.1 Slopes

The topography of each deposit was described using the following table of terms in the Individual Site Reports.

Topography is described in the following terms:

Single Slopes	Complex Slopes	Slope %	Slope °
flat	flat depressional	0 - 2	0 - 1
gently sloping	undulating, smoothly rounded	2 - 5	1 - 3
moderately sloping	rolling ridgy, choppy	5 - 15	3 - 8
steeply sloping	kettled, knobby	15 - 60	8 - 31
precipitous	precipitous	> 60	> 31

"Region" is general area around the site location and is generally within 1500' of the test hole(s).

"Site" refers to the area within 100' of the test hole(s).

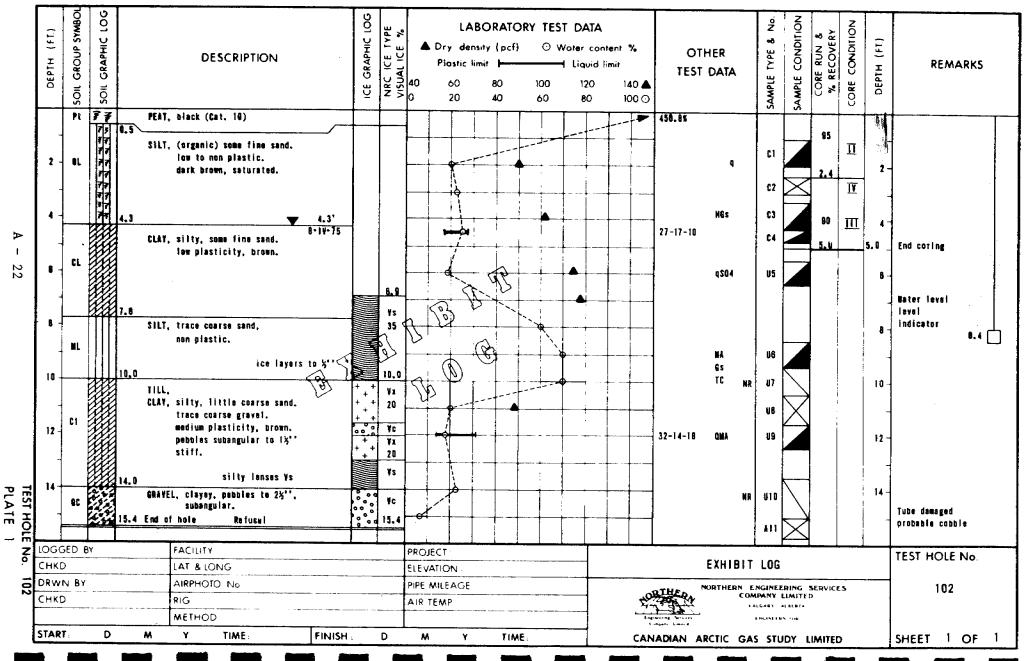
The degree of slope should be measured whenever possible by handlevel or inclinometer even if the site is to be surveyed accurately at a later date.

Northern Engineering Services -

REFERENCES:

- "Unified Soil Classification System" Technical Memorandum 3-357 prepared for Office, Chief of Engineering, by Waterways Experiment Station, Vicksburg, Mississippi, Corps of Engineers, U.S. Army. Volume I, March 1953.
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TEST HOLE LOG



SAMPLE CONDITION SOIL GRAPHIC LOG SOIL GROUP SYMBOL ICE GRAPHIC LOG ź CORE CONDITION NRC ICE TYPE VISUAL ICE % LABORATORY TEST DATA CORE RUN & % RECOVERY DEPTH (FT.) SAMPLE TYPE & DEPTH (FT.) 🔺 Dry density (pcf) 👘 🔿 Water content 🐐 OTHER DESCRIPTION REMARKS Plastic limit ⊣ —— Liquid limit TEST DATA 100 120 140 📥 80 60 20 40 60 80 100 🖸 Ν 8 910111213 (14) Т 56 7 $2\overline{3}$ (4) 23 **TEST HOLE** TEST HOLE No. PROJECT Z o LOGGED BY FACILITY ELEVATION : CHKD LAT. & LONG NORTHERN ENGINEERING SERVICES PIPE MILEAGE DRWN BY: AIRPHOTO No COMPANY LIMITED CHKD RIG : AIR TEMP LALGARY ALBERTA ENGINEERS FOR METHOD i mard SHEET OF FINISH : D м Y TIME CANADIAN ARCTIC GAS STUDY LIMITED START: Ð M Y TIME:

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TEST HOLE LOG

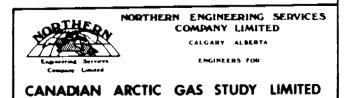
				-	CLASSIFICATION SYSTEM			
	MAJOR	0 I V I S I ON	GROUP Symbol	GRAPHIC Symbol	TYPICAL MATERIALS	LABORATOF CLASSIFICAT CRITERIA		
SIEVE)	NNARSE	CLEAN GRAVELS	GW		L GRADED GRAVELS, AND GRAVEL - SAND MIXT TLE OR NO FINES	URES. $C_{u} = \frac{0.60}{0.10} > 4$ $C_{c} = \frac{(0.30)^2}{0.10} \times \frac{1}{2}$	1 to 3	
200 51	LF DF C	(NO APPRECIABLE FINES)	GP		RLY GRADED GRAVELS, AND GRAVEL SAND MI ES. LITTLE OR NO FINES		G	
SCILS R THAN NO	GRAVELS GRAVELS More Than Half of Coarse Fraction Larger Than No 4 Sieve	DIRTY GRAVELS	GM		TY GRAVELS, GRAVEL - SAND - SELT WIXTURE			
	GRAV KORE NORE NO	(WITH FINES)	GC	6 8 9 0 6 8 9 8 6 6 8 9 8 6 7 10 10	YEY GRAVELS, GRAVEL SAND - (SILT) CLAY TURES			
	F COARSE Than	CLEAN SANDS	SW		GRADED SANDS, GRAVELLY SANDS LITTLE D	R $C_{U} \cdot \frac{D_{60}}{D_{10}} > 6 C_{c} = \frac{(D_{30})^{2}}{C_{10}}$		
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ND 200	SILTS BELOW - A - NEGLICIBLE ORGANIC CONTENT	w _L > 50	MH		DRGANIC SILTS, MICACEOUS OR DIATOMACEOUS, FINE IDY, OR SILTY SOILS			
SOLLS	LINE ON CCHART CRGANIC	₩ _L < 30	CL		GANIC CLAYS OF LOW PLASTICITY, GRAVELLY Y, OR SILTY CLAYS, LEAN CLAYS	CLASSIFICATIO ACCORDING		
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FINE Half By		W _L > 50	Сн		GANIC CLAYS OF HIGH PLASTICITY, FAT CLAY			
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SILT	(non plastic) (plastic)	No 200	10	l trac	2. BOUNDARY CLASSIFICATIONS POSSESSIN GIVEN COMBINED GROUP SYMBOLS. & g MIXTURE WITH CLAY BINDER BETWEEN S 3. TOUGHNESS AND DRY STRENGTH INCREAS WHEN COMPARING SOILS AT EQUAL LIQU	G CHARACTERISTICS OF TWO GRI GW-GC IS A WELL-GRADED GRA AND 12% E WITH INCREASING PLASTICITY	DUPS ARE VEL SAND	
		OVERSIZE MATERI	L		NORTHEAN ENG	INEERING SERVICES	TABLE	
COBBL	ed or subround ES 3 inch to	8 inch ROCK	FRAGMENTS	> 3 inch : yard in vol	TALEA CALEA		1	
OVULU	ERS > 8 incl				A - 24		1	

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TABLE 2

GROUND ICE CLASSIFICATION

<u></u>				
Category	Group Symbol	Subgroup Symbol	Graphic Symbol	Description
		F		Undifferentiated
		Nf		Poorly bonded or friable frozen soil
Non-visible Ice	N	Nbn		Well bonded frozen soil with no excess ice
		Nbe		Well bonded frozen soil with excess ice. Free water present when sampl thawed
Visible Ice		٧x	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Individual ice crystals or inclusions
less than one inch thick	v	Vc		lce coatings on particle
		۷r		Random or irregularly oriented ice formations
		٧s		Stratified or distinctly oriented ice formations
Visible Ice greater than		ICE + soil type		lce greater than one inch thick with soil inclusions
one inch thick	ICE	ICE		lce greater than one inch thick without soil inclusions



Adapted from NRC 7576

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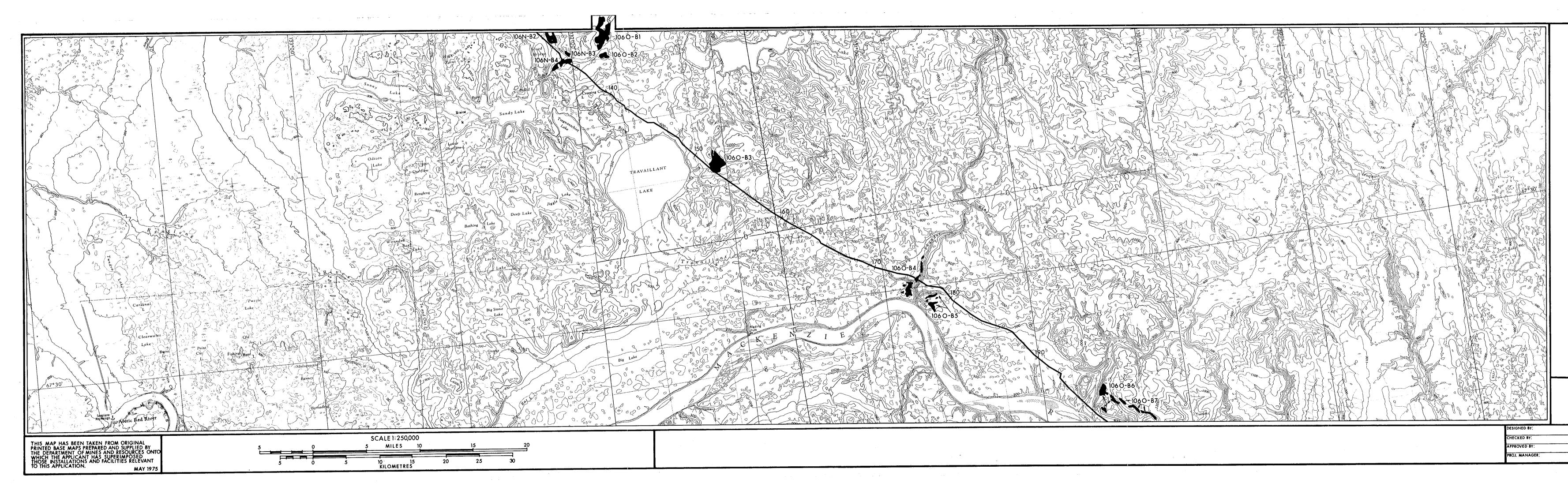
7

APPENDIX B

Location Maps

of

1975 Summer Borrow Investigations



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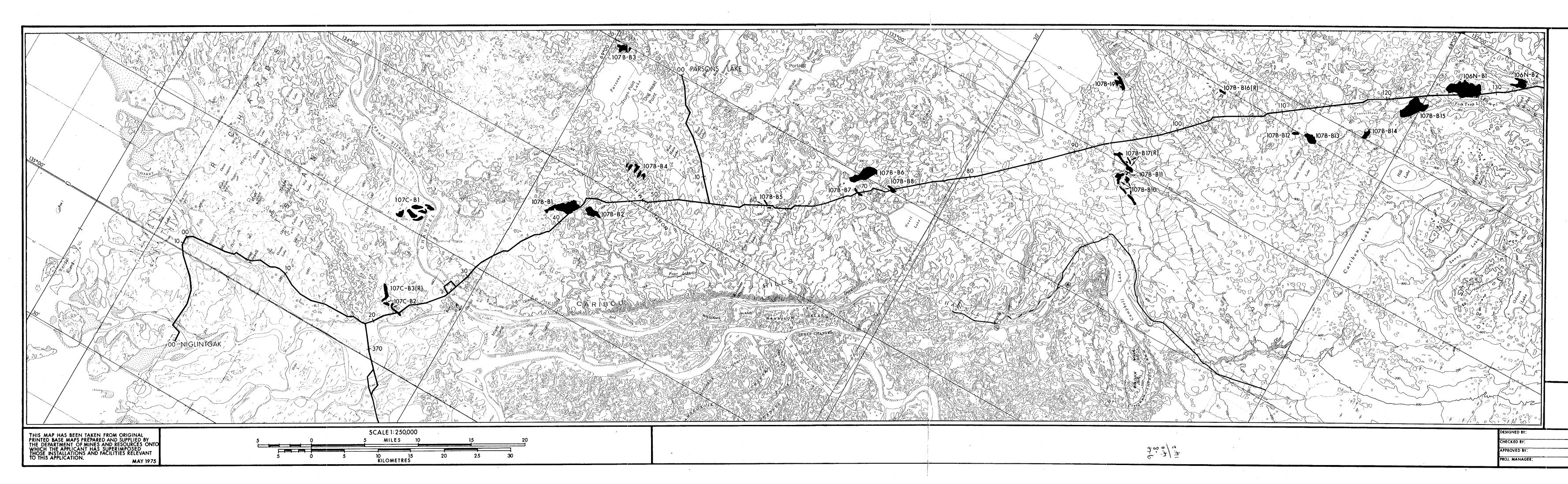
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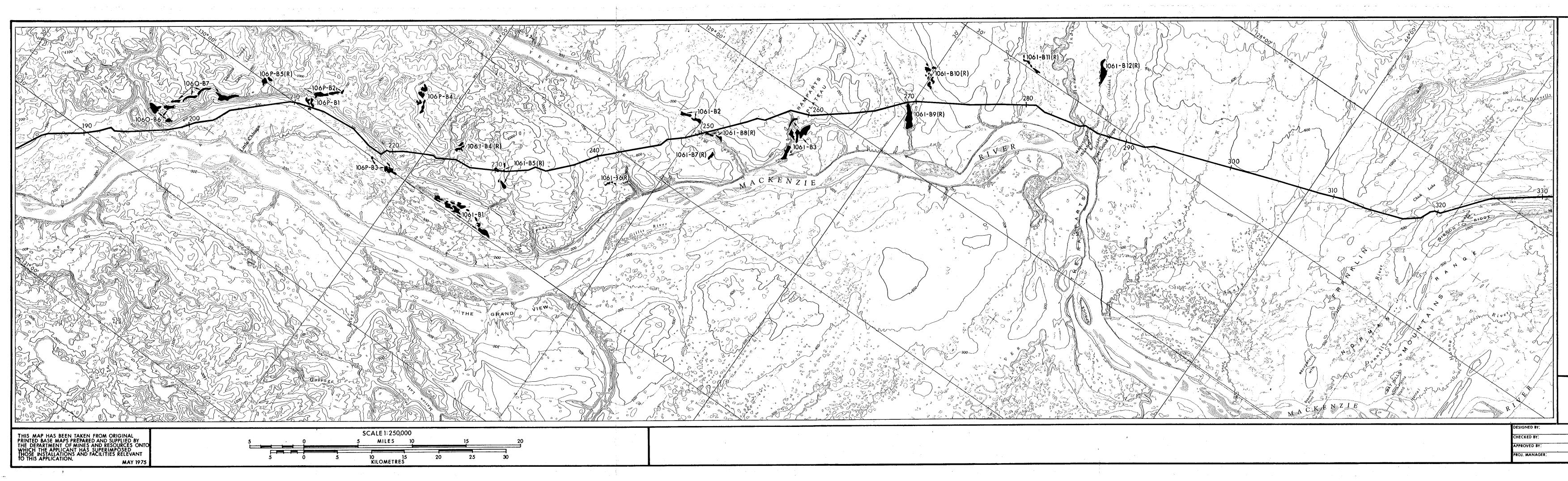
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DEPOSIT OUTLINE NESCL DEPOSIT NUMBER RECONNAISSANCE SITE - SOME DETAILED WORK DONE BY NESCL PROPOSED GAS PIPELINE ROUTE (MARCH 1976) WITH MILE POST.

LOCATION MAPS 1975 SUMMER BORROW INVESTIGATION

NORTHERN ENGINEERING SERVICES	REVISED	
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CANADIAN ARCTIC GAS STUDY LIMITED	DWG. NO.: 1B-0211-1006	

APPENDIX C

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Resistivity Measurement with Inductive Coupling Equipment

at

Several Gravel Pits in the Calgary Area

APPENDIX C - Resistivity Measurements with Inductive Coupling Equipment at Several Gravel Pits in the Calgary Area

1. Introduction

Borrow material is required for construction of the proposed gas pipeline and associated facilities. Sources of borrow material have been identified by photo methods and some of the deposits have been probed by drilling and conventional geophysical methods.

In general the conventional geophysical measurements have added little information about the nature, depth or extent of the deposits. For geophysical measurements to be of value in reconnaissance exploration for granular material deposits a rapid method of resistivity mapping is required that can quickly scan the deposit and the surrounding areas. Also, the depth of exploration in most instances should be limited to 20-30 ft.

A dipole-dipole system was designed for shallow exploration, but was not available in time for the 1975 borrow program along the pipeline route. In December, the instrument was tested at several active gravel pits in the Calgary area. This appendix gives the results of these tests.

2.

The Inductive Coupling System

Soil types can often be distinguished by their electrical resistivity. The resistivity ranges encountered for certain soil types vary from area to area, but invariably gravel deposits are found to have higher resistivities than glacial tills or lacustrian deposits. Sands and gravels can often not be separated on the basis of electrical resistivity.

To establish the relation between soil types and resistivity, in a region, requires substantial amounts of data. The recent development of non-contact methods has made it possible to acquire area coverage and large amounts of data at a low cost. The method that appears particularly attractive measures the mutual coupling between two loop antennas carried above the ground.

In the inductive coupling system two small antenna loops (magnetic dipoles) are separated by a fixed distance. In the instrument, shown in Figure 1, the loops are in the horizontal plane and the separation distance between the loops is 3.6 m. One dipole transmits electromagnetic waves at a frequency of 39 kilohertz. The transmitted waves induce current flow in the ground; the magnetic field of that current flow is measured by the receiving dipole. The received signal can be related to the resistivity of the ground.

The instrument is light weight (15 lbs.) and is carried by a shoulder strap approximately 0.8 m above the ground. No contact with the ground is required for a measurement, so that readings can be taken continuously along a traverse.

The frequency and separation of the system are chosen so that the depth of exploration depends mainly on the separation distance of the dipoles. The depth of exploration on gravel

deposits is approximately $2\frac{1}{2}$ times the separation distance or about 9 m (30 ft). Similar instruments with larger depth of exploration are also available.

Over ground uniform with depth the instrument would measure the true resistivity of the ground. Over layered ground the resistivity measured is influenced by the resistivities of all the layers within the depth of exploration. Computer models are required to derive the layered structure from the measurements.

Results

3.

Five gravel deposits were investigated in the Calgary area. In all these <u>pits</u> traverses were made:

- (1) right above the face of the cut (on the gravel),
- (2) in the bottom of the pit, where presumably most gravel was excavated, and
- (3) when possible, at locations near the pit, outside the gravel deposit.

Table I lists the gravel pits and the range of apparent resistivities observed in each of the three categories listed above. The conclusion that can be drawn from Table I is that in Pit 1, 2, 4 and 5, the difference in resistivity between gravel and surrounding material is at least a factor 2. The gravel in Pit #3 contained a large amount of fines.

In order to calculate the depth of gravel from resistivity data, one would in general make, for a specific site, a few independent measurements of resistivity with other methods. Since this was not done, the calibration curve (shown in Figure 2) relating the apparent resistivity to depth of gravel is tentative. Normally, one would make a separate calibration curve for each pit. There are also other factors that could obscure the simple picture shown in Figure 2, such as substantial changes in the quality of gravel with depth. Nevertheless, for illustrating the use of geophysics in this appendix this curve is used for all five pits.

Next, the results of measurements at each quarry are discussed:

No. 1, Standard General, Ogden Pit, North Wall

Figure 3 shows a layout of some of the traverses made near the North Wall of the pit, and Figure 4 and 5 show resistivity profiles along the traverses. The resistivity profile along line 4 has been interpreted in terms of depth of gravel with the aid of Figure 2; the data show that the granular deposit terminates at the northeast corner of the property indicated by a rapid decrease in resistivity. The gravel is more extensive on the western side (line 6), since the resistivity remains high on line 6. Also on line 5 (Figure 5) the resistivity can be seen to increase gradually towards the west. From Figure 2 one estimates the gravel deposit to be more than 10 m (30 ft) thick on line 6; and, as shown on Figure 4 for example less than 2 m (6 ft) at station 400 on line 4.

These data clearly show the advantage of continuous resistivity readings. Boundaries can be delineated and drill holes can be planned at selected points, and the information can be extrapolated between the holes.

No. 2, Standard General, Ogden Pits, East Wall

Figure 6 shows the layout of some of the traverses near the East Wall of the Standard General, Ogden Pit. Of interest are the resistivity profiles perpendicular to the pit face (10, 11, 12) shown in Figure 7. These lines clearly show a decreasing resistivity towards the hill, indicating that the gravel deposit terminates near the base of the hill as is shown by the interpretation in Figure 7. Figure 8 shows the profiles of some of the lines parallel to the face of the cut. These lines also show the substantial difference in resistivity between gravel (line 7), and surrounding material (line 9). Figure 2 can be used to relate the decrease in resistivity to depth of gravel.

No. 3, Burnco, Ogden Pit

Figure 9 shows the layout of some of the lines at the Burnco, Ogden Pit. The values of the resistivities along these lines are listed in Talbe II. The resistivities measured above the face of the cut are the lowest found in the gravel pits investigated in the Calgary area. From Figure 2 one would estimate less than 4 m (l2 ft) of gravel. However, this gravel had a high content of fines, and probably needs a separate calibration curve.

The ground water table in the bottom of the pit was within a few feet from the surface.

No. 4, Burnco, Canyon Meadows

Short lines were measured on top of the faces of the Burnco, Canyon Meadows Pit. The layout of the lines is shown in Figure 10. The data are listed in Talbe III. The data show resistivities greater than 100 ohm-meters on the lines on top of the pit. At the bottom of the pit most values are less than 100 ohm-meters, although there are apparent substantial pockets of gravel left locally in the bottom of the pit. The depth of gravel on top of the cut faces is estimated from Figure 2 to be about 20 feet on line 2, and more than 30 feet on line 3.

No. 5, Consolidated Concrete, Bearspaw Pit

Several traverses were run on the Bearspaw Pit. The approximate layout of the lines is shown in Figure 11.

The data on the line at the North South Road Allowance is listed in Talbe IV. The resistivity values found along this traverse were the highest found on gravel deposits in the Calgary area. These resistivities are indicative of thick high quality gravel.

The location of the lines run near the fence of the property from the South East Corner are shown in Figure 11. The resistivity profiles for line 1 and line 6 are given in Figure 12. The data show a rapid decrease in resistivity at station 400 of both lines; this decrease is no doubt due to thinning of the gravel beds.

Table V lists the values measured along the lines of the top and the bottom of the Bearspaw Pit, East-West Section. 4.

Conclusion

The resistivity data obtained on the gravel pits in the Calgary area showed that gravel deposits can be delineated from the surrounding materials by non-contact inductive coupling methods. The depth of gravel can be estimated from computer model curves, but independent measurements of the resistivity of gravel would be necessary to arrive at an acceptable accuracy. —Northern Engineering Services –

TABLE I Range of Apparent Resistivities in ohm-meters Measured On and Off Gravel Deposits In Active Quarries in the Calgary Area

No.	Quarry Name	On Gravel, Above Face of Cut	At Bottom of Pit	Out of Gravel in Surrounding Material
1	Standard General, Ogden Pit North Wall	140-160	30-70	20-50
2	Standard General, Ogden Pit East Wall	140-160	20-50	20-50
3	Burnco, Ogden Pit South Gravel Base	60-80	20-30	60-80
4	Burnco, Canyon Meadows	110-160	-	50-30
5	Consolidated Concrete Bearspaw	130-250	90-50	50-70

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TABLE II

Apparent Resistivities Measured Along the Top And Bottom of Burnco, Ogden Pit. The Approximate Locations of the Line are Shown in Figure 8

Station, meters	Top of Line	Pit 1	Apparent Resistivity ohm-meters
0			80
25			-
50			-
75			70
100			70
125			65
150			70
175			80
200			80
225			80
250			80
275			60
300			55
325			60
350			65
375			70
400			6.5
425			85
450			70
475			70
500			65
525			70
550			65
575			65
600			80

Table	II,	continued
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Station, meters	Line 3 Top of Pit	Apparent Resistivity ohm-meters
0		80
25		75
50		55
75		65
100		60
125		60
150		60
175		55
200		50
225		55
250		65
275		70
300		60
325		55
350		50
375		55
400		60
425		65
450		70
475		70
500		65
525		70
550		80
575		65
600		70

Station, meters	Bottom of Pit Line 4	Apparent Resistivity ohm-meters
0		25
25		20
50		20
75		20
100		25
125		25
150		20
175		20
200		20
225		20
250		20
275		20
300		25
325		25
350		20
375		20
400		25
425		25
450		25
475		25
500		25
525		25
550		25
575		25
600		25

Table II, continued

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TABLE III

On Top of Pit Walls Line 2 Apparent Resistivity Stations, meters ohm-meters

List of Apparent Resistivities Measured On Survey Lines at Burnco Pit, Canyon Meadows

Line 3

0	15	50
25	15	50
50	15	50
75	15	50
100	15	55
125	15	50
150	14	μO
175	13	35
200	13	35

Table III, continued

Station, meters	Line 4	Apparent Resistivity ohm-meters
· .		
0		115
25		130
50		140
75		160
100		160
125		150
150		150
175		150
200		155
225		150
250		155
275		160
300		160

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Bottom of Pit

Line 5

0	65	ō
25	80)
50	95	5
75	110)
100	110)
125	130)
150	100)
200	95	;
225	65	,

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Station, meters	Line 7	Apparent Resistivity ohm-meters
0		130
25		90
50		70
75		70
100		60
125		65
150		70
175		80
200		85
225		95
250		85
275		65
300		65

Table III, continued

Line 6

0	12	0
25	13	0
50	12	5
75	5	5
100	6	50
125	7	70
150	8	30
175	8	35
200	11	0
225	11	10
250	10)0
275	10	00
300	2	90

TABLE IV

Apparent Resistivities Measured Along a Traverse Near the North-South Road Allowance in the Bearspaw Pit

tation, meters	Apparent Resistivity ohm-meters
0	170
25	220
50	200
75	220
100	240
125	210
150	220
175	250
200	220
225	220
250	250
275	220
300	250
325	200
350	200
375	200
400	200
425	200
450	200
475	200
500	100
525	200
550	220
575	220
600	200
625	190
650	140

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