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TO ESTABLISHING A COMMUNITY GRAVEL BORROW PIT FOR

LOCATION BURWASH LANDING AND DESTRUCTION BAY, YUKON

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**REPORT ON
GEOTECHNICAL STUDY RELATIVE
TO ESTABLISHING A COMMUNITY GRAVEL BORROW PIT FOR
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FEBRUARY, 1983 CG10047**

**Prepared for
DEPARTMENT OF INDIAN AFFAIRS AND NORTHERN
DEVELOPMENT, CANADA
Ottawa, Ontario**

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Calgary, Alberta**

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SUMMARY

A detailed geotechnical investigation of three existing gravel pit reserves along the Alaska Highway (YTG #10981, DIAND #11574 and YTG #10983) was undertaken, to provide information on the basis of which to establish a community borrow pit for the use of Burwash Landing and Destruction Bay, Yukon. It is intended that the chosen pit will satisfy the concrete aggregate and gravel fill requirements of the two communities.

Following a review of existing information, a comprehensive drilling and laboratory testing program was carried out. In all, 45 boreholes were drilled and sampled within the three deposits. Laboratory testing consisted of moisture content determinations and, on selected samples, visual petrographic analysis, sieve analysis, and Los Angeles abrasion and sulphate soundness tests. Borehole logs and laboratory test results are presented.

Principle findings of the study are as follows:

- a) The M.P. 1086.2 site is a low volume deposit of fair to poor quality aggregate. With a 3:1 gravel-overburden stripping ratio, development does not appear warranted unless the overburden is used as fill material.
- b) Reserves for the M.P. 1087.6 deposit are estimated at 22 300 m³ proven and 81 500 m³ probable, of good quality aggregate. This will be suitable for most construction purposes, with crushing and screening required to produce concrete aggregate.
- c) At M.P. 1095.1 proven reserves are 90 000 m³ of good quality aggregate, greater than 200 000 m³ probable. Again though suitable for most purposes, the gravel will require crushing to produce concrete aggregate.



It is concluded that, while additional testing is needed in the southern section (when improved access is available), the borrow reserve at M.P. 1095.1 (YTG #10983) is most suitable for development as a large volume, good quality, gravel pit for the use of the two communities.



1.0 INTRODUCTION

Hardy Associates (1978) Ltd. was retained by the Department of Indian Affairs and Northern Development to carry out necessary geotechnical testing and assessment studies in connection with establishing a community gravel pit for Burwash Landing and Destruction Bay, Yukon. Authorization to proceed with the study was given on November 16, 1982 by Mr. G. N. Faulkner, Assistant Deputy Minister, Northern Affairs. Completed contract documents for the work were returned to Mr. G.Y. Williams, DIAND Contract Services Division, on December 13, 1982.

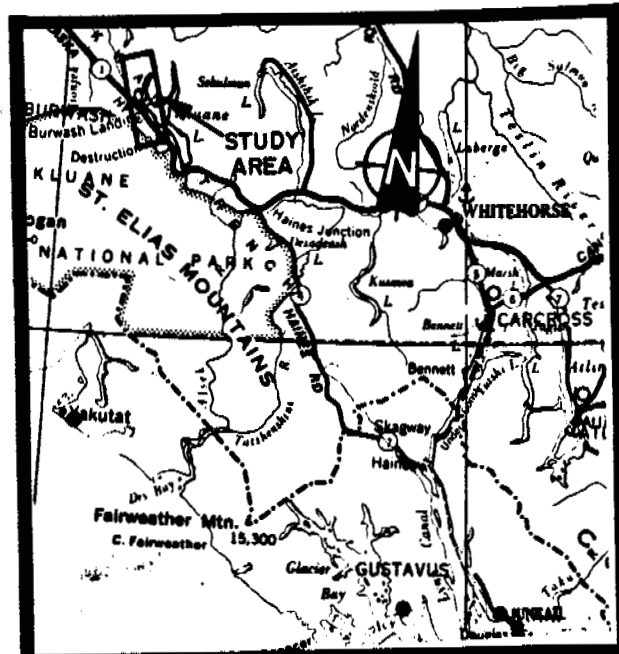
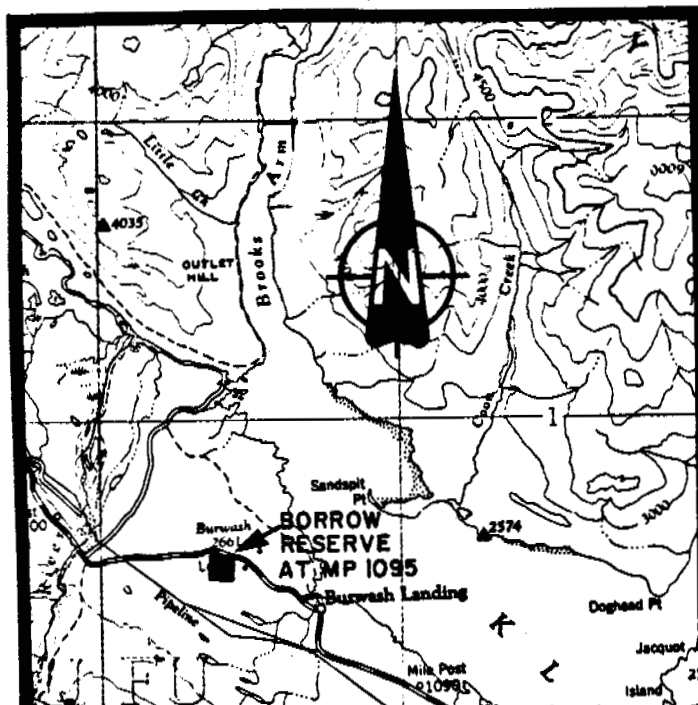
1.1 SCOPE OF STUDY

The prime objective of the study was to evaluate three existing borrow pit reserves, in connection with establishing a community borrow pit for the use of Burwash Landing and Destruction Bay. The chosen pit is to satisfy the demands for concrete aggregate and gravel fill for both communities. The three reserves are located adjacent to the Alaska Highway, between MP's 1086 and 1096 (Figure 1).

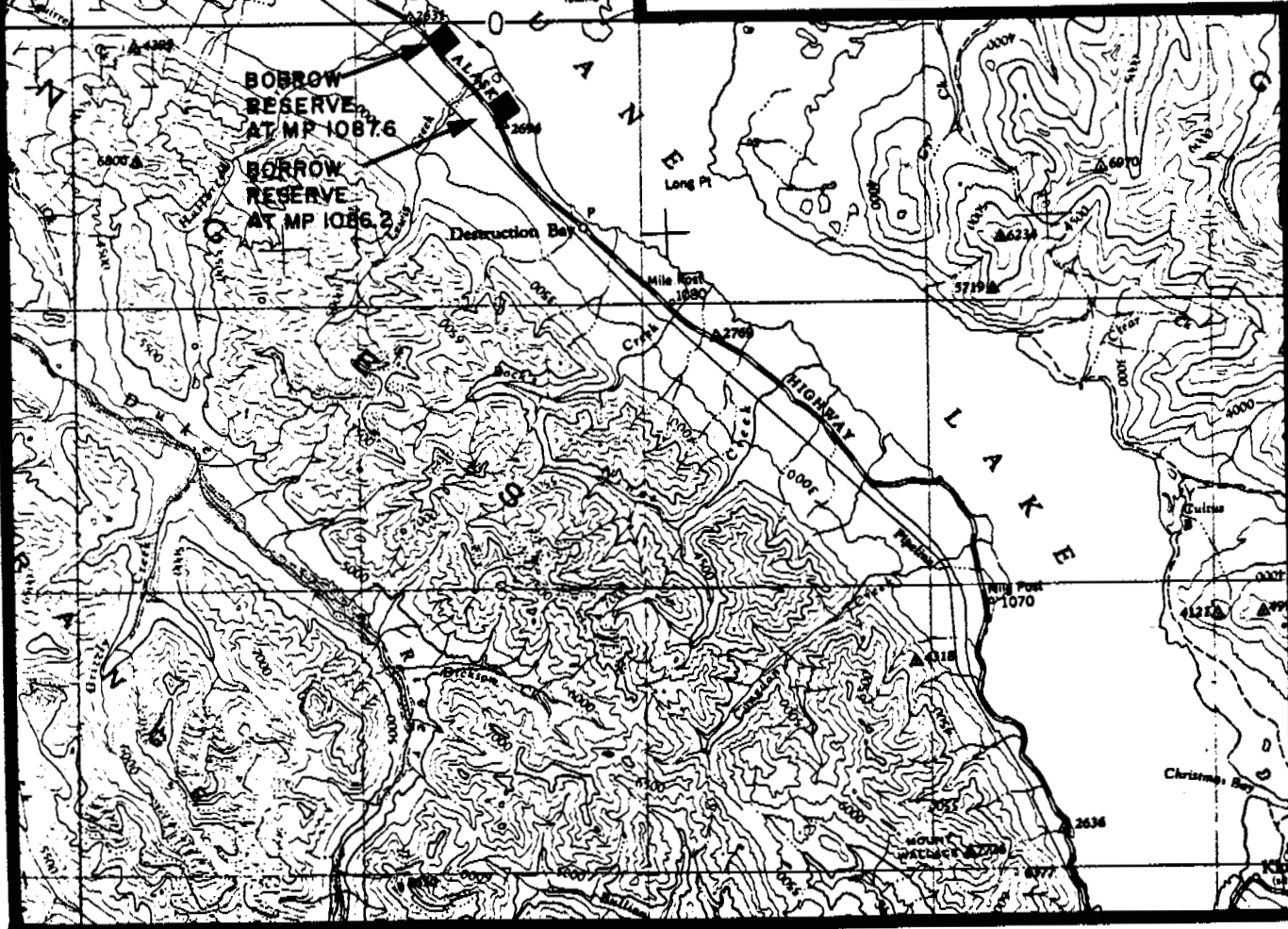
1.2 TERMS OF REFERENCE

Terms of reference for the study, as established in our Contract No. 82-348 with Department of Indian Affairs and Northern Development, were to:

1. Carry out a detailed field drilling program at the following existing borrow pit reserves;



KEY PLAN



SCALE 1:250,000



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LOCATION PLAN

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FIG 1

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- a) YTG Gravel Pit #10981 M.P. 1086.2 (KMP 1737.9)
- b) DIAND Gravel Pit #11574 M.P. 1087.6 (KMP 1740.2)
- c) YTG Gravel Pit #10983 M.P. 1095.1 (KMP 1752.2)

- 2. Conduct testing on representative samples to confirm the quality of the material in each pit and its suitability for various uses.
- 3. Prepare and submit a brief report, discussing the study methodology and presenting its results, providing an assessment of available aggregate volumes and suitability for various community uses, and presenting recommendations for pit development.

2.0 GEOLOGICAL SETTING

2.1 RELIEF AND TOPOGRAPHY

Physiographically, the borrow reserve sites lie in the Shawkwak Trench, along the northeast side of the Kluane Ranges, St. Elias Mountains (Bostock, 1969). The M.P. 1086.2 and 1095.1 sites have undulating topography and slope gently to the north towards Kluane Lake, while the topography of borrow reserve at M.P. 1087.6 is hummocky, with a maximum relief of approximately 8 m to 10 m. Elevations of the three sites range from 821 m above sea level (asl) to 806 m asl (Figure 1).

2.2 BEDROCK GEOLOGY

According to Rampton (1981):

"The eugeosynclinal sequence of the Kluane Ranges and adjacent areas north of the Slims River consists primarily of



argillite, volcanic, and greenstone rocks of Permo-Triassic age."

2.3 SURFICIAL GEOLOGY

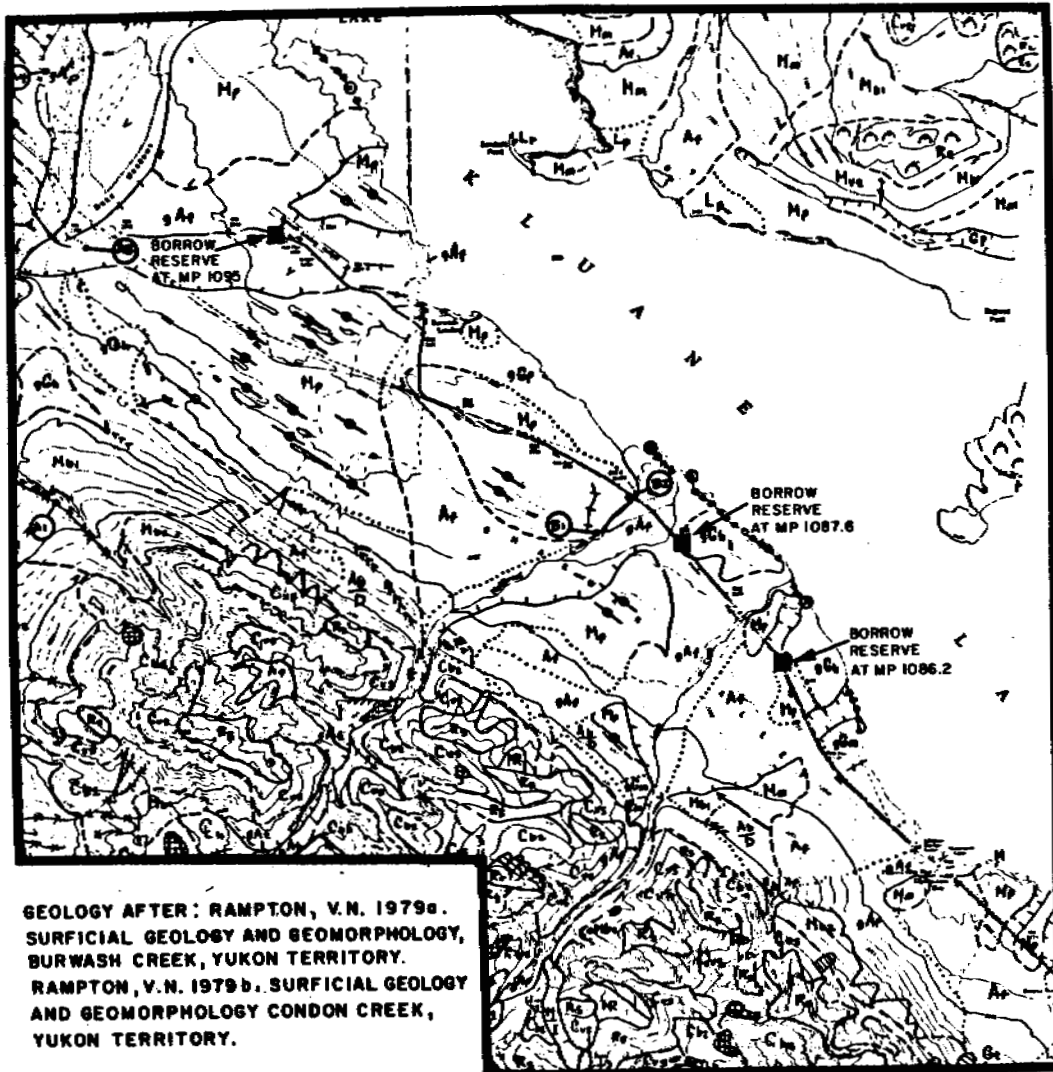
The surficial geology of the Burwash Landing/Destruction Bay area is shown on Figure 2 (after Rampton, 1979a; 1979b).

The Alaska Highway in this area follows the base of the Kluane Ranges, St. Elias Mountains, across a series of large coalescing alluvial fans which overlie glaciofluvial and morainal deposits (Rampton, 1977a; 1979b). As a result, the surficial geology is fairly complex and the three borrow reserves are all located on different surficial deposits. Thus, the borrow reserve at M.P. 1086.2 is located on a late Wisconsinan morainal deposit, which includes patches of glaciofluvial outwash material, the M.P. 1087.6 site is situated on a glaciofluvial kame terrace, and the M.P. 1095.1 site lies on a large alluvial fan of the Duke River (Figure 2).

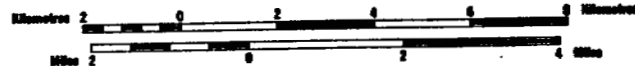
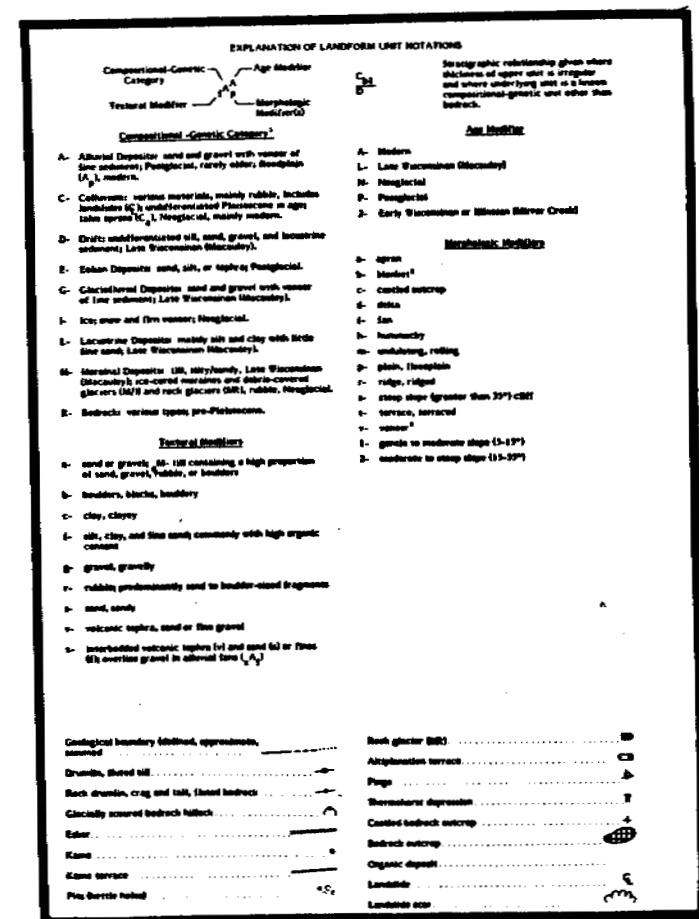
The detailed surficial geology of the borrow sites is shown on Plates C1 to C3 (Appendix "C"), and described in Section 5.0.

2.4 DRAINAGE

The study areas slope towards Kluane Lake and have, for the most part, excellent surface drainage. Local depressional areas, however, are poorly drained and organic-infilled, for example, the extreme north-east corner of the M.P. 1086.2 site and the southern portion of the M.P. 1095.1 site. The poorly-drained organic areas are outlined on the individual site mosaics, in Appendix "C".



GEOLOGY AFTER: RAMPTON, V.N. 1979a.
SURFICIAL GEOLOGY AND GEOMORPHOLOGY,
BURWASH CREEK, YUKON TERRITORY.
RAMPTON, V.N. 1979b. SURFICIAL GEOLOGY
AND GEOMORPHOLOGY CONDON CREEK,
YUKON TERRITORY.



REVISIONS

REFERENCES

SCALE

DATE

MADE

CHKD.

APPD.



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SURFICIAL GEOLOGY

No. CG10047

FIG 5

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2.5 PERMAFROST

The study area lies within the northern section of the discontinuous permafrost zone (Brown, 1967). Permafrost may be expected in all undisturbed areas with high ice content material occurring in the poorly drained areas. Permafrost was not encountered (to the depths drilled) in areas that have been stripped of vegetation. Low ice content permafrost can be expected in the higher, well drained, areas. During the field drilling program, permafrost was present at the M.P. 1095.1 site; no massive ice was encountered.

Expected active layer depths are in the range 0.5 m to 1.5 m, depending on material grain size and vegetation cover. Generally, coarse-grained soils with light vegetation will thaw to greater depths than fine-grained soils with heavy vegetation cover.

3.0 FIELD PROGRAM

A total of 45 boreholes was drilled on the three deposits: 15 boreholes at M.P. 1086.2, 10 holes at M.P. 1087.6 and 20 boreholes at M.P. 1095.1. Drilling was carried out between November 24 and 29, 1982. Borehole locations are shown on the photomosaic site plans (Plates C1 to C3) in Appendix "C".

3.1 METHODOLOGY

The drill rig utilized for this program was a CME 750 auger rig, supplied by Midnight Sun Drilling Ltd. of Whitehorse. Boreholes were augered and sampled under the supervision of a Hardy Associates (1978) Ltd. soil engineer. Except where



conditions prohibited, borings were put down to a maximum depth of 6 m.

Grab samples were taken at a regular interval from each borehole for moisture profile determination and sieve analysis. Bulk samples were obtained at selected sites for more detailed laboratory testing (see Section 4.0).

3.2 RESULTS

Borehole logs are presented, on Plates A1 to A45, in Appendix "A". The test drilling results for each borrow reserve are summarized and evaluated in Section 5.0.

4.0 LABORATORY TEST PROGRAM

Grab and bulk samples were retained from the boreholes and shipped to the Hardy Associates (1978) Ltd.'s Calgary laboratory for the detailed testing.

4.1 LABORATORY TEST PROCEDURES

Grab samples were taken from all test holes for sieve analysis (ASTM C136-82) and moisture content determinations. In addition, representative samples of coarse aggregate were tested for: petrographic analysis (ASTM C295), Los Angeles abrasion (ASTM C535-81) and soundness (ASTM C88-76).



4.2 LABORATORY TEST RESULTS

The results of the laboratory testing program are presented on Plates B1 to B22 and Tables B1 to B5 in Appendix "B". Test descriptions and criteria for evaluating the results are also provided.

In summary, petrographic analysis of five samples from the M.P. 1087.6 and 1095.1 deposits gave PN values ranging from 100.2 to 116.2. Los Angeles abrasion tests resulted in losses (for 50 revolutions) ranging from 13.4 to 20.4 percent. Sulphate soundness testing produced losses ranging from 0.33 to 2.66 percent. Results for the individual deposits are presented in Section 5.0.

5.0 DEPOSIT EVALUATIONS

The deposits are evaluated below, in terms of their potential as sources of coarse granular aggregate, with respect to: available volumes, material type and quality, development criteria and possible community uses.

5.1 EVALUATION CRITERIA

Proven and probable reserves (and overburden volumes) have been computed for each deposit. Proven coarse aggregate volume was calculated, assuming a 100 m setback from the Alaska Highway, using average granular material thickness extrapolated over an area extending approximately 15 m in all directions from the boreholes. Overburden volume was calculated similarly. In view of the stratigraphic variability at the M.P. 1086.2 site, the calculated proven



volume for that deposit was also reduced by a 20 percent contingency factor.

Probable reserves were calculated assuming the same proven deposit thickness and extrapolating over the area of the deposit considered, on the basis of airphoto interpretation, to be of geologically similar origin. No contingency allowance was included. In the case of the M.P. 1095.1 reserve, deposit thickness for calculation purposes was assumed to be 6 m, even though the presence of permafrost precluded drilling to this depth in all instances.

In evaluating the materials for possible community use, the granular materials classification presented on Table 1, (provided previously to us by DIAND), was used.

5.2 BORROW RESERVE AT M.P. 1086.2 (YTG #10981)

5.2.1 Deposit Description

This potential borrow site is located approximately 5 km northwest of Destruction Bay and 10 km southeast of Burwash Landing (Figure 1).

The site is located on Late Wisconsinan morainal deposits, which contain patches of outwash material (Rampton, 1979a). The site has undulating topography, with a maximum relief of 5 m. Drainage is good, except in the eastern part (which is low-lying). A portion of the site (in the vicinity of an existing pit) has been stripped of vegetation but the remainder is heavily treed (Plate C1).

TABLE 1

CLASSIFICATION OF GRANULAR MATERIALS
(after DIAND)

SOURCE QUALITY DESCRIPTION	GENERAL DESCRIPTION OF MATERIAL	MINIMUM TECHNICAL IDENTIFICATION PARAMETERS	SUGGESTED USES OF MATERIAL
Excellent	Well graded sands and gravel, suitable for use as aggregate with a minimum of processing	Petrographic Number: 160 max. Los Angeles Abrasion Loss: 35% max. Soundness Loss (Magnesium Sulphate): 12% max., and meeting other requirements of CSA A23.1-1973	Portland cement, and asphaltic concrete aggregate, masonry sand, concrete block, surface coarse and roofing aggregate.
Good	Well graded sands and gravels, with varying quantities of silt.	Petrographic Number: 200 max. Los Angeles Abrasion Loss: 60% max. Fines greater than 10% passing the 200 sieve can be removed with minimum of processing	Granular base and subbase. Winter sand backfill for trenches and slabs. Pads for structures. Select backfill.
Fair	Poorly graded sands and gravels, with or without substantial silt content	Petrographic Number: 250 max. Can be processed to meet local frost susceptibility criteria	Granular subbase. General backfill material, pads for equipment.
Poor	Poorly graded granular soils of high silt content, possibly containing very weak particles and deleterious materials	Nil	General non-structural fill.



5.2.2 Field Investigation

Fifteen boreholes (BH's C1 to C15) were put down, on November 26 and 27, 1982. Borehole locations are shown on Plate C1, while logs are presented on Plates A1 to A15 and laboratory test results in Appendix "B" (Plates B1 to B5).

5.2.3 Material Type

Coarse, poorly graded, dirty gravel was encountered in ten of the boreholes; overburden thickness ranged from 3 m to nearly 6 m. The gravel occurs at shallowest depth in the northwestern part and at slightly greater depths close to the eastern edge of the site. The overburden, probably a glacial till, ranges from clayey silt to silty and gravelly sand. Permafrost was not encountered in any of the boreholes. Only BH C14 was found to be wet at completion.

5.2.4 Available Reserves

Coarse aggregate occurs predominantly in the northwestern portion of the deposit. An area of 8400 m² was outlined by the test drilling, with an average deposit thickness of 1.3 m. On this basis, proven reserves of 11 000 m³ of coarse granular material are indicated. However, overburden thickness averages 3.8 m, giving a stripping ratio of roughly 3:1.

5.2.5 Material Quality

Grain size analyses were conducted on five samples from this deposit; results are presented on Plates B1 to B5 (Appendix "B"). The coarse aggregate is, in general, poorly graded and



dirty. Fines content varies from 7 to 31 percent, with an average of 21.8 percent.

Moisture contents range from about 2 percent to 9 percent for the gravels, with an average of 5 percent. Excepting BH C14, with a moisture content of 22 percent, the overburden also has low moisture contents (in the 5 to 10 percent range).

Detailed testing was not carried out on material from this deposit.

5.2.6 Community Uses

Generally, the coarse aggregate from this deposit has a high fines content and is of fair to poor quality (Table 1). On this basis, the material is suitable for use as granular subbase, general fill and pad construction.

The overburden material consists predominantly of silty sand and silt. It is of poor quality but could possibly be useful as general non-structural fill (Table 1). The material will be difficult to work, however, and frost susceptible.

5.2.7 Development Considerations

This borrow reserve has excellent all-weather access, via the Alaska Highway, to both communities.

The economics of extracting the gravel, with stripping ratio of 3:1, are poor unless the overburden can be utilized for general fill purposes. In any event, extraction will be



limited to the frost-free period, since winter development will be slow and costly (the material will be extremely difficult to rip in a frozen state).

5.3 BORROW RESERVE AT MP 1087.6 (DIAND #11574)

5.3.1 Deposit Description

This deposit is situated 7 km southeast of Burwash Landing and 8 km northwest of Destruction Bay (Figure 1).

The higher part of the site comprises a glaciofluvial kame terrace and alluvial fan deposits form the surrounding terrain. Most of the site is occupied by the kame terrace, which has up to 10 m of relief and is well drained.

As shown on Plate C2, a portion of this reserve has been excavated previously for granular borrow, and the vegetation has been partially stripped in the area around the existing pit. The undeveloped portion is sparsely to densely treed.

5.3.2 Field Investigations

Ten boreholes were drilled at this site, all to a depth of 6.0 m. Boreholes A1 and A3 were located at the base of the kame terrace, on alluvial fan deposits, while BH's A2, A6, A7 and A8 were located in the bottom of the existing pit. The remainder of holes were on top of the kame terrace. Access to much of the deposit was restricted by the dense forest cover and only a limited area could be tested. Borehole locations are shown on Plate C2 (Appendix "C"), detailed logs in Appendix "A" (Plates A16 to A25).



5.3.3 Material Type

Granular material was encountered in all boreholes, with overburden thickness ranging up to 2 m (average 0.45 m). Boreholes A1 and A3, encountered sand and dirty gravel, while borings in the bottom of the existing pit (A2, A7 and A8) intersected 6.0 m of clean but poorly graded gravel. The remaining terrace, encountered poorly graded, generally clean, gravel, with some sand lenses; overburden averaged 0.5 m in thickness.

5.3.4 Available Volumes

The greatest potential for granular material exists in the kame terrace, already partially developed by the existing excavation. Available reserves exist in three areas:

- a) North of the existing pit.
- b) Underlying the existing pit.
- c) South of the excavation.

Test drilling to the north of the existing pit (BH's A4 and A5) proves coarse aggregate reserves of 5000 m³, assuming an average overburden thickness of 1.3 m. Estimated probable reserves for this portion of the deposit are 18 000 m³.

Boreholes A2, A6, A7 and A8, within the existing pit (area: 2100 m²), intersected greater than 6 m of clean, poorly graded, medium to coarse gravel, giving reserves of 12 600 m³, with no overburden. It is unlikely, however, that the pit will be extended below the level of the surrounding terrain, so that proven reserves from this portion of the deposit, are



estimated at about half the above total, or 6300 m³. An additional 7200 m³ of material occurs in the vicinity of BH A6, giving probable reserves of 13 500 m³.

Boreholes A9 and A10, to the east of the existing pit, indicate greater than 6 m of coarse aggregate over an area of 1800 m², or proven reserves of approximately 11 000 m³. On the average, 60 percent of this material is expected to be gravel sized, with the remainder predominantly sand. No overburden was encountered in this area. Probable reserves are estimated in the order of 50 000 m³, extending over an area of 10 000 m². Overburden up to 1.5 m thick is expected over much of the latter area.

Total reserves for the M.P. 1087.6 deposit are 22 300 m³ proven and 81 500 m³ probable.

5.3.5 Material Quality

Moisture contents for this deposit are shown on the pertinent borehole logs (Plates A16 to A25), and grain size curves are presented Plates B8 to B10. Generally, the aggregate is coarse and poorly graded, with a low fines content. Testing of a sample from BH A4, gave a Los Angeles abrasion loss of 13.4 percent (Plate B6), a sulphate soundness loss of 0.33 percent (Plate B7), and petrographic number (PN) of 100.2 (Table B2). The PN for a sample from BH A2 was also 100.2 (Table B1).

5.3.6 Possible Community Uses

The results of the laboratory testing indicate the aggregate from this deposit is of good quality (Table 1), suitable for



most construction purposes. The coarseness and poor grading of the material suggest crushing will be necessary to meet the specifications for concrete aggregate. Fines may need to be added before the material can be used for road subgrades, bases or surface coarse, in the event crushing does not increase the fines content sufficiently.

5.3.7 Development Consideration

This deposit has an adequate volume of good quality material centrally located between the two communities, to warrant development.

Development should be continued from the existing excavation, both deepening and widening the work area. A 100 m buffer zone should be kept between the pit and the Alaska Highway. Overburden, where encountered, should be separated and stockpiled along the base of the kame terrace, for later use in rehabilitation and reclamation (or possibly to increase fines content of aggregate used as surface course). If possible, the topsoil should be stockpiled separately.

Extraction should ideally be timed for the summer season. Although moisture and fines content are low enough to allow winter development, this is usually a slower and more costly process than summer development.



5.4 BORROW RESERVE AT MP 1095.1 (YTG #10983)

5.4.1 Deposit Description

This borrow site is, located on the south side of the Alaska Highway, 4 km and 18 km northwest of Burwash Landing and Destruction Bay, respectively.

The deposit is situated on a portion of the Duke River alluvial fan. The site is flat to gently sloping, has a maximum of 5 m to 6 m relief, and is moderately well drained. Depressional areas on the site tend to have poor drainage. Plate C3 shows general site conditions.

Adjacent to the highway, the site has been stripped of vegetation and excavated for borrow to a shallow depth. The remainder of the study area is heavily treed, with poor access (Plate C3).

5.4.2 Field Investigations

A total of twenty boreholes (B1 to B20) was drilled, on November 27 and 28, 1982, to a maximum depth of 6.0 m. Several holes could not be completed to the full depth because of auger refusal on boulders and/or permafrost. As shown on Plate C3, boreholes are distributed mainly in the northern portion of the borrow reserve, since the heavy tree cover prevented drilling test holes further back on the site. Detailed borehole logs are presented on Plates B26 to B45.



5.4.3 Material Type

All borings, except BH B17, encountered coarse and poorly graded, subrounded to subangular, gravel, with a low moisture and fines content, and some sand pockets. Overburden was absent in most of the holes as the site had previously been cleared and partially stripped. The extreme western portion of the deposit, which is low-lying and wet, is underlain by peat and/or silt (1.0 m to 3.0 m deep). Permafrost was encountered in many of the boreholes, particularly in the southern part where the vegetation has not been completely stripped.

5.4.4 Available Reserves

Test drilling has proven coarse aggregate in an area of roughly 20 000 m² (taking into account the 100 m setback from the Alaskan Highway). Assuming a 4.5 m minimum deposit thickness, 90 000 m³ of predominantly coarse granular material is indicated, with little or no overburden. Since a deposit thickness of at least 6 m appears likely for most of the site (but could not be proven due to permafrost), probable reserves are estimated at considerably greater than 200 000 m³. This probable volume should be treated with caution, however since drilling operations were limited to the northernmost one third of the site, due to very poor access.

5.4.5 Material Quality

Grain size curves are shown on Plates B11, B14, B17, B18, B21, B22 and B23. The aggregate is generally coarse and poorly graded, with a fines contents ranging from 1 percent to 7 percent. Material from borehole B4 had a PN of 108.3 (Table



B3) a Los Angeles abrasion loss of 18.5 percent (Plate B12), and a sulphate soundness loss of 0.71 percent (Plate B13). Aggregate from BH B9 had a PN of 116.2 (Table B4), an abrasion loss of 18.9 percent (Plate B15) and a soundness loss of 2.66 percent (Plate B16). Finally, material from BH B14 had a PN of 111.7 (Table B5), had an abrasion loss of 20.4 percent (Plate B19) and a soundness loss of 2.42 percent (Plate B20).

5.4.6 Possible Community Uses

The results of the laboratory testing indicate the aggregate is of good quality (Table 1). The grain size curves indicate crushing and processing will be required to produce a material that is suitable for most construction requirements.

5.4.7 Development Considerations

This proposed borrow site has excellent access, via the Alaska Highway, to both communities and is a large volume source of good to excellent quality aggregate. Since a small borrow pit is currently located on the site, development should proceed by expansion of this existing excavation.

Landuse regulations require that a 100 m buffer zone be maintained between the development and the Alaska Highway. As a result much of the existing pit will fall into this buffer zone. Additional development should be away from this setback area.

Test drilling encountered difficulties in penetrating the frozen gravels and it is expected that excavation will meet with the same problem. Development of the pit, therefore, should be a summer operation. Permafrost is not expected to



be encountered for the initial 4 or 5 m from the surface in the portion of the deposit that has been stripped of its surface vegetation. Expansion beyond this area will likely encounter permafrost near the ground surface, and a thaw-strip cycle method of mining in frozen ground is recommended. This involves exposing a large surface area of granular material to solar radiation to promote thawing. Excavation of unfrozen material may then be completed in layers or strips, as the thaw front progresses. Generally, coarse granular material will thaw from 0.2 m to 0.4 m per day. Site clearing well prior to development also promotes deeper thawing of the active layer.

Material obtained during a summer operation can be used directly or may be stockpiled for use during the winter months. Moisture and fines contents are generally low enough to permit winter development. However, ripping of undisturbed gravel is slower and more costly than the same process during the summer or excavating from a stockpile.

6.0

CONCLUSIONS

Findings of the study with respect to the three possible community gravel pit sites are, in summary, as follows:

- a) The M.P. 1086.2 site is a low volume deposit of fair to poor quality aggregate. With a 3:1 gravel-overburden stripping ratio, development does not appear warranted unless the overburden is used as fill material.
- b) Reserves for the M.P. 1087.6 deposit are estimated at 22 300 m³ proven and 81 500 m³ probable, of good quality aggregate. This will be suitable for most construction



purposes, with crushing and screening required to produce concrete aggregate.

- c) At M.P. 1095.1 proven reserves are 90 000 m³ of good quality aggregate, greater than 200 000 m³ probable. Again though suitable for most purposes, the gravel will require crushing to produce concrete aggregate.

The M.P. 1086.2 site is a small volume source of poor quality gravel, with a high stripping ratio. The study results suggest that development is probably not warranted, even if the frost susceptible overburden materials were used for fill.

Based on material quality both the M.P. 1087.6 and 1095.1 sites are candidates for development as a community gravel pit. However, proven and probably aggregate volumes at the latter are considerably in excess of those of the former. Additional testing in the southern part of the M.P. 1095.1 deposit (which presently has poor access) will likely prove out considerably greater volumes.



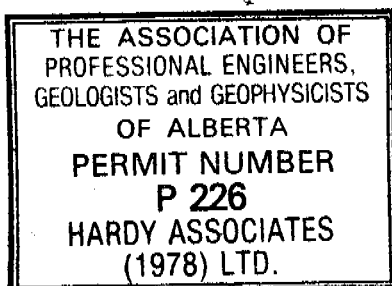
It is our conclusion that the M.P. 1095.1 borrow reserve (YTG #10983) is most suited to development as a community gravel pit for Burwash Landing and Destruction Bay. It will be necessary to set up a crushing and screening operation to produce concrete aggregate: the material may be used for fill in the pit-run state or with only limited processing.

Respectfully Submitted,

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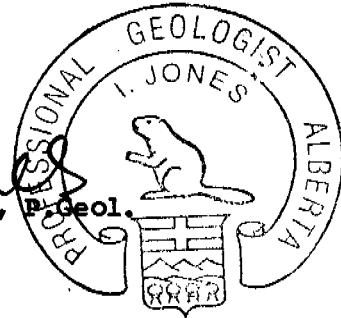
Per:

G. Dupuy, P.Geol.



Per:

I. Jones, M.Sc., P.Geol.



Per:

M. Stepanek, M.Sc., P.Eng.

GD:IJ:MS/lr
0.333



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APPENDIX "A"
BOREHOLE LOGS



EXPLANATION OF TERMS AND SYMBOLS

The terms and symbols used on the borehole logs to summarize the results of field investigation and subsequent laboratory testing are described in the following pages.

It should be noted that materials, boundaries, and conditions have been established only at the borehole locations, and are not necessarily representative of subsurface conditions elsewhere across the site.

TEST DATA

Data obtained from laboratory and field testing are shown on the grid at the appropriate depth interval.

The natural moisture (water) content of the soil at the time of drilling is plotted against depth, together with the plastic and liquid limits where determined.

Abbreviations, graphic symbols, and relevant test method designations are as follows:

○	w	natural moisture content (ASTM D 2216)
□	w _p	plastic limit (ASTM D 424)
△	w _L	liquid limit (ASTM D 423)
	NP	non plastic soil
→		seepage
▼		observed water level

Other abbreviations and symbols are as shown on the borehole log sheet.

DEPTH

The depth of borehole below existing ground surface is shown. Corresponding elevations sometimes are shown with respect to the datum given.

SOIL CLASSIFICATION AND DESCRIPTION

Soils are classified and described according to their engineering properties and behaviour.

The soil of each stratum is described using the Unified Soil Classification System¹ modified slightly so that an inorganic clay of "medium plasticity" is recognized.

The use of modifying adjectives may be employed to define the actual or estimated percentage range by weight of minor components. This is similar to a system developed by D.M. Burmister.²

The soil classification system is shown in greater detail on page 3.

1. "Unified Soil Classification System", Technical Memorandum 3-357 prepared for Office, Chief of Engineering, by Waterways Experiment Station, Vicksburg, Mississippi, Corps. of Engineers, U.S. Army. Vol. 1, March 1953.

2. American Society for Testing and Materials. Procedures for Testing Soils, "Suggested Methods of Testing for Identification of Soils", 4th Ed; pp 221-233, Dec. 1964.



SOIL SAMPLES

CONDITION — This column graphically indicates the depth and condition of the sample:



undisturbed



disturbed



not recovered

TYPE — The type of sample is indicated in this column as follows:

- A auger sample
- B block sample
- C rock core, or frozen soil core
- D drive sample
- P Pitcher tube sample
- U tube sample (usually thin-walled)
- W wash or air return sample
- O other (see report text)

PENETRATION RESISTANCE — Unless otherwise noted this column refers to the number of blows (N) of a 140 pound (63.5 kg) hammer freely dropping 30 inches (0.76 m) required to drive a 2 inch (50.8 mm) O.D. open-end sampler 0.5 feet (0.15 m) to 1.5 feet (0.45 m) into the soil, or until 100 blows have been applied, in which case, the penetration is stated. This is the standard penetration test referred to in ASTM D 1586.

OTHER TESTS

In this column are tabulated results of other laboratory tests as indicated by the following symbols:

*C	Consolidation test
Fines	Percentage by weight smaller than #200 sieve
D _R	Relative density (formerly specific gravity)
k	Permeability coefficient
*MA	Mechanical grain size analysis and hydrometer test (if appropriate)
pp	Pocket penetrometer strength
*q	Triaxial compression test
q _u	Unconfined compressive strength
*SB	Shearbox test
SO ₄	Concentration of water-soluble sulphate
*ST	Swelling test
TV	Torvane shear strength
VS	Vane shear strength (undisturbed-remolded)
ε _f	Unit strain at failure
γ	Unit weight of soil or rock
γ _d	Dry unit weight of soil or rock
ρ	Density of soil or rock
ρ _d	Dry density of soil or rock

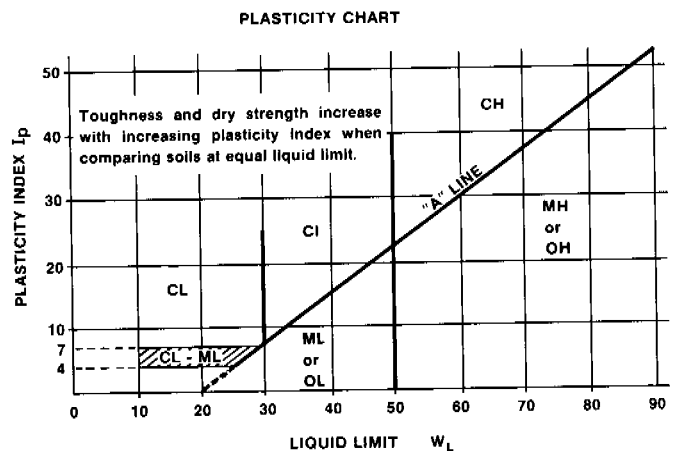
* The results of these tests usually are reported separately.

SOIL CLASSIFICATION SYSTEM (MODIFIED U.S.C.)

MAJOR DIVISION			GROUP SYMBOL	GRAPHIC SYMBOL	COLOR CODE	TYPICAL DESCRIPTION	LABORATORY CLASSIFICATION CRITERIA	
HIGHLY ORGANIC SOILS			PI		ORANGE	PEAT AND OTHER HIGHLY ORGANIC SOILS	STRONG COLOR OR ODOR, AND OFTEN FIBROUS TEXTURE	
COARSE-GRAINED SOILS (MORE THAN HALF BY WEIGHT LARGER THAN NO. 200 SIEVE SIZE)	GRAVELS MORE THAN HALF COARSE FRACTION LARGER THAN NO. 4 SIEVE SIZE	CLEAN GRAVELS	GW		RED	WELL-GRADED GRAVELS, GRAVEL-SAND MIXTURES, < 5% FINES	$C_u = \frac{D_{60}}{D_{10}} > 6$ $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}} = 1 \text{ to } 3$	
			GP		RED	POORLY-GRADED GRAVELS, AND GRAVEL-SAND MIXTURES, < 5% FINES	NOT MEETING ALL ABOVE REQUIREMENTS	
		DIRTY GRAVELS	GM		YELLOW	SILTY GRAVELS, GRAVEL-SAND-SILT MIXTURES > 12% FINES	ATTERBERG LIMITS BELOW "A" LINE OR $I_p < 4$	
			GC		YELLOW	CLAYEY GRAVELS, GRAVEL-SAND-CLAY MIXTURES > 12% FINES	ATTERBERG LIMITS ABOVE "A" LINE, $I_p > 7$	
	SANDS MORE THAN HALF COARSE FRACTION SMALLER THAN NO. 4 SIEVE SIZE	CLEAN SANDS	SW		RED	WELL-GRADED SANDS, GRAVELLY SANDS, < 5% FINES	$C_u = \frac{D_{60}}{D_{10}} > 4$ $C_c = \frac{(D_{30})^2}{D_{10} \times D_{60}} = 1 \text{ to } 3$	
			SP		RED	POORLY-GRADED SANDS, OR GRAVELLY SANDS, < 5% FINES	NOT MEETING ALL ABOVE REQUIREMENTS	
		DIRTY SANDS	SM		YELLOW	SILTY SANDS, SAND-SILT MIXTURES > 12% FINES	ATTERBERG LIMITS BELOW "A" LINE OR $I_p < 4$	
			SC		YELLOW	CLAYEY SANDS, SAND-CLAY MIXTURES > 12% FINES	ATTERBERG LIMITS ABOVE "A" LINE OR $I_p > 7$	
FINE-GRAINED SOILS (MORE THAN HALF BY WEIGHT PASSES NO. 200 SIEVE SIZE)	SILTS BELOW "A" LINE ON PLASTICITY CHART; NEGLECTIBLE ORGANIC CONTENT		ML		GREEN	INORGANIC SILTS AND VERY FINE SANDS, ROCK FLOUR, SILTY SANDS OF SLIGHT PLASTICITY	$w_L < 50$	SEE CHART BELOW
			MH		BLUE	INORGANIC SILTS, MICACEOUS OR DIATOMACEOUS, FINE SANDY OR SILTY SOILS	$w_L > 50$	
	CLAYS ABOVE "A" LINE ON PLASTICITY CHART; NEGLECTIBLE ORGANIC CONTENT		CL		GREEN	INORGANIC CLAYS OF LOW PLASTICITY, GRAVELLY, SANDY, OR SILTY CLAYS, LEAN CLAYS	$w_L < 30$	
			CI		GREEN-BLUE	INORGANIC CLAYS OF MEDIUM PLASTICITY SILTY CLAYS	$w_L > 30, < 50$	
			CH		BLUE	INORGANIC CLAYS OF HIGH PLASTICITY, FAT CLAYS	$w_L > 50$	
	ORGANIC SILTS & ORGANIC CLAYS		OL		GREEN	ORGANIC SILTS AND ORGANIC SILTY CLAYS OF LOW PLASTICITY	$w_L < 50$	
			OH		BLUE	ORGANIC CLAYS OF HIGH PLASTICITY	$w_L > 50$	

- All sieve sizes mentioned on this chart are U.S. Standard, ASTM E11.
- Boundary classifications possessing characteristics of two groups are given combined group symbols eg GW-GC is a well-graded gravel-sand mixture with clay binder between 5% and 12%.
- Soil fractions and limiting textural boundaries are in accordance with the Unified Soil Classification System, except that an inorganic clay of medium plasticity (CI) is recognized.
- The following adjectives may be employed to define percentage ranges by weight of minor components:

and	50 - 36%
some	35 - 21%
little	20 - 11%
trace	10 - 1%



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HARDY ASSOCIATES (1978) LTD.

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BOREHOLE LOGS

M.P. 1086.2

**PROJECT**

BURWASH LANDING - DESTRUCTION BAY

GRAVEL STUDY

MP 1086.2

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 26, 1982

JOB NO. CG 10047

HOLE NO. C-1

WATER CONTENT

Wp - □

W-O

$$W_L \cdot \Delta$$

PERCENT %

10 20 30 40 50 60

SOIL DESCRIPTION

SOIL SAMPLE**DRILL TYPE****DATUM**

SURFACE ELEVATION

CONDITION

TYPE

CONCENTRATION

Rotary

Rotary

OTHER TESTS

DEPTH

FORMS SYMBOL

SILT some clay and organics,
dark brown

1

GRAVEL silty, brown, fine to medium, poorly graded

A1

Grain size
(see Pl. B-1)

2

SAND silty, little gravel, very fine to fine-grained

3

4

--less gravel

5

-- trace gravel

6

-- very fine-grained sand, little gravel

A2

Bottom of Hole at 6.0m

Plate A-1



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PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1086.2

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 26, 1982

JOB NO. CG 10047

HOLE NO. C-2

WATER CONTENT

Wp - □ W - O W_L - Δ

PERCENT %

10 20 30 40 50 60

DEPTH

m

SOIL SYMBOL

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SOIL SAMPLE

CONDITION

TYPE

PENETRATION

RESISTANCE

DRILL TYPE

Rotary

OTHER TESTS

1

2

3

4

5

6

SILT sandy, organic, reddish-brown

SAND very gravelly, some silt, trace clay, dry, (Till-like)

GRAVEL some silty sand, dirty

SAND silty, very fine to fine-grained

--- little gravel

A1

A2

Grain size
(see Pl. B-2)

Bottom of Hole at 6.0m

Plate A-2



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BOREHOLE LOG

PROJECT BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1086.2

LOGGED/DWN. JD/TF		CKD.	GD	DATE OF INVEST. Nov. 26, 1982		JOB NO. CG 10047		HOLE NO. C-3			
WATER CONTENT			DEPTH m	SOIL SYMBOL	SOIL DESCRIPTION	SOIL SAMPLE			DRILL TYPE		
Wp - □	W - ○	WL - △				CONDITION	TYPE	PENETRATION RESISTANCE	OTHER TESTS		
PERCENT %					DATUM						
10	20	30	40	50	60	SURFACE ELEVATION					
						TOPSOIL organic, silty clay, dark brown				A1	
						SAND very fine to fine-grained, silty, some gravel, little clay, (Till-like)					
						GRAVEL sandy, some silt, to 25mm Ø, poorly graded, very fine to fine-grained sand				A2	
						--- silty, brown					
						Bottom of Hole at 6.0m					

Plate A-3



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PROJECT

BURWASH LANDING - DESTRUCTION BAY

GRAVEL STUDY

MP 1086.2

LOGGED/DWN. JD/TF

CKD. GD

DATE OF INVEST. Nov. 26, 1982

JOB NO. CG 10047

HOLE NO. C-4

WATER CONTENT

Wp - □ W - O W_L - Δ

PERCENT %

10 20 30 40 50 60

DEPTH

m

SOIL SYMBOL

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SOIL SAMPLE

CONDITION

TYPE

PENETRATION
RESISTANCE

DRILL TYPE

Rotary

OTHER TESTS

1

2

3

4

5

6

SILT organics, sandy, reddish-brown

SAND silty, very fine-grained, little clay

-- some gravel to 25mm Ø, some silt, trace clay

A1

GRAVEL some silty sand, poorly graded, subangular to subrounded

A2

Bottom of Hole at 6.0m

Grain size
(see Pl. B-3)

Plate A-4



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PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1086.2

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 26, 1982

JOB NO. CG 14007

HOLE NO. C-5

WATER CONTENT

Wp - □ W - O W_L - Δ

PERCENT %

10 20 30 40 50 60

DEPTH

m

SOIL SYMBOL

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SOIL SAMPLE

CONDITION

TYPE

PENETRATION
RESISTANCE

DRILL TYPE

Rotary

OTHER TESTS

1

2

3

4

5

6

TOPSOIL organic, reddish-brown
SAND silty, brown, very fine-
grained, little clay
-- trace gravel

A1

GRAVEL sandy, some silt, some
clay, (Till-like)

A2

Grain size
(see Pl. B-4)

Bottom of Hole at 6.0m

Plate A-5



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BOREHOLE LOG

PROJECT BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1086.2

LOGGED/DWN. JD/TF		CKD. GD	DATE OF INVEST. Nov. 26, 1982	JOB NO. CG 10047	HOLE NO. C-6		
WATER CONTENT			SOIL DESCRIPTION		SOIL SAMPLE		DRILL TYPE
Wp - □	W - ○	W _L - △	DATUM	CONDITION	TYPE	PENETRATION RESISTANCE	Rotary
PERCENT %			SURFACE ELEVATION				OTHER TESTS
10	20	30	40	50	60	DEPTH m	SOIL SYMBOL
							TOPSOIL silty, sand, some organics, dark brown
						1	SAND silty, brown, dry, very fine-grained, little clay --- trace gravel
						2	
						3	
						4	--- very gravelly, some silt and clay, (Till-like)
						5	
						6	
							Bottom of Hole at 6.0m

Grain size
(see Pl. B-5)

A1

Plate A-6



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PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1085.2

LOGGED/DWN. JD/TF

CKD.

GD

DATE OF INVEST. Nov. 26, 1982

JOB NO. CG 10047

HOLE NO. C-7

WATER CONTENT

Wp - □ W - O W_L - Δ

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SOIL SAMPLE

CONDITION

TYPE

PENETRATION
RESISTANCE

DRILL TYPE

Rotary

OTHER TESTS

1

--- trace gravel

2

--- little to some gravel

3

4

5

--- trace gravel

6

Bottom of Hole at 6.0m

⊗ A1

Plate A-7



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BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1086.2

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 26, 1982

JOB NO. CG 10047

HOLE NO. C-8

WATER CONTENT

W_p - □ W - O W_L - Δ

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

DATUM

CONDITION

TYPE

PENETRATION
RESISTANCE

OTHER TESTS

SURFACE ELEVATION

FILL sand, coarse, some silt,
brown

PEAT dark brown, fibrous, some
organic silt

SAND silty, medium to coarse-
grained, brown, some clay

1

2

3

4

5

6

--- trace gravel

GRAVEL some very fine sand,
trace silt

A1

Bottom of Hole at 6.0m

Plate A-8



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BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1086.2

LOGGED/DWN.	JD/TF	CKD.	GD	DATE OF INVEST.	Nov. 26, 1982	JOB NO.	CG 10047	HOLE NO.	C-9		
WATER CONTENT				DEPTH m	SOIL SYMBOL	SOIL DESCRIPTION		SOIL SAMPLE		DRILL TYPE	
Wp - □ W - ○ W _L - △ PERCENT %						DATUM	CONDITION	TYPE	PENETRATION RESISTANCE	Rotary	
10 20 30 40 50 60				SURFACE ELEVATION						OTHER TESTS	
				1	SAND silty, brown, very fine-grained, some clay	X	A1				
				2						---	silty, fine-grained, trace gravel, dark brown
				3							
				4	---	little gravel	X	A2			
				5		GRAVEL sandy, little silt, subangular					
				6		Bottom of Hole at 6.0m					

Plate A-9



PROJECT	BURWASH LANDING - DESTRUCTION BAY GRAVEL STUDY	MP 1086.2
---------	---	-----------

LOGGED/DWN.		JD/TF	CKD.	GD	DATE OF INVEST.		JOB NO.		HOLE NO.			
WATER CONTENT						SOIL DESCRIPTION		SOIL SAMPLE		DRILL TYPE		
Wp - □ W - ○ W _L - △ PERCENT % 10 20 30 40 50 60						DATUM		CONDITION	TYPE	PENETRATION RESISTANCE		
DEPTH m						SURFACE ELEVATION					OTHER TESTS	
						1		--- little to some gravel, fine-grained sand		X A1		
						2						
						3						
						4						
						5		--- boulders Bottom of Hole at 4.5m Refusal on boulders				



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BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1086.2

LOGGED/DWN. JD/TF

CKD. GD

DATE OF INVEST. Nov. 26, 1982

JOB NO. CG 10047

HOLE NO. C-11

WATER CONTENT

W_p - □ W - ○ W_L - △

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

OTHER TESTS

DATUM

SURFACE ELEVATION

CONDITION

TYPE

PENETRATION

RESISTANCE

TOPSOIL organic, reddish-brown

SILT sandy, light brown, fine-grained sand, (Till-like)

--- some gravel, trace clay

A1

A2

Bottom of Hole at 6.0m

Plate A-11



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BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1086.2

LOGGED/DWN. JD/TF

CKD.

GD

DATE OF INVEST. Nov. 26, 1982

JOB NO. CG 10047

HOLE NO. C-12

WATER CONTENT

Wp - □ W - ○ W_L - △

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

DATUM

CONDITION

TYPE

PENETRATION
RESISTANCE

OTHER TESTS

SURFACE ELEVATION

TOPSOIL organic, sandy, brown

SILT sandy, brown, little to
some clay, (Till-like)

1

2

--- trace gravel

3

--- clayey, little gravel

4

5

--- trace gravel

A1

6

Bottom of Hole at 6.0m

Plate A-12



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BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1086.2

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 26, 1982

JOB NO. CG 10047

HOLE NO. C-13

WATER CONTENT

W_p - □ W - ○ W_L - △

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

DATUM

CONDITION

TYPE

PENETRATION
RESISTANCE

SURFACE ELEVATION

OTHER TESTS

1

2

3

4

5

6

SILT sandy, greyish-brown,
(Till-like)

-- trace clay, gravel

A1

A2

Bottom of Hole at 6.0m

Plate A-13



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BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1086.2

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 26, 1982

JOB NO. CG 10047

HOLE NO. C-14

WATER CONTENT

W_p - □ W - ○ W_L - △

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

DATUM

SURFACE ELEVATION

CONDITION

TYPE

PENETRATION

RESISTANCE

OTHER TESTS

PEAT topsoil, dark brown

CLAY organic, silty, brown, wet

--- medium to high plastic, trace organics

GRAVEL some clayey silt

Bottom of Hole at 2.6m

A1

Plate A-14

BOREHOLE LOG

PROJECT	BURWASH LANDING - DESTRUCTION BAY GRAVEL STUDY
---------	---

MP 1086.2

LOGGED/DWN.	JD/TF	CKD.	GD	DATE OF INVEST.	Nov. 27, 1982	JOB NO. CG	10047	HOLE NO.	C-15
-------------	-------	------	----	-----------------	---------------	------------	-------	----------	------

WATER CONTENT						DEPTH m	SOIL SYMBOL	SOIL DESCRIPTION		SOIL SAMPLE			DRILL TYPE	
W _p - □	W - ○	W _c - △	PERCENT %					DATUM	CONDITION	TYPE	PENETRATION RESISTANCE	Rotary		
10	20	30	40	50	60			SURFACE ELEVATION				OTHER TESTS		
						1		FILL silt, sandy, some fine gravel, brown						
						2		PEAT organics, sandy, reddish-brown						
						3								
						4	SILT organic, sandy, some gravel, grey							
						5								
						6		GRAVEL some silty sand, subangular		X	A1			
						Bottom of Hole at 6.0m								
												</		



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BOREHOLE LOGS
M.P. 1087.6

**PROJECT**

**BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY**

MP 2087.6

LOGGED/DWN. JD/TF

CKD. GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. A-1

WATER CONTENT

Wp - □ W - O W_L - Δ

10 20 30 40 50 60

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SOIL SAMPLE

CONCLUSION

TYPE

ENERGY

DISCUSSION

DRILL TYPE

Rotary

OTHER TESTS

1

2

3

4

5

6

FILL gravel, crushed, mixed
with sandy clayey silt

GRAVEL medium subangular, well-graded, some sand and silt

SAND silty, dark brown, very fine to fine-grained, little to some clay

-- trace gravel

GRAVEL coarse, subangular, some
silty sand, black

A1

A2

Bottom of Hole at 6.0m

Plate A-16



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BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1087.6

LOGGED/DWN. JD/TF

CKD.

GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. A-2

WATER CONTENT

Wp - □ W - ○ W_L - Δ

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SOIL SAMPLE

CONDITION

TYPE

PENETRATION
RESISTANCE

DRILL TYPE

Rotary

OTHER TESTS

FILL gravel, crushed, trace sand

GRAVEL fine to medium, trace sand, clean

1

2

3

4

5

6

--- medium, some sand

Bottom of Hole at 6.0m

A1

A2

Petrographic
Analysis
(Table B-1)
L.A. Abrasion
(Pl. B-6)
Sulphate
Soundness
(Pl. B-7)

Plate A-17



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BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1087.6

LOGGED/DWN. JD/TF

CKD. GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. A-3

WATER CONTENT

W_p - □ W - ○ W_L - △

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

OTHER TESTS

DATUM

SURFACE ELEVATION

CONDITION

TYPE

PENETRATION
RESISTANCE

1

SAND fine, silty, some medium
gravel, brown

2

SILT sandy, trace volcanic ash,
brown

A1

3

SAND fine to medium-grained,
silty, dark brown

4

--- trace gravel

5

--- coarse, little silt, some
gravel, dark brown

6

— trace coarse gravel

Bottom of Hole at 6.0m

Plate A-18



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PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1087.6

LOGGED/DWN.		JD/TF	CKD.	GD	DATE OF INVEST.		Nov. 27, 1982		JOB NO.		CG 10047		HOLE NO.		A-4	
WATER CONTENT					DEPTH m	SOIL SYMBOL	SOIL DESCRIPTION		SOIL SAMPLE			DRILL TYPE		OTHER TESTS		
Wp - □ W - ○ WL - △ PERCENT %							DATUM		CONDITION	TYPE	PENETRATION RESISTANCE	Rotary				
					SURFACE ELEVATION											
						SILT sandy, brown, frozen			A1			Petrographic Analysis (Table B-2) Sulphate Soundness (Pl. B-7) L.A. Abrasion (Pl. B-6)				
						GRAVEL medium, some sandy silt, unfrozen										
						clean, trace sandy silt, coarse, subangular, well-graded										
						Bottom of Hole at 6.0m										

Plate A-19



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BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1087.6

LOGGED/DWN. JD/TF

CKD. GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. A-5

WATER CONTENT

W_p - □ W - ○ W_L - △

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

DATUM

CONDITION

TYPE

PENETRATION
RESISTANCE

SURFACE ELEVATION

OTHER TESTS

1

2

3

4

5

6

SILT sandy, reddish-brown

GRAVEL medium, some sandy silt,

A1

--- trace brown silty sand

Bottom of Hole at 6.0m

Plate A-20



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PROJECT

BURWASH LANDING - DESTRUCTION BAY

GRAVEL STUDY

MP 1087.6

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. A-6

WATER CONTENT

Wp - □ W - ○ W_L - △

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

DATUM

SURFACE ELEVATION

CONDITION

TYPE

PENETRATION

RESISTANCE

OTHER TESTS

1

GRAVEL to 20mm ϕ , well-graded,
some silty sand

2

-- coarse, to 50mm ϕ , angular,
poorly graded, few fines

3

-- 25-50mm ϕ , subangular

4

5

-- 20mm ϕ , well-graded

6

Bottom of Hole at 6.0m

A1

A2

A3

Grain size
(see Pl. B-8)

Plate A-21



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PROJECT

BURWASH LANDING - DESTRUCTION BAY

GRAVEL STUDY

MP 1087.6

LOGGED/DWN. JD/TF

CKD. GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. A-7

WATER CONTENT

W_p - □ W - ○ W_c - △

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

DATUM

CONDITION

TYPE

PENETRATION
RESISTANCE

Rotary

SURFACE ELEVATION

OTHER TESTS

GRAVEL 20mm Ø, subangular, some
silty sand, brown

1

⊗ A1

2

3

--- medium gravel

⊗ A2

4

5

--- sandy, dark brown

6

Bottom of Hole at 6.0m

Plate A-22



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BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1087.6

LOGGED/DWN. JD/TF

CKD.

GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. A-8

WATER CONTENT

Wp - □ W - ○ W_L - △

PERCENT %

10 20 30 40 50 60

DEPTH

m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

DATUM

CONDITION

TYPE

PENETRATION
RESISTANCE

OTHER TESTS

SURFACE ELEVATION

GRAVEL poorly graded, some
sand, brown

1

fine, some sand

2

3

4

5

6

sandy, dark brown

A1

A2

Grain size
(see Pl. B-9)

Bottom of Hole at 6.0m

Plate A-23



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PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1087.6

LOGGED/DWN. JD/TF

CKD. GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. A-9

WATER CONTENT

W_p - □ W - ○ W_L - △

PERCENT %

10 20 30 40 50 60

DEPTH

m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

DATUM

CONDITION

TYPE

PENETRATION
RESISTANCE

OTHER TESTS

SURFACE ELEVATION

SAND silty, reddish-brown, dry,
very fine-grained, trace clay

--- some gravel, to 100mm Ø, poorly
graded

GRAVEL some silty sand, reddish-
brown

⊗ A1

⊗ A2

Bottom of Hole at 6.0m

Plate A-24



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BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1087.6

LOGGED/DWN.

JD/TF

CKD. GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. A-10

WATER CONTENT

W_p - □ W - ○ W_L - △

PERCENT %

10 20 30 40 50 60

DEPTH

m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

OTHER TESTS

DATUM

SURFACE ELEVATION

CONDITION

TYPE

PENETRATION

RESISTANCE

GRAVEL to 25mm ϕ , little
sand, brown

1

--- gravel sizes to 50mm ϕ

2

--- finer gravel sizes,
poorly graded

3

4

5

SAND trace coarse gravel, dark
brown

6

Bottom of Hole at 6.0m

A1

A2

Grain size
(see Pl. B-10)

Plate A-25



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BOREHOLE LOG

PROJECT

BURVASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST.

Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. B-1

WATER CONTENT

Wp - □ W - ○ W_L - Δ
PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

OTHER TESTS

DATUM

SURFACE ELEVATION

SILT sandy, trace volcanic ash,
brown

GRAVEL coarse-grained, 75mm,
medium graded

SAND coarse, silty, some gravel

GRAVEL medium, subangular,
little silty sand

-- finer, to 25mm Ø

-- trace cobbles

Bottom of Hole at 6.0m

CONDITION

TYPE

PENETRATION
RESISTANCE

A1

A2

A3

J.A. Abrasion
(Pl. B-13)
Sulphate
Soundness
(Pl. B-16)

Plate A-26



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BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. B-2

WATER CONTENT

Wp - □ W - ○ W_L - △

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SOIL SAMPLE

CONDITION

TYPE

PENETRATION
RESISTANCE

DRILL TYPE

Rotary

OTHER TESTS

1

2

3

TOPSOIL organic, volcanic ash

GRAVEL coarse, to 50mm ϕ ,
sandy, clean

--- cobbles, frozen

Bottom of Hole at 2.5m
Refusal on frozen cobbles

A1

Grain size
(see Pl. B-11)

Plate A-27



PROJECT BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. B-3

WATER CONTENT

Wp - □

W-O

$$w_t = \Delta$$

PERCENT %

10 20 30 40 50 60

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SOIL SAMPLE

CONCLUSION

TYPE

PERMEATION
RESISTANCE

DRILL TYPE

Rotary

OTHER TESTS

GRAVEL coarse, to 75mm Ø, medium
graded, little sandy silt

1 2 --- finer gravel to 65mm Ø

3 --- cobbles

Bottom of Hole at 3.0m
Refusal on cobbles

A1

Plate A-28



PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. B-4

WATER CONTENT

Wp - □

W-O

 $w_1 - \Delta$

PERCENT %

10 20 30 40 50 60

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

DATUM

SURFACE ELEVATION

GRAVEL coarse, to 75mm ϕ , some silty sand
-- finer gravel, 20mm ϕ , poorly graded

-- cobbles

-- coarse gravel, to 50-75mm ϕ ,
some silty sand, grey

-- coarse, subangular to subrounded

Bottom of Hole at 6.0m

CONDITION

TYPE

PENETRATION

Rotary

OTHER TESTS

Petrographic Analysis
(Table B-3)
L.A. Abrasion
(Pl. B-12)
Sulphate
Soundness
(Pl. B-13)

Plate A-29



PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY MD 100

MP 1095.1

LOGGED/DWN.

JD/TF

ÇKD.

GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. B-5

WATER CONTENT

Wp - □

W-Q

 $W_1 - \Delta$

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

GRAVEL coarse, to 75mm ϕ , trace
silty sand

-- finer gravel, to 25mm Ø, well-graded, some silty sand

1

2

3

4

-- coarser gravel, subangular to
to subrounded

... cobbles

Bottom of Hole at 4.0m
Refusal on cobbles

SOIL SAMPLE

CONDITION

TYPE

PENETRATION

RESISTANCE

DRILL TYPE

Rotary

OTHER TESTS

Plate A-30



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BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN.		JD/TF	CKD.	GD	DATE OF INVEST.		Nov. 27, 1982		JOB NO.		CG 10047		HOLE NO.		B-6	
WATER CONTENT				DEPTH m	SOIL SYMBOL	SOIL DESCRIPTION		SOIL SAMPLE			DRILL TYPE					
Wp - □ W - ○ W _L - △ PERCENT %						DATUM		CONDITION	TYPE	PENETRATION RESISTANCE	OTHER TESTS					
10 20 30 40 50 60						SURFACE ELEVATION										
						GRAVEL to 50mm ø, some silty sand, dark brown										
				1		--- cobbles		⊗	A1							
				2												
				3		--- trace cobbles		⊗	A2							
				4												
						--- cobbles, frozen										
				5		Bottom of Hole at 4.5m Refusal on cobbles and permafrost										

Plate A-31



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PROJECT

BURWASH LANDING - DESTRUCTION BAY

GRAVEL STUDY

MP 1095.1

LOGGED/DWN. JD/TF

CKD.

GD

DATE OF INVEST. Nov. 27, 1982

JOB NO. CG 10047

HOLE NO. B-7

WATER CONTENT

Wp - □ W - O W_L - Δ

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SOIL SAMPLE

CONDITION

TYPE

PENETRATION
RESISTANCE

DRILL TYPE

Rotary

OTHER TESTS

1

2

3

4

SILT organic, sandy, reddish-brown

GRAVEL coarse, clean, poorly graded

-- subangular to subrounded

-- cobbles

-- finer gravel

-- cobbles, frozen

⊗ A1

⊗ A2

Grain size
(see Pl. B-14)

Bottom of Hole at 4.0m
Refusal on frozen cobbles

Plate A-32



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PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN.	JD/TF	CKD.	GD	DATE OF INVEST.	Nov. 27, 1982	JOB NO.	CG 10047	HOLE NO.	B-8
WATER CONTENT				SOIL DESCRIPTION			SOIL SAMPLE		DRILL TYPE
Wp - □ W - ○ W _L - △				DATUM			CONDITION	TYPE	PENETRATION RESISTANCE
PERCENT %				SURFACE ELEVATION					
10	20	30	40	50	60	DEPTH m	SOIL SYMBOL	OTHER TESTS	
						1		SILT organic, sandy, reddish-brown, frozen GRAVEL to 35mm Ø, some silty sand, angular, frozen	
						2		A1	
						3			
						4		A2	
						Bottom of Hole at 4.0m Refusal on frozen cobbles			

Plate A-33



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PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN. JD/TF		CKD.	GD	DATE OF INVEST. Nov. 28, 1982		JOB NO. CG 10047		HOLE NO. B-9		
WATER CONTENT			DEPTH m	SOIL SYMBOL	SOIL DESCRIPTION	SOIL SAMPLE			DRILL TYPE	
Wp - □	W - ○	W _L - △				CONDITION	TYPE	PENETRATION RESISTANCE	OTHER TESTS	
PERCENT %					DATUM					
10	20	30	40	50	60	SURFACE ELEVATION				
							FILL sand, silty, coarse, some gravel, frozen			
							GRAVEL angular, to 25mm ϕ , some silty sand, unfrozen			
							finer, gravel to 15mm			
							coarser, to 35mm			
							subangular to subrounded, poorly graded			
							Bottom of Hole at 6.0m			
							A1		Petrographic Analysis (Table B-4) L.A. Abrasion (Pl. B-15) Sulphate Soundness (Pl. B-16)	
							A2			

Plate A-34



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BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN.	JD/TF	CKD.	GD	DATE OF INVEST.	Nov. 28, 1982	JOB NO.	CG 10047	HOLE NO.	B-10		
WATER CONTENT				SOIL SYMBOL	SOIL DESCRIPTION		SOIL SAMPLE		DRILL TYPE		
Wp - □ W - ○ W _L - Δ					DATUM		CONDITION	TYPE	PENETRATION RESISTANCE		
PERCENT %					SURFACE ELEVATION						
10	20	30	40	50	60	DEPTH m			OTHER TESTS		
						1		GRAVEL some silty sand, frozen		A1	
						2		Bottom of Hole at 1.0m Refusal in frozen gravel			

Plate A-35



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BOREHOLE LOG

PROJECT BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN.	JD/TF	CKD.	GD	DATE OF INVEST.	Nov. 28, 1982	JOB NO.	CG 10047	HOLE NO.	B-11	
WATER CONTENT				SOIL DESCRIPTION			SOIL SAMPLE		DRILL TYPE	
Wp - □ W - ○ W_L - △				DATUM			CONDITION	TYPE	PENETRATION RESISTANCE	
PERCENT %				SURFACE ELEVATION						
10	20	30	40	50	60					
							1	A1	Grain size (see Pl. B-17)	
										2
										3
										4
										5
										6
--- coarse gravel						A2				
Bottom of Hole at 6.0m										
Plate A-36										



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PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN. JD/TF CKD. GD DATE OF INVEST. Nov. 28, 1982 JOB NO. CG 10047 HOLE NO. B-12

WATER CONTENT			DEPTH m	SOIL SYMBOL	SOIL DESCRIPTION	SOIL SAMPLE			DRILL TYPE
Wp - □	W - O	W _L - Δ				CONDITION	TYPE	PENETRATION RESISTANCE	OTHER TESTS
PERCENT %					DATUM				
10 20 30 40 50 60					SURFACE ELEVATION				
			1		GRAVEL occasional cobbles, some silty sand, frozen	⊗	A1		
			2		--- medium gravel, to 25mm Ø, unfrozen, poorly graded				
			3		--- gravel to 25mm Ø	⊗	A2		
			4						
			5						
			6		--- more coarse sand	⊗	A3		
					Bottom of Hole at 6.0m				

Plate A-37



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BURWASH LANDING - DESTRUCTION BAY

GRAVEL STUDY

MP 1095.1

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 28, 1982

JOB NO. CG 10047

HOLE NO. B-13

WATER CONTENT

Wp - □ W - ○ W_L - Δ

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

DATUM

CONDITION

TYPE

PENETRATION
RESISTANCE

OTHER TESTS

SURFACE ELEVATION

FILL gravel, coarse

SILT organic, sandy,
dark brown

GRAVEL coarse, subangular,
clean

--- coarse, poorly graded

--- more coarse sand

Bottom of Hole at 6.0m

⊗ A1

⊗ A2

Grain size
(see Pl. B-18)

Plate A-38



PROJECT BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 28, 1982

JOB NO. CG 10047

HOLE NO. R-14

WATER CONTENT

$W_p - \square$ $W - \bigcirc$ $W_L - \Delta$

PERCENT %

10 20 30 40 50 60

DEPTH

SOIL SYMBOL

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SAND silty, some gravel, brown,
frozen, (Fill?)

GRAVEL to 65mm, angular, some
silty sand, unfrozen

-- coarse, subangular to
subrounded, poorly graded

-- sandy, coarse, dark brown

Bottom of Hole at 6.0m

SOIL SAMPLE

CONCLUSION

TYPE

CONCLUSION

RESEARCH

DRILL TYPE

Rotary

OTHER TESTS

Petrographic Analysis
(Table B-5) -
L.A. Abrasion
(Pl. B-19) -
Sulphate -
Soundness
(Pl. B-20)

Plate A-39



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BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 28, 1982

JOB NO. CG 10047

HOLE NO. B-15

WATER CONTENT

Wp - □ W - O W_L - Δ

PERCENT %

10 20 30 40 50 60

DEPTH

m

SOIL SYMBOL

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SOIL SAMPLE

CONDITION

TYPE

PENETRATION
RESISTANCE

DRILL TYPE

Rotary

OTHER TESTS

1

2

3

4

5

6

GRAVEL to 65mm, subangular,
some silty sand

--- coarse, poorly graded

--- frozen

Bottom of Hole at 6.0m

⊗ A1

⊗ A2

Plate A-40



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BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 28, 1982

JOB NO. CG 10047

HOLE NO. B-16

WATER CONTENT

W_p - □ W - ○ W_L - △

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

SOIL SAMPLE

DRILL TYPE

Rotary

OTHER TESTS

DATUM

SURFACE ELEVATION

CONDITION

TYPE

PENETRATION
RESISTANCE

TOPSOIL dark brown, some
volcanic ash

GRAVEL coarse, sandy, poorly
graded

1

2

--- coarse, poorly graded, trace
sand

3

4

--- finer gravel 25mm, frozen

5

--- cobbles

6

Bottom of Hole at 5.2m
Refusal on frozen cobbles

⊗ A1

⊗ A2

Grain size
(see Pl. B-21)

Plate A-41



HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY

MP 1095.1

LOGGED/DWN.	JD/TF	CKD.	GD	DATE OF INVEST.	Nov. 28, 1982	JOB NO.	CG 10047	HOLE NO.	B-17
WATER CONTENT				SOIL DESCRIPTION			SOIL SAMPLE		DRILL TYPE
Wp - □ W - ○ W _L - △				DATUM			CONDITION	TYPE	PENETRATION RESISTANCE
PERCENT %				SURFACE ELEVATION					
10	20	30	40	50	60	DEPTH m	SOIL SYMBOL	OTHER TESTS	
						1	X	TOPSOIL organic	
						2		SILT sandy, brown, some organics	
						3	X	A1	
						4		A2	
								--- frozen	
								Bottom of Hole at 3.0m Refusal on permafrost	

Plate A-42



HARDY ASSOCIATES (1978) LTD.
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BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY

GRAVEL STUDY

MP 1095.1

LOGGED/DWN. JD/TF

CKD. GD

DATE OF INVEST. Nov. 28, 1982

JOB NO. CG 10047

HOLE NO. B-18

WATER CONTENT

Wp - □ W - ○ WL - △

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SOIL SAMPLE

CONDITION

TYPE

PENETRATION
RESISTANCE

DRILL TYPE

Rotary

OTHER TESTS

GRAVEL coarse, little
sand, brown, unfrozen

1

2

3

4

5

6

---coarse, poorly graded, trace
sand

--- more sand

⊗ A1

⊗ A2

⊗ A3

Grain size
(see Pl. B-22)

Bottom of Hole at 6.0m

Plate A-43



HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

BOREHOLE LOG

PROJECT

BURWASH LANDING - DESTRUCTION BAY

GRAVEL STUDY

MP 1095.1

LOGGED/DWN. JD/TF

CKD. GD

DATE OF INVEST. Nov. 28, 1982

JOB NO. CG 10047

HOLE NO. B-19

WATER CONTENT

Wp - □ W - O W_L - Δ

PERCENT %

10 20 30 40 50 60

DEPTH
m

SOIL SYMBOL

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SOIL SAMPLE

CONDITION

TYPE

PENETRATION
RESISTANCE

DRILL TYPE

Rotary

OTHER TESTS

1

SILT organic, sandy, reddish-brown

2

SAND trace silt and fine gravel, frozen

A1

3

grey clay mixed with sand

4

GRAVEL some silty sand, frozen

5

Bottom of Hole at 4.0m
Refusal on frozen ground

Plate A-44



PROJECT

BURWASH LANDING - DESTRUCTION BAY
GRAVEL STUDY MD 10

MP 2095.1

LOGGED/DWN.

JD/TF

CKD.

GD

DATE OF INVEST. Nov. 28, 1982

JOB NO. CG 10047

HOLE NO. B-20

WATER CONTENT

Wp - □

W-O

$$W_1 = \Delta$$

PERCENT %

10 20 30 40 50 60

DEPTH

附

SOIL DESCRIPTION

DATUM

SURFACE ELEVATION

SILT organic, sandy, some
volcanic ash, reddish-brown,
frozen

GRAVEL coarse, rounded, some
silty sand, frozen

1

2

3

Bottom of Hole at 3.0m
Refusal on coarse, frozen gravel

SOIL SAMPLE

CONCLUSION

TYPE

PENETRATION

A1

A2

DRILL TYPE

Rotary

OTHER TESTS

Grain size
(see Pl. B-23)

Plate A-45



HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

APPENDIX "B"
LABORATORY TEST RESULTS



APPENDIX "B"
LABORATORY TEST RESULTS

B.1 GRAIN SIZE ANALYSIS (ASTM C136-82)

Sieve analysis of aggregate samples provides a gradation for the bulk natural material, which may be compared with ideal curves for concrete aggregate, asphalt, etc.

B.2 LOS ANGELES ABRASION TEST (ASTM C535-81)

This test provides information on the hardness and roughness of an aggregate. A definite relationship exists between the strength of concrete and the quality of its constituent coarse aggregate, as measured by the Los Angeles Abrasion test. For most applications, a loss of less than 30 percent after 50 revolutions, is considered to indicate a good quality aggregate.

B.3 SULPHATE SOUNDNESS TEST (ASTM C88-76)

This test provides an indication of any structural weakness that may be present in the aggregate. A general relationship exists between the percentage weight loss in the test with the compressive strength and freezing and thawing durability of concrete made from the aggregate. In general, coarse aggregate is considered acceptable if the weighted loss is less than 12 percent, after 5 cycles.



B.4

PETROGRAPHIC ANALYSIS (ASTM C-295)

Petrographic analysis consists of a visual examination of aggregate particles and identification on the basis of mineralogy. Particles are assigned a rating on the basis of the known soundness or deleterious nature of the mineral type, a rating of 1 being the best and 10 being the worst. The weighted percentage of each mineral type is then multiplied by this rating number to produce a petrographic number (PN) for the aggregate. The following classification, recommendation by Ontario Hydro petrographers, is used in this report.

<u>PN</u>	<u>RATING</u>
100-110	Excellent
111-125	Good
126-140	Fair
141-155	Poor
155	Unsuitable

TABLE NO. B-1

SUMMARY OF ROCK TYPES COARSE FRACTION

M.P. 1087.6 Borehole A-2 Depth 5.8 m - 6.0 m

ROCK TYPE	CLASSIFICATION	WEIGHTED PERCENTAGES OF CONSTITUENTS IN EACH SIEVE FRACTION									Total Weighted Composition
		4"	3"	2"	1½"	1"	¾"	½"	3/8"	#4	
Plutonics-acid	Good					1.1	1.7	2.5	1.0	3.2	9.5
Greenstone-ultra basic					3.0	1.6	4.0	8.4	4.8	11.8	33.6
Carbonates							1.1	1.1	0.6	1.7	4.5
Metamorphics						2.6	4.0	11.2	12.3	22.2	52.3
Volcanics	Fair									0.1	0.1
					3.0	5.3	10.8	23.2	18.7	39.0	100.0

PN = 100.2

TABLE NO. B-2

SUMMARY OF ROCK TYPES COARSE FRACTION

M.P. 1087.6 Borehole A-4 Depth 3.0 m - 3.3 m

ROCK TYPE	CLASSIFICATION	WEIGHTED PERCENTAGES OF CONSTITUENTS IN EACH SIEVE FRACTION									Total Weighted Composition
		4"	3"	2"	1½"	1"	3/4"	½"	3/8"	#4	
Plutonics-acid	Good				2.4	3.4	3.9	3.9	3.1	4.5	21.2
Greenstone-ultra basic					3.6	2.2	5.2	9.5	5.6	7.8	33.9
Carbonates						1.1	0.8	1.4	0.4	1.0	4.7
Metamorphics					1.2	3.4	5.2	7.8	9.2	13.3	40.1
Carbonates (weathered, soft)	Fair							0.1			0.1
					7.2	10.1	15.1	22.7	18.3	26.6	100.0

PN = 100.2

TABLE NO. B-3

SUMMARY OF ROCK TYPES COARSE FRACTION

M.P. 1095.1 Borehole B-4 Depth 5.5 m - 5.8 m

ROCK TYPE	CLASSIFICATION	WEIGHTED PERCENTAGES OF CONSTITUENTS IN EACH SIEVE FRACTION									Total Weighted Composition
		4"	3"	2"	1½"	1"	¾"	½"	3/8"	#4	
Plutonics-acid	Good				1.5	3.4	4.3	3.5	4.6	4.1	21.4
Greenstone-ultra basic					1.5	3.6	3.8	3.3	2.9	2.6	17.7
Carbonates						1.2	1.7	1.8	0.8	0.9	6.4
Metamorphics					2.2	9.1	9.9	15.5	7.5	6.9	51.1
Volcanics	Fair						0.6	1.6	0.2	0.1	2.5
Carbonates (weathered, soft)							0.1	0.3			0.4
	Poor										
Volcanics (weathered, soft)							0.1	0.4			0.5
					5.2	17.3	20.5	26.4	16.0	14.6	100.0

PN = 108.3

TABLE NO. B-4

SUMMARY OF ROCK TYPES COARSE FRACTION

M.P. 1095.1 Borehole B-9 Depth 2.8 m - 3.0 m

ROCK TYPE	CLASSIFICATION	WEIGHTED PERCENTAGES OF CONSTITUENTS IN EACH SIEVE FRACTION									Total Weighted Composition
		4"	3"	2"	1½"	1"	3/4"	½"	3/8"	#4	
Plutonics-acid	Good				1.9	0.9	3.4	4.6	4.3	4.8	19.9
Quartzite						0.9					0.9
Greenstone-ultra basic						3.2	2.9	4.8	2.6	4.6	18.1
Carbonates					0.9	0.9	1.5	2.5	1.1	1.4	8.3
Metamorphics					0.9	4.6	5.0	12.5	9.6	14.2	46.8
Volcanics	Fair					0.9	1.2	1.0	0.8	0.7	4.6
Volcanics (slightly weathered, soft, friable)	Poor							0.6	0.3	0.5	1.4
					3.7	11.4	14.0	26.0	18.7	26.2	100.0

PN = 116.2



HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

GRAIN SIZE CURVE

PROJECT NO. CG 10047

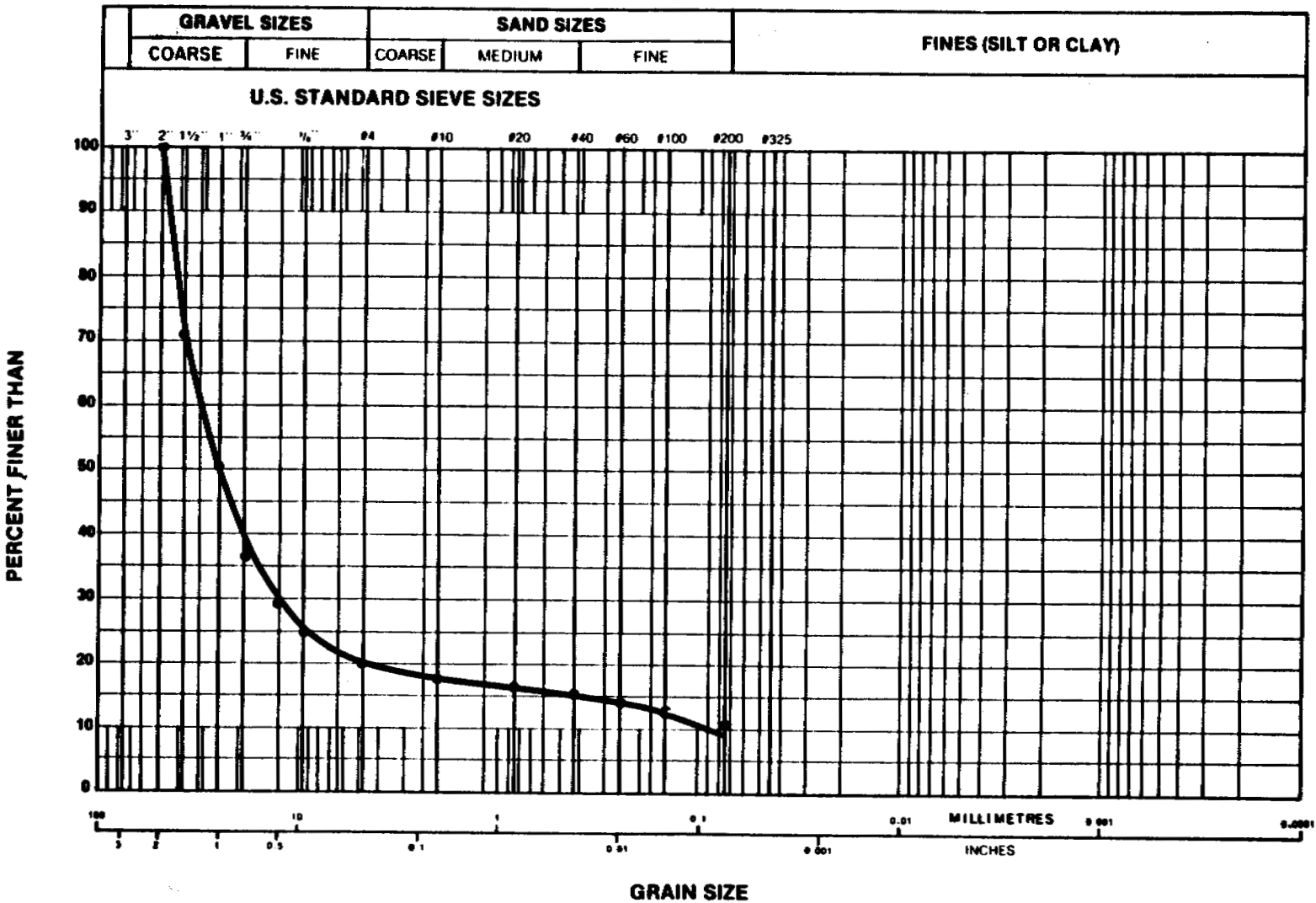
CLIENT

BOREHOLE C1 MP 1086.2

SAMPLE A1

DEPTH (m) 1.0 - 1.5

TECHNICIAN SK DATE TESTED 82.12.21



D_{10} = _____ mm.
 D_{30} = _____ mm.
 D_{60} = _____ mm.
 C_u = _____
 C_c = _____

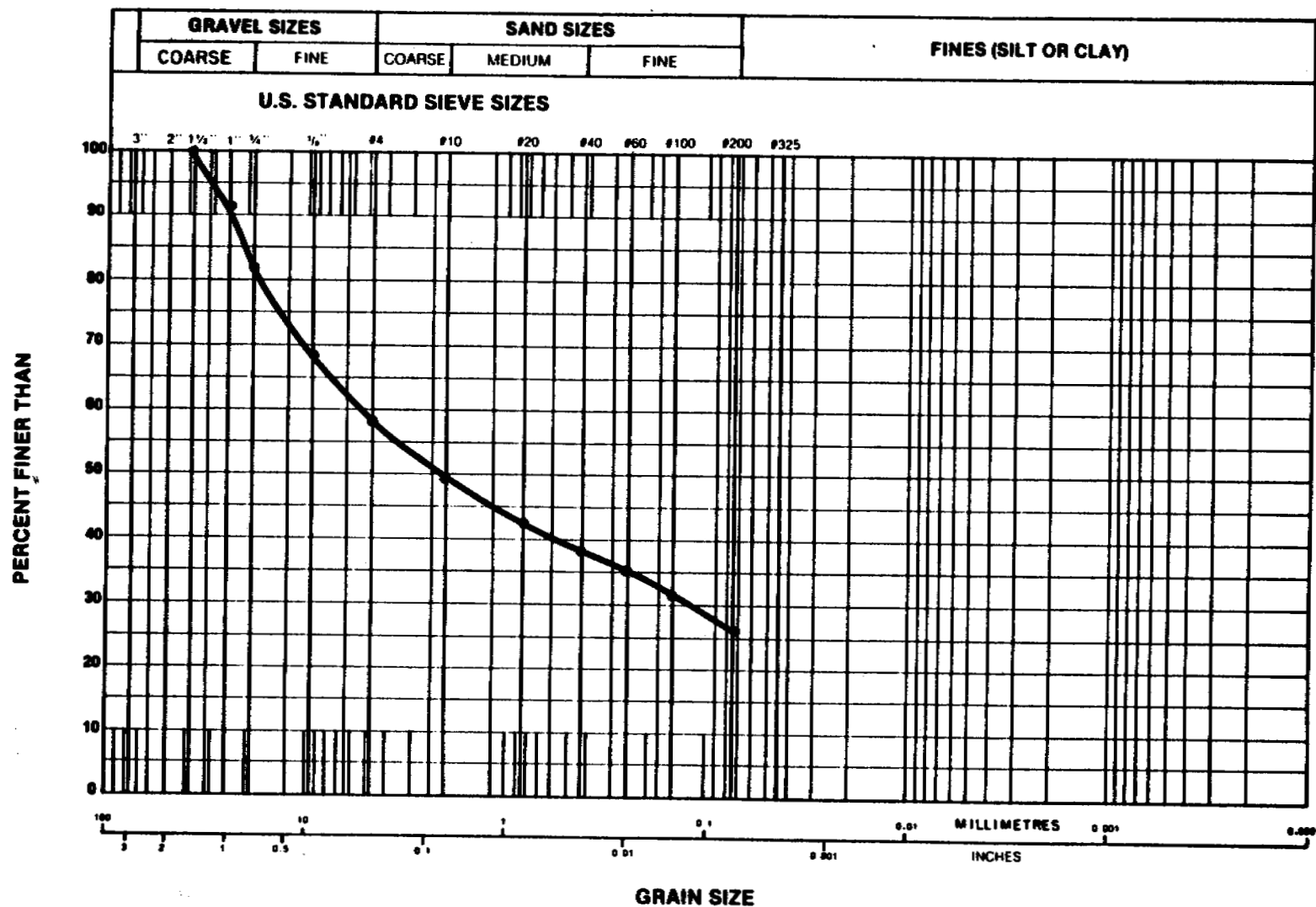
GRAVEL	79.0 %	SAND	10.0 %	FINES	11.0 %	SOIL GROUP	GM
--------	--------	------	--------	-------	--------	------------	----

NOTE: UNIFIED SOIL CLASSIFICATION SYSTEM



HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

GRAIN SIZE CURVE



GRAVEL	42.0%	SAND	32.0 %	FINES	26.0 %	SOIL GROUP	GM
--------	-------	------	--------	-------	--------	------------	----

NOTE: UNIFIED SOIL CLASSIFICATION SYSTEM

D₁₀ = _____ mm.
D₃₀ = _____ mm.
D₆₀ = _____ mm.
C_u = _____
C_c = _____

PROJECT NO. CG 10047

CLIENT

BOREHOLE C2 MP 1086.2

SAMPLE A1

DEPTH (m) 1.0 - 1.5

TECHNICIAN AB DATE TESTED 82.12.15



HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

GRAIN SIZE CURVE

PROJECT NO. CG 10047

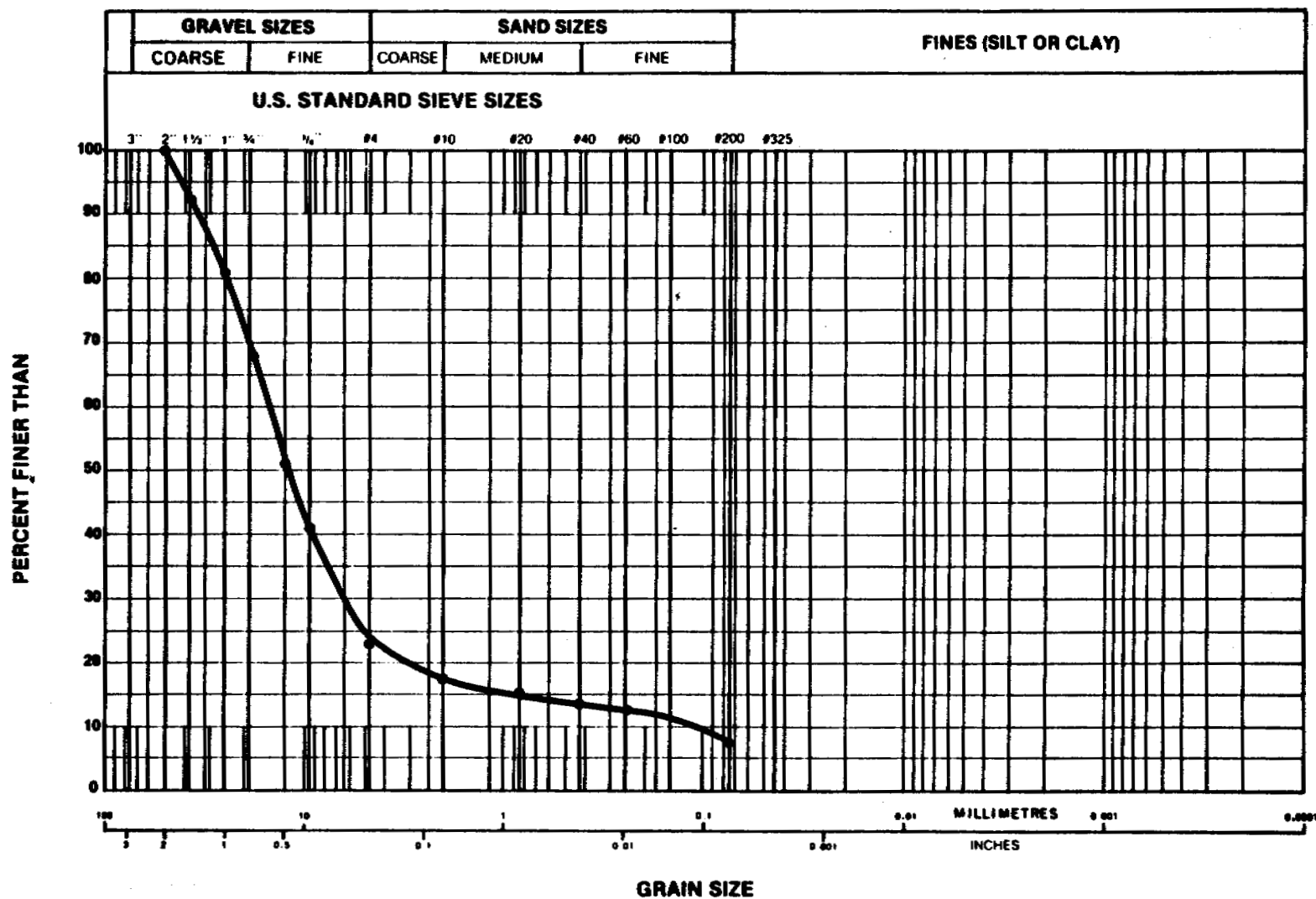
CLIENT

BOREHOLE C4 MP 1086.2

SAMPLE A2

DEPTH (m) 3.5 - 4.0

TECHNICIAN AB DATE TESTED 82.12.17



D_{10} = _____ mm.
 D_{30} = _____ mm.
 D_{60} = _____ mm.
 C_u = _____
 C_c = _____

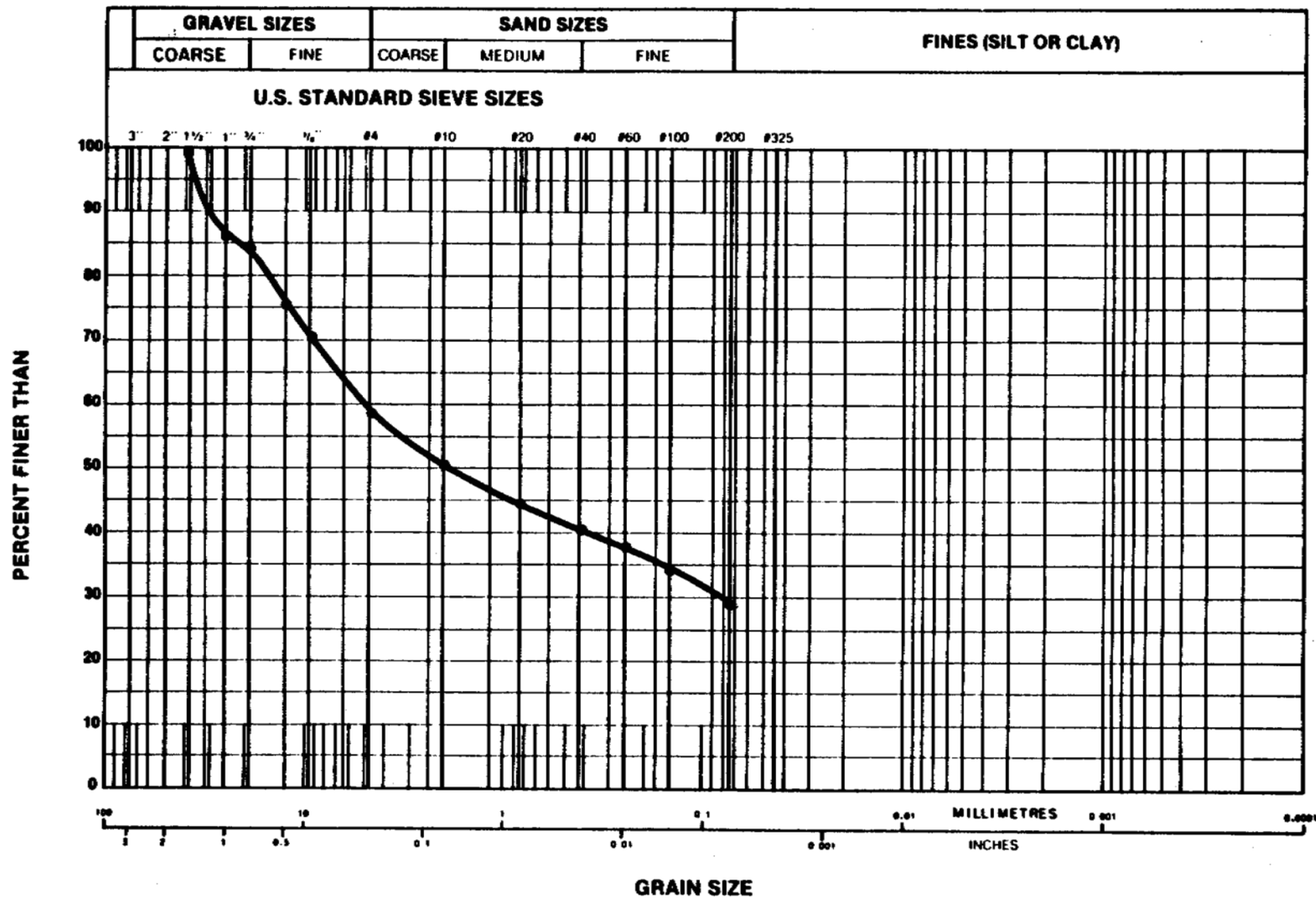
GRAVEL	77.0 %	SAND	16.0 %	FINES	7.0 %	SOIL GROUP	GM
--------	--------	------	--------	-------	-------	------------	----

NOTE: UNIFIED SOIL CLASSIFICATION SYSTEM



HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

GRAIN SIZE CURVE



GRAVEL	42.0 %	SAND	29.0 %	FINES	29.0 %	SOIL GROUP
--------	--------	------	--------	-------	--------	------------

NOTE: UNIFIED SOIL CLASSIFICATION SYSTEM

D_{10} = _____ mm.
 D_{30} = _____ mm.
 D_{60} = _____ mm.
 C_u = _____
 C_c = _____

PROJECT NO. CG 10047

CLIENT

BOREHOLE C5 MP 1086.2

SAMPLE A2

DEPTH (m) 5.5 - 6.0

TECHNICIAN AB

DATE TESTED 82.12.16



HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

GRAIN SIZE CURVE

PROJECT NO. CG 10047

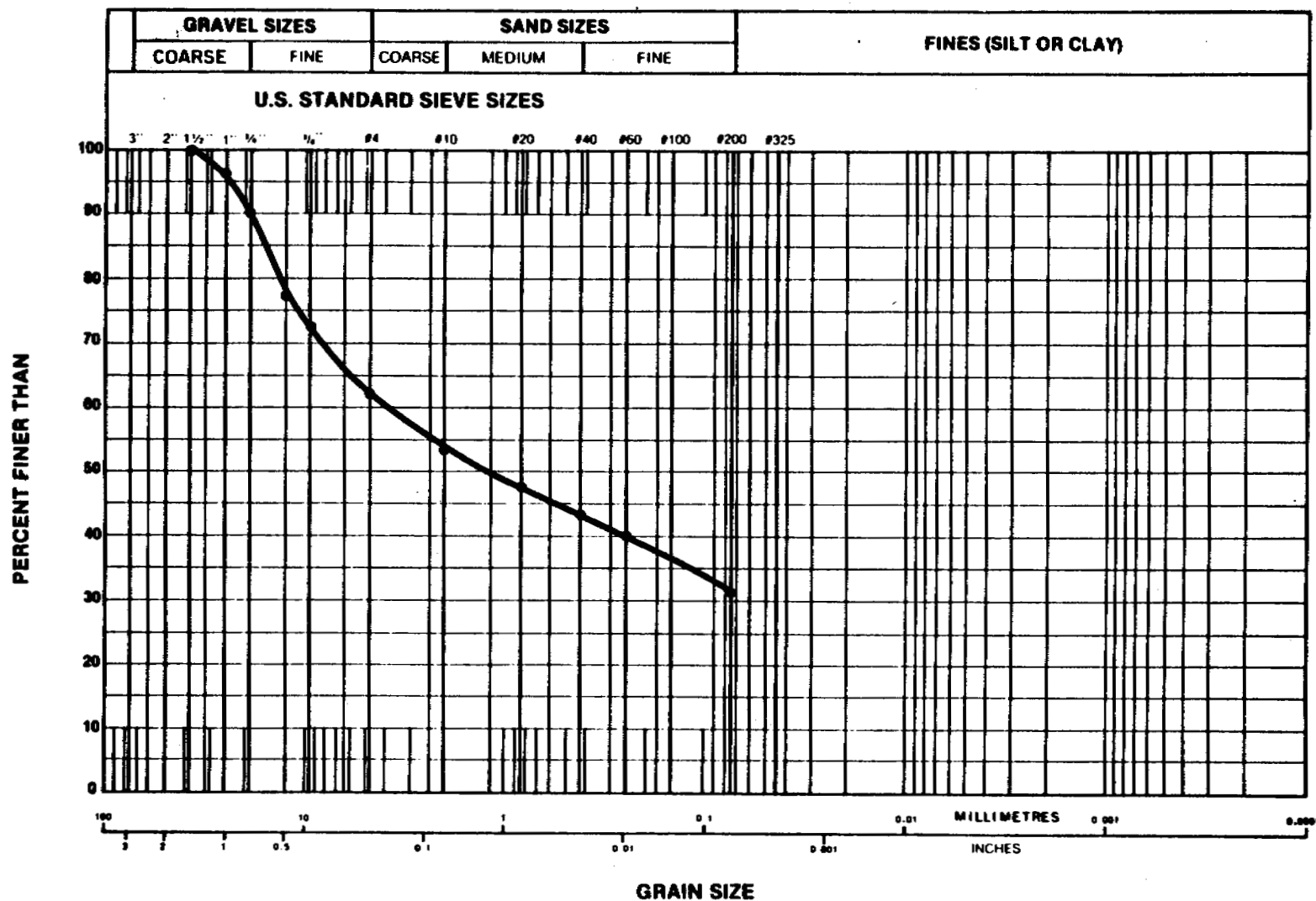
CLIENT

BOREHOLE C6 MP 1086.2

SAMPLE A1

DEPTH (m) 4.0 - 4.5

TECHNICIAN AB DATE TESTED 82.12.15



D_{10} = _____ mm.
 D_{30} = _____ mm.
 D_{60} = _____ mm.
 C_u = _____
 C_c = _____

GRAVEL	38.0 %	SAND	31.0 %	FINES	31.0 %	SOIL GROUP
--------	--------	------	--------	-------	--------	------------

NOTE: UNIFIED SOIL CLASSIFICATION SYSTEM



HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

**LOS ANGELES ABRASION
TEST REPORT**

TO: Mr. G. Dupuy, P. Eng.,
Hardy Associates (1978) Ltd.,
221 - 18 Street S.E.,
CALGARY, Alberta.
T2E 6J5

OFFICE Calgary
FILE 4195-CG-10047
DATE January 31, 1983
CLIENT P.O.
C.C.

PROJECT: Burwash/Destruction Bay Gravel Samples

TH A-4, MP 1087.6
3.0 - 3.3 m Pit Run
SOURCE TYPE OF SAMPLE Material
DATE SAMPLED Dec./82 DATE RECEIVED Dec. 16/82 SAMPLED BY Client
DATE TESTED Jan. 27/83

MATERIAL GRADING: 'A'			
ACTUAL SIEVE SIZES		AMOUNT	
—	1 1/2" + 1"	1250.0	g
—	1" + 3/4"	1251.0	g
—	3/4" + 1/2"	1249.7	g
—	1/2" + 3/8"	1249.5	g
		TOTAL SAMPLE	5000.2 g
NO. OF REVOLUTIONS 500			
NO. OF SPHERES 12		TOTAL SAMPLE	5000.2 g
WT. OF SPHERES 4988.1 g		+ # 12 MATERIAL AFTER	4328.9 g
		- # 12 MATERIAL AFTER	671.3 g
LOSS = $\frac{5000.2 - 4328.9}{5000.2} \times 100 = 13.4\%$			

COMMENTS: Test performed in accordance with A.S.T.M. C-131

REPORT CERTIFIED

TECHNICIAN E.K.

PLATE B-6

BURNABY • CALGARY • DAWSON CREEK • EDMONTON • LETHBRIDGE • PRINCE GEORGE • RED DEER • WINNIPEG

HT53 79/1

**HARDY ASSOCIATES (1978) LTD.**

CONSULTING ENGINEERING & PROFESSIONAL SERVICES

SOUNDNESS OF AGGREGATE**SULPHATE TEST REPORT**

TO: Mr. G. Dupuy, P. Eng.,
Hardy Associates (1978) Ltd.,
Geotechnical Division,
221 - 18 Street S.E.,
CALGARY, Alberta.
T2E 6J5

FILE: 4195-CG-10047
DATE: February 7, 1983
CLIENT P.O.: -
C.C.: -

PROJECT BURWASH LANDING/DESTRUCTION BAY COMMUNITY GRAVEL STUDY

TH A4, MP.10876 Pit Run
SOURCE 3.0-3.3 Material
DATE SAMPLED Dec./82 DATE RECEIVED Dec. 16/82
SAMPLED BY Client
DATE TESTED Jan. 31/83

SOLUTION Magnesium Sulphate				NUMBER OF CYCLES 5			
COARSE AGGREGATE				FINE AGGREGATE			
SIEVE SIZE		ORIGINAL GRADING PERCENT	Weighted AVERAGE PERCENT LOSS	SIEVE SIZE		ORIGINAL GRADING PERCENT	WEIGHED AVERAGE PERCENT LOSS
PASSING	RETAINED			PASSING	RETAINED		
3 IN.	2 IN.			3/8 IN.	NO. 4		
2 IN.	1 - 1/2 IN.	7.2	-	NO. 4	NO. 8		-
1 - 1/2 IN.	1 IN.	10.1	0.03	NO. 8	NO. 16		-
1 IN.	3/4 IN.	15.1	0.01	NO. 16	NO. 30		-
3/4 IN.	1/2 IN.	22.7	0.09	NO. 30	NO. 50		-
1/2 IN.	3/8 IN.	18.3	0.04	NO. 50	NO. 100		-
3/8 IN.	NO. 4 IN.	26.6	0.16	NO. 100			-
TOTALS		100.0	0.33	TOTALS		-	-

SIZE FRACTION	NO. PARTICLES	QUALITATIVE EXAMINATION OF PLUS 3/4" MATERIAL	
3" - 2"	ORIGINAL		
	FINAL		
2" - 1 1/2"	ORIGINAL		
	FINAL		
1 1/2" - 1"	ORIGINAL 12	Some pit holes were observed.	
	FINAL 12	Some pit holes, and cracking was observed.	
1" - 3/4"	ORIGINAL 40	Some pit holes were observed.	
	FINAL 40	Some pit holes were observed.	

COMMENTS:



REPORT CERTIFIED

TECHNICIAN R.L.D.

TESTED
IN ACCORDANCE
WITH ASTM C88

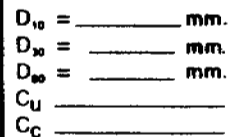
219 BURNABY 18 CALGARY STREET DAWSON CREEK SE CALGARY EDMONTON ALBERTA GRANDE PRAIRIE T2E 6J5 LETHBRIDGE (403) 272-8761 PRINCE GEORGE TWX RED DEER 610-821-1388 WINNIPEG

MT42 - 11/79

PLATE B-7



PROJECT NO.	CG 10047
CLIENT	
BOREHOLE SAMPLE	A-6 MP 1087.6 A1
DEPTH (m)	1.5 - 1.5
TECHNICIAN	AB DATE TESTED 82.12.16



GRAVEL	91.0 %	SAND	4.5 %	FINES	5.5 %	SOIL GROUP	GP
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NOTE: UNIFIED SOIL CLASSIFICATION SYSTEM



HANDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

GRAIN SIZE CURVE

PROJECT NO. CG 10047

CLIENT

BOREHOLE A-10 MP 1087.6

SAMPLE A1

DEPTH (m) 1.5 - 2.0

TECHNICIAN AB

DATE TESTED 82.12.17

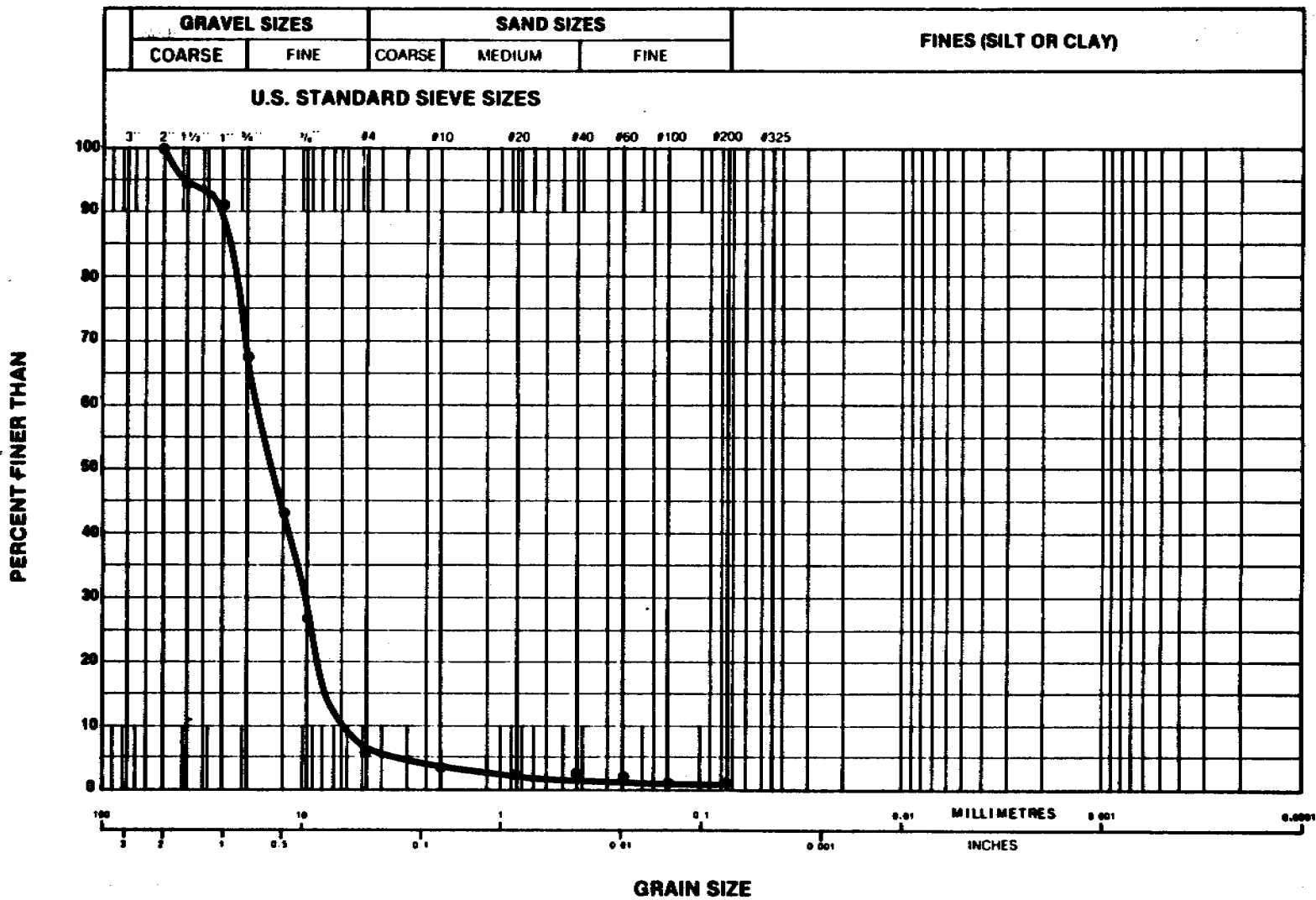


TABLE NO. B-5

SUMMARY OF ROCK TYPES COARSE FRACTION

M.P. 1095.1 Borehole B-14 Depth 4.0 m - 4.2 m

ROCK TYPE	CLASSIFICATION	WEIGHTED PERCENTAGES OF CONSTITUENTS IN EACH SIEVE FRACTION									Total Weighted Composition
		4"	3"	2"	1½"	1"	¾"	½"	3/8"	#4	
Plutonic-acid	Good				1.3	4.4	6.1	6.8	4.7	6.7	30.0
Greenstone-ultra basic					2.8	1.0	1.4	2.9	2.4	3.3	13.8
Carbonates						1.0	1.8	1.6	1.1	1.3	6.8
Metamorphics					2.8	4.8	7.8	10.1	7.6	12.7	45.8
Volcanics	Fair					0.4	0.5	0.8	0.3	0.1	2.1
Volcanics (weathered, soft)	Poor						0.1	0.6	0.3	0.5	1.5
					6.9	11.6	17.7	22.8	16.4	24.6	100.0



HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

GRAIN SIZE CURVE

PROJECT NO. CG 10047

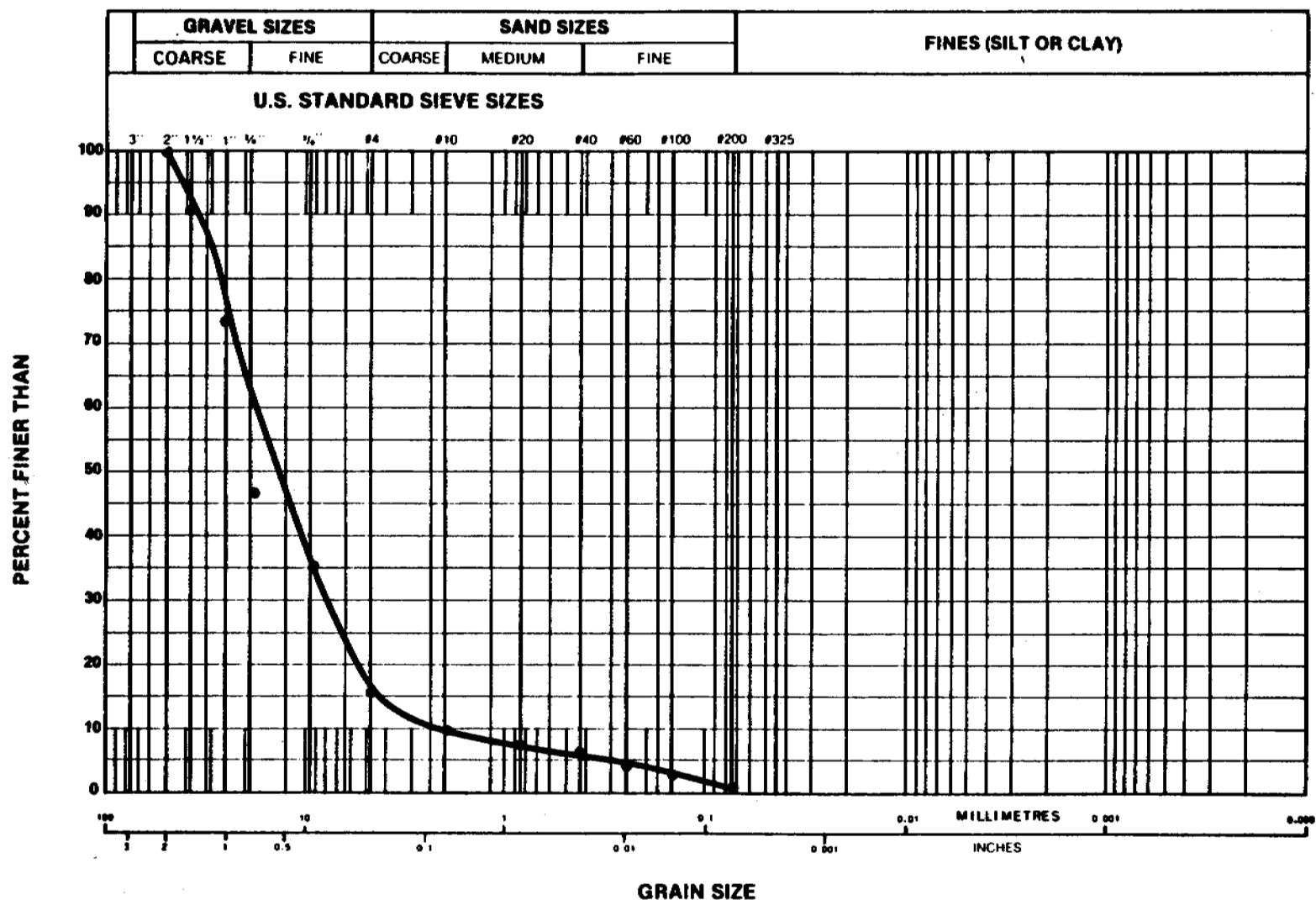
CLIENT

BOREHOLE B2 MP 1095.1

SAMPLE A1

DEPTH (m) 1.5 - 2.0

TECHNICIAN AB DATE TESTED 82.12.



D_{10} = _____ mm.
 D_{30} = _____ mm.
 D_{60} = _____ mm.
 C_u = _____
 C_c = _____

GRAVEL	85.0 %	SAND	13.0 %	FINES	2.0 %	SOIL GROUP	GP
--------	--------	------	--------	-------	-------	------------	----

NOTE: UNIFIED SOIL CLASSIFICATION SYSTEM



HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

**LOS ANGELES ABRASION
TEST REPORT**

TO: Mr. G. Dupuy, P. Eng.,
Hardy Associates (1978) Ltd.,
221 - 18 Street S.E.,
CALGARY, Alberta.
T2E 6J5

OFFICE Calgary
FILE 4195-CG-10047
DATE January 27, 1983
CLIENT P.O.
C.C.

PROJECT: BURWASH LANDING/DESTRUCTION BAY COMMUNITY GRAVEL STUDY

TH B4 MP 1095.1 Pit Run
SOURCE 5.5 - 5.8 m MATERIAL
DATE SAMPLED Dec./82 DATE RECEIVED Dec. 16/82 SAMPLED BY Client
DATE TESTED Jan. 27/83

MATERIAL GRADING: 'A'			
ACTUAL SIEVE SIZES		AMOUNT	
—	1 1/2" + 1"	1249.5	g
—	1" + 3/4"	1250.7	g
—	3/4" + 1/2"	1250.8	g
—	1/2" + 3/8"	1249.2	g
		TOTAL SAMPLE	5000.2 g
NO. OF REVOLUTIONS 500			
NO. OF SPHERES 12		TOTAL SAMPLE	5000.2 g
WT. OF SPHERES 4987.8 g		+ # 12 MATERIAL AFTER	4076.3 g
		- # 12 MATERIAL AFTER	923.9 g
$\text{LOSS} = \frac{5000.2 - 923.9}{5000.2} \times 100 = 18.5\%$			

COMMENTS: Test performed in accordance with A.S.T.M. C-131

REPORT CERTIFIED

TECHNICIAN E.K.

PLATE B-12

BURNABY • CALGARY • DAWSON CREEK • EDMONTON • LETHBRIDGE • PRINCE GEORGE • RED DEER • WINNIPEG

UMC 70/1

**HARDY ASSOCIATES (1978) LTD.**

CONSULTING ENGINEERING & PROFESSIONAL SERVICES

**SOUNDNESS OF AGGREGATE
SULPHATE TEST REPORT**

TO: Mr. G. Dupuy, P. Eng.,
Hardy Associates (1978) Ltd.,
Geotechnical Division,
221 - 18 Street S.E.,
CALGARY, Alberta.
T2E 6J5

FILE: 4195-CG-10047
DATE: February 7, 1983
CLIENT P.O.: -
C.C.: -

PROJECT BURWASH LANDING/DESTRUCTION BAY COMMUNITY GRAVEL STUDY

TH B4, MP.1095.1 Pit Run
SOURCE 5.5-5.8 m TYPE OF SAMPLE Material SAMPLED BY Client
DATE SAMPLED Dec./82 DATE RECEIVED Dec. 16/82 DATE TESTED Jan. 31/83

SOLUTION Magnesium Sulphate				NUMBER OF CYCLES 5			
COARSE AGGREGATE				FINE AGGREGATE			
SIEVE SIZE		ORIGINAL GRADING PERCENT	Weighted AVERAGE PERCENT LOSS	SIEVE SIZE		ORIGINAL GRADING PERCENT	WEIGHED AVERAGE PERCENT LOSS
PASSING	RETAINED			PASSING	RETAINED		
3 IN.	2 IN.			3/8 IN.	NO. 4		
2 IN.	1 - 1/2 IN.	5.2	-	NO. 4	NO. 8		-
1 - 1/2 IN.	1 IN.	17.3	0.02	NO. 8	NO. 16		-
1 IN.	3/4 IN.	20.5	0.01	NO. 16	NO. 30		-
3/4 IN.	1/2 IN.	26.4	0.41	NO. 30	NO. 50		-
1/2 IN.	3/8 IN.	16.0	0.15	NO. 50	NO. 100		-
3/8 IN.	NO. 4 IN.	14.6	0.12	NO. 100			-
TOTALS		100.0	0.71	TOTALS		-	-

SIZE FRACTION	NO. PARTICLES	QUALITATIVE EXAMINATION OF PLUS 3/4" MATERIAL	
3" - 2"	ORIGINAL		
	FINAL		
2" - 1 1/2"	ORIGINAL		
	FINAL		
1 1/2" - 1"	ORIGINAL 22	Some cracks and pit holes were observed.	
	FINAL 22	Some cracks and splitting was observed.	
1" - 3/4"	ORIGINAL 39	Some pit holes were observed.	
	FINAL 39	Some cracks were observed.	

COMMENTS:



REPORT CERTIFIED

J. W. Dillingham, C.E.T.

TECHNICIAN

R.L.D.

TESTED
IN ACCORDANCE
WITH ASTM C88

219 BURNABY 18 CALGARY 18 STREET, S.E. DAWSON CREEK CALGARY, EDMONTON ALBERTA. T2E 6J5 (403) 272-8761 PRINCE GEORGE TWX RED DEER 610-821-1388 WINNIPEG

HT42 - 11/78

PLATE B-13

**HARDY ASSOCIATES (1978) LTD.**

CONSULTING ENGINEERING & PROFESSIONAL SERVICES

**LOS ANGELES ABRASION
TEST REPORT**

OFFICE Calgary
 FILE 4195-CG-10047
 DATE January 31, 1983
 CLIENT P.O.
 C.C.

TO: Mr. G. Dupuy, P. Eng.,
 Hardy Associates (1978) Ltd.,
 Geotechnical Division,
 221 - 18 Street S.E.,
 CALGARY, Alberta.
 T2E 6J5

PROJECT: BURWASH LANDING/DESTRUCTION BAY COMMUNITY GRAVEL STUDY

TH B-1, MP 1095.1, 5.0-5.5 m

TH B-9

Pit Run

SOURCE 2.8 - 3.0 m

TYPE OF SAMPLE Material

SAMPLED BY Client

DATE SAMPLED Dec./82

DATE RECEIVED Dec. 16/82

DATE TESTED Jan. 27/83

MATERIAL GRADING: 'A'

ACTUAL SIEVE SIZES		AMOUNT	
—	1 1/2" + 1"	1252.0	9
—	1" + 3/4"	1249.2	9
—	3/4" + 1/2"	1249.0	9
—	1/2" + 3/8"	1250.4	9
		TOTAL SAMPLE	5000.6
NO. OF REVOLUTIONS		500	
NO. OF SPHERES		12	
WT. OF SPHERES		4987.8	9
		+ # 12 MATERIAL AFTER	4054.4
		- # 12 MATERIAL AFTER	946.2
LOSS = $\frac{5000.6 - 946.2}{5000.6} \times 100 = 18.9\%$			

COMMENTS:

Test performed in accordance with A.S.T.M. C-131
 TH B-1 and TH B-9 materials were combined to make up
 L.A. Abrasion Sample.

REPORT CERTIFIED

TECHNICIAN E.K.

PLATE B-15

**HARDY ASSOCIATES (1978) LTD.**

CONSULTING ENGINEERING & PROFESSIONAL SERVICES

SOUNDNESS OF AGGREGATE**SULPHATE TEST REPORT**

TO: Mr. G. Dupuy, P. Eng.,
Hardy Associates (1978) Ltd.,
Geotechnical Division,
221 - 18 Street S.E.,
CALGARY, Alberta.
T2E 6J5

FILE: 4195-CG-10047
DATE: February 7, 1983
CLIENT P.O.: -
C.C.: -

PROJECT BURWASH LANDING/DESTRUCTION BAY COMMUNITY GRAVEL STUDY

TH B1, MP.1095.1 5.0-5.5m
TH B9, MP.1095.1 Pit Run

SOURCE 2.8 - 3.0 m TYPE OF SAMPLE Material SAMPLED BY Client
DATE SAMPLED Dec./82 DATE RECEIVED Dec. 16/82 DATE TESTED Feb. 1/83

SOLUTION Magnesium Sulphate				NUMBER OF CYCLES 5			
COARSE AGGREGATE				FINE AGGREGATE			
SIEVE SIZE		ORIGINAL GRADING PERCENT	Weighted AVERAGE PERCENT LOSS	SIEVE SIZE		ORIGINAL GRADING PERCENT	WEIGHED AVERAGE PERCENT LOSS
PASSING	RETAINED			PASSING	RETAINED		
3 IN.	2 IN.			3/8 IN.	NO. 4		-
2 IN.	1 - 1/2 IN.	3.7	-	NO. 4	NO. 8		-
1 - 1/2 IN.	1 IN.	11.4	0.08	NO. 8	NO. 16		-
1 IN.	3/4 IN.	14.0	0.06	NO. 16	NO. 30		-
3/4 IN.	1/2 IN.	26.0	0.73	NO. 30	NO. 50		-
1/2 IN.	3/8 IN.	18.7	0.82	NO. 50	NO. 100		-
3/8 IN.	NO. 4 IN.	26.2	0.97	NO. 100			-
TOTALS		100.0	2.66	TOTALS		-	-

SIZE FRACTION	NO. PARTICLES	QUALITATIVE EXAMINATION OF PLUS 3/4" MATERIAL	
3" - 2"	ORIGINAL		
	FINAL		
2" - 1 1/2"	ORIGINAL		
	FINAL		
1 1/2" - 1"	ORIGINAL 16	Some cracking was observed.	
	FINAL 16	Some pit holes, flaking and cracking was observed.	
1" - 3/4"	ORIGINAL 44	Some cracking was observed.	
	FINAL 44	Some pit holes, flaking, and cracking was observed.	

COMMENTS: TH #1 & TH #9 material was combined to make up Soundness Test Sample.



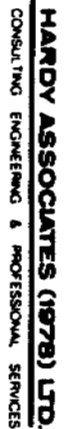
REPORT CERTIFIED

TECHNICIAN R.L.D.

TESTED
IN ACCORDANCE
WITH ASTM C88

219 BURNABY 18 CALGARY 18 STREET, S.E. DAWSON CREEK CALGARY, ALBERTA. T2E 6J5 (403) 272-8761 TWX 610-821-1388
WINNIPEG

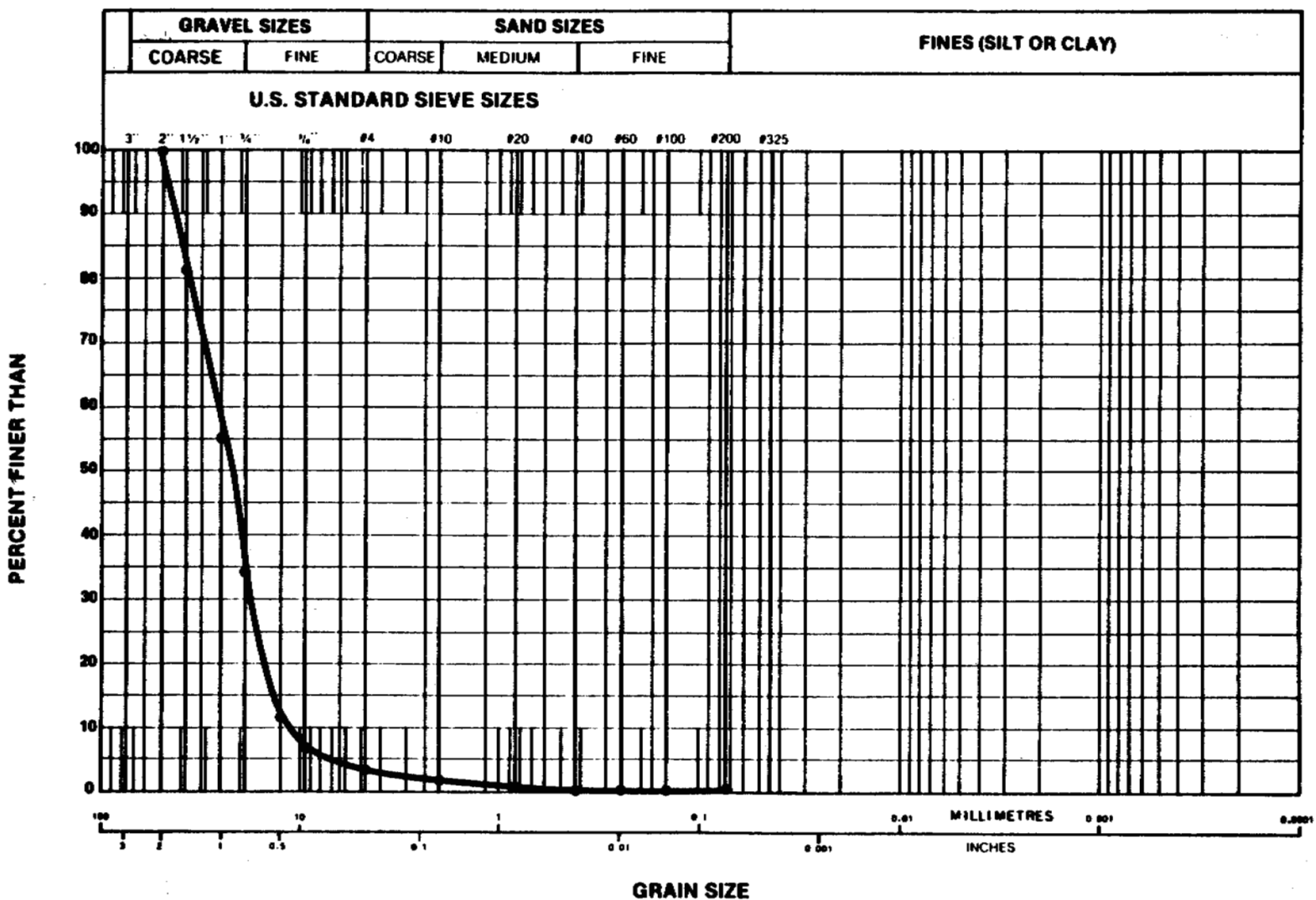
MT42-11/79
PLATE B-16



PROJECT NO.	CG 10047
CLIENT	
BOREHOLE SAMPLE	B13 MP A1
DEPTH (m)	2.3 - 2.0
TECHNICIAN	SK
	DATE

PROJECT NO.	CG 10047
CLIENT	
BOREHOLE SAMPLE	B13 MP 1095.1 A1
DEPTH (m)	2.3 - 2.5
TECHNICIAN	SK DATE TESTED

DATE TESTED 82.12.19



GRAVEL	96.0	%	SAND	3.0	%	FINES	1.0	%	SOIL GROUP	GP
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NOTE: UNIFIED SOIL CLASSIFICATION SYSTEM

$D_{10} =$ _____ mm.
 $D_{30} =$ _____ mm.
 $D_{60} =$ _____ mm.
 C_u _____
 C_c _____



HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

**LOS ANGELES ABRASION
TEST REPORT**

TO: Mr. G. Dupuy, P. Eng.,
Hardy Associates (1978) Ltd.,
221 - 18 Street S.E.,
CALGARY, Alberta.
T2E 6J5

OFFICE Calgary
FILE 4195-CG-10047
DATE Jan. 31, 1983
CLIENT P.O.
C.C.

PROJECT: BURWASH LANDING/DESTRUCTION BAY COMMUNITY GRAVEL STUDY

TH B-14, MP 1095.1 Pit Run
SOURCE 4.0 - 4.2 m Material
DATE SAMPLED Dec./82 TYPE OF SAMPLE DATE RECEIVED Dec. 16/82
SAMPLED BY DATE TESTED Client Jan. 27/83

MATERIAL GRADING: 'A'			
ACTUAL SIEVE SIZES		AMOUNT	
—	1 1/2" + 1"	1252.1	g
—	1" + 3/4"	1250.9	g
—	3/4" + 1/2"	1249.8	g
—	1/2" + 3/8"	1247.9	g
		TOTAL SAMPLE	5000.7 g
NO. OF REVOLUTIONS		500	
NO. OF SPHERES		12	
WT. OF SPHERES		4987.7 g	
		+ # 12 MATERIAL AFTER	3981.5 g
		- # 12 MATERIAL AFTER	1019.2 g
$\text{LOSS} = \frac{5000.7 - \#12}{\text{TOTAL SAMPLE}} \times 100 = \frac{1019.2}{5000.7} \times 100 = 20.4\%$			

COMMENTS: Test performed in accordance with A.S.T.M. C-131

REPORT CERTIFIED

TECHNICIAN E.K.

PLATE B-19

BURNABY • CALGARY • DAWSON CREEK • EDMONTON • LETHBRIDGE • PRINCE GEORGE • RED DEER • WINNIPEG

4752 70/11

**HARDY ASSOCIATES (1978) LTD.**

CONSULTING ENGINEERING & PROFESSIONAL SERVICES

SOUNDNESS OF AGGREGATE**SULPHATE TEST REPORT**

TO: Mr. G. Dupuy, P. Eng.,
Hardy Associates (1978) Ltd.,
Geotechnical Division,
221 - 18 Street S.E.,
CALGARY, Alberta.
T2E 6J5

FILE: 4195-CG-10047
DATE: February 7, 1983
CLIENT P.O.: -
C.C.: -

PROJECT BURWASH LANDING/DESTRUCTION BAY COMMUNITY GRAVEL STUDY

TH B14, MP. 1095.1 Pit Run
SOURCE 4.0-4.2 m TYPE OF SAMPLE Material
DATE SAMPLED Dec./82 DATE RECEIVED Dec. 16/82 SAMPLED BY Client
DATE TESTED Feb. 1/83

SOLUTION Magnesium Sulphate				NUMBER OF CYCLES 5			
COARSE AGGREGATE				FINE AGGREGATE			
SIEVE SIZE		ORIGINAL GRADING PERCENT	Weighted AVERAGE PERCENT LOSS	SIEVE SIZE		ORIGINAL GRADING PERCENT	WEIGHED AVERAGE PERCENT LOSS
PASSING	RETAINED			PASSING	RETAINED		
3 IN.	2 IN.			3/8 IN.	NO. 4		
2 IN.	1 - 1/2 IN.	6.9	-	NO. 4	NO. 8		-
1 - 1/2 IN.	1 IN.	11.6	0.24	NO. 8	NO. 16		-
1 IN.	3/4 IN.	17.7	0.57	NO. 16	NO. 30		-
3/4 IN.	1/2 IN.	22.8	0.17	NO. 30	NO. 50		-
1/2 IN.	3/8 IN.	16.4	0.42	NO. 50	NO. 100		-
3/8 IN.	NO. 4 IN.	24.6	1.02	NO. 100			-
TOTALS		100.0	2.42	TOTALS		-	-

SIZE FRACTION	NO. PARTICLES	QUALITATIVE EXAMINATION OF PLUS 3/4" MATERIAL
3" - 2"	ORIGINAL	
	FINAL	
2" - 1 1/2"	ORIGINAL	
	FINAL	
1 1/2" - 1"	ORIGINAL 17	Some pit holes were observed.
	FINAL 17	Some pit holes and cracking was observed.
1" - 3/4"	ORIGINAL 42	Some pit holes and cracking was observed.
	FINAL 41	Some pit holes, splitting, and flaking was observed.

COMMENTS:



REPORT CERTIFIED

TECHNICIAN R.L.D.

TESTED
IN ACCORDANCE
WITH ASTM C88

219 BURNABY 18 CALGARY STREET, S.E. CALGARY, ALBERTA. T2E 6J5 (403) 272-8761 TWX 610-821-1388
DAWSON CREEK EDMONTON GRANDE PRAIRIE LETHBRIDGE PRINCE GEORGE RED DEER WINNIPEG

HT42 - 11/79

PLATE B-20



HARDY ASSOCIATES (1978) LTD.
CONSULTING ENGINEERING & PROFESSIONAL SERVICES

GRAIN SIZE CURVE

PROJECT NO CG 10047

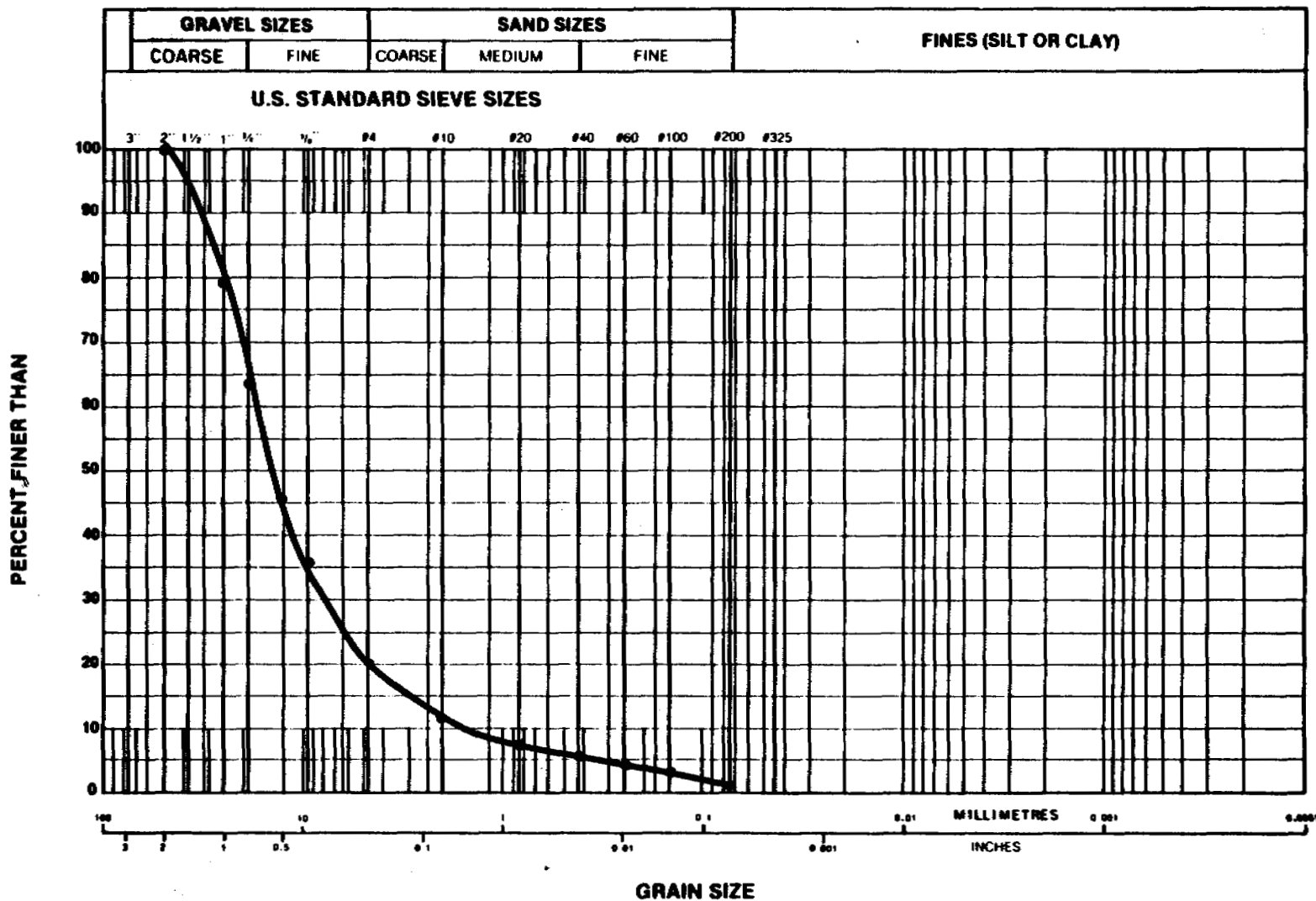
CLIENT

BOREHOLE B16 MP 1095.1

SAMPLE A1

DEPTH (m) 1.8 - 2.0

TECHNICIAN SK DATE TESTED 82.12.20



D_{10} = _____ mm.
 D_{30} = _____ mm.
 D_{60} = _____ mm.
 C_u = _____
 C_c = _____

GRAVEL	80.0%	SAND	19.0%	FINES	1.0%	SOIL GROUP	GP
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NOTE: UNIFIED SOIL CLASSIFICATION SYSTEM



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GRAIN SIZE CURVE

PROJECT NO. CG 10047

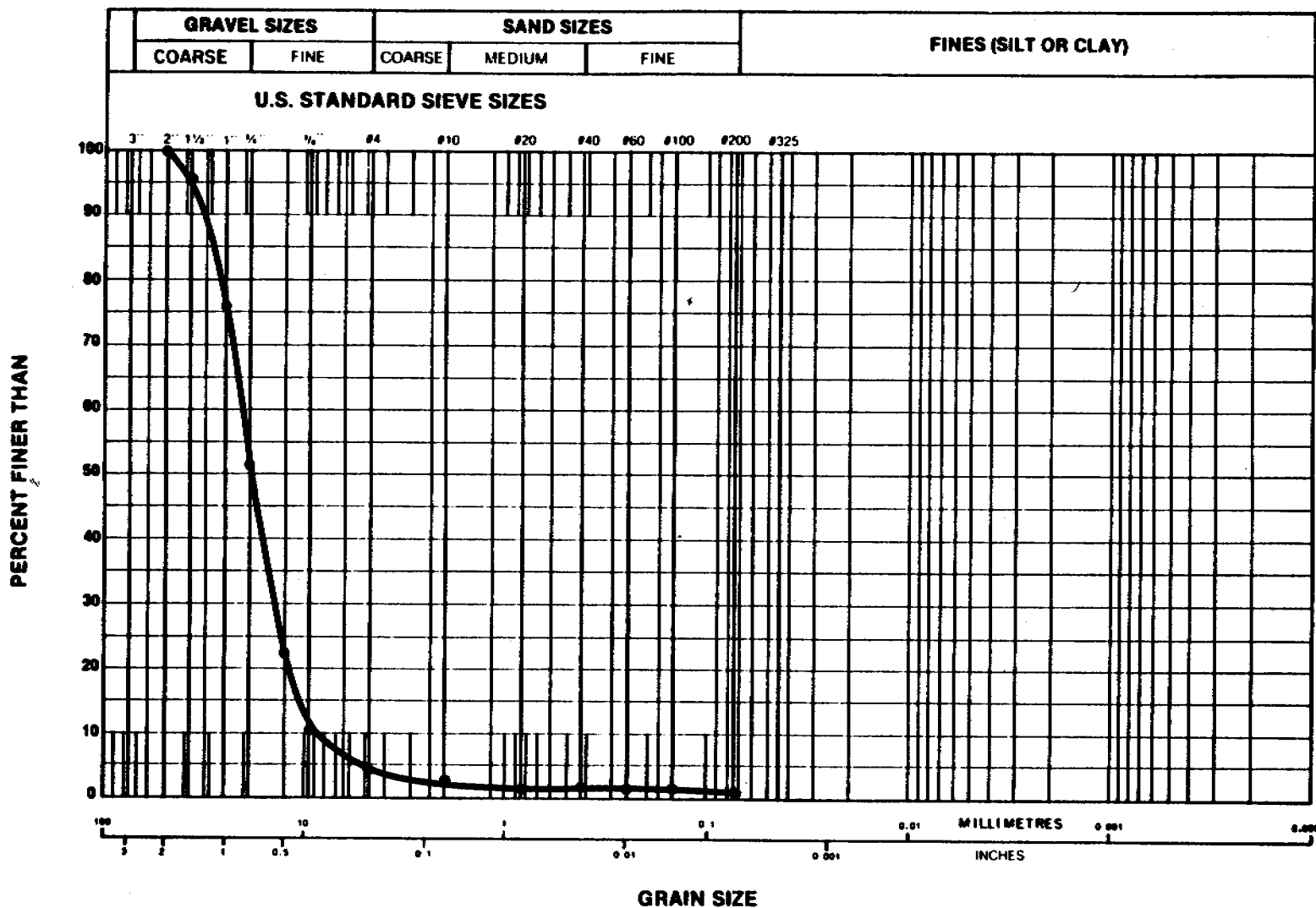
CLIENT

BOREHOLE B18 MP 1095.1

SAMPLE A2

DEPTH (m) 4.3 - 4.5

TECHNICIAN AB DATE TESTED 82.12.16





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GRAIN SIZE CURVE

PROJECT NO. CG 10047

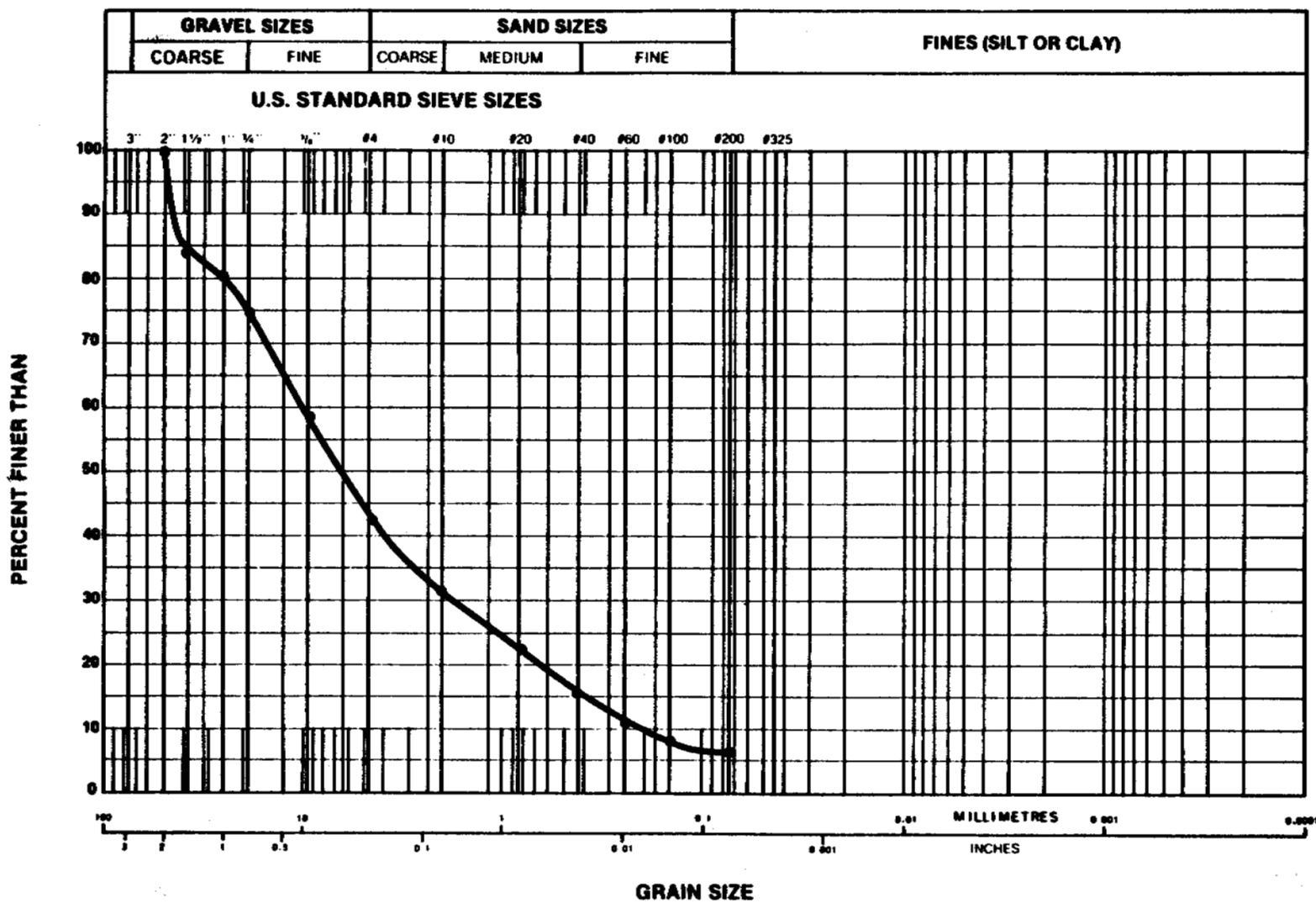
CLIENT

BOREHOLE B20 MP 1095.1

SAMPLE A2

DEPTH (m) 2.8 - 3.0

TECHNICIAN AB DATE TESTED 82.12.17



GRAVEL	58.0%	SAND	36.0 %	FINES	6.0 %	SOIL GROUP	GW
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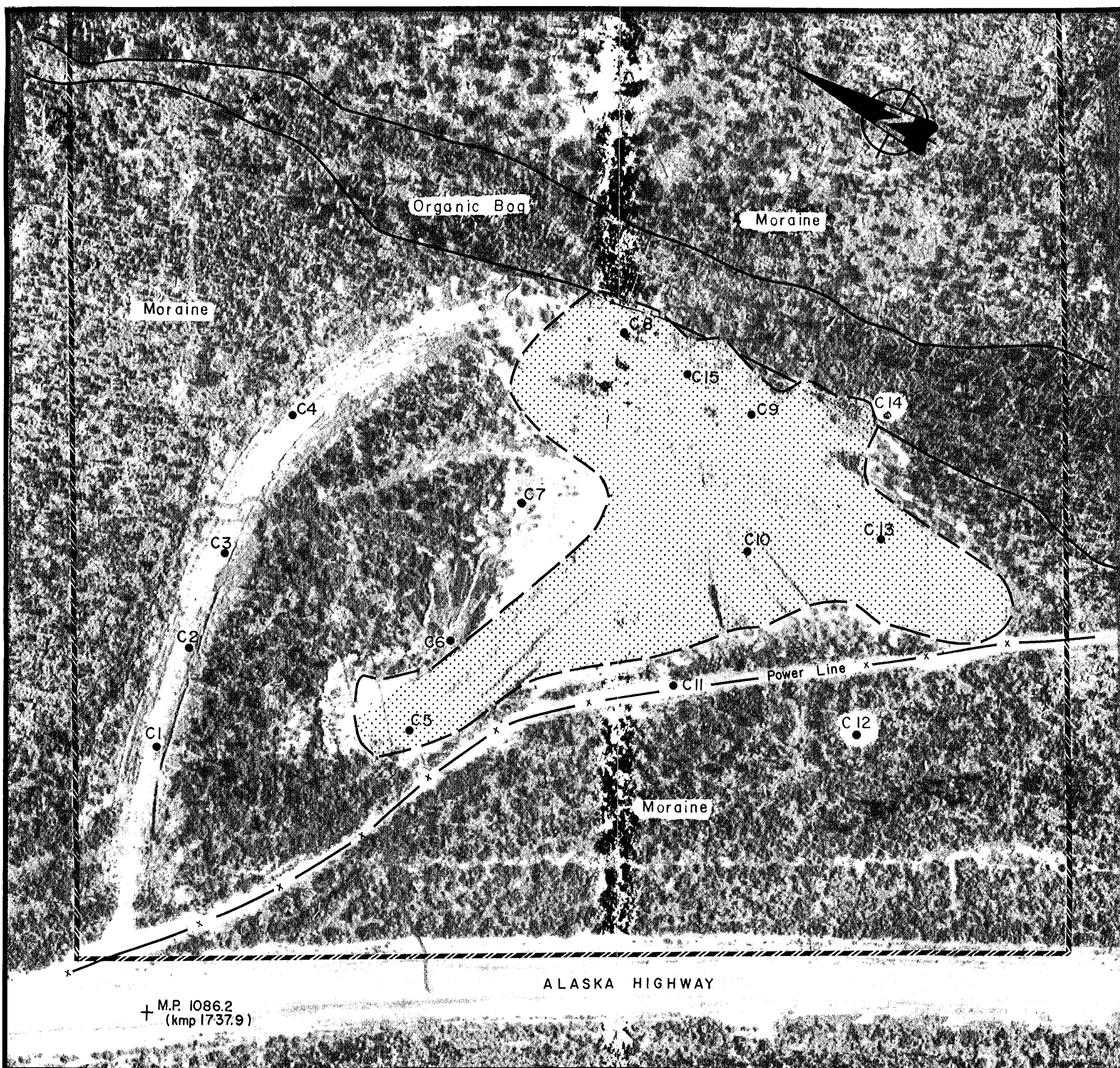
NOTE: UNIFIED SOIL CLASSIFICATION SYSTEM

D₁₀ = _____ mm.
D₃₀ = _____ mm.
D₆₀ = _____ mm.
C_u = _____
C_c = _____







HARDY ASSOCIATES (1978) LTD.
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APPENDIX "C"
BORROW RESERVE SITE PLANS



LEGEND

-  APPROXIMATE RESERVE BOUNDARY
-  TERRAIN TYPE BOUNDARY
-  EXISTING BORROW PIT
-  BOREHOLE LOCATION

Scale 1:1000 (approx.)

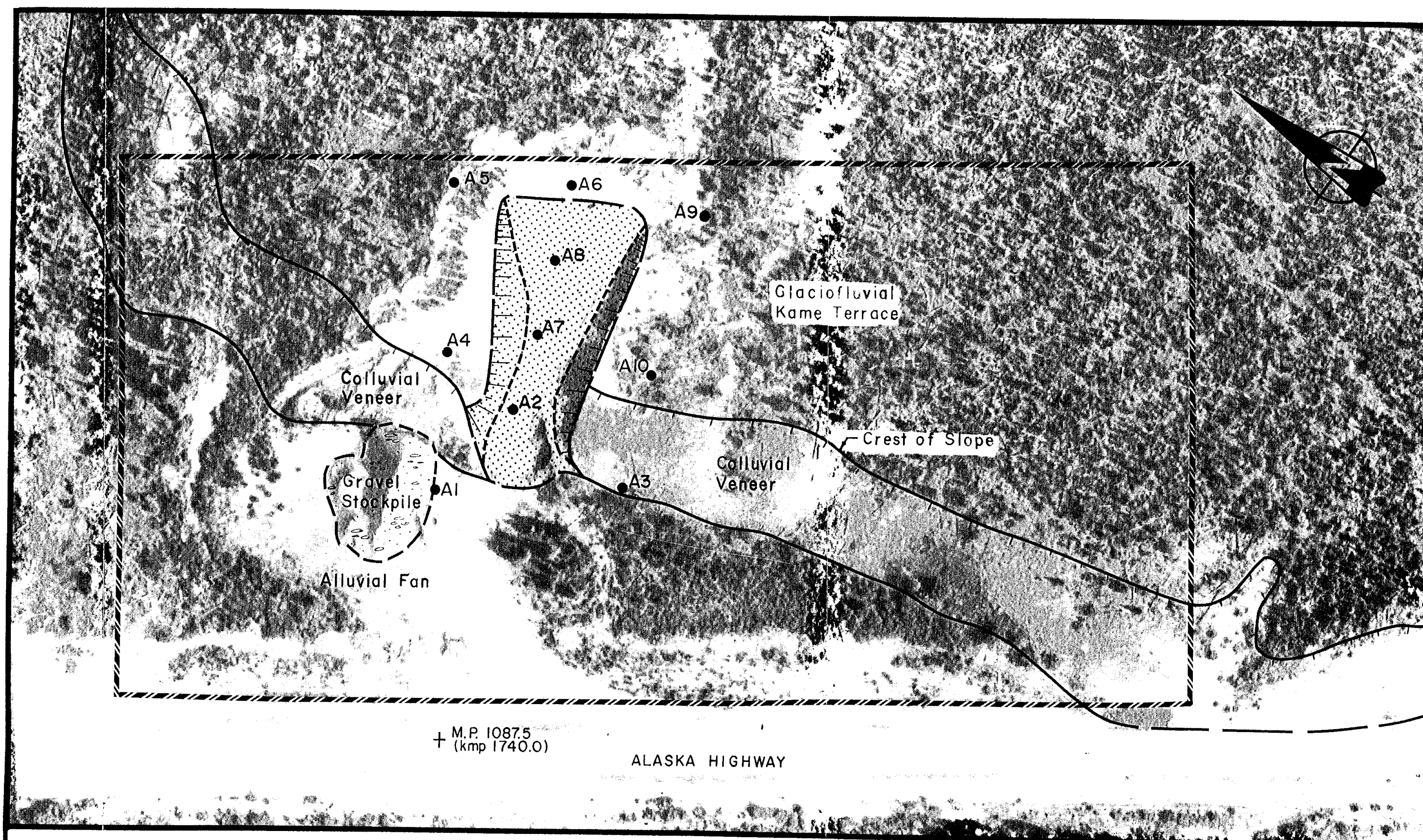


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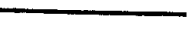
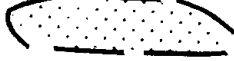

BORROW RESERVE YTG PIT #10981 M.P. 1086.2 SITE PLAN

CG 10047

PLATE C1



LEGEND

-  APPROXIMATE RESERVE BOUNDARY
-  TERRAIN TYPE BOUNDARY
-  EXISTING BORROW PIT
-  BOREHOLE LOCATION

Scale 1:1000 (approx)

BORROW RESERVE DIAND PIT #11574
M.P. 1087.6
SITE PLAN

CG10047

PLATE C2



- LEGEND**
- APPROXIMATE RESERVE BOUNDARY
 - TERRAIN TYPE BOUNDARY
 - EXISTING BORROW PIT
 - BOREHOLE LOCATION

Scale 1:1000 (approx.)

HARDY ASSOCIATES (1978) LTD.

CONSULTING ENGINEERS & PROFESSIONAL SERVICES

BORROW RESERVE YTG PIT #10983

M.P. 1095.6

SITE PLAN

CG10047
PLATE C3