## GEOTECHNICAL/GEOLOGICAL INVESTIGATION OF SELECTED GRANULAR RESOURCE PROSPECTS: BEAUFORT SEA

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## GEOTECHNICAL/GEOLOGICAL INVESTIGATION OF SELECTED GRANULAR RESOURCE PROSPECTS: BEAUFORT SEA

Part of the Northern Oil and Gas Action Program (NOGAP)
Project A4 - Granular Resources Inventory

#### SUBMITTED TO:

Indian and Northern Affairs Canada Hull, Quebec

#### PREPARED BY:

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#### EXECUTIVE SUMMARY

The discovery of petroleum reserves north of the Mackenzie Delta has led the Government of Canada to anticipate possible future demands for granular resources in the region to support oil and gas development. As a result, Indian and Northern Affairs Canada (INAC) has compiled a comprehensive granular resource inventory as part of the Northern Oil and Gas Action Program (NOGAP) Project A4. Geological models have been developed in an attempt to explain known offshore borrow areas and to predict other possible similar occurrences.

An offshore geotechnical investigation was completed during March of 1994 for INAC at specific geological and granular resource targets within a south-central region of the Beaufort Sea, just north of Richards Island. The intent of the investigation was to obtain geotechnical data for use in ground truthing geophysical interpretations and in evaluating the suitability of the derived geological models for prospective granular resource sites. The investigation comprised 19 boreholes that were sampled to a maximum penetration of 14.5 m.

This report describes the investigation that was conducted and presents a summary of the geotechnical data that was collected.



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## 1.0 INTRODUCTION

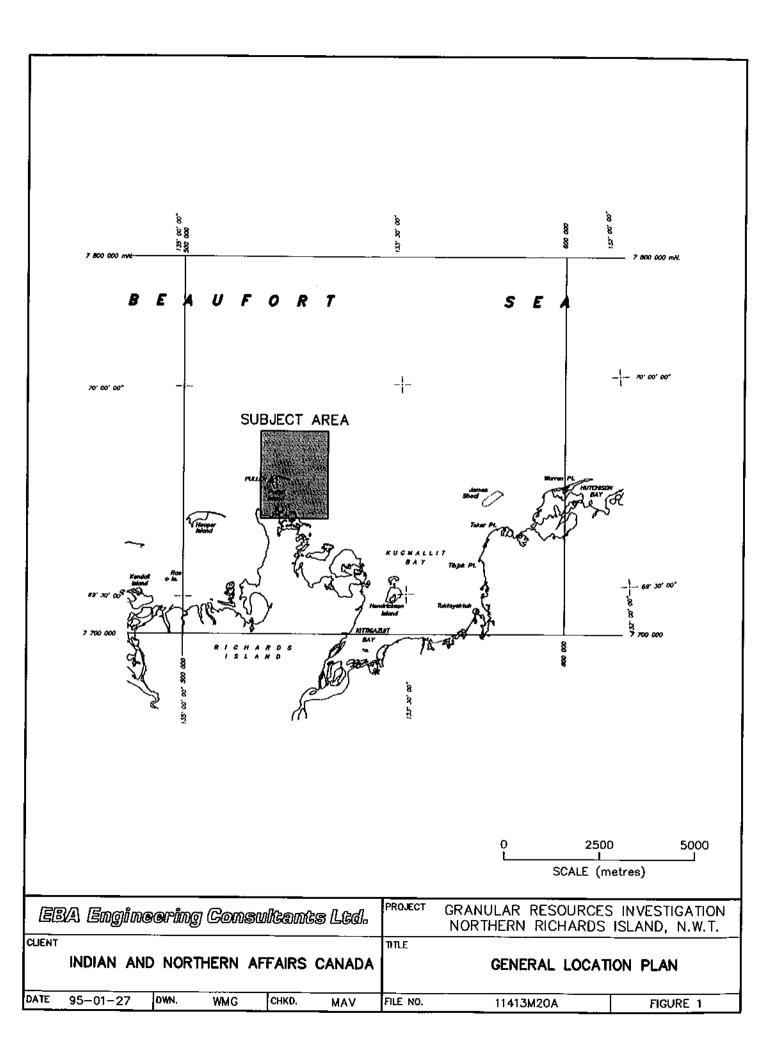
Indian and Northern Affairs Canada (INAC) has compiled a comprehensive granular resource inventory of the MacKenzie Delta in order to prepare for anticipated oil and gas development in the region. The compilation work has been carried out as part of the Northern Oil and Gas Action Program (NOGAP) Project A4. The inventory currently includes both proven and prospective borrow sources. The NOGAP granular resource program has used existing bathymetric, geophysical, geological and geotechnical data collected by both industry and government. The Geological Survey of Canada, Atlantic Geoscience Centre (GSC-AGC) has developed preliminary geological models in an attempt to explain the known offshore borrow areas and to predict other possible similar occurrences.

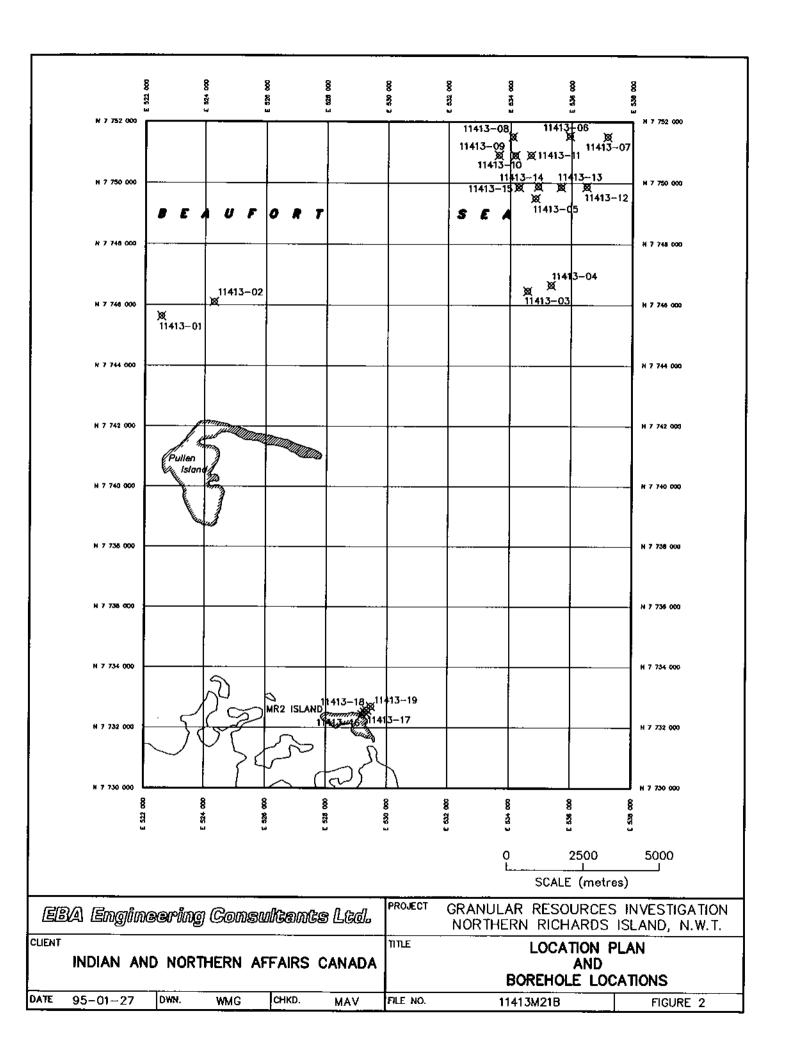
EBA Engineering Consultants Ltd. (EBA) was retained by INAC to carry out a geotechnical investigation to obtain data for use in ground truthing geophysical interpretations and in evaluating the suitability of the derived geological models for prospective granular resource sites. EBA's work was authorized by Contract No. A7134-3-0048/01-ST. Mr. R.J. Gowan, P.Geol., Geotechnical Advisor for the Natural Resources and Environment Branch of INAC, served as the designated Scientific Authority for the project.

This report describes the geotechnical investigation that was carried out in the south-central Beaufort Sea, north of Richards Island, during the 1994 winter field season and presents a summary of geotechnical data collected. The investigation reported herein is one component of the 1994 project conducted on behalf of INAC; two other components of this project are each reported under separate cover (EBA, 1994a; 1994b). The investigation was conducted to provide ground truthing at specific geological and granular resource targets that had been identified by an earlier separate study completed by Lewis Geophysical Consulting (1994).

The field work, for the offshore portion of this study, was conducted between March 8 and 21, 1994. A brief summary of daily operations is presented in Appendix A. Figure 1 presents a map showing the subject area investigated during the 1994 field season. Borehole locations are presented in Figure 2. A total of 19 boreholes were completed during the offshore portion of the 1994 field program. The boreholes are numbered 11413-01 through 11413-19.







## 2.0 FIELD INVESTIGATION

#### 2.1 EXECUTION OF THE INVESTIGATION

The successful completion of the project required not only familiarity with anticipated geotechnical conditions, but also both extensive and recent, relevant experience in planning and conducting winter offshore geotechnical programs. EBA and Midnight Sun Drilling Co. Ltd. provided technical expertise for planning the winter arctic geotechnical program on behalf of INAC.

Logistical options were limited due to the lack of exploration activity in the Beaufort - MacKenzie Region, so a self-contained skid camp was used as the base of operations. The camp facility comprised four sleds which included a fuel sloop, a generator trailer, a kitchen/washroom facility and an accommodations trailer. Ancillary equipment required to clear and maintain ice roads included a Cat 966 rubber-tire loader, and a D-6 Cat.

The equipment and camp was mobilized from Inuvik to the remote camp location at the North Head of Richards Island. The camp was assembled on the MacKenzie River at Inuvik and subsequently moved along the Tuktoyaktuk ice road to Kittigazuit Bay. The camp departed the existing ice road moving northwards, passing along the west side of Hendrickson Island, then proceeded northwest past Hansen Harbour to the North Head of Richards Island. The Cat 966 rubber-tire loader was used to clear an access trail, while the D-6 Cat pulled the skid camp.

Several companies, each under individual government contracts, were involved in conducting the site investigation. The companies and their respective responsibilities were as follows:

- · INAC provided the location of individual borings.
- EBA planned the field program, directed and logged the borings, conducted laboratory testing of the soil samples, and prepared this report.
- Midnight Sun Drilling Co. Ltd. (MSD) provided and operated the drilling equipment, soil sampling tools, camp, ancillary support equipment required to clear and maintain ice roads and a scout/bear monitor.



 Challenger Survey and Services Ltd. (CSS) provided locations as determined during a post-mission survey using differential GPS techniques.

#### 2.2 DRILLING AND SAMPLING

Drilling and sampling operations were conducted using MSD's CME 750, top drive, rotary drill rig mounted on an all-terrain rubber tire carrier. The drill rig was enclosed in a tarpaulin-covered frame for protection from arctic weather. Drilling was conducted "open hole" (i.e. without the use of downhole conductor casing). Seawater was used as a flushing medium in all boreholes. The only drilling additive was sodium chloride (NaCl), which was used to further depress the freezing point of the circulated seawater.

Selection of an appropriate sampler for encountered ground conditions was made by EBA's on-site representative, Mr. M.A. Valeriote, R.E.T. Samples were generally obtained at 0.6 m intervals. Soils were generally sampled with a thin-walled shelby tube, advanced by a single stroke of the rig hydraulics. Occasionally, a Standard Penetration Test (SPT) drive sampler was used in noncohesive soils. In Borehole 11413-05, well-bonded permafrost samples were obtained using a standard Longyear NQ core barrel, which provided a 47 mm diameter core. In Boreholes 11413-16 through 11413-19, which were drilled on behalf of Geological Survey Canada, Terrain Sciences Division (GSC-TSD), a CRREL core barrel was also used to obtain permafrost samples. Borehole logs are presented in Appendix B. The borehole locations and completion depths are summarized in Table 1.

At the conclusion of the field program, all soil samples, except those retained by GSC-TSD, were shipped to EBA's Edmonton laboratory for index and classification testing. Results of these tests are presented on the borehole logs, where appropriate, and on laboratory test summary sheets in Appendix C. Particle size distribution curves are presented in Appendix D.

#### 2.3 SAMPLE HANDLING

#### 2.3.1 Geological Target Samples for GSC-AGC

Sampling tubes containing geological target samples for GSC-AGC were fully extruded upon receipt at surface. The samples were wrapped in cellophane to ensure minimal moisture loss and then encased in a split-tube, heavy-wall plastic liner. In an attempt to minimize possible disturbance, these samples were not visually logged



at the drill rig. The samples were sent to the Inuvik Research Centre where awaiting GSC-AGC personnel visually logged the samples and prepared subsamples, split from the main working sample, for laboratory testing.

In Inuvik, each sample was split in half longitudinally allowing one portion to be used as a working sample and the remaining portion to be saved for archive purposes. The working samples were then shipped to EBA's Edmonton laboratory for index and classification testing. Upon completion of the laboratory test program, these samples were forwarded to GSC-AGC in Dartmouth, N.S.

## 2.3.2 Geological Target Samples for GSC-TSD

All unfrozen samples were fully extruded and visually logged while attempting to minimize disturbance. The samples were wrapped in cellophane and aluminum foil to effect minimal moisture loss and then encased in a split-tube, heavy wall plastic liner. Well-bonded frozen soils were fully extruded upon recovery and visually logged. These samples were then sealed in a polyethylene sleeve. All samples, irrespective of lithology, were placed in cardboard core boxes and initially forwarded to the Inuvik Research Centre. Subsequently, GSC-TSD forwarded these samples to their laboratory facility in Ottawa.

## 2.3.3 Granular Resource Target Samples

All granular resource target samples were fully extruded and visually logged upon immediate recovery at surface. Representative subsamples for moisture content, particle size distribution analysis, and porewater salinity determination were selected, wherever possible, from the mid-point of the sample length to avoid disturbed zones. These samples were sealed in labelled polyethylene bags and forwarded to EBA's Edmonton laboratory.

#### 3.0 LABORATORY TESTING PROGRAM

A laboratory testing program was carried out for samples that were retained by EBA for testing in EBA's Edmonton facility. The testing program included moisture content, Atterberg limits, particle size distribution, and porewater salinity determinations. Test results are presented on the borehole logs, were appropriate, and on summary tables in Appendix C. Particle size distribution curves are presented in Appendix D.



BOREHOLE LOCATION SUMMARY TABLE 1

				UTM Coordinates (Zone 8)	tes (Zone 8)			
EBA Borehole Number	Target Type	Target Designation	Requested by	Northing (m)	Easting (m)	Seabed Penetration (m)	Water Depth (m)	Date Drilled
11413-01	Geologic	GS6-4-S	INAC	7 745 632.1	522 548.7	10.5	7.2	1994 03 09
11413-02	Geologic	GS6-3-S	INAC	7 746 098.6	524 298.4	11.0	7.2	1994 03 10
11413-03	Geologic	PS2-1-S	INAC	7 746 466.5	534 579.8	13.0	6.3	1994 03 11
11413-04	Geologic	PS2-5-S	INAC	7 746 653.3	535 344.9	11.5	6.3	1994 03 12
11413-05	Geologic	Permafrost	GSC-TSD	7 749 497.0	534 832.7	14.5	8.3	1994 03 14
11413-06	Geologic	Non-Permafrost	GSC-TSD	7 751 537.4	535 938.2	11.5	9.2	1994 03 15
11413-07	Granular	C1-9-S	INAC	7 751 507.8	537 165.4	4.7	9.2	1994 03 16
11413-08	Granular	C1-10-S	INAC	7 751 507.6	534 082.7	5.5	9.3	1994 03 16
11413-09	Granular	C1-7-S	INAC	7 750 910.6	533 631.4	5.0	8.9	1994 03 17
11413-10	Granular	C1-6-S	INAC	7 750 899.2	534 164.8	5.3	9.1	1994 03 17
11413-11	Granular	C1-5-S	INAC	7 750 906.0	534 679.3	1.4	8.9	1994 03 18
11413-12	Granular	C14-S	INAC	7 749 873.9	536 489.3	4.7	8.2	1994 03 18
11413-13	Granular	C1-3-S	INAC	7 749 858.4	535 654.7	4.6	8.3	1994 03 19
11413-14	Granular	C1-2-S	INAC	7 749 883.3	534 913.2	1.4	8.3	1994 03 19
11413-15	Granular	C1-1-S	INAC	7 749 856.8	534 276.7	5.9	8.5	1994 03 19
11413-16	Geologic	Nearshore MR2 Island	GSC-TSD	7 732 423.8	529 201.3	11.0	6.0	1994 03 20
11413-17	Geologic	Nearshore MR2 Island	GSC-TSD	7 732 509.4	529 272.6	3.4	7	1994 03 21
11413-18	Geologic	Nearshore MR2 Island	GSC-TSD	7 732 576.3	529 347.6	7.0	6.0	1994 03 21
11413-19	Geologic	Nearshore MR2 Island	GSC-TSD	7 732 701.8	529 470.0	12.2	2.3	1994 03 21
NOTE:								

INAC: Indian and Northern Affairs Canada GSC-TSD: Geological Survey of Canada, Terrain Sciences Division All coordinates supplied by Challenger Survey and Services Ltd. Coordinates provided are based on the North American 1927 (NAD27) datum.

### 4.0 GEOLOGY

#### 4.1 GENERAL GEOLOGICAL HISTORY

The following discussion of regional surficial geology is based on a synthesis that was prepared by EBA for inclusion in a report by Swan Wooster Engineering Co. Ltd. (1982), which was submitted as a support document for a 1982 joint-industry Environmental Impact Statement (EIS) for Hydrocarbon Development in the Beaufort Sea - MacKenzie Delta Region. It is consistent with the regional geologic model proposed by M.J. O'Connor (1982), which has been adopted by the Geological Survey of Canada as a general model for this region.

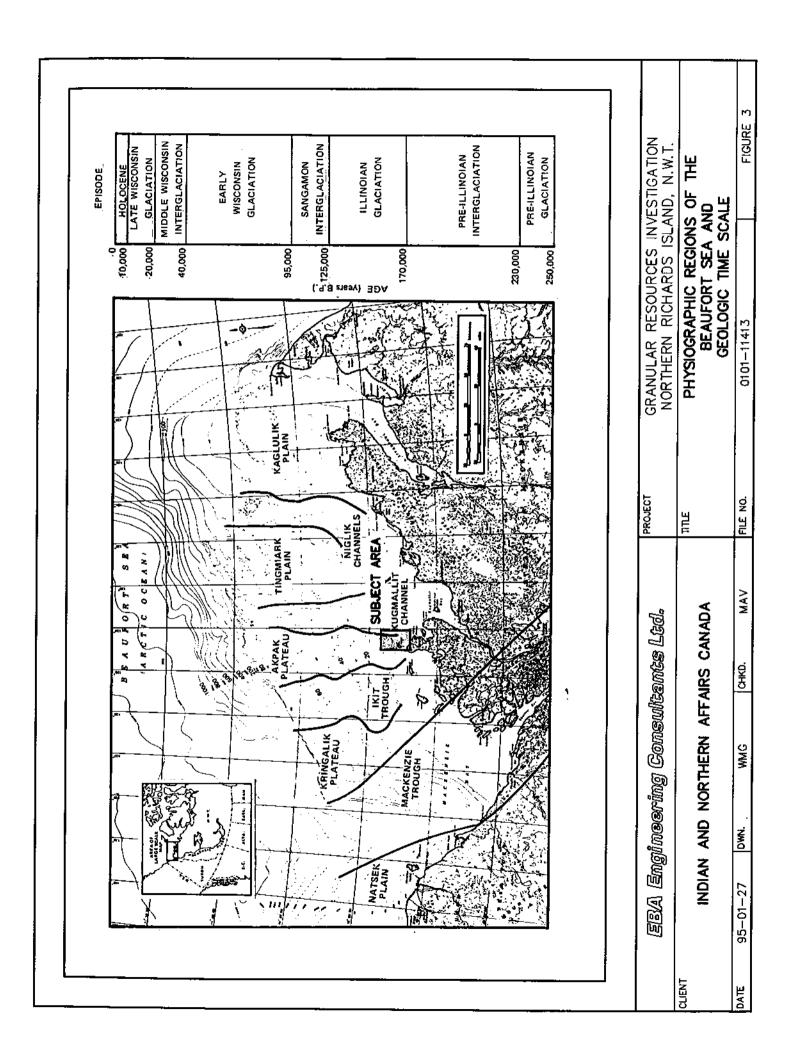
Figure 3 presents the major physiographic regions within the Canadian Beaufort Sea Continental Shelf as identified in the EIS. The figure also presents a geologic time scale that is pertinent to seabed sediment deposition.

The area that was investigated during the 1994 winter field program is within the physiographic region known as the Akpak Plateau. The soils that were encountered below the surficial Holocene sediments are thought to be of Wisconsinan age. The overall distribution of the sediments across the area has been largely influenced by two major sea-level fluctuations during the Wisconsin Stage. Depression of the sealevel by as much as 140 m below present levels has been suggested, coincident with the maximum Mid-Wisconsinan ice advance. The furthest advance for the ice sheet at that time is thought to have been to a line extending approximately from near Herschel Island to the Tuktoyaktuk Peninsula.

During the Middle Wisconsin Stage (prior to about 35,000 years ago), a large fluviodeltaic or glaciofluvial plain developed that extended over most of the western Canadian Beaufort Sea. The precise age and extent of the deltaic plain is not certain, but is thought to be at least as old as the Middle Wisconsinan glacial retreat. Detritus released during the retreat of the ice sheet is the probable source of the deltaic sediments on the plain.

The late Wisconsin Stage was marked by a final glacial advance, during which sealevels were depressed by as much as 100 m below present levels (about 20,000 years ago). Most of the area exposed by the depression in sea-level experienced a periglacial climate similar to that prevailing in the High Arctic Islands today.





Permafrost aggradation accompanied the cooler climate, and development of sparse vegetation also occurred.

The exposure of the shelf also allowed subaerial erosion and deposition to take place. There is evidence in seismic records of the development of shallow thermokarst lakes on the exposed surface. A thick layer of uniform fine-grained sand deposited across the Akpak Plateau, and Tingmiark and Kaglulik Plains during this period appears to be of fluvio-deltaic origin. This deposit lies unconformably on the older, partially eroded, deltaic sequence.

During this period of sea level depression, a significant distributary of the prehistoric MacKenzie River cut a deep channel (the Kugmallit Channel) through the fine-grained sands, establishing a route for drainage and imposing deposition control that remains active to the present.

The Late Wisconsinan ice front is thought to have begun its retreat about 20,000 years ago. The Kugmallit Channel, as one of the three main distributaries of the MacKenzie River system, is likely to have undergone further modification. Complex cycles of erosion and deposition would have been experienced locally as a result of increased volumes of sediment-laden meltwater.

As the sea-level rose during the Late Wisconsinan marine transgression, the relatively warm, shallow water thawed parts of the frozen land surface. Extensive reworking of the deltaic plain by glacial meltwater, wave and current action resulted in redeposition of the surface material in sequences reflecting the uneven advance of the sea over the land surface. Finer-grained sediments (silts and clays) were deposited in the deep water of the local drainage channels and over areas of low current activity. This process, combined with sideslope instability and a sustained influx of fine-grained material from the MacKenzie River, contributed to the substantial infilling of the Kugmallit Channel. This infill material consists predominantly of normally consolidated silts and clays, although in some areas, thick sand deposits are present.

#### 4.2 SURFICIAL GEOLOGY OF THE SOUTHERN BEAUFORT SHELF

A general stratigraphic model of the surficial geology of the upper 100 m of the Beaufort Shelf has been proposed for the area north of Richards Island (Blasco et al., 1990, as referenced in Blasco and Lewis, 1990). The sediments of Units A to E are probably less than 25,000 years old, and Units A, B and the upper part of C may be



largely Holocene in age (less than 10,000 years old). A brief summary of each of the five units is presented in the following:

#### Unit A

Marine clays deposited on the shelf under the less dynamic wave and current conditions of the offshore, generally in water depths greater than 10 m. Unit A is soft and less than half a metre to a few metres thick. Unit A is disrupted and reworked by ice keels. The contact with the underlying Unit B complex is usually gradational (increasing silt content), and where present may be destroyed by ice scouring.

#### Unit B

Complex sequence of transgressive sediments related to deposition under the high energy wave and current conditions of shallow water regimes during the last sea-level rise across the shelf. Sediment type is coarser grained than Unit A and is usually composed of interbedded and layered silts and clays. Basal strata of Unit B may contain interbedded sands and sands and gravels related to the reworking of underlying Unit C sediments during transgression. Depositional environments represented by Unit B include barrier islands, relict beaches, lagoons, tidal inlets etc.

#### Unit C

Sediments that were in situ prior to the last transgression and were deposited during the last regressive cycle form Unit C strata. In this area, Unit C represents a broad coastal outwash plain of possible glaciofluvial origin. The unit is primarily a fine-grained sand with minor silt-clay interbeds. Depressions in the irregular upper surface of Unit C may represent relict thaw lakes or channels of the old coastal plain. The thickness of Unit C varies but is usually about 20 to 40 m thick. Discontinuous ice-bearing sediments are present.

#### Unit D

Unit D forms a thick (possibly 20 to 40 m) stiff silt to clayey silt layer underlying Unit C in the area and may represent sediments of an earlier transgressive cycle. These sediments may be discontinuously ice-bearing and well-bonded at the contact with the underlying sands of Unit E.



#### Unit E

Unit E is a widespread sand layer found approximately 60 m below the seabed under Unit D in this area. The sands are well-bonded and form the top of the main permafrost body.

#### 4.3 SURFICIAL SEDIMENTS OF THE AKPAK PLATEAU

The sediment sequence of the Akpak Plateau is complex, varying both laterally and with depth. The Akpak Plateau is underlain by Unit C sands (and localized gravels) that outcrop on the seabed adjacent to the Kugmallit Channel. Shoreward towards the southwest, Unit C sands dip under a complex sequence of Unit B strata that consist of interbedded layered silts and clayey silts. These Unit B transgressive sediments achieve a thickness of 14 m on the above section and may thicken and become more spatially variable in shallower water.

The distribution of ice-rich permafrost within the surficial sediments of the Akpak Plateau is laterally and vertically discontinuous, but appears to be confined to Unit C sediments.

#### 5.0 SITE STRATIGRAPHY

#### 5.1 GENERAL SUBSURFACE CONDITIONS

The stratigraphy encountered during this investigation varied due to the aerial extent covered. The geological model for the inland portion of Akpak Plateau describes a complex sediment sequence comprising a layer of marine clays (Unit A); overlying a set of transgressive, shallow-water sediments (Unit B); overlying a stratum of coastal outwash plain deposits (Unit C). Prior to the last transgression, the Unit C deposits formed an irregular palaeo-surface that was subjected to extensive modification by fluvial, glacial, thermokarst, lacustrine, aeolian, and littoral processes.

Detailed descriptions of textural variations, consistency, and colour are provided on the borehole logs presented in Appendix B. These descriptions, which are generally based on both field descriptions and laboratory test data, except as noted below, are used to compile a generalized stratigraphy for the target areas.

The borehole logs for the holes drilled on behalf of the Geological Survey of Canada, Terrain Sciences Division (GSC-TSD) are included in Appendix B for presentation



purposes. All samples obtained from these boreholes were retained by GSC-TSD. No discussion regarding the soil conditions at these latter locations has been included in this report.

#### 5.2 STRATIGRAPHY OF GEOLOGICAL TARGETS (GSC-AGC)

Four boreholes were drilled to obtain information for use in ground truthing geophysical interpretations and in evaluating the suitability of the derived geologic models. (This evaluation will be undertaken later by INAC and GSC-AGC.) Accordingly, it is not the intent of this study to summarize the stratigraphic conditions nor assign unit designations per the proposed geologic model outlined in Section 4.2. Boreholes 11413-01 and 11413-02 were drilled approximately 2 km north of Pullen Island in an area that has been named "New Prospect". Boreholes 11413-03 and 11413-04 were drilled approximately 6 km northeast of Pullen Island in an area that is known as "Breaker's Shoal".

Figure 4 presents diagnostic profiles of measured moisture contents and percentages of clay, silt, sand, and gravel from samples recovered from the New Prospect area. Figure 5 presents similar diagnostic profiles for the Breaker's Shoal area.

#### 5.3 STRATIGRAPHY OF GRANULAR RESOURCE PROSPECT

Based upon samples recovered from Boreholes 11413-06 through 11413-15, drilled at or adjacent to the Granular Resource Prospect, the following presents a simplified stratigraphic description of the soils encountered.

SOIL STRATIGRAPHIC UNIT	DEPTH BELOW SEABED (m)
Clay (CL) - silty, trace of sand, very thin laminae, low plastic, dark olive grey	0 to 1.5*
Sand (SM) - some silt to silty, trace to some clay, fine-grained, dark olive grey	0 to >5.9**

Note: \* Except for BH 11413-06, which penetrated a 9.3 m layer of surficial clay.

\*\* Determination limited by maximum depth of borehole penetration.



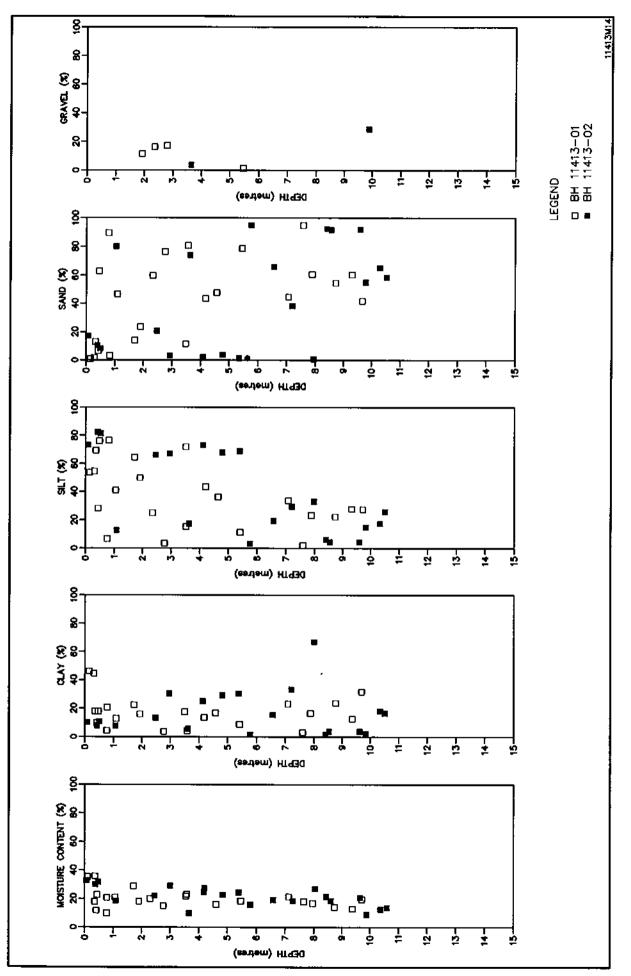


FIGURE 4 NEW PROSPECT DIAGNOSTIC PROFILES
PERCENTAGES MOISTURE, CLAY, SILT, SAND,
AND CLAY VS. DEPTH

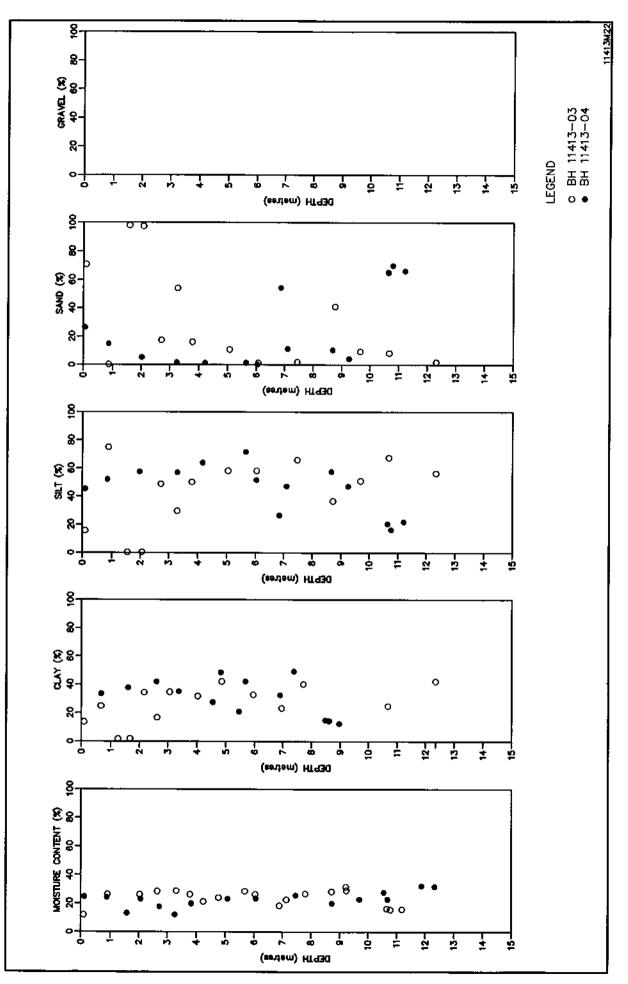


FIGURE 5 BREAKER'S SHOAL DIAGNOSTIC PROFILES
PERCENTAGES MOISTURE, CLAY, SILT, SAND,
AND CLAY VS. DEPTH

The uppermost unit sampled was the "Clay"; however, this unit was not encountered at all borehole locations. This material was described as being low plastic, thinly laminated, and thinly interbedded with silt or silty fine-grained sand. This unit was not encountered at three of the ten boreholes drilled. The surficial cohesive layer was less than 1.5 m thick in all but one of the seven boreholes were encountered. At Borehole 11413-06, the surficial cohesive layer extended to 9.3 m below seabed.

The underlying "Sand" unit was observed to be fine-grained containing varying contents of both silt and clay. Thin interbeds of silt and clay were observed within the sand unit. The presence of disseminated organics and shell fragments was noted in several samples.

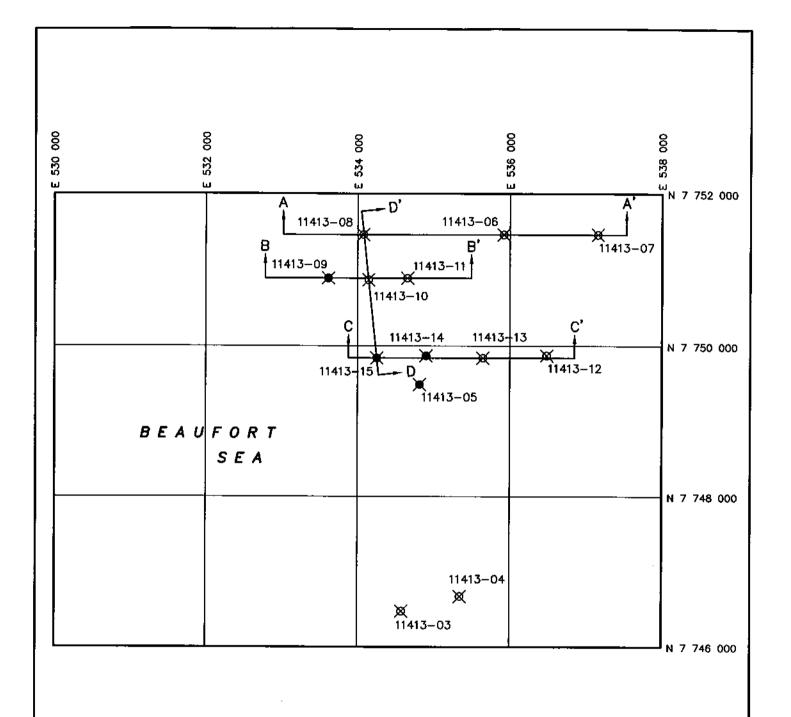
Four stratigraphic cross-sections have been prepared at the locations shown in Figure 6. The four stratigraphic cross-sections are shown in Figures 7 and 8. Results of selected soil properties from the classification and index tests conducted are presented in the form of a diagnostic profile in Figure 9.

#### 5.4 PERMAFROST AND GROUND ICE

Permafrost is defined as the thermal condition under which any earth materials such as rock and soil, that has existed below 0°C for at least two consecutive years, without regard to the phase composition of moisture present in the pore spaces. Marine sediments encountered at depths of up to 50 m beneath the Beaufort Sea have porewater salinities that range between 20 and 40 ppt, resulting in a freezing point depression that averages at least 1.5 C°. As a result, these soils can exist at temperatures below 0°C but exhibit no significant ice bonding or segregated ice. Because fine-grained seabed soils in the Beaufort Sea display similar mineralogical compositions, it is anticipated that unfrozen water contents will not be significantly affected by variations in mineralogy. For the purposes of this investigation, soil has been designated "frozen" only if visible ice and/or ice bonding was encountered.

In the vicinity of the Granular Resource Prospect, visible ice and/or well-bonded soil was encountered in samples obtained from within the sand unit in Boreholes 11413-05, 11413-09, 11413-13, and 11413-14. The borehole locations where visible ice and/or well-bonded soil were encountered are presented in Figure 6.





0 500 1000 1500 2000 L | L | SCALE (metres)

**LEGEND** 

▼ - VISIBLE ICE AND/OR WELL-BONDED SOIL ENCOUNTERED

<b>E</b> E	A Engino	ering C	Sonsul	lcan0	ts Ltd.	PROJECT	GRANULAR RESOURCES NORTHERN RICHARDS	
CLIENT	INDIAN AND	NORTH!	ERN AF	FAIRS	CANADA	nile STR	GRANULAR RESOURCES ATIGRAPHIC CROSS—SEC	
DATE	95-01-27	DWN.	WMG	CHKD.	MAV	FILE NO.	11413M25B	FIGURE 6

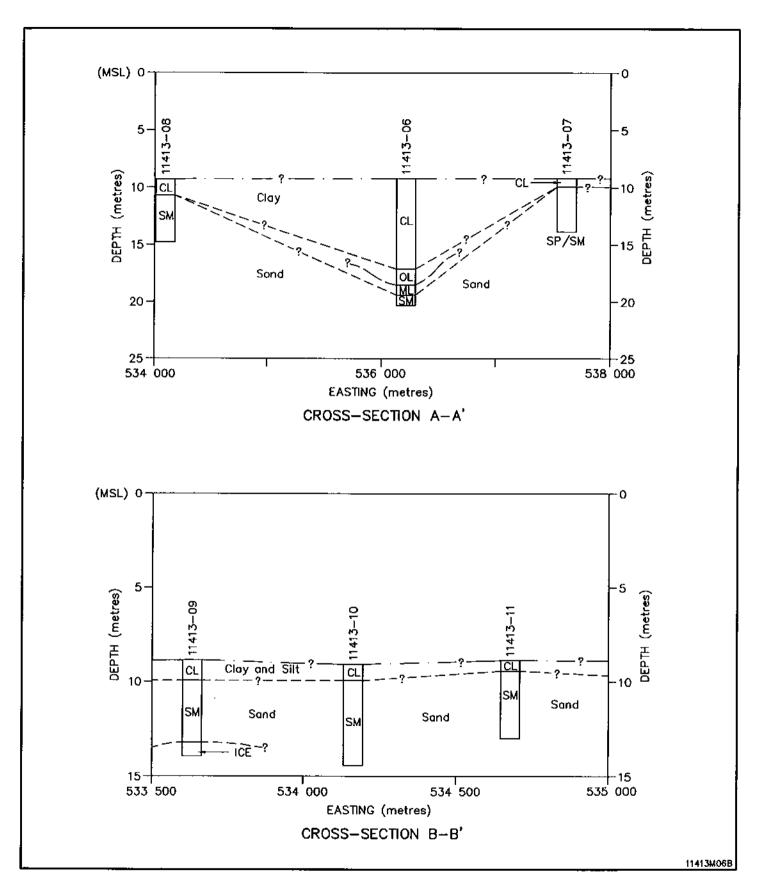


FIGURE 7 GRANULAR RESOURCE TARGET STRATIGRAPHIC CROSS—SECTIONS

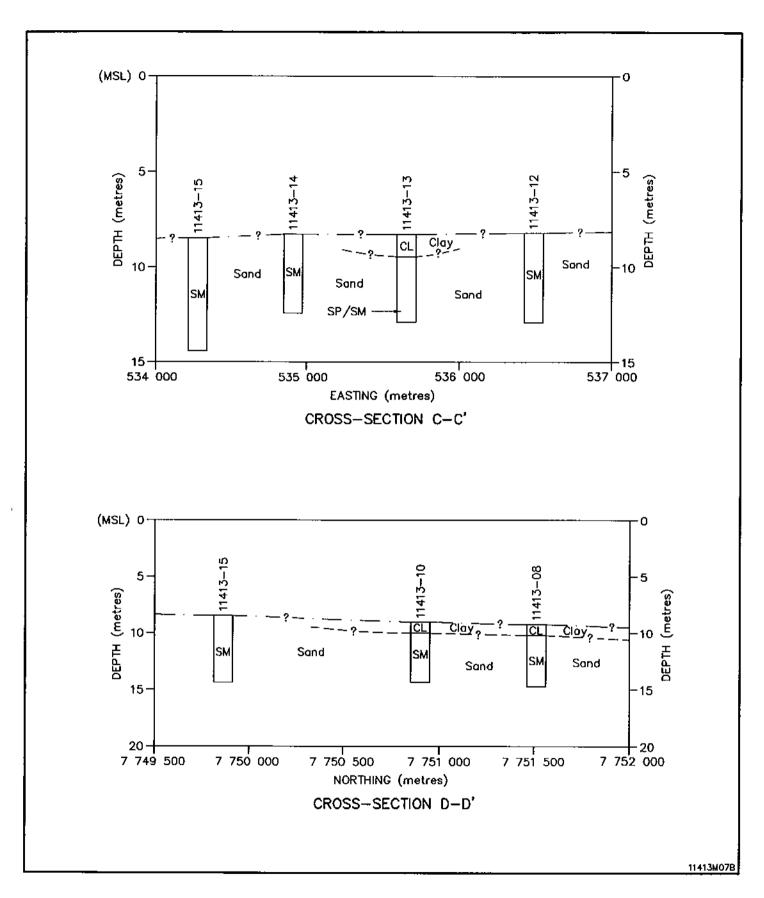
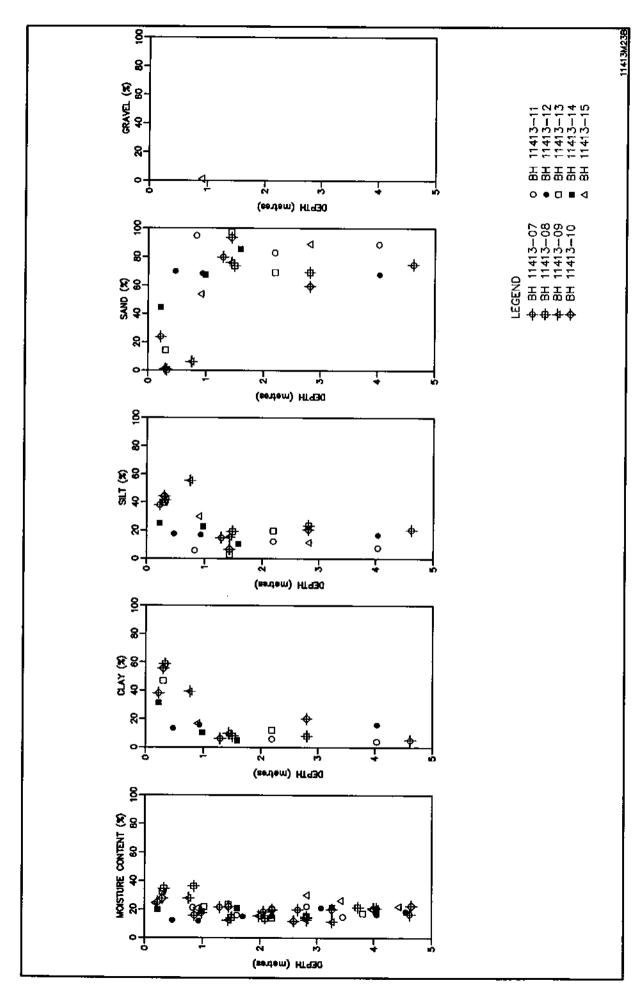


FIGURE 8 GRANULAR RESOURCE TARGET STRATIGRAPHIC CROSS—SECTIONS



GRANULAR RESOURCE TARGET PERCENTAGE MOISTURE, CLAY, SILT, SAND, AND GRAVEL VS. DEPTH Φ FIGURE

### 6.0 DISCUSSION

#### 6.1 GRANULAR RESOURCE PROSPECT EVALUATION

The seabed soils penetrated have been assigned to two broad units, as previously outlined in Section 5.3, on the basis of engineering properties. The particle size distribution curves obtained are presented in Appendix D, and a composite grading envelope from the sand samples tested from the Granular Resource Prospect (Borehole No. 11413-07 to 11413-15 inclusive) are presented in Figure 10.

Only six samples, on which a gradation analysis was conducted, contained a total fines content (material less than 80 microns) that was less than 15%, and a D50 averaging approximately 180 microns. Composite gradation curves derived from the sand samples tested having a total fines content of less than 15% and greater than 15% are presented in Figures 11 and 12, respectively.

Due to the seabed clay encountered at a number of locations and the fines content determined for the underlying stratum, in association with environmental concerns (i.e. turbidity), the area evaluated is not considered a favourable granular resource prospect.



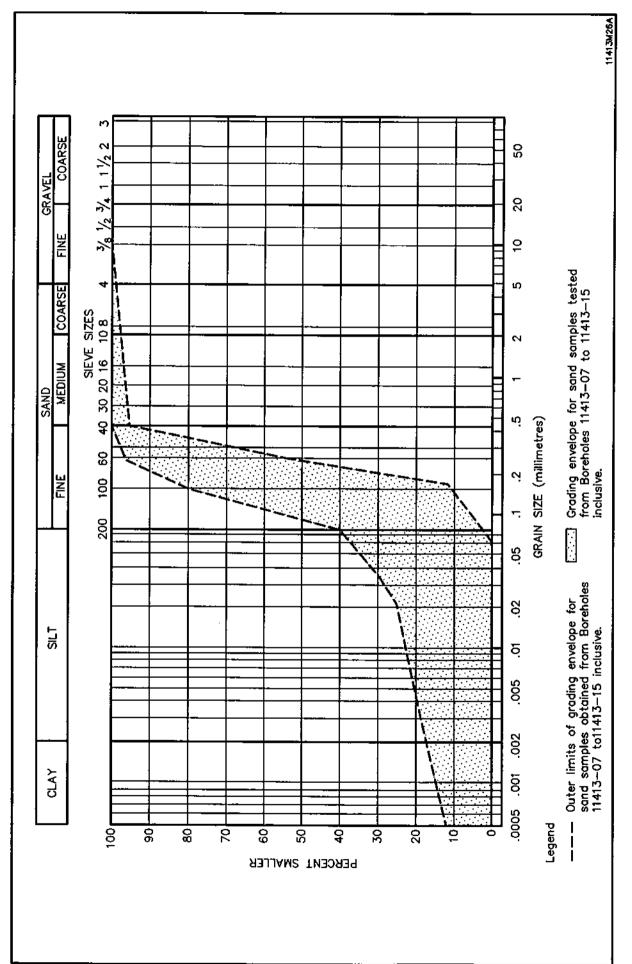


FIGURE 10 COMPOSITE GRADING ENVELOPE

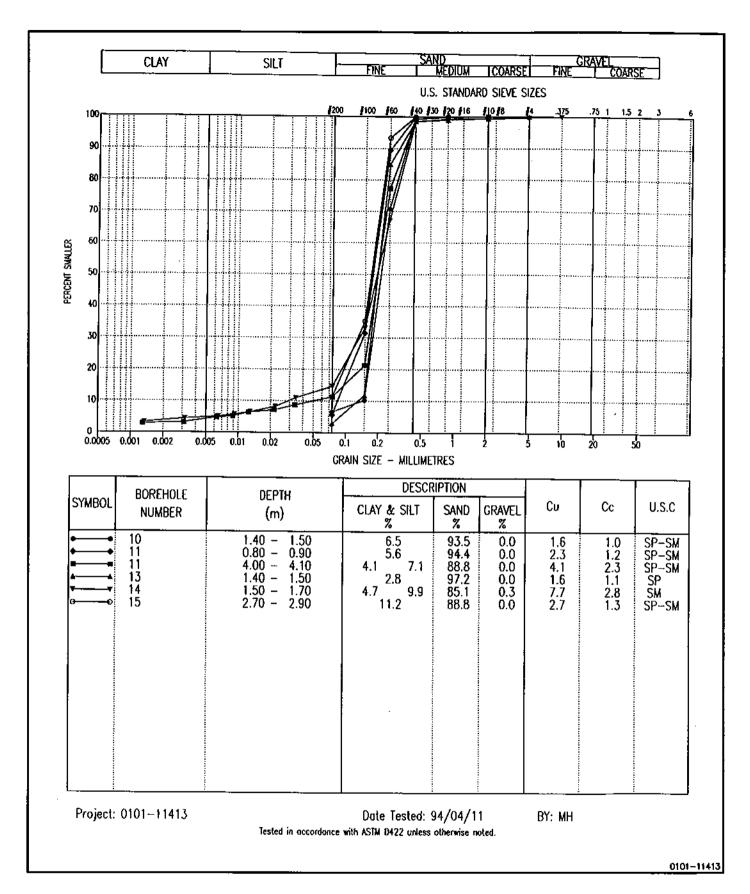


FIGURE 11 GRADATION ANALYSIS FOR SAMPLES CONTAINING LESS THAN 15% FINES

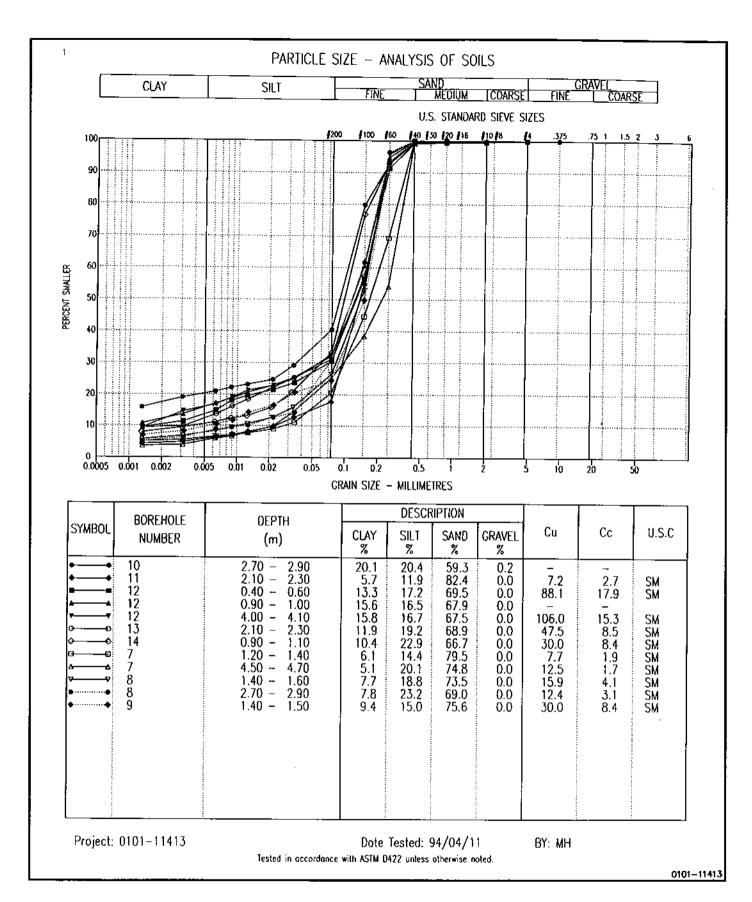


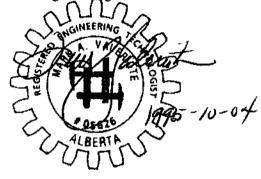
FIGURE 12 GRADATION ANALYSIS FOR SAMPLES CONTAINING GREATER THAN 15% FINES

## 7.0 CLOSURE

The geotechnical information contained in this report was obtained from samples collected during the 1994 winter program carried out for INAC. EBA Engineering Consultants Ltd. has appreciated the opportunity to work on this project and would like to acknowledge the cooperation and guidance provided by Mr. R. Gowan of INAC, Mr. S. Blasco of the GSC-AGC, Mr. S. Dallimore of the GSC-TSD, and Midnight Sun Drilling Co. Ltd.

Respectfully submitted,

EBA Engineering Consultants Ltd.

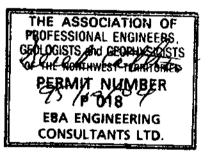


M.A. Valeriote, R.E.T.



D.C. Cathro, P.Eng. Chief Engineer, Frontier Division

MAV/DCC/tr





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# APPENDIX A OPERATIONAL CALENDAR



# OPERATIONAL CALENDAR GEOTECHNICAL INVESTIGATIONS BEAUFORT SEA, RICHARDS ISLAND AND CARIBOU CREEK, NWT

## Friday March 4, 1994

08:00	Scheduled departure from Edmonton to Inuvik; plane delayed.
10:15	• Depart Edmonton.
14:30	<ul> <li>Arrive Inuvik.</li> <li>Pick-up rental truck.</li> <li>Check into Finto Motor Inn</li> <li>Pick-up freight at Points North and transfer to field camp located at Arctic Tire.</li> </ul>
16:00	<ul> <li>Contact Continental Helicopters regarding possible March 5 charter.</li> <li>Fuel rental truck.</li> <li>Arctic Tire continue to prepare camp.</li> </ul>

## Saturday, March 5, 1994

Saturday, 1474	<u> </u>
08:00	Awaiting call from Continental Helicopters regarding weather conditions.
10:00	Pick-up supplies from various local stores.
11:45	• Received message from Continental Helicopters; unable to fly today due to weather.
12:15	Drive to Source 222 located south of Inuvik.
14:30	Camp has been moved to the Tuk ice road.
Evening	<ul> <li>Phone conversation with R.J. Gowan (DIAND)</li> <li>Telephone call from S. Blasco (GSC)</li> <li>Telephone call from D. Jamieson (MSD)</li> </ul>



## Sunday March 6, 1994

- Meet D. Jamieson (MSD) at camp; preparations on-going.
- Camp begins moving north on Tuk ice road (loader, with fuel sloop, flat deck, kitchen, utility and sleeper trailers in tow).
- Arrange reconnaissance flight to Pullen Island, North Head of Richards
   Island and Source 222 at Caribou Creek with Continental Helicopters.
- Depart from Continental Helicopter's hangar.
- 12:40 Arrive at Pullen Island.
- Monitor Pullen #4 monument with GPS receiver.
- Airborne, reconnaissance 6C-1, 6C-2, 4B-1 and Source 222.
- 15:15 Return to Continental's hangar.
- 16:00 Fuel rental truck.
  - Check material availability at the Northern Store as requested by MSD.
- Telephone call from D. Jamieson (MSD), camp presently at Bar-C.
   Recent snowfall makes going slow. Plan to camp overnight south of Kittigazuit.

## Monday, March 7, 1994

- 08:00
   Make project logistic arrangements in Inuvik.
- Phone call from D. Jamieson (MSD); plane coming from Whitehorse with MSD freight on-board delayed in Whitehorse. Began clearing ice road to North Head at 08:30.
- 10:30
   Unable to start rental truck.
- 13:15 R.J. Gowan (DIAND) arrives Inuvik.



20:45

21:30

• Loader returns to camp.

• D6 returns to camp.

14:00	•	Pick-up air cargo for MSD.
14:30	•	Meet R.J. Gowan at Inuvik DIAND office.
16:00	•	Meet with S. Blasco at Inuvik Research Centre.
17:15	•	Pick-up repaired rental truck.
19:00	•	Depart Inuvik for camp.
20:45	•	Turn off Tuk ice road; heading to North Head.
23:30	•	Camp stops in position; loader still on route with fuel sloop.
March 8, 199	4	
08:00		Making final camp arrangements.  Loader and D6 cat widening ice road between camp and the Tuk ice road.
10:00	•	Meeting with R.J. Gowan (DIAND) to discuss offshore borehole locations, and program planning.  Prepare field equipment.
13:00	•	Depart camp to layout "New Prospect" boreholes located approx. 4 km north of Pullen Island. D6 cat clearing access road to "New Prospect" location.
18:30	•	Access cleared to two borehole locations at "New Prospect" site, return to camp.
19:05	•	Arrive camp, loader still working on ice road.  MSD drill rig and drill container in camp.



## March 9, 1994

- Leave camp; haul rig on low boy pulling drill shack behind.
- Rig on-site at BH 11413-02 ("New Prospect" GS6-3-S).
- Rig off-loaded; move to BH 11413-01 ("New Prospect" GS6-4-S).
- Rig on location BH 11413-01. Auger ice hole to draw water. Auger ice hole at borehole location prepare to drill.
- 14:00 Trip in HW casing.
- 20:30 Recover last sample; trip out.
- HW casing out of hole, rig down. Move all equipment to BH 11413-02 ("New Prospect" GS6-3-S).
- On location; prepare equipment to overnight on location.
- 22:00 Leave for camp.
- 22:30 Arrive at camp.

#### March 10, 1994

- 08:00
   Meeting to review MSD daily bills to date.
- 09:15 Leave camp.
- On location BH 11413-02 ("New Prospect" GS6-3-S). Preparation prior to drilling on-going.
- 11:45 Trip in HW casing.
- 12:20 Recover sample #1
- Final sample recovered.



19:30	•	All casing out of hole rig down, load drill rig on to low boy trailer. Prepare equipment to overnight on location.
20:00	•	Depart for camp.
20:30	•	Arrive camp.

## March 11, 1994

08:00	• Depart camp, travel to BH 11413-02 ("New Prospect" GS6-3-S).
09:00	<ul> <li>Move rig on low boy, pull drill shack with loader to BH 11413-03 ("Breaker's Shoal PS2-1-S).</li> </ul>
10:30	<ul> <li>Drill rig and drill shack on site. Set up and prepare to drill.</li> </ul>
12:15	• Recover sample #1.
20:45	Recover final sample; trip out.
21:15	Drill secure, depart for camp.
21:45	Arrive camp.

## March 12, 1994

08:15	Depart from camp.
08:35	• On site at "Breaker's Shoal" BH 11413-03.
09:00	• Move drill rig and ancillary equipment to BH 11413-04.
09:15	On location; set up to drill.
11:30	• Recover sample #1.
20:30	Recover final sample, trip out.



21:00	Leave	for	camp.
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21:30 • Arrive at camp.

## March 13, 1994

08:15	<ul> <li>Depa</li> </ul>	rt camp.
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08:45
 On site at BH 11413-04. Rig move.

Move to BH 11413-05 "Permafrost" GSC-TSD.

10:45 • On location set up to drill.

12:15 • Recover sample #1.

19:00 • Recover sample #16, trip out.

20:15 • Depart for camp.

20:45 • Arrive camp.

## March 14, 1994

• High winds from the west; decide to attempt to travel to rig.

08:30 • On-site BH 11413-05.

 Too windy to attempt rig move, decision made to extend hole in permafrost with NQ coring.

11:45 • HW casing set to 9.7 m.

• NQ core run #1; trial run to clear material in HW casing.

• End of borehole at 14.4 m after nine core runs. Trip out; secure rig.

16:30 • Depart for camp.



- 17:00
- · Arrive camp.
- Meeting with R.J. Gowan, discuss progress to date and schedule.

## March 15, 1994

- 08:00
- Depart camp.
- 08:35
- Arrive at rig located at BH 11413-05.
- 09:15
- · Begin rig move.
- 09:45
- On location BH 11413-06 "Non Permafrost", set up to drill.
- 11:00
- · Auger hole through ice, trip in HW casing.
- 11:25
- Recover first sample.
- 18:30
- · Recover final sample; trip out.
- 19:20
- · Depart from drill site.
- 19:55
- Arrive at camp.

## March 16, 1994

- 08:00
- Depart camp.
- 08:45
- Arrive at drill rig. Unable to start D6, tarp in and heat with master heaters, repair blade on loader.
- 11:15
- Begin move from BH 11413-06 to BH 11413-07.
- 11:45
- · On location, set up.
- 12:50
- Auger ice hole, trip in.
- 14:45
- Recover final sample, trip out.



16:20	• Begin move to BH 11413-08.
17:15	On location.
17:50	Trip in HW casing.
20:15	BH 11413-08 complete, trip out.
20:50	• Depart for camp.
21:30	Arrive camp.
March 17, 19	94
08:00	• Depart from camp.
08:45	<ul> <li>Arrive at drill rig located at BH 11413-08. Service drill rig. D6 clearing access to BH 11413-09.</li> </ul>
09:15	Prepare to move drill rig.
09:30	Begin rig move.
10:15	• Rig on location BH 11413-09.
10:45	• Recover sample #1.
-13:30	Recover final sample, trip out.
14:45	Begin rig move to BH 11413-10.
15:00	• Rig on location.
15:45	Recover first sample.
18:15	Borehole 11413-10 complete, trip out.
18:45	• Move rig to BH 11413-11.



17:55

18:30

19:15

20:00

19:00	•	Rig on location, prepare equipment to overnight on site.
19:15	•	Depart for camp.
20:00	•	Arrive camp.
March 18, 19	94	
08:00	•	Depart from camp. High winds overnight created snow drifts along ice road between camp and BH 11413-11. Loader clearing road with MSD and EBA personnel following behind.
09:30	•	Arrive at drill rig.
10:15	•	Auger ice hole, trip in HW casing.
13:00	•	Recover final sample trip out.
13:45	•	Begin rig move to BH 11413-12.
14:15	•	On location, set up to drill.
15:25	•	Recover first sample.
17:15	•	Recover final sample, trip out.

• Begin rig move to BH 11413-13.

• On location, pad cleared, set up.

• Depart drill site for camp.

• Arrive camp.



## March 19, 1994

08:00	Depart camp.
08:35	<ul> <li>Arrive at drill rig which is set up on BH 11413-13, auger ice hole and trip in HW casing.</li> </ul>
09:15	Obtain first sample.
10:50	Recover final sample, trip out.
11:30	• Begin rig move to BH 11413-14.
12:15	• On location BH 11413-14, set up to drill.
15:10	Borehole 11413-14 complete, trip out casing.
15:45	• Begin rig move to BH 11413-15.
16:00	• Rig on location.
16:45	Trip in HW casing.

Move drill rig to the location where low-boy trailer will pick it up.

## 20:30 • Leave site for camp.

• Recover final sample trip out.

21:00 • Arrive camp.

## March 20, 1994

19:20

20:15

08:00	<ul> <li>Crew departs camp with low-boy trailer to pick up drill rig.</li> </ul>
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- Drill rig arrives on site at MR2 Island location, off load drill rig.
- 12:00 Begin drilling BH 11413-16.



16:00	• Borehole complete, move to BH 11413-17.
17:15	Begin drilling.
20:00	Trip out hollow steam augers.
20:15	Depart drill site for camp.
20:30	Arrive camp.
March 21, 19	DQA
Maich 21, 12	<del> </del>
08:00	Depart from camp.
08:15	Arrive at drilling located at BH 11413-17.
08:45	<ul> <li>Begin drilling with solid augers to advance borehole to 13.7 m below top of ice.</li> </ul>
10:15	• Thermistor string installed in BH 11413-17, move drill rig to next location.
11:15	Begin drilling BH 11413-18 using solid augers.
12:00	Borehole complete; trip out.
12:30	Rig move.
13:15	• On location and set up at BH 11413-19.
14:00	Begin drilling.
18:30	Borehole terminated due to heaving sand; trip out.
19:30	Thermistor string installed, depart for camp.
19:50	Arrive camp.



## March 22, 1994

- Depart camp for drill rig located at BH 11413-19. Move drill to low bed trailer and load; travel to Target 6C-2.
- 12:00 Rig arrives at Target 6C-2, off load.
- D6 cat arrives at Target 6C-2, clear snow drift to access shoreline.
- 14:00 Begin rig move.
- On site BH 11413-20, set up.
- 15:15 Begin drilling.
- 18:00 End of borehole 11413-20.
- 18:30 Begin rig move.
- 19:00 Set up and ready to drill BH 11413-21.
- 20:00 End of shift; depart for camp.
- 20:30 Arrive camp.

## March 23, 1994

- 08:00
   Depart camp for drill rig.
- Arrive at drill rig, continue drilling and sampling BH 11413-21.
- Complete BH 11413-21, trip out and move rig.
- 13:00 Begin drilling and sampling BH 11413-22.
- 14:15 Complete BH 11413-22.
- On location BH 11413-23, begin drilling and sampling.



17:00	<ul> <li>Borehole complete; move equipment to Target 6C-1.</li> </ul>
17.00	Doronore complete, move equipment to rarger 00-1.

- 19:30 On location Target 6C-1.
- 20:00 Arrive at camp.

## March 24, 1994

08:00	•	Depart	camp.
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- Arrive at Target 6C-1, drill rig and ancillary equipment parked on ice road. Move to Borehole 11413-24.
- 99:30 Begin drilling BH 11413-24.
- Borehole complete, move rig to BH 11413-25.
- 13:30 Borehole 11413-25 complete, move rig to BH 11413-26.
- 14:30 Begin drilling BH 11413-26.
- Borehole 11413-26 complete, move equipment to ice road.
- Depart from ice road to camp.
- Depart camp with truck & trailer to haul D6 cat back to camp.

## March 25, 1994

- 08:00 Prepare for camp move.
- 08:45
   D6 departs pulling camp.
- 17:30 On location at Skiff Point.
- 18:15 Travel via snowmobile to conduct site reconnaissance.



20:15 • Arrive back at camp.

## March 26, 1994

- Depart from camp via snowmobile to select access route to travel to Target 4B-1.
- Return to camp, prepare drill rig and D6.
- 11:00 Depart from camp.
- 13:45 Arrive on location BH 11413-27,
- BH 11413-27 complete, move rig to BH 11413-28.
- "White out" conditions, depart drill site for camp.
- 17:30 Arrive at camp.

## March 27, 1994

- Travel from camp on snowmobiles to the drill rig and D6 which were left overnight on location.
- Return to camp to drop off snowmobile to geophysicist.
- 09:30 Return to drill rig.
- Arrive at drill rig, rig is moving to camp due to cold temperature and blowing snow. Drill shack (shelter) was not moved to drill location.
- Arrive at camp; prepare to demob camp to Inuvik.
- 14:45 Begin camp move.
- Camp on Tuk ice road at approx km 140. Depart for Inuvik.
- 17:30 Arrive Inuvik.



## March 28, 1994

• 00:80	Demob EBA	equipment from ca	mp located on the ice	road at Inuvik.
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Make arrangements with Challenger to conduct post-mission survey.
 Arrange with Continental Helicopters to conduct post mission survey.

11:45 Depart Inuvik for Caribou Creek. (Source 222).

• Off load drill rig and D6 at Caribou Creek, move to borehole location.

14:15 • Begin drilling BH 11413-28.

15:45 • Complete drilling BH 11413-28.

16:00 • Begin drilling BH 11413-29.

17:00 • Complete drilling BH 11413-29.

17:15 • Begin drilling BH 11413-30.

18:15 • Complete drilling BH 11413-30.

18:30 • Depart Caribou Creek.

19:15 • Arrive Inuvik.

## March 29, 1994

08:00 • Depart Inuvik.

• Arrive at Caribou Creek site, move drill rig to BH 11413-31.

10:00 • Begin drilling.

11:00 • BH 11413-31 complete.

11:15 • Begin drilling BH 11413-32.



12:15	• BH 11413-32 complete. Move rig to low bed trailer.
12:30	DIAND Land Use Officers on-site.
13:15	Depart Caribou Creek.
14:00	Brief meeting with M. Collie at DIAND office.
15:00	Finalize bills with MSD.

## March 30, 1994

08:00	<ul> <li>Deliver soil samples and EBA equipment to Points North Transport.</li> </ul>
13:00	Vic Hut (Challenger Surveys) arrives Inuvik.
14:00	<ul> <li>Locate survey control movements in Inuvik, conduct post mission survey at Caribou Creek site.</li> </ul>
19:30	Survey complete, arrive Inuvik.

## March 31, 1994

07:45	• Depart Inuvik for Continental Helicopter's hangar.
08:45	<ul> <li>Depart Continental hangar to conduct post-mission survey.</li> </ul>
19:50	• Depart Target 6C-2 (Wallace Bay), return to Inuvik.
20:45	Arrive at Continental hangar, unload helicopter.
21:15	Arrive Inuvik.



## April 1, 1994

09:00	•	Depart Inuvik for Continental Helicopter's hangar.
09:30	•	Depart hangar to complete post-mission survey at Target 6C-1, 6C-2 and 4B-1.
15:50	•	Post-mission survey complete, depart Target 4B-1 for Inuvik.
16:35	•	Arrive Inuvik airport.
18:30	•	Depart Inuvik on AC Flight #8958.
22:00	•	Arrive Edmonton International Airport.



# APPENDIX B BOREHOLE LOGS



## GENERAL CONDITIONS

#### A.1 USE OF REPORT AND OWNERSHIP

This geotechnical report pertains to a specific site and development. It is not applicable to adjacent sites nor is it valid for types of development other than that to which it refers. Any variation from the site, or development, necessitates a geotechnical review in order to determine the validity of the design concepts evolved herein.

This report is not to be reproduced in part or in whole without consent in writing from EBA Engineering Consultants Ltd. (EBA). Additional copies of the report, if required, may be obtained upon request. Isolated information, logs of borings, or profiles are not to be reproduced, copied or transferred.

## A.2 NATURE AND EXACTNESS OF SOIL DESCRIPTION

Classification and identification of soils are based upon commonly accepted methods employed in professional geotechnical practice. This report contains descriptions of the systems and methods used. Where deviations from the system prevail, they are specifically mentioned.

Classification and identification of soil and geologic units are judgmental in nature as to both type and condition. EBA does not warrant conditions represented herein as exact, but infers accuracy only to the extent that is common in practice.

#### A.3 LOGS OF BORINGS

The boring logs are a compilation of conditions and classification of soils as obtained from field observations and laboratory testing of selected samples. Soil zones have been interpreted. Change from one geologic zone to the other, indicated on the logs as a distinct line, is in fact, transitional. The extent of transition is interpretive. Any circumstance which requires precise definition of soil zone transition elevations may require special evaluation.

## A.4 STRATIGRAPHIC AND GEOLOGIC SECTIONS

The stratigraphic and geologic sections indicated on drawings contained in this report are evolved from logs of borings. Stratigraphy is known precisely only at the locations of the borings. Actual geology and stratigraphy between borings may vary from that shown on these drawings. Natural variations in geologic conditions are inherent and a function of historic environment. EBA does not represent the conditions illustrated as exact but recognizes that variations will exist. Where knowledge of exact locations of geologic units is necessary, it is cautioned that such determination requires special attention.

#### A.5 GROUNDWATER CONDITIONS

Groundwater conditions represented in this report refer only to those observed at the times recorded on logs of borings, and/or within the text of this report. These conditions vary with geologic detail between borings; annual, seasonal and special meteorologic conditions; and with construction activity. Where instruments have been established to record groundwater variations on an ongoing basis, the records will be specifically referred to. Interpretation of groundwater conditions from observations and records is judgmental and constitutes an evaluation of circumstances as influenced by geology, meteorology and construction activity. Deviations from these observations, may occur. No other warranty. express, or implied, is made by EBA.

## A.6 PROTECTION OF EXPOSED GROUND

Excavation and construction operations expose geologic materials to meteorological elements. Many geologic materials deteriorate rapidly upon exposure to climatic elements. Severe deterioration of materials may be caused by precipitation and/or the action of frost on exposures. Unless otherwise specifically indicated in this report, walls and floors of excavations must be protected from elements, particularly all forms of moisture, desiccation from arid conditions and frost action.

## SYSTEM INTERNATIONAL UNITS

QUANTITY	NAME	SYMBOL	EXPRESSED IN TERMS OF OTHER SI UNITS	EXPRESSED IN TERMS O BASE AND SUPPLEMENTARY UNITS
SI UNITS	·			
length	metre	m		
mass	kilogram	kg		
time	second	5		
electric current	ampere	A		
thermodynamic temperature	kelvin	K		
amount of substance	mole	mol		
luminous intensity	candela	çd		
SI SUPPLEMENTARY UNITS				
plane angle	radian	rad		
solid angle	steradian	sr		
EXAMPLES OF SI DERIVED UNITS WITH SPE	CIAL NAMES	•		
frequency	hertz	Hz	1/s	s:1
force	newton	N	m - kg/s²	m,⊹kg - s²
pressure, stress	pascal	Pa	N/m²	m <sup>-1</sup> - kg · s <sup>2</sup>
energy, work, quantity of heat	joul <b>e</b>	J	N - m	m² - kg - s²
power, radiant flux	watt	w	J/s	m² · kg · s ³
EXAMPLES OF SI DERIVED UNITS WITHOUT	SPECIAL NAMES			
velocity - linear	metre per second		m/s	m · s <sup>.1</sup>
- angular	(radian per second)		rad/s	rad - s 1
acceleration - linear	(metre per second) per second		m/s <sup>2</sup>	m · š <sup>.2</sup>
- angular	(radian per second) per second		rad/s²	rad - s <sup>2</sup>
concentration (of amount of substance)	mote per cubic metre		mo!/m³	mol · m·3
dynamic viscosity	pascal second		Pa · s	$m^{-1} + kg + s^{-1}$
moment of force	newton metre		N · m	m² · kg · s²
surface tension	newton per metre		N/m	kg · s <sup>, z</sup>
heat flux density, irradiance	watt per square metre		W/m²	kg⊹\$³
heat capacity, entropy	joula per kelvin		J/K	m2 + s-2 K-1
specific heat capacity, specific entropy	joule per kilogram kelvin		J/(kg - K)	m² - s -2 - K 1
specific energy	joule per kilogram		J/kg	m2 · 5·2
thermal conductivity	watt per metre kelvin		W/(m · K)	m - kg - s <sup>-3</sup> - K <sup>-1</sup>

## OTHER UNITS PERMITTED FOR USE WITH SI

QUANTITY	NAME	SYMBOL	DEFINITION
time	minute	min	1 min = 60 s
	hour	h	1 h = 3,600 s
	day	đ	1 d = 86,400 s
	year	a	
plane angle	degree	÷	1' = ('/180) rad
	minute	•	1' = (^/10,800) rad
	second	.,	1" = (*/648,000) rad
area	hectare	há	1 ha = 10,000 m²
valume	litre	L	1,000 L = 1 m <sup>3</sup>
temperature	degree Celsius	⁺C	0° C = 273.15° K
			temperature interval 1 C = 1 K
mass	tonne	t	1 t = 1,000 kg = 1 Mg

,000,000,000,000,000,000 = 1018	exa	E	0.1 = 10 <sup>1</sup>	deci*	d
1,000,000,000,000,000 = 1016	peta	ρ	0.01 = 10 <sup>2</sup>	centi*	c
1,000,000,000,000 = 1012	tetra	T	$0.001 = 10^{-3}$	milli	m
1,000,000,000 = 109	giga	G	$0.000,001 = 10^{8}$	micro	M
1,000,000 = 106	mega	М	0.000,000,001 = 10 9	nano	п
1,000 = 103	kilo	k	$0.000,000,000,001 = 10^{-12}$	pico	р
100 = 10°	hecto*	h	$0.000,000,000,000,001 = 10^{-15}$	femto	f
10 = 101	deca*	da	$0.000,000,000,000,000,001 = 10^{18}$	atto	a

\* to be avoided where possible



				_	UNIFIED SOIL	CLASSIFICATION†
	MAJO	OR DIVIS	IONS	GROUP SYMBOLS	TYPICAL NAMES	CLASSIFICATION CRITERIA
sieve"  AVELS  r more of  r faction  No. 4 sieve  CLEAN GRAVELS			GRAVELS	GW	Well-graded gravels and gravel-sand mixtures, little or no fines	$C_{c} = \frac{D_{60} D_{10}}{\frac{2}{G}} \qquad Greater than 4$ $C_{c} = \frac{(D_{30})^{2}}{D_{10} \times D_{50}} \qquad Between 1 and 3$
.S Sieve*	GRAVELS 50% or more of coarse fraction retained on No. 4 sieve	CLEAN	GP	Poorly-graded gravels and gravel-sand mixtures, little or no fines	Not meeting both criteria for GW  Not meeting both criteria for GW  Not meeting both criteria for GW  Atterberg limits plot below 'A' line or plasticity index less than 4  Atterberg limits plot above 'A' line and plasticity index greater than 7  Atterberg limits plot above 'A' line quiring use of dual symbol and plasticity index greater than 7	
IIOS Q	No. 20	GF 50% coar	GRAVELS WITH FINES	GM	Silty gravels, gravel-sand-silt mixtures	Atterberg limits plot below 'A' line Atterberg limits plotting or plasticity index less than 4 in hatched area are bor-
AINE	E-GRAINE	GRA WI	GC	Clayey gravels, gravel-sand clay mix- tures	Atterberg limits plot above 'A' line quiring use of dual symbols  Atterberg limits plot above 'A' line quiring use of dual symbols	
ARSE-GF		coarse 4 sieve	CLEAN SANOS	sw	Well-graded sands and gravelly sands, little or no fines	and plasticity index greater than 7 bols $C_{0} = D_{60}/D_{10}  \text{Greater than 6}$ $C_{0} = D_{60}/D_{10}  \text{Greater than 6}$ $C_{0} = \frac{(D_{30})^{2}}{D_{10} \times D_{60}}  \text{Between 1 and 3}$ Not meeting both criteria for SW  Atterberg limits plot below 'A' line or plasticity index less than 4  Atterberg limits plotting in hatched area are borderine classifications re-
8		SANDS More than 50% of coarse Iraction passes No. 4 sieve	CLEAN	SP	Poorly - graded sands and gravelly sands, little or no fines	Section 10 Section 1 Section 1 and 3  Co = (D <sub>30</sub> ) <sup>2</sup> Co = (D <sub>30</sub> ) <sup>2</sup> Between 1 and 3  Not meeting both criteria for SW  Not meeting both criteria for SW  Atterberg limits plot below 'A' line or plasticity index less than 4  Atterberg limits plotting in hatched area are bor-
			IDS TH ES	SM	Silty sands, sand-silt mixtures	Atterberg limits plot below 'A' line Atterberg limits plotting in hatched area are bor-
			SANDS WITH FINES	sc	Clayey sands, sand-clay mixtures	Atterberg limits plot above 'A' line quiring use of dual symbols  Atterberg limits plot above 'A' line quiring use of dual symbols
		AYS	sailts and fine fraction of coars  Inorganic clays of tow to medium plasticity, gravelly clays, tandy clays, sifty clays, lean clays  CL plasticity, gravelly clays, tandy clays, sifty clays, lean clays	ML	rock flour, silty or clayey fine	PLASTICITY CHART For classification of fine-grained
SOILS	200 sieve	SILTS AND CLAYS		grained toils Atterburg limits plotting in hatched CH		
FINE-GRAINED SOILS	sasses No.	SILT	תו ,	OL	Organic silts and organic silty clays of low plasticity	E 30 Equition of A line: PI = 0.731CL - 201
FINE-GF	50% or more passes No. 200 sieve	CLAYS	2036	мн	Inorganic silts, micaceous or diato- maceous fine sands or silts, elastic silts	20 CL MH & OH
	S	SILTS AND CLAYS	greater than 50%	СН	Inorganic clay of high plasticity, fat clays	10 7 4 35 ML & OL
		SILT	84,6	он	Organic clays of medium to high plasticity	0 10 20 30 40 50 60 70 80 90 100 L(QUID LIMIT
н	GHLY	ORGANIC	SOILS	PT	Peat, muck and other highly organic soils	*Based on the material passing the 3 in. {75 mm} sieve †ASTM Designation D 2487, for identification procedure see D 2488

## **GROUND ICE DESCRIPTION**

#### ICE NOT VISIBLE

GROUP SYMBOLS	SYMBOLS	SUBGROUP DESCRIPTION	
] 	Nf	Poorly-bonded or friable	17
N	Nbn	No excess ice, well-bonded	
	Nbe	Excess ica, walt - bonded	

#### NOTE:

- Duel symbols are used to indicate borderline or mixed ice classifications
- 2. Visual estimates of ice contents indicated on borehole logs ± 5%.

  3. This system of ground ice description has been modified from NRC Technical Memo 79, Guide to the Field Description of Permafrost for Engineering Purposes. Purposes

#### LEGEND

Soil

ice 💮

#### VISIBLE ICE LESS THAN 50% BY VOLUME

GROUP SYMBOLS	8YMBOLS	SUBGROUP DESCRIPTION	
v	Vx	Individual ice crystals or inclusions	
	Vc	Ice coatings on particles	3
	Vr	Random or irregularly oriented ice formations	
	Vs	Stratified or distinctly oriented ice formations	

#### VISIBLE ICE GREATER THAN 50% BY VOLUME

ICE	ICE + Soil Type	ice with sait inclusions	
	ICE	ice without soil inclusions (greater than 25 mm (1 in.) thick)	

GEOLG	IGICAL EVALUATION	INDIAN AN	IN MADTUE	RN AFFAIRS CANA	D.A.			DODEHOLE	- NO. 1	1417 0	
느	T "CS6-4-S NEW PROSPECT"	<del>                                     </del>		HW CASING	JUA		$\rightarrow$	BOREHOLE PROJECT		<u> 1413-0</u>	-
	ORT SEA WATER DEPTH: 7.2m	<del></del>		5632.1 E522548.	7		-	ELEVATION			
	LE TYPE DISTURBED NO RECOVER	<u> </u>		■ A-CASI		Г		HELBY TUBE		CORE	_
					<u> </u>	1		1	<u> </u>		
DEPTH(m)	SOIL		GR	OUND ICE	TURE (C	TYPE	E NO	10	SALINITY (	opt)∎ 80 40	(£)
DEPI	DESCRIPTION		DES	CRIPTION	EMPERATURE (C)	SAMPLE	SAMPLE	PLASTIC I	M.C.	LIQUID	DEPTH(ft)
0.0	CLAY (CL) — silty, trace of sand, trace of shell fragments, homogeneous, moist		Not frozer	1	-		1	20	40 6	08 0	0.0
-	to wet, dark olive grey (5Y 3/2)  - low plastic, very dark grey (5Y 3/1)				-1.2		2	••,	•		شسترستة
- - -							3	• •			2.0
1.0 - - -							4	•			4.0
-							5				6.0 e.u
— 2.0 - - - -	SAND (SM) — silty, trace of shell fragments and coal fragments, fine grained, massive, wet to saturated, non plastic, dark olive grey(5Y 3/2)				:		6	•			8.0
- - - 3.0	<ul> <li>some rounded gravel</li> <li>5mm thick black organic lense</li> <li>with interbedded clay lenses</li> </ul>						7	•			10.0
- - -	<ul><li>organic wood fragments</li><li>very dark grey (5Y 2.5/1)</li></ul>						8				12.0
- - 4.0					-0.21		9	•			14.0
- 5.0	SAND (SM) AND SILT — some clay, trace of gravel and organics, with interbedded lenses of silty clay, moist, non plastic, very dark grey (5Y 3/1)						10	•			16.0
	— shell fragments						11	•			18.0
6.0							12				<u> </u>
	A ENGINEERING CONSULT	<u>, П</u>	<u>Т ТР</u>	LOGGED BY: SEE		ш.		COMPLE	TION DEP	TH: 10.5 m	F
ĽL		CIVIH	LID.	REVIEWED BY: M.					TE: 94/0	3/09	
/02/14 03	EDMONTON, ALBERTA	_		Fig. No: 11413-	-01					Page 1	of 2

		DIAN AN	ND NORTHER	N AFFAIRS CANADA	1		Ţ	BOREHOLE	NO: 1	1413-0	1
	·		ME750 c/w I				-	PROJECT N			
				632.1 <u>E522548.7</u>			_	ELEVATION:		<del>- ` ´                                  </del>	
SAMPI	E TYPE DISTURBED NO RECOVERY	$\square$	SPT	A-CASING	;	, Щ	j SH	ELBY TUBE	[]	CORE	-,
ОЕРТН(м)	SOIL DESCRIPTION			UND ICE	TEMPERATURE (C)	SAMPLE TYPE	SAMPLE NO	10 PLASTIC	ALINITY (2 20 M.C.	ppt) ■ 30 40 LIQUID	DEPTH(ft)
6.0	CAUD (CA) AND CHIT							20	40 8	80 80	
- 7.0	SAND (SM) AND SILT — (continued)			i	~0.81		12 13				22.0
	- 15mm thick organic lense						15				24.0
- 8.0	CLAY (CL) — silty, with interbedded lenses of silty sand, moist, low plastic, very dark grey to black clay, olive grey sand						16				26.0 28.0 28.0
9.0	- 200mm thick sand lense						18				30.0
- - 10.0		j		;			9				32.0
-	END OF BOREHOLE (10.5 metres)  Note: Logged by Geological Survey of Canado, Atlantic Geoscience Centre					4					34.0
- 11.0	personnel.										38.0
EF	BA ENGINEERING CONSULTAN	VTS	LTD	LOGGED BY: SEE				_		PTH: 10.5 m	
ewan in	EDMONTON, ALBERTA	.,	<b></b> .	REVIEWED BY: MAY Fig. No: 11413-0				COMPLET	t: 94/0	03/09 Page 2	of 2

GEOL	OGICAL EVALUATION .	ΙΝΠΙΑΝ ΔΝΟ Ν	NORTHERN AFFAIRS CANADA		_		BOREHOLE NO: 11413-02	
<b></b>	ET "GS6-3-S NEW PROSPECT"	<b> </b>	50 c/w HW CASING	•	_	$\rightarrow$	PROJECT NO: 0101-11413	
BEAU	FORT SEA WATER DEPTH: 7.2m		8 N7746098.6 E524298.4			$\rightarrow$	ELEVATION: -7.20 (m)	_
SAME	PLE TYPE DISTURBED NO RECOVERY	r SPT	A-CASINO	3			HELBY TUBE CORE	
DEPTH(m)	SOIL DESCRIPTION		GROUND ICE DESCRIPTION	remperature (c)	SAMPLE TYPE	SAMPLE NO	■ SALINITY (ppt) ■ 10 20 30 40  PLASTIC M.C. LIQUIO	DEPTH(ft)
0.0	SILT (ML) - some sand, trace of clay, fine	Not	frozen	-			20 40 60 80	0.0
-	groined, uniform, with thin interbedded silty clay lenses, wet to saturated, non plastic, dark olive grey (5Y 3/2)	NOT	Irozen			2		2.0
- 1.0 - - - - -	— trace of coarse grained rounded gravel, trace of shelf fragments					3	dhumumhumumh	4.0
- - - - 2.0 -	- organics and coal fragments  disseminated throughout  CLAY (CL) — silty, trace of sand, trace of organics disseminated throughout,					4	Line of the state	6.0
- - - - - 3.0	with interbedded lenses of clayey silt and silty sand, maist to wet, low plastic, very dork grey (5Y 3/1)					5		8.0 10.0
- - - - -		į				7		12.0
4.0    	— shell fragments disseminated lhroughout					8		14.0
- - 5.0 - - -	- massive			0.08		9		8.0
6.0	- with interbedded lenses of silty sond, dark grey		LOCOED BY OFF	NOTE		1)	•	;
E)	BA ENGINEERING CONSULT	ANTS LI	TD. LOGGED BY: SEE I				COMPLETION DEPTH: 11.0 m COMPLETE: 94/03/10	$\dashv$
5/02/14 0	EDMONTON, ALBERTA		Fig. No: 11413-0			_	Page 1 of	2

GEOLG	OCICAL EVALUATION	INDIAN AND NORTH	ERN AFFAIRS CANADA			BOREHOLE	NO: 1141.	3 02
	T "GS6-3-S NEW PROSPECT"	DRILL: CME750 c/				<del></del>	0: 0101-114	
	ORT SEA WATER DEPTH: 7.2m		746098.6 E524298.4			_	-7.20 (m)	
SAMP	LE TYPE DISTURBED NO RECOVER		■ A-CASING			SHELBY TUBE	CORE	
DEPTH(m)	SOIL DESCRIPTION	GI	ROUND ICE	RE (C)	3 5		SALINITY (ppt) ■ 20 30 4	DEPTH(ft)
6.0	CLAY (CL) (applicated)			- 1	1	20	40 60 8	30
- 7.0	CLAY (CL) — (continued)  — dark grey to black			į				22.0
					1			24.0
8.0	SAND (SP/SM) — trace of silt, clay, shell fragments and rounded gravel, black organics throughout, with interbedded lenses of silty clay, non plastic, dark grey (5Y 4/1) — fine fibrous organics disseminated throughout, massive	!		-0.04	11			28.0
- 9.0 -	<ul> <li>inclined 30mm lense of coarse fibrous organics, 20mm long wood fragment</li> </ul>				1			30.0
10.0	- some silt, some clay -				18			34.0
-	END OF BOREHOLE (11.0 metres)  Note: Logged by Geological Survey of Canada, Atlantic Geoscience Centre personnel.				19			36.0
12.0	A Discourance concurr	1 March 1 mg	LOGGED 8Y: SEE N	IOTE			ION DEPTH: 1	<u> </u>
	BA ENGINEERING CONSULT  EDMONTON, ALBERTA	ANTS LTD.	REVIEWED BY: MAV Fig. No: 11413-02				E: 94/03/10	age 2 of 2
5/02/14 D3	TOPE							

GEOLO	GICAL EVAI	LUATION		INDIAN A	ND NORTH	IERN AFFAIRS CANADA	<del>-</del>		[ E	BOREHOLE	NO: 1	1413-03	3
TARGE	T "PS2-1-	-s breaker's sho	AL"	DRILL: C	ME750 c/	w HW CASING		-		PROJECT N			·
	ORT SEA					746466.5 E534579.8				LEVATION:	-6.30 (	m)	-
SAMP	LE TYPE	DISTURBED	NO RECOVERY		SPT	A-CASING	3		∏ SH	elby tube		CORE	
DEPTH(m)		SO Descri				ROUND ICE	TEMPERATURE (C)	SAMPLE TYPE	SAMPLE NO		SALINITY (pp 20 30		DEPTH(ft)
2		DESCRI	PHON		Մե	SCRIPTION	TEMPE	SAM	SA	PLASTIC	M.C.		범 
0.0	gra gra	<b>1)</b> — some silt, so vel and shell fragi ined, uniform, wel i plastic, dark oliv	to solurated,		Not froz	en			1	20	40 60	80	0.0
1.0	org thir	) — silty, trace of onic pockets throu interbedded sand stic, dark olive gre	ughout, with Henses, low	<b>-</b>					2	•			2.0
									3	•			4.0
2.0									4				6.0
									5	•			8.0
3.0									6	•			10.0
4.0	– mas	sive							7	•			12.0
	– trac	e of shell fragmer	nts						8 .				14.0
5.0	– very	dark grey to blac	k						9	•			16.0
									10				- 18.0
_6.0 1∵1	) A 17314		COMOTION	A NIMO	I WL	LOGGED BY: SEE	NOTE	Ш		COMPLET	ION DEPT	H: 13.0 m	<u> </u>
Li	SA LIN		CONSULTA	ANTS	LTD.	REVIEWED BY: MAY	V				E: 94/03	3/11	
02/14 03	2029	<u>EDMONTO</u>	N, ALBERTA			Fig. No: 11413-0	)3			1		Page 1	of 3

GEOLO	GICAL EVALUATION	INDIAN AND NORTHE	RN AFFAIRS CANADA		BOREHOLE NO: 11413-03	
	T "PS2-1-S BREAKER'S SHOAL"	DRILL: CME750 c/w	-		PROJECT NO: 0101-11413	
-	ORT SEA WATER DEPTH: 6.3m	UTM ZONE: 8 N774		-	ELEVATION: -6.30 (m)	
	LE TYPE DISTURBED NO RECOVERY		A-CASING		SHELBY TUBE CORE	
ОЕРТН(м)	SOIL DESCRIPTION	GR	OUND ICE SCRIPTION	SAMPLE TYPE SAMPLE TYPE SAMPLE TYPE	SALINITY (ppt) = 10 20 30 40  PLASTIC M.C. LIQUID	DEPTH(ft)
6.0	CLAY (CL) ~ (continued)				20 40 60 80	20.0
- - - - - - 7.0	- mossive			11		- 20.0 - 22.0
				13	5	— 24.0 –
- 8.0 -	- 15mm thick lense of fine grained			14		— 26.0 -
-	silty sand, dark olive grey			15		28.0 
- 9.0 - -				16		- 30.0 -
- - - 10.0				17		- 32.0 -
-				18		- 34.0 -
— 11.0 - - - - -				19		- 36.0 -
12.0	A DIAMERDIA CANCER	ANIMO LED	LOGGED BY: SEE NO	20	COMPLETION DEPTH: 13.0 m	- 38.0 - -
EE	BA ENGINEERING CONSULT	ANTS LTD.	REVIEWED BY: MAV	,,, <u>,</u>	COMPLETE: 94/03/11	$\dashv$
<del> 5/02/14 03</del>	EDMONTON, ALBERTA		Fig. No: 11413-03		Poge 2	of 3

GEOLOGIC	CAL EVAL	UATION		INDIAN A	ND NORTH	ERN AFFAIRS CANA	DA		<del></del> T	BOREHOL	E NO:	114	13-03	ζ
TARGET "	'PS2-1-	S BREAKER'S SHO				W HW CASING			<del></del>	PROJECT				
BEAUFOR	T SEA	WATER DE	PTH: 6.3m	UTM ZON	IE: 8 N77	46466.5 E534579.	8			ELEVATION	√: -6.3	0 (m)	-	
SAMPLE	TYPE	DISTURBED	NO RECOVERY	$\boxtimes$	SPT	A-CASI	NG		∏ Sł	HELBY TUB	<u> </u>	Co	RE	
DEPTH(m)		SO DESCRI				COUND ICE	TEMPERATURE (C)	SAMPLE TYPE	SAMPLE NO	10 PLASTIC	I SAUNITY 20 M.C		40 LIOUID	DEPTH(ft)
12.0 CI	AV (CL)	. (aastisusd)	<del></del>					$\downarrow$		20	40	60	80	<u> </u>
	DAT (GL)	– (continued)							21	F	• 1			40.9 40.9
- 13.0 FA	ID OE BO	DREHOLE (13.0	matros						22					42.
	Note: Cana	Logged by Geolog ado, Atlantic Geos annel.	jical Survey of											44,0
- 14.0														46.1
- 15.0														48.4
							5 5 5 5 5 5							50.
- 16.0														52.0
														54.(
- 17.0														56.0
							:							58.0
18.0   IZID A	DMC		CONOLLIM	A NIMO	I WIL	LOGGED BY: SEE	NOTE			COMPL	TION D	EPTH.	13.0 m	
ГRA	LENC		CONSULT	ANTS	LTD.	REVIEWED BY: M	AV				TE: 94			
02/14 03:23Pk		EDM <u>ONTO</u>	<u>n, alberta_</u>			Fig. No: 11413-	-03						Page 3	of 3

OF OLO	Olon Curr	LIATIONI	<del> </del>	ILIO ALCONO	UD NORTH	TON AFFERDO OF THE			T.	20052-5	10 44	447 ^	
	GICAL EVAL	uation S Breaker's Shoa			· · · · - · - · - · - · - · - · - ·	RN AFFAIRS CANA HW CASING	NUA		_	BOREHOLE NO PROJECT NO		413-04	}
	ORT SEA	WATER DEP				16653.3 E535344	a		—⊬	LEVATION:			
	E TYPE	DISTURBED	NO RECOVERY		SPT	######################################				ELBY TUBE	-0.30 (ii	- <u>i-</u>	
		SOI				OUND ICE		TYPE	- 9		LINITY (ppt) 20 30		(£)
DEPTH(m)		DESCRI			DES	SCRIPTION	TEMPERATURE (C)	SAMPLE	SAMPLE	PLASTIC -	M.C.	FIOND	DEPTH(ft)
0.0	blac thro sand plas	- silty, trace of sk organics dissem ughout, with intertal lenses and string tic, dark olive grey	iinated bedded silty gers, low		Not froze	1			1	20	40 60	80	0.0
- - - 1.0 -	– with strin to b	k (5Y 2.5/1) clay silt and silt s gers, very dark gr lack (5Y 2.5/1) c organic coal frag	rey (5Y 3/1)						3				4.0
- - 2.0	– mas:	sive, very dark gre	ey to black						4				6.0 6.0
- - - - - - - - 3.0									5				8.0
J.U	– 2mm	thick black organ	nic lense						6	•			10.0
- 4.0									7	<u> </u>			12.0
									8				14.0
- 5.0									9	. •			16.0
6.0	– homo	ogeneous							10	•			18.0
	3	GINEERING	СОМСПП	 A NI파이	1 MD	LOGGED BY: SE		<u></u> -		COMPLETI			·
	DA EIV		N, ALBERTA	GIVIH	ыπ.	REVIEWED BY: I Fig. No: 11413				COMPLETE	94/03/	/12 Page 1	of 2

CEOLO	OGICAL EVAL	LIATION		INICIANI A	NO NOOTUE	RN AFFAIRS CANADA			<del> ,</del>	DODELIALE	NO. 114	17 04	
		-S BREAKER'S SHOA				HW CASING				BOREHOLE PROJECT NO		<u>13-04</u>	•
	ORT SEA	WATER DEF				16653.3 E535344.9			-	ELEVATION:			
	LE TYPE	DISTURBED	NO RECOVERY		SPT	A-CASING	,	П		HELBY TUBE	0.50 (11)		
DEРТН(m)		S0 DESCRI			GR	OUND ICE SCRIPTION	TEMPERATURE (C)	SAMPLE TYPE	SAMPLE NO	10 PLASTIC	AUNITY (ppt) II 20 30 M.C.	40	DEPTH(ft)
6.0	CLAY (CL	) - (continued)								20	40 60	80	20.0
- - - -	– 10n	nm thick fine grain se, very dark grey				4 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9			11				22.0
7.0	— trac	e of shell fragmer	nts						12	•			24.0
- - - 8.0		nm thick fine grain	ed silt sand						14	Ħ			25.0
- - - - - 9.0	lens	se							15	•			28.0
-									16	<b>⊢</b>			32.0
- 10.0	coa diss prec moi	) — silty, some alerse grained sand perminated throughout dominately fine grast, non plastic, very (5Y 3/2)	particles out, iined, uniform,						18				— 34.0 _
- 11.0 - - -	END OF B	OREHOLE (11.5	metres)						19	•			— 36.0 —
12.0	Con	Logged by Geologi ada, Atlantic Geos connel		:									- 3 <b>8</b> .0
E]		GINEERING EDMONTO	CONSULTA N. ALBERTA	ANTS	LTD.	LOGGED BY: SEE N REVIEWED BY: MAV Fig. No: 11413-0	'				ION DEPTH: E: 94/03/1		of 2

CEO! 4	ogical eval	HATION	<del></del> -	INDIAN 4	NO NODE	EDM AFERIOC ANNACE		DODE : 0: 5	NO 11117 OF	
	T "PERMAFI					ERN AFFAIRS CANADA • HW CASING		_	NO: 11413-05 10: 0101-11413	)
	ORT SEA					49497 E534832.7		<del></del>	-8.30 (m)	. <u>.</u>
	LE TYPE	DISTURBED	NO RECOVERY		SPT	= A-CASING	П	SHELBY TUBE	CORE	
DEPTH(m)					GF	ROUND ICE	6 Lu		SALINITY (ppt) III 20 30 40	DEPTH(ft)
BG		DESCR	IPTION		DE	SCRIPTION	TEMPER SAMP	PLASTIC  PLASTIC  20	M.C. LIQUID 1 40 60 80	330
0.0		— clayey, massiv stic, grey	re, moist, low		Not froze	n		1		0.0
- 1,0	fine	/SM) — trace of grained, uniform yish brown	silt and organics, , non plastic,	· <b>-</b>				2		4.0
- 2.0								3		6.0
- 3.0		e of fibrous orgo Iaminae	nics, with thin					5		8.0
- <b>3.0</b>								6		10.0
- 4.0		e to some silt, tro rel, with very thin						7		12.0
	- trace	e of coarse grain	ed gravel					В		_
- 5.0	CLAY (CL)	— silty, trace of	hlack					9		16.0
6.0	orga thro	nic pockets disse ughout, moist to tic, dark alive gre	minated wel, low				1	0		— 18.0 —
	BA ENG	GINEERING	CONSULTA	ZTN A	LTD	LOGGED BY: MAV			ION DEPTH: 14.5 m	
141	211 DIII		N, ALBERTA	ичго	цIV.	REVIEWED BY: MAV Fig. No: 11413-0		COMPLET	E: 94/03/14 Page 1	of 3
/02/14 D.	3 26PW	TD III O I I I	, HUDDINIA		_	[14], AO, 11713 U.		1	i age i	9, 9

[ <u>050.0</u>	OVOLUS FUNDAMENTON	Г								<del>-</del>	
	CICAL EVALUATION		NO NORTHERN A				$\rightarrow$	BOREHOLE N		<u>3-05</u>	
J	T "PERMAFROST"  ORT SEA WATER DEPTH: 8.3m		ME750 c/w HW ( E: 8 N7749497		··	-	-	PROJECT NO		415	
	LE TYPE DISTURBED NO RECOVERY			<del></del>		П		ELEVATION: -			
SAMIL	T ILLE MO RECORER	<u>' 🖂</u>		A-CASING		Li	∏ 2⊦	ielby Tube	COR	E	
DEPTH(m)	SOIL		GROUN	D ICE	FEMPERATURE (C)	SAMPLE TYPE	ON 3	■ SA 10 2	LINITY (ppt) <b>■</b> 20 30	40	DEPTH(ft)
DEPT	DESCRIPTION		DESCRI	PTION	TEMPERA	SAMPL	SAMPLE	PLASTIC I	M.C.	LIQUID	DEPī
6.0	CLAY (CL) - (continued)							20 4	0 60	80	20.0
	SAND (SP/SM) — trace of some silt, fine grained, uniform, non plastic			;			11				22.0
7.0 - - - - -	– 300mm thick interbedded clay lense			:			13				24.0
8.0							14				26.0
- - - - - - - 9.0			Frozen, Nbn, w	ell bonded	-1.21		15				— 28.0 —
-  -  -  -  -	— with interbedded clay lenses						16				- 30.0
- - - 10.0							17				-· 32.0
- -	<ul> <li>some silt, fine to medium grained sand, predominately fine grained</li> </ul>		Nbn				18				— 34.0 —
- 11.0 - -							19				— 36.0 —
12.0			li a	20ED DV 110:			20	Tooles say	DN DEDT		- 3B.O -
EF	BA ENGINEERING CONSULT	'ANTS		GGED BY: MAV VIEWED BY: MAV	/				ON DEPTH: : 94/03/14		
!	EDMONTON, ALBERTA		[INL	. No: 11413-0				COMPLETE		Page 2	of 3
5/02/14 03	2790									-9- 2	J. U

GEOLOGICAL EVALUATION	INDIAN AND NORTHERN AFFAIRS CANADA		BOREHOLE NO: 11413-05	5
TARGET "PERMAFROST"	DRILL: CME750 c/w HW CASING		PROJECT NO: 0101-11413	
BEAUFORT SEA WATER DEPTH: 8.3m	UTM ZONE: 8 N7749497 E534832.7		ELEVATION: -8.30 (m)	
SAMPLE TYPE DISTURBED 🛮 NO RECOVER	Y SPT = A-CASING	S [[]	HELBY TUBE CORE	
SOIL DESCRIPTION	GROUND ICE	TEMPERATURE (C) SAMPLE TYPE SAMPLE NO	■ SALINITY (ppt) ■ 10 20 30 40	DEPTH(ft)
DESCRIPTION	DESCRIPTION	SAMPLE T		DEPI
12.0 SAND (SP/SM) - (continued)		20	20 40 60 80	40.
		21		<u> </u>
- 13.0 — some silt to silty, medium grained sand particles disseminated throughout	Nbn	22		42
		23		6 44.
- 14.0		24		:::بالسسسياسية 46
END OF BOREHOLE (14.5 metres)  Note: Geological Survey of Canada, Terrain Sciences Division, Target "Permafrost". Borehole #94GSCBH01.				<del>Լլ. ու 18</del>
All samples retained by GSC-TSD.				50. E 50.
- 16.0				52. 52.
				54.
- 17.0				56. 56.
18.0				58.
EBA ENGINEERING CONSULT	ANTS LTD LOCGED BY: MAY	· · · · · · · · · · · · · · · · · · ·	COMPLETION DEPTH: 14.5 m	
EDMONTON, ALBERTA	REVIEWED BY: MAV Fig. No: 11413-05		COMPLETE: 94/03/14 Page 3	of 3

GEOLC	GICAL EVAL	UATION		ΙΝΩΙΔΝ Α	ND NORTHER	IN AFFAIRS CANADA			BOREHOLE	MO: 114	13 00	·
TARGET "NONPERMAFROST"							BOREHOLE NO: 11413-06 PROJECT NO: 0101-11413					
	ORT SEA		PTH: 9.2m	DRILL: CME750 c/w HW CASING UTM ZONE: 8 N7751537.4 E535938.2					ELEVATION:		-	
SAMPLE TYPE DISTURBED NO RECOVER									HELBY TUBE	3.20 (III)		
DEPTH(m)		<b>S</b> 0	<u> </u>			OUND ICE	<u> </u>	T	<b>=</b> 9	AUNITY (ppt) 1 20 30		(ft)
	-	DESCR			DES	CRIPTION	TEMPERATURE (C)	SAMPLE	1	M.C. 40 60	£IQUI0 ————————————————————————————————————	DEPTH(ft)
0.0	gra poc	— sitty, with ver ined sand lamina kets disseminated st, low plastic, of	e, black organic I throughout,		Not frozen			1				0.0
- 1.0								2				4.0
	– stiff	(est.), dark olive	grey					3				6.0
- 2.0	– silt	content increasing	ą, consistency			:		4				8.0
- 3.0	dec	reasing, becoming	g firm (est.)					5				10.0
4.0								7				12.0
								8				— 14.0 —
5.0								9				— 16.0 —
6.0	- very	thin laminae, eve	n, nonparallel					10				— 18.0 –
EF	BA ENG	GINEERING	CONSULTA	ANTS	LTD.	LOGGED BY: MAV REVIEWED BY: MAV				ON DEPTH:		
			N, ALBERTA	·	_ •	Fig. No: 11413-0			COMPLETE	: 94/03/1	J	

GEOLG	ogical evaluation	INDIAN A	นก มกอา	HERN AFFAIRS CANADA	<del></del>		Т	BOREHOLE 1	10. 114:	17 00	<del>.      </del>	
-	T "NONPERMAFROST"			/w HW CASING	<del>-</del>		$\rightarrow$	BOREHOLE NO: 11413-06 PROJECT NO: 0101-11413				
	ORT SEA WATER DEPTH: 9.2m	<del></del>		751537.4 E535938.2			$\overline{}$	ELEVATION: -9.20 (m)				
SAMP	LE TYPE DISTURBED NO RECOV		SPT	A-CASING				HELBY TUBE				
ЭЕРТН(m)	SOIL			ROUND ICE	TEMPERATURE (C)	TYPE	8	■ SA	LINITY (ppl) ■ 20 30		DEPTH(ft)	
6.0	DESCRIPTION		D.	ESCRIPTION	TEMPERA	SAMPLE	SAMPLE	PLASTIC I 20	M.C. 40 60	LIQUID 80	DEPT	
- - -	CLAY (CL) — (continued)  — thin lense of fine groined sond, son	ie					11				20.0	
- - - 7.0 -	silt, trace of black organics  - black organics disseminated throughout	į					12				22.0	
- - - -	— with very thin interbedded silty sand lenses						13				24.0	
8.0	ORGANIC SILT (OL) — trace to some clay, fibrous/organics throughout, moist, firm to stiff (est.), low plastic, dark grey						14				26.0	
- 9.0 - -	SILT (ML) — sandy, trace to some clay, fine grained sand, moist to wet, no to low plastic, light grey						16				30.0	
- - 10.0							17				— 32.0 —	
-   -   -	<ul> <li>trace of clay, sand content</li> <li>increasing with depth</li> <li>SAND (SM) AND SILT - trace of clay, fine grained, uniform, wet, non plastic,</li> </ul>		Note: G	eological Survey of			18				- 34.0 -	
- 11.0	olive grey trace of coarse grained sand particles		Canac Divisio "Nonf	da, Terrain Sciences on, Torget Permafrost". ole #94GSCBH2.	i		19				- 36.0 -	
	SILT (ML) — sandy, trace of shell fragments, homogeneous, non plosti dark olive grey END OF BOREHOLE (11.5 metres)	·	All sai GSC-	mples retained by ISD.							- 38.0 -	
	BA ENGINEERING CONSUL	 Т	T TID	LOGGED BY: MAV		<u></u>			ON DEPTH:			
٤			ыD.	REVIEWED BY: MAN				COMPLETE	: 94/03/15			
/02/14 03	EDMONTON, ALBERTA	_		Fig. No: 11413-0	D					Page 2	ot 2	

GRANI	JLAR RESOURCE EVALUATION	INDIAN	ND NORTH	RN AFFAIRS CANAE	}Δ			BOREHOLE	NO: 1	1413-0	7
	T "C1-9-S"	ORILL: CME750 c/w HW CASING  UTM ZONE: 8 N7751507.8 E537165.4					$\rightarrow$	PROJECT N			<i>'</i>
	ORT SEA WATER DEPTH: 9.2m						$\rightarrow$	ELEVATION: -9.20 (m)			
	LE TYPE DISTURBED NO RECOVERY		SPT	A-CASIN		Γ		HELBY TUBE		CORE	
					1	T		]		7 20.15	T
Ê	SOIL		GR	OUND ICE	) H	NPE	9	<b>■</b> S	AUNITY (	opl) <b>=</b>	1 🚓
DEPTH(m)				COND TOD	ATUR		띺	10	20 .	30 40 <u> </u>	Į ₹
뜅	DESCRIPTION		DES	SCRIPTION	TEMPERATURE (C)	SAMPLE TYPE	SAMPLE	PLASTIC	M.C.	LIQUID	DEPTH(ft)
					<u> </u>	က်	O		40 6	08 03	
0.0	CLAY (CL) - silty, (60mm thick)		Not frozer	1				- 20			0.0
	SAND (SP) - trace of silt, (40mm thick)						1	•			Ē
	CLAY (CL) — silty, sandy, black organic pockets disseminated throughout,	i									F
	very thin laminae, even, non										·Ę
	parallel, moist to wet, firm (est.),										2.0
	non lo low plastic, dark olive grey										Ē
1.0	SAND (SP) — trace of silt, homogeneous,						2	•			Ē
	fine grained, uniform, wet, non										Ē
	plastic, olive grey SILT (ML) — trace to some clay, black						3	•	-		4.0
	organic pockets disseminated	i									Ē
	throughout, very thin laminae, even,										Į.
	non parallel, moist to wet, firm					] [					Ē
	(est.), non to low plastic, dark olive grey								: :		6.0
2.0	SAND (SM) — some silt, trace of clay,						4	•			E
	trace of coarse grained subrounded	i			İ						Ę-
	gravel particles disseminated										E
	throughout, shell fragments										8.0
	<ul> <li>homogeneous, massive, olive</li> </ul>						5	•			Ē
3.0		į			İ						Ę
						П					10.0
						/		:			Ē
						/	6				
						V					<u> </u>
						П					12.0
						Ш					Ę
4.0							7	•			Ē
											Ē
											14.0
											Ē
i							8	•;		:	Ė
	END OF BOREHOLE (4.7 metres)										È E
5.0		İ					l				16.0
J.0											Ē
		į									E
								1 1			
ļ									ļļ		18.0
ĺ							İ		:		
									.		
6.0				LOOPED BY 1111	<u> </u>			Tool 15- 5-	AU 6 =	<u> </u>	Ē
EI	BA ENGINEERING CONSULT.	ANTS	LTD.	LOGGED BY: MAY REVIEWED BY: MA				COMPLETE		TH: 4.7 m	
	EDMONTON ALBERTA			Fig. No: 11413-				COMPLER	L. 94/L	13/16 Page 1	of 1
02/14 0	322V			17.19. 110. 11.170	<u> </u>			<u> </u>		. ogc 1	

CRANI	JLAR RESOURCE EVALUATION	INFOIAN AN	ก พกัดเมาต	N AFFAIRS CANADA			Т	BOREHOLE	<u>ΜΟ:</u> 1	1413-08	_	
	I "C1-10-S"	DRILL: CME750 c/w HW CASING						PROJECT NO: 0101-11413				
	ORT SEA WATER DEPTH: 9.3m	UTM ZONE: 8 N7751507.6 E534082.7						ELEVATION: -9.30 (m)				
	LE TYPE DISTURBED NO RECOVERY			A-CASING	····-	П		ELBY TUBE		CORE		
					1			1000		Javine	Ţ <u> </u>	
ε	SOIL		GRO	UND ICE	IEMPERATURE (C)	TYPE	일	<b>■</b> S	SALINITY (p	opt) =	<u> </u>	
DEPTH(m)			ONO	OND TOB	ATUR	ļu,	SAMPLE	10	ALINITY (p 20 3	6 40	DEPTH(ft)	
EP	DESCRIPTION		DES	CRIPTION	PER	SAMPLE	AMF	PLASTIC	M.C.	LIQUID	H H	
					1	[S	S	20	40 6	0 80		
0.0	CLAY (CL) - silty, with very thin		Not frozen							00	0.0	
ŀ	interbedded sand lenses 2mm thick,										Ė	
-	wet to saturated, low plastic, grey			,			1	•	•		È.	
-		:									2.0	
-	— clay content decreasing with depth,	Ì				$\sqcup$					2.0	
-	black organic pockets disseminated throughout, very thin laminae, even,						2	•	•		E	
1,0	non parallel										Ē	
}	·									:	4.0	
<u> </u>	SAND (SM) - silty to some silt, trace of										E	
-	clay and fine grained gravel, fine			i			3	•		•	Ē	
-	grained, uniform, moist, compact (est.), non plastic, olive brown										Ē	
-	(est.), non plustic, olive brown										6.0	
<u> </u>											E	
<u>}</u>							4	•			<u> </u>	
_		į									E	
[- i	- organic packets, shell fragments										8.0	
-											Ē	
-							5	•			Ē	
- - 3.0						П				ļļ <u>.</u>	Ę.,.	
						П					10.0	
-						f	6				Ę	
						/	۱ ۱					
-						Ш					12.0	
-	<ul> <li>trace of coarse grained sand particles, wet, loose (est.)</li> </ul>	1					7	•			E	
- 4.0	purities, wet, loose (est.)	1				1			-		Ė	
- "											Ē	
						Н					E 14.0	
							-				Ē Ē	
- ]							8				F	
-						/ [		1 :				
- [						$\vdash$		:	:		16.0	
— 5.0 -						/					Ē	
-		1		.			9					
-		ļ				/						
_	END OF BOREHOLE (5.5 metres)								······································		18.0	
_								: !			E.	
6.0											Ē	
	DA ENCIMERDING CONCILIO	A NITTO	וייים ו	LOGGED BY: MAV		Ш		COMPLET	ION DEF	PTH: 5.5 m	<del>-</del>	
<b>L</b> 1	BA ENGINEERING CONSULT	SIMA	ыD.	REVIEWED BY: MAY				COMPLET		3/16		
5/02/14 0:	EDMONTON, ALBERTA			Fig. No: 11413-0	18					Page_1	of 1	

GRANULAR RESOURCE EVALUATION	on I ii	N DNA NAIDN	ORTHERN AFFAIRS CANAD	)A	_	BOREHOLE	NO: 1141	3-09		
TARGET "C1-7-S"			0 c/w HW CASING			PROJECT NO: 0101-11413				
BEAUFORT SEA WATER	——————————————————————————————————————		N7750910.7 E533631.4			ELEVATION: -8.90 (m)				
SAMPLE TYPE DISTURBED	NO RECOVERY	<u> </u>				SHELBY TUBE				
<b>픋</b>	SOIL RIPTION		GROUND ICE DESCRIPTION	TEMPERATURE (C)	SAMPLE TYPE	2	SALINITY (ppl) ■	L dinon OF PTH(ft)		
0.0 CLAY (CL) — silty, trace thin laminae, ever wet, stiff (est.), la olive grey	n, non porallel,	Not	frozen			20	40 60	80 0.0		
SAND (SM) - some silt, grained, uniform,	medium laminoe,						<b>—</b>	2.0		
even, non parallel (est.), non plastic brown  - 2.0								6.0		
- silty - silty -				:				E 8.0		
- 3.0					5			10.0		
interbedded silt an	d clay lenses, wet				6			12.0		
ICE – massive		Froze	en					14.0		
- 5.0 END OF BOREHOLE (5.	0 metres)							16.0		
6.0			LOCCED BY 141			COURT	TION SCOTUS	18.0		
EBA ENGINEERIN	NG CONSULTA	NTS LT	D. LOGGED BY: MAY				TION DEPTH: 5 TE: 94/03/17	.U M		
EDMON	TON, ALBERTA		Fig. No: 11413-			00.111		Page 1 of 1		

GRANL	LAR RESOURCE EVALUATION	INDIAN A	ND NORTHER	RN AFFAIRS CANADA	Α	_	Tí	BOREHOLE	NO.	1141	3-10	1	
TARGE	I "C1-6-S"		ME750 c/w	· · · · · · · · · · · · · · · · · · ·			-	PROJECT NO: 0101-11413					
BEAUF	ORT SEA WATER DEPTH: 9.1m		UTM ZONE: 8 N7750899.2 E534164.8						ELEVATION: -9.10 (m)				
SAMP	E TYPE DISTURBED NO RECOVERY		SPT	☐ A-CASIN		П		IELBY TUBE		COR	 E		
DEPTH(m)	SOIL DESCRIPTION			OUND ICE CRIPTION	TEMPERATURE (C)	YPE	SAMPLE NO			(ppt) ■ 30	40 LIQUID	оертн(nt)	
					<u> </u>	S	S	20	40	60	<del></del>   80		
0.0	CLAY (CL) — silty, black organic pockets disseminated throughout, shell fragments, thin laminae, even, non parallel, saturated becoming moist, stiff (est.), low plastic, dork olive grey		Not frozen	,,			1			60	<u>SU</u>	2.0	
1.0  - - -	SAND (SP/SM) — trace of silt and shell fragments, fine grained, uniform, maist, compact (est.), non plastic, alive grey  CLAY (CL) — silty, very thin lominae, wovy, non parallel, maist to wet, firm (est.), low plastic, very dark				7		3					4.0	
- 2.0 	grey to block SAND (SP/SM) — trace of silt, fine grained, uniform, moist to wet, compact (est.), non plastic, very dark grey to block						4	•				6.0	
- - - - - - -	- olive grey SILT (ML) - some clay, trace of sand,     shell fragments and coarse fibrous     organics, moist, very dark grey to     black SAND (SM) - silty, clayey, fine grained,				-0.27		5	•	•			8.0 - - 10.0	
- - - - - - - - -	uniform, moist to wet, non plastic, olive brown				-0.26		7	•					
-												— 14.O	
- - - - 5.0	<ul> <li>trace of coarse grained sand particles disseminated throughout, dilatant, wet</li> </ul>						9					— 16.0 —	
<b>6.</b> 0	END OF BOREHOLE (5.3 metres)											— 18.0 -	
	BA ENGINEERING CONSULT	ANTS	LTD	LOGGED BY: MAV	<b></b>	· · ·		COMPLET					
דרד		аны	ыīD.	REVIEWED BY: MA				COMPLET	TE: 94,			- (	
5/02/14 03	EDMONTON, ALBERTA			Fig. No: 11413-	10			1			Page 1	01 ]	

GRANI	JLAR RESOURCE EVALUATION	INI	NAN AI	ND NORTHER	n affairs canad	Δ		1	<u></u> ይህይΕኩህ፣	N∩- 1	11/117 1	1	
	T "C1-5-S"		DRILL: CME750 c/w HW CASING						BOREHOLE NO: 11413-11 PROJECT NO: 0101-11413				
$\vdash$	ORT SEA WATER DEP		UTM ZONE: 8 N7750906 E534679.3						ELEVATION: -8.90 (m)				
	LE TYPE DISTURBED	NO RECOVERY			A-CASIN	G	Π		SHELBY TUBE CORE				
DEPTH(m)	SOI	L		'	UND ICE	EMPERATURE (C)	TYPE	2	i	Saunity (	<u>.</u>	OEPTH(ft)	
DEP	DESCRI	PTION		DES	CRIPTION	TEMPERA	SAMPLE	SAMPLE	PLASTIC	M.C.	FIÓRII	) DEPJ	
0.0	CLAY (CL) — silty, trace of stragments, wet, firm (plastic, dark olive grey	est.), low		Not frozen					20	40 (	60 80	0.0	
- 1.0	SAND (SP/SM) — trace of s fragments, fine graine dilatant, saturated, no olive grey	d, uniform,						1				2.0	
- - -	– thin interbedded clay l – some silt, trace of cla					-0.25		2				4.0 	
- 2.0		,, ,,,,				0.23		٤				6.0	
- - -	SAND (SM) — silty, trace of — mica platelets dissemin throughout	ŕ				-0.45		3	•	•		8.0	
- 3.0	<ul> <li>with thin horizontally belienses, 3 to 5mm thic apart</li> </ul>					-0.17		4	•			10.0	
- - - - - - 4.0	SILT (ML) — sondy, trace of dork grey SAND (SM) — trace to some clay, fine grained, unif	silt, trace of				-0.11		5				12.0	
- - - -	non plastic, olive grey END OF BOREHOLE (4.1 m	etres)				U.11						14.0	
- - - 5.0 -												16.0	
- - - -												18.0	
6.0					1,00050				1001	Tra		<u></u>	
EF	BA ENGINEERING	CONSULTAN	STV	LTD.	LOGGED BY: MAV REVIEWED BY: MA	v			<del></del>	TION DEI TE: 94/0	PTH: 4,1 m 33/18	_	
	EDMONTON	N, ALBERTA			Fig. No. 11413-				COMPLE	.ic. 34/l		1 of 1	
05/02/14 00	3-37PW									_	- 7*		

GRANU	ILAR RESOURCE EVALUATION	INDIAN AN	ND NORTHERN AFFAIRS CANADA	Α		BOREHO	F NO: 1	1413-12	
	I "C1-4-S"		ME750 c/w HW CASING				NO: 0101		
BEAUF	ORT SEA WATER DEPTH: 8.2m		E: 8 N7749873.9 E536489.3	<u> </u>		_	N: -8.20 (		
	E TYPE DISTURBED NO RECOVERY				ПП	SHELBY TUE		CORE	
DEРТН(m)	SOIL DESCRIPTION		GROUND ICE DESCRIPTION	IRE (C)	YPE		■ SALINITY (p 20 34	<del></del>	DEPTH(ft)
				#	S	20	40 60	) 80	
0.0	SAND (SM) — some silt, some ctay, homogeneous, with thin horizontal interbedded clayey silt lense 5mm thick, fine grained, uniform, moist, non plastic, dark olive grey — coarse grained gravel particles,		Not frozen			1			2.0
1.0  - -	subrounded, smooth, 25mm diameter - inclined bedding planes, moist to wet, non plastic, dark olive grey			-0.32		2			4.0
- - - - 2.0				-0.45		3 •			6.0 – 6.0
- - -		;		-0.52	-	•	•		8.0
- 3.0	- wet								10.0
- - - - - 4.0				-0.23	7				12.0
		į							14.0
- - - - 5.0	END OF BOREHOLE (4.7 metres)			-0.25	8				16.0
- J.U									18.0
6.0			hoose by the			1 100	[ ] [ ] [ ] [ ] [ ] [ ] [ ] [ ] [ ] [ ]	70 43	
	BA ENGINEERING CONSULT EDMONTON, ALBERTA	ANTS	LTD. LOGGED BY: MAV REVIEWED BY: MA Fig. No: 11413-				LETION DEP LETE: 94/0		of 1

GRANU	LAR RESOURCE EVALUATION	INDIAN AND NOR	THERN AFFAIRS CANADA	4		BOREHOLE NO:	11413–13	
	F "C1-3-S"	DRILL: CME750				PROJECT NO: 010		
-	ORT SEA WATER DEPTH: 8.3m		7749858.4 E535654.7			ELEVATION: -8.30		_
	E TYPE DISTURBED NO RECOVERY		☐ A-CASINO			SHELBY TUBE	CORE	_
DEPTH(m)	SOIL DESCRIPTION		GROUND ICE DESCRIPTION	TEMPERATURE (C)	YPE S	PLASTIC M.C.		DEPTH(ft)
0.0	CLAY (CL) — silty, some sand, fine grained, uniform, very thin interbedded horizontal sand lenses	Not fro	ozen			1		2.0
— 1.0 - - - - -	SAND (SP) — trace of silt and shell fragments, fine grained, uniform, wet, non plastic — 100mm thick interbedded silt lense — 75mm thick interbedded sondy silt					3		4.0
- - 2.0 - - -	lense SAND (SM) — some silt, some clay, homogeneous, fine grained, uniform, inclined bedding planes, slightly dilatant, moist to wet, non plastic, dark olive grey — silty, dilatant, wet			-0.08	2	4		8.0
3.0 				0.07	5			10.0
- - - 4.0	ICE - trace of silt	Frozen			7		1	12.0
- - -	<ul> <li>coarse grained grovel particles,</li> <li>smooth, subrounded</li> <li>becomes clear ice</li> </ul>						1	14.0
- - - 5.0	END OF BOREHOLE (4.6 metres)							16.0
-							# H	18.0
6.0								
E]	BA ENGINEERING CONSULT EDMONTON, ALBERTA	ANTS LTD	LOGGED BY: MAV REVIEWED BY: MAY Fig. No: 11413-1			COMPLETION DE COMPLETE: 94/		<u> </u>

BEAUFO SAMPLE	"C1-2-S"  ORT SEA WATER DEPTH: 8.3m		ME750 c/w H				-			<u> 11413–1</u>	
SAMPLE			neroo cy m i	IW CASING			_   F	PROJECT N	10: 010	1-11413	
	T TVDE MAISTHERE AND DESCRIPTION	UTM ZON	E: 8 N7749	883.3 E534913.2				LEVATION	-8.30	(m)	
(w)	E TYPE DISTURBED 🖊 NO RECOVERY		SPT	A-CASINO	;		SH	ELBY TUBE		CORE	
DEPTH(m)	SOIL DESCRIPTION			UND ICE	TEMPERATURE (C)	SAMPLE TYPE	SAMPLE NO	10 PLASTIC	SALINITY ( 20 M.C.	(pp1) ■ 30 40 LIQUIO 60 80	DEPTH(ft)
0.0	SAND (SM) - cloyey, silty, trace of black organic pockets, moist, low plostic, dark grey		Not frozen		-0.64		1	•			0.0
· 1.0	SAND (SM) — silty, some clay, fine grained, uniform, maist to wet, non plastic, dark olive grey				-0.38		2				2.0
	SAND (SM) — trace to some silt, trace of clay, fine grained, uniform, dilatant, wet, non plastic, olive grey	:			-0.41		3	•			6.0
2.0		:					5				
3.0	- some silt to silty		Frozen			/ 	6	•			
4.0	– some silt		60mm thick	ice lense	-0.3		7				12.0
E	ND OF BOREHOLE (4.1 metres)								·		14.0
5.0		-									16.0
				i				- :   			18.0
6.0									· .		Ē
EΒ	A ENGINEERING CONSULT	ANTS		LOGGED BY: MAV	,					PTH: 4.1 m	
	EDMONTON, ALBERTA			REVIEWED BY: MAY Fig. No: 11413-1				COMPLE	IL: 94/	03/19 Page	1 of 1

CDANI	PAD OCCUPAC EVALU	LATION	Luisia	ND NOTHER	I LEENING ONNIN						44.7.46	<u> </u>
	JLAR RESOURCE EVALU T "C1-1-S"	ATION			N AFFAIRS CANADA	4		_	BOREHOLE		<u> 413 15</u>	)
		JER DEPTH: 8.5m		ME750 c/w H	1W CASING 856.8 E534276.7			$\rightarrow$	PROJECT N			
	LE TYPE DISTUR			NE: 0 N7749 ]SPT			-		ELEVATION:	<u> </u>	<u> </u>	<u>-</u> -
SAMI	CE THE DISTON	DED NO WECK	VERT A	1 261	A-CASING	T	ᆫ	∏ 2ı	HELBY TUBE		CORE	
DEPTH(m)		SOIL		GRO	UND ICE	FEMPERATURE (C)	SAMPLE TYPE	E N0	<b>■</b> \$	ALINITY (ppi 20 30	ı) <b>=</b> 40	H(E)
DEPT	DES	SCRIPTION		DESC	CRIPTION	TEMPERA	SAMPLI	SAMPLE	PLASTIC	M.C.	LIQUID	DEPTH(ft)
0.0		fine grained, unifor	m,	Not frozen		-0.71		1	20	40 60	80	0.0
-	(250mm thick SAND (SM) - silty, s											2.0
1.0	fragment disse	eminated throughout uniform, wet, non	,			-0.68		2	•	•		
} - - -	– very thin intert thick	pedded silt lense 5m	m					3				€ 4.0
- 2.0							Ц					6.0
- 2.0 - - -							$\left  \left  \right  \right $	4				بيسي
- - -	– some silt					0.09		5				8.0 8.0
3.0	– very small waa platelets throu	d fragment, mica ghout										10.0
- - -						0.02		6	•			12.0
4.0		nated throughout,	of			0.06		7	• • • • • • • • • • • • • • • • • • •			
- - -	plastic, dark of SAND (SM) — silty, h grained, unifor	pockets, moist, low live grey nomogeneous, fine m, wet, non plastic,				0.08		8				14.0
- - 5.0	olive grey				:							16.0
- - -								9		-		18.0
6.0	END OF BOREHOLE	(5.9 metres)		lce particle sampler	recovered in			10				
EF	BA ENGINEER	RING CONSII	LTANTS	LTD	LOGGED BY: MAV				COMPLET			
"				, ענים	REVIEWED BY: MA		<b></b>		COMPLET	E: 94/03	·	_,.
95/02/14 03	<u> </u>	<u>ONTON, ALBERT</u>	H		Fig. No: 11413-1	10					Page 1	of 1

GEOLG	ogical evaluation	INDIAN A	nd northern affairs canada		TBO	OREHOLI	E NO:	11413	-16
	T "NEARSHORE MR2 ISLAND"		ME750 c/w CRREL CORE BARRE		_			)1-1141,	
NORTI	H POINT RICHARDS ISLAND, N.W.T.		IE: 8 N7732423.8 E529201.3				l: -0.86		
SAMP	LE TYPE DISTURBED NO RECOVER		SPT = A-CASING	ŢŢ		LBY TUBE		CORE	-
DEРТН(m)	SOIL		GROUND ICE	$\alpha \mapsto -1$	2   	10	i Salinity 20	(ppt) ■ 30 40	DEPTH(ft)
DEP	DESCRIPTION		DESCRIPTION	TEMPERATUI SAMPLE	SAMPLE	PLASTIC	M.C.		
- 0.0	SAND (SP) — trace of silt, fine grained, uniform, brown		Frozen, Nbn		1 2	20	40	60 80	0.0
-	– some silt				3				2.0
1.0 - - -	ORGANIC SILT (OL) AND PEAT — black — becoming fine grained peat, strong				4				4.0
- - - - 2.0	organic odour  ICE AND ORGANIC SILT – massive, olive		Cloudy ice		5				6.0
  -  -  -  -  -  -	brown silt				6				8.0
3.0	— sill content increasing with depth				7				10.0
- - - - - 4.0					8				12.0
-  -  -  -  -					9				14.0
- - - 5.0	ORGANIC SILT (OL) AND PEAT — very dork brown to block				0				16.0
-  -  -  -	– light olive grey	ļ			1				18.0
6.0	SILT (ML) — some clay, very dark grey to		Vr 10% 2–5mm thick		2				
E)	BA ENGINEERING CONSULT EDMONTON, ALBERTA	rants	LTD. LOCGED BY: MAV REVIEWED BY: MAV Fig. No: 11413-1				ETION DE ETE: 94/		0 m ge 1 of 2

GEOLO	OGICAL EVALUATION	INDIAN A	ND NORTHERN	I AFFAIRS CANADA			1	80REHOLE	NO.	1141.	3_16	<u> </u>
	T "NEARSHORE MR2 ISLAND"			RREL CORE BARRE			<del></del>	PROJECT I				•
	POINT RICHARDS ISLAND, N.W.T.	<del> </del>		123.8 E529201.3				ELEVATION				
	LE TYPE <b>D</b> ISTURBED NO RECOVERY		SPT	■ A-CASING				IELBY TUBE		CORE		
DEPTH(m)	SOIL		GRO	JND ICE	EMPERATURE (C)	TYPE	8	i	Salinity 20	(ppt) ■ 30 4	10	DEPTH(ft)
병	DESCRIPTION		DESC	RIPTION	TEMPER	SAMPLE	SAMPLE 1	PLASTIC	M.C		LIQUIO ——	DEP
6.0	black SILT (ML) — (continued)						12	20	40	60 8	30	20.0
- - - - - - 7.0	SAND (SM) AND SILT — with very thin black organic lenses, fine grained, uniform		Nbn				13					22.0
- - -	— iron oxide stained lenses						14					24.0
- - - 8.0	<ul> <li>coarse grained sond particles disseminated throughout</li> </ul>		Nbn, trace o	of visible ice			15					26.0
,	<ul> <li>thin interbedded horizontal silt lenses 2–5mm thick</li> </ul>		Vr 2mm thic	k			16					28.0
- 9.0 - - -							17					30.0
- - - - - 10.0	SILT (TILL) (ML) — trace to some sand, trace of gravel and clay, iron oxide staining evident, low plastic, dark olive grey		Vr<5%				18					32.0
- - - -	SAND (SM) — silty, fine grained, uniform, grey		Nbn				19	· .				34.0
- 11.0 : - -	END OF BOREHOLE (11.0 metres)  Note: Geological Survey of Canada, Terrain Sciences Division, Target			ŗ								36.0
12.0	"Near Shore". Borehole #94GSCMR2-H All samples retained by GSC. GSC thermistor string installed.	01										— 38.0 -
	BA ENGINEERING CONSULT EDMONTON, ALBERTA	ANTS	ւրլը, ի	LOGGED BY: MAV REVIEWED BY: MAV Fig. No: 11413-11		, I	\ 	COMPLE		/03/20	1.0 m	of 2

TARGET "NEARSHORE MR2 SLAND."  INDRIH PONT RICHARDS SLAND, N.W.I.  SAMPLE TYPE  SOIL  DESCRIPTION  DESCRIPTIO	GEOLOGICAL EVALUATION	Indian and Northern Affairs Canada	BOREHOLE NO: 11413-17
NORTH POINT RICHARDS ISLAND, N.W.I.  SAMPLE TYPE SIDSTURBED NO RICCOREY SPT SIA-CASING SELBY TUBE CORE  SOIL  DESCRIPTION  BESCRIPTION  BESCRIPTION  BESCRIPTION  BESCRIPTION  BESCRIPTION  BOSTURBED NO RICCOREY  SOIL  DESCRIPTION  BESCRIPTION			
SAMPLE TYPE DISTURBED NO RECOVERY SPI A-CASING SELEN TUBE COME  SOIL SOIL DESCRIPTION DESCRIPTION  ON SAND (SP/SM) — trace to some sill, fine grained, uniform, light brownish grey with depth SAND (SP/SM) — trace to some sill, fine grained, uniform, olive brown  ORGANIC SILT (OL) — black becoming grey with depth SAND (SP/SM) — trace to some silt, fine grained, uniform, olive brown  ORGANIC SILT (OL) — clayer, with fibrous organics throughout, safurated, black  Frozen  ORGANIC SILT (OL) — clayer, with fibrous organics throughout, safurated, black  Frozen  ORGANIC SILT (OL) AND PEAT — strong organics throughout, safurated, black  All samples retained by GSC. Borehole #94GSCMR2-02  All samples retained by GSC.  Borehole advanced to 12.3 metres using solid ougers to facilitate the installation of a GSC thermistor string. No samples were obtained between 3.4 and 12.3 metres.			· · · · · · · · · · · · · · · · · · ·
SOIL DESCRIPTION DESCRIPTION DESCRIPTION  ORGANIC SILT (OL) — black becoming grey with depth SAND (SP/SM) — trace to some silt, fine grained, uniform, light brownish grey ORGANIC SILT (OL) — black becoming grey with depth SAND (SP/SW) — trace to some silt, fine grained, uniform, olive brown  ORGANIC SILT (OL) — clayey, with fibrous organics throughout, saturated, black  To organic stroughout, saturated,  DESCRIPTION  Frozen (seasonal) Note (SP/SW) — trace to some silt, fine grained, uniform, olive brown  To organic stroughout, saturated,  To organic stroughout, saturated,  To some strong organic door, brown  END OF BORHOLE (3.4 metres) Note: Ceological Survey of Canada, Terrain Sciences Divisions, Target "Near Shore". Barehole #94GSCMR2-02  All samples retained by GSC.  Borehole advanced to 12.3 metres using solid augers to facilable the installation of a GSC thermistor string. No samples were obtained between 3.4 and 12.3 metres.	· · · · · · · · · · · · · · · · · · ·		<u> </u>
ORGANIC SILT (OL) – block becoming grey with depth SAND (SP/SM) – trace to some silt, fine grained, uniform, light brownish grey with depth SAND (SP/SM) – trace to some silt, fine grained, uniform, olive brown  ORGANIC SILT (OL) – clayey, with fibrous organics throughout, saturated, black  - 20  ORGANIC SILT (OL) – clayey, with fibrous organics throughout, saturated, black  - 20  ORGANIC SILT (OL) AND PEAT – strong organic odour, brown  END OF BORTHOLE (J.4 metres) Note: Ceological Survey of Canada, lerrain Sciences Divisions, Target  "Near Share". Borehole #946SCMR2-02  All samples retained by GSC.  Borehole advanced to 12.3 metres using solid ougers to facilatate the installation of a GSC thermistor string. No samples were obtained between 3.4 and 12.3 metres.	SOIL DESCRIPTION		SALINITY (pot)
SAND (SP/SM) — trace to some sill, fine groined, uniform, light brownish grey  ORGANIC SILT (OL) — black becoming grey with depth  SAND (SP/SM) — trace to some silt, fine groined, uniform, olive brown  ORGANIC SILT (OL) — clayey, with fibrous organics throughout, saturated, black  -2.0  ORGANIC SILT (OL) — clayey, with fibrous organics throughout, saturated, black  Frozen  Frozen  Frozen  Au  Frozen  Au  Frozen  Au  Service (Seasonal)  Ns/N 30%  Vs 5—10%  Au  Frozen  Au  Au  Frozen  Frozen  Au  Frozen  Frozen  Au  Au  Frozen  Frozen  Au  Au  Frozen  Frozen  Au  Au  Frozen  Au  Au  Frozen  Au  Au  Frozen  Au  Frozen  Au  Au  Frozen  Frozen  Au  Frozen  Au  Au  Frozen  Au  Au  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Au  Frozen  Frozen  Au  Frozen  Frozen  Au  Frozen  Frozen	,		· · · · · · · · · · · · · · · · · · ·
grained, uniform, olive brown  ORGANIC SILT (OL) — clayey, with fibrous organics throughout, saturated, black  -2.0  ORGANIC SILT (OL) AND PEAT — strong organic adour, brown END OF BOREHOLE (3.4 metres) Note: Ceological Survey of Canada, Ierrain Sciences Divisions, Target "Near Share". Borehole #94GSCMR2—02  All samples retained by GSC. Borehole advanced to 12.3 metres using solid augers to facilatate the installation of a GSC thermistor string. No samples were obtained between 3.4 and 12.3 metres.	grained, uniform, light brownish grey  ORGANIC SILT (OL) — black becoming grey  with depth	Vs/Vr 30%	0.0
organics throughout, saturated, black  20  ORGANIC SILT (OL) AND PEAT — strong organic odour, brown END OF BOREHOLE (3.4 metres) Note: Geological Survey of Canada, Terroin Sciences Divisions, Torget "Near Shore". Borehole #94GSCMR2-02  All samples retained by GSC. Borehole advanced to 12.3 metres using solid augers to facilated the installation of a GSC thermistor string. No samples were obtained between 3.4 and 12.3 metres.	grained, uniform, olive brown	Not frozen 3	4.0
ORGANIC SILT (OL) AND PEAT — strong organic odour, brown END OF BOREHOLE (3.4 metres) Note: Geological Survey of Canada, Ierrain Sciences Divisions, Target "Near Shore". Borehole #94CSCMR2-02  All samples retained by GSC. Borehole advanced to 12.3 metres using solid augers to facilatate the installation of a GSC thermistor string. No samples were obtained between 3.4 and 12.3 metres.	organics throughout, saturated, black	4	6.0
ORGANIC SILT (OL) AND PEAT — strong organic odour, brown END OF BOREHOLE (3.4 metres) Note: Geological Survey of Canada, Ierrain Sciences Divisions, Target "Near Shore". Borehole #94GSCMR2-02  All samples retained by GSC.  Borehole advanced to 12.3 metres using solid augers to facilate the installation of a GSC thermistor string. No samples were obtained between 3.4 and 12.3 metres.		Frozen	8.0
Ierrain Sciences Divisions, Target "Near Shore". Borehole #94CSCMR2-02  All samples retained by GSC.  Borehole advanced to 12.3 metres using solid augers to facilatate the installation of a GSC thermistor string. No samples were obtained between 3.4 and 12.3 metres.	ORGANIC SILT (OL) AND PEAT — strong  organic odour, brown  END OF BOREHOLE (3.4 metres)	5	10.
Borehole advanced to 12.3 metres using solid augers to facilatate the installation of a GSC thermistor string. No samples were obtained between 3.4 and 12.3 metres.	Terrain Sciences Divisions, Target "Near Shore". Borehole #94GSCMR2-	02	12.
between 3.4 and 12.3 metres.	Borehole advanced to 12.3 metres using solid augers to facilatate the installation of a GSC thermistor		14.0
	between 3.4 and 12.3 metres.		18.0
EBA ENGINEERING CONSULTANTS LTD.  LOCGED BY: MAV COMPLETION DEPTH: 3.4 m	······································		<b>f</b>
INCACHED BY, MAY COMPECTE. 54/03/21		INLYIL TILD DI, MAY	COMPLETE: 94/03/21 Page 1 of 1

GEOLO	GICAL EVALUATION	INDIAN AND I	NORTHERN AFFAIRS CANADA			Т	BOREHOLE I	NO: 114	13_18	
<u> </u>	- T DA - ED - E		50 c/w SOLID FLIGHT AUGE			_	PROJECT NO			
NORTH	·		8 N7732576.3 E529347.6			$\rightarrow$	ELEVATION:			
SAMPI	LE TYPE DISTURBED 🖊 NO RECOVERY	IAS 🔀	T 🗏 A-CASING			St	HELBY TUBE	<b>∏</b> co	RE	
ОЕРТН(т)	SOIL DESCRIPTION		GROUND ICE DESCRIPTION	EMPERATURE (C)	SAMPLE TYPE	SAMPLE NO	■ Sx 10 PLASTIC	AUNITY (ppl) ■ 20 30 ■ M.C.	40 LIQUID	DEPTH(ft)
				TEM	SA	ζŞ	1	•		
0.0	SAND (SP) — trace of silt, fine grained, uniform, alive brown	Fro	ozen (seasonal)				20	40 60		0.0
- 1.0	Note: Stratigraphy other than that al seabed was not determined									- 4.0
- - - - 2.0		Not	t frozen							- 6.0
									unatkonna	8.0
- 3.0 - - - -										12.0
4.0										14.0
- - - - - 5.0	Note: Geological Survey of Canada, Terrain Sciences Division, Target "Near Share". Barehole #94GSCMR2-0	)3							<u></u>	16.0
-	No Samples were retained by GSC.  Borehole was advanced using solid augers to determine depth to permafrost.  END OF BOREHOLE (7.0 metres)	Fro	zen al 6.6 metres							18.0
6.0	<del></del> .	A NIMO 7	TID LOGGED BY: MAV		Ш		COMPLETI	ión depth:	70 m	
El	BA ENGINEERING CONSULT	ANTS L	REVIEWED BY: MAN	/				E: 94/03/2		
5/02/14 03	EDMONTON, ALBERTA		Fig. No: 11413-1	8					Page 1 of	12

GEOLG	OGICAL EVALUATION	INDIAN AN	VD NORTHE	RN AFFAIRS CANADA	 A		Į į	BOREHOLE NO: 11413-19	
	T "NEARSHORE MR2 ISLAND"		4E750 c/w		- 1 		-	PROJECT NO: 0101-11413	<u>-</u>
<del></del>	POINT RICHARDS ISLAND, N.W.T.			2701.8 E529470			_	LEVATION: -2.30 (m)	
	LE TYPE DISTURBED NO RECOVERY			■ A-CASIN	G			ELBY TUBE CORE	
DEPTH(m)	SOIL DESCRIPTION		GR(	OUND ICE CRIPTION	FEMPERATURE (C)	SAMPLE TYPE	SAMPLE NO	SALINITY (ppt) = 10 20 30 40  PLASTIC M.C. LIQUID	DEPTH(ft)
0.0	SAND (SP) — trace of silt, fine grained,		Not frozen		2			20 40 60 80	0.0
- - - -	uniform, wet, compact (est.), non plastic, olive grey  - some silt, trace of gravel, very thin						1		_ — 2.0
- 	inclined organic lenses 1—2mm thick						2		-· 4.0
- - - - - 2.0							3		- - 6.0
-	<ul> <li>very thin horizontal organic lenses, black</li> <li>150mm thick lense of sandy gravel, trace of shell fragments</li> </ul>				:		4		- 8.0
- - 3.0 - -	<ul> <li>coorse fibrous organics and wood fragments</li> </ul>						6		- 10.0
4.0						$\bigvee$	7		- 12.0 -
	ORGANIC SILT (OL) — black SAND (SM) — silty, with very thin interbedded organic lenses, fine						8		- 14.0
- - - 5.0 -	SILT (TILL) (ML) — some clay, trace to some sond, trace of fine grained gravel, organic pockets, moist, very								- 16.0
-	stiff (est.), low plastic, olive brown						9		- 18.0
6.0				TLOCOCO DV 1411				TOURD ETION DEDTU 40.0	
E]	BA ENGINEERING CONSULT EDMONTON, ALBERTA	ANTS	LTD.	LOGGED BY: MAV REVIEWED BY: MA Fig. No: 11413-	V	,		COMPLETION DEPTH: 12.2 m  COMPLETE: 94/03/21  Page 1	of 3

GEOLO	OGICAL EVALUATION	INDIAN AND NORTHERN AFFAIRS CANADA	BOREHOLE NO: 11413-19
	T "NEARSHORE MR2 ISLAND"	DRILL: CME750 c/w HW CASING	PROJECT NO: 0101-11413
	I POINT RICHARDS ISLAND, N.W.T.	UTM ZONE: 8 N7732701.8 E529470	ELEVATION: -2.30 (m)
SAMPI	LE TYPE DISTURBED 🛮 NO RECOVE	RY SPT = A-CASING	SHELBY TUBE CORE
DEPTH(m)	SOIL DESCRIPTION	GROUND ICE DESCRIPTION	SAMPLE TYPE  SAMPLE NO  SAMPLE TYPE  Outloon  DEPTH(ft)
6.0 - -	SILT (TILL) (ML) — (continued) — dark olive grey		10
7.0			22.0
- - -			24.0
8.0	SAND (TILL) (SM) — silty, trace to some gravel, trace of clay		11 26.0
- - - - - - - -			28.0
9.0 - - - -	<ul> <li>200mm thick lense of fine grained sand, moist, olive grey</li> </ul>		12
- - -	— trace to some coarse grained gravel		32.0
— 10.0 - - -	SAND (SP) — trace of silt, fine grained		34.0
- - 11.0 -	<ul> <li>Note: Sand heaving inside casing when drilling was stopped to attempt to sample.</li> </ul>		13
- - - 12.0			38.0
	BA ENGINEERING CONSUL	TANTS ITD LOGGED BY: MAV	COMPLETION DEPTH: 12.2 m
ומו	EDMONTON, ALBERTA	INCAICHEO OI. MAY	COMPLETE: 94/03/21 Page 2 of 3
95/0 <b>2/</b> 14 03	15289 DDMONTON, ADDELLIA		1 ruge 2 01 3

	· ·		-	RN AFFAIRS CANAD	)A		_					13-1	9
			ME750 c/w								01-1		
				2701.8 E529470							(m) <u>0</u>		
SAMPL	E TYPE DISTURBED NO RECOVERY		SPT	A-CASIN	10	_Ц	∐SH	ELBY	TUBE		∭ co	)re 	
DEPTH(m)	SOIL DESCRIPTION			OUND ICE CRIPTION	TEMPERATURE (C)	SAMPLE TYPE	SAMPLE NO	PLAS	10	ALINIT 20 M.	(ppt) + 30 C.	■ 40 LIQUID	DEPTH(ft)
12.0	SAND (SP) - (continued)				<del> </del>				20	40	60	80	<u> </u>
.	END OF BOREHOLE (12.2 metres)						ĺ						40.0
	Borehole terminated due to heaving sond  Note: Geological Survey of Canada,  Terrain Sciences Division, Torget  "Near Shore". Borehole #94GSCMR2—	į											42.0
- 13.0	All samples were retained by GSC.	V4											Frankrin
	GSC thermistor string installed to 8 metres below mudline.												44.0
- 1 <b>4.0</b>		:											46.0
- 15.0													48.0
13.0													50.0
- 16.0													52.0
													54.0
- 17.0		:					f						56.0
18.0				LOGGED BY: MAN	,			Too	up: cī	ION 1	)EDTU	133-	58.0
ΕE	BA ENGINEERING CONSULT	ANTS	LTD.	REVIEWED BY: MAY							)EPTH:	: 12.2 m 21	
<i>105111</i> 61	EDMONTON, ALBERTA			Fig. No: 11413-				100	., CC1	a*	7 337		3 of 3

# APPENDIX C SUMMARY OF LABORATORY TESTING



LABORATORY TEST RESULT SUMMARY

Sample	Sample In	nterval	Moisture	Salinity	Líquid Limít	Plastic Limit	Piasticity	USC Classification	Clay	Silt	Sand	Gravel	
	(ω)	(m)	(%)	(ppt)				- Cacconicano	(%)	(%)	(%)	(%)	
•	0.00	0.30	35.0						45.7	53.4	. o	0.0	
7	0.30	0.33	35.6						44.2	54.2	9.	0.0	
8	0.34	0.40	17.9						17.8	69.2	13.0	0.0	
8	0.40	0.45	11.8						9.4	28.0	62.6	0.0	
2	0.30	0.61	22.8						17.6	75.9	6.5	0.0	
ო	0.61	0.91									) ;	!	
ო	0.72	0.77	10.3						4.1	6.6	89.3	0.0	
ო	0.78	0.83	20.8						20.5	9.92	2.9	0.0	
4	0.91	1.37										l	
4	1.05	1.10	20.8						13.0	40.5	46.5	0.0	
2	1.52	1.98	29.0						22.2	64.2	13.6	0.0	
2	1.90	1.95	17.8						15.6	49.6	23.6	11.2	
မှ	2.13	2.59	20.0						•	24.5	59.5	16.0	
7	2.74	3.20										 	
7	2.75	2.80	15.0						3.6	3.3	76.4	16.7	
<b>∞</b>	3.35	3.81	23.1						4.4	14.9	80.7	0.0	
<b>ω</b>	3.50	3.55	21.9						17.2	71.6	11.2	0.0	
တ	3.96	4.52	23.8						13.4	43.3	43.3	0.0	
10	4.57	5.08											
10	4.60	4.65	16.1						16.6	36.0	47.4	0.0	
=	5.18	5.74	18.4						8.7	10.9	79.1	1.3	
12	5.79	6.35											
13	6.40	98.9											
4	98.9	96.9											
15	7.01	7.62											
15	7.10	7.15	21.6						22.5	33.3	44.2	0.0	
16	7.62	8.23	16.9						16.6	23.1	60.3	0.0	
16	7.60	7.65	17.9						3.0	2.1	94.9	0.0	
17	8.23	8.84											
18	8.75	8.80	14.2						23.4	22.1	54.5	0.0	
#	8.84	9.45											
<del>1</del> 9	9.35	9.40	13.0						12.4	27.6	0.09	0.0	
<del>0</del>	9.45	10.01	19.6						31.3	27.4	41.3	0.0	
20	10.06	10.52											
	Number 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		Sample In from from from (m) (m) (m) 0.00 0.30 0.34 0.40 0.30 0.78 0.78 1.52 1.90 1.90 1.90 1.90 1.90 1.90 1.90 1.90	Sample Interval from to (m) (m) (m) (m) (m) (100 0.30 0.30 0.34 0.40 0.45 0.30 0.34 0.45 0.30 0.31 0.72 0.77 0.72 0.77 0.78 0.91 1.95 1.90 1.95 2.74 3.20 2.75 2.80 3.35 3.81 3.50 3.55 3.96 4.52 4.57 5.08 4.65 6.96 6.96 6.96 6.96 6.96 6.96 6.96 6	from to Content to Content to Content to Content to Content to Content to Content to Content to Content 0.30 0.30 35.0 0.34 0.45 0.45 11.8 0.40 0.45 11.8 0.40 0.72 0.77 10.3 0.78 0.83 20.8 0.91 1.37 10.5 1.90 1.95 17.8 2.13 2.59 20.0 2.74 3.20 2.74 3.20 2.75 2.80 15.0 3.35 3.81 2.3.1 3.35 3.81 2.3.1 3.50 3.55 2.1.9 2.74 3.20 2.75 2.80 15.0 2.74 3.20 2.75 2.80 15.0 2.74 3.20 2.75 2.80 15.0 2.75 2.80 2.00 2.74 3.20 2.75 2.80 15.0 2.74 18.4 5.79 6.35 6.46 6.86 6.86 6.86 6.96 6.86 6.96 6.86 6.96 6.86 6.96 6.86 6.96 6.86 6.96 6.86 6.96 6.86 6.96 6.86 6.96 6.86 6.96 6.9	Sample Interval Moisture Salinity from to Content to Content to Content to Content to Content to Content (m) (m) (m) (gbt) (gb	Sample Interval         Moisture         Salinity         Limit           (m)         (m)         (ppt)         Limit           (m)         (m)         (ppt)         Limit           (m)         (m)         (m)         (m)         (m)         Limit           (m)         (m	Sample Interval         Moisture (m)         Moisture (ppt)         Liquid (ppt)         Plastic (mit)           (m)         (m)	Sample Interval (m)         Moisture (ppt) (ppt)         Limit (mit of pasticity (m))         Plasticity (m) (m)         Plasticity (m) (m)         Content (m)         Limit (mit of pasticity (m))         Limit (mois of pasticity (m))         Content (m)         Limit (mois of pasticity (m))         Limit (mois of pasticity (mois of pasti	Sample Interval (m)         Mosisture (ppt)         Light (ppt)         Plastic (ppt)         USC           (m)         (m) </td <td>from (m) (m) (msture Salinity (m) (m) (msture Salinity (m) (msture Salinity (m) (msture Salinity (m) (msture Salinity (mstar) (msture Salinity (msture Salinity (msture Salinity (msture Salinity (msture Salinity (msture Salinity (msture Salinity (mstar) (msture Salinity (msture Salinity (msture Salinity (msture Salinity (msture Salinity (msture Salinity (mstar)</td> <td>Sample Interval         Moisture Moisture to Content         Liguid         Plastic Plasticity (Moisture Cassification (Moisture Content to Content to Content to Content (Moisture Cassification (Moisture Cassification Content to Content (Moist Cassification Content Cassification Content (Moistan Cassification Content Cassification</td> <td>from trom (m)         (m) (m)         (m) (m) (m)         Movisture Salinity         Light Limit         Inmit Limit         Index Classification (%)         (%)</td>	from (m) (m) (msture Salinity (m) (m) (msture Salinity (m) (msture Salinity (m) (msture Salinity (m) (msture Salinity (mstar) (msture Salinity (msture Salinity (msture Salinity (msture Salinity (msture Salinity (msture Salinity (msture Salinity (mstar) (msture Salinity (msture Salinity (msture Salinity (msture Salinity (msture Salinity (msture Salinity (mstar)	Sample Interval         Moisture Moisture to Content         Liguid         Plastic Plasticity (Moisture Cassification (Moisture Content to Content to Content to Content (Moisture Cassification (Moisture Cassification Content to Content (Moist Cassification Content Cassification Content (Moistan Cassification Content Cassification	from trom (m)         (m) (m)         (m) (m) (m)         Movisture Salinity         Light Limit         Inmit Limit         Index Classification (%)         (%)

0101-11413	1413					LABORAT	LABORATORY TEST SUMMARY	SUMMARY					Page 2 of 10
Borehole	Sample	Sample Interval	nterva!	Moisture	Salinity	Liquid Limit	Plastic Limit	Plasticity	USC	Clay	Silt	Sand	Gravel
		(E)	(E)	(%)	(ppt)			V and	Classification	(%)	(%)	(%)	(%)
11413-02	,	0.00	0.15	32.6						ი. ი	73.1	16.9	0.1
11413-02	Ø	0.31	0.51	30.1						7.7	82.1	10.2	0.0
11413-02	8	0.30	0.68	31.9						10.5	81.3	8.2	0.0
11413-02	ო	92.0	1.37	18.4					₽	7.5	12.3	80.0	0.2
11413-02	4	1.52	2.01										!
11413-02	ß	2.13	2.62										
11413-02	5	2.45	2.50	22.0						13.3	66.1	20.6	0.0
11413-02	9	2.74	3.23	29.1						30.1	6.99	3.0	0.0
11413-02	7	3.35	3.84										
11413-02	7	3.61	3.66	10.3						5.3	17.3	74.0	4.6
11413-02	œ	3.96	4.45	24.9									
11413-02	æ	4.10	4.20	27.4		32	21	11	ರ	24.8	73.0	2.5	0.0
11413-02	თ	4.57	5.06										
11413-02	თ	4.80	4.85	22.9						28.9	9.79	3.5	0.0
11413-02	10	5.18	5.66	24.4						30.2	68.6	1.2	0.0
11413-02		5.79	6.10										
11413-02	1	5.78	5.82	15.7						<del>.</del> 5.	3.0	94.9	9.0
11413-02	12	6.40	92.9	19.2						15.3	19.1	65.6	0.0
11413-02	13	7.01	7.57										
11413-02	13	7.20	7.25	18.6						32.8	29.2	38.0	0.0
11413-02	4	7.62	8.10										
11413-02	15	8.00	8.05	27.3						9.99	32.6	9.0	0.0
11413-02	15	8.23	8.64	21.4					SP/SM	<del>1</del> .5	5.9	92.6	0.0
11413-02	16	8.55	8.60	18.6						3.7	4. 6.3	92.0	0.0
11413-02	9	8.84	9.05										
11413-02	17	9.45	9.81	20.8						3.7	4.3	92.0	0.0
11413-02	18	9.84	9.87	6.9						2.5	14.6	54.6	28.6
11413-02	18	10.06	10.62	12.8						17.8	17.2	65.0	0.0
11413-02	19	10.50	10.55	13.7						16.3	25.4	58.3	0.0
11413-02	19	10.67	11.02										

LABORATORY TEST SUMMARY

0101-11413

Sample	Sample Interval	Interval	Moisture	Salinity	Liquid	Plastic	Plasticity	281 181	Clay	Silt	Sand	Gravel
Number	from (m)	9 (E	Content (%)	(bbt)	Ligi Ligi Ligi Ligi Ligi Ligi Ligi Ligi	į.	Index	Classification	(%)	(%)	(%)	(%)
-	0.00	0.51				:						/=:\
-	0.05	0.10	12.0						58.7	45.1	26.2	0.0
α	0.61	1.09	26.5						33.4	52.1	14.5	0.0
ო	1.22	1.70										!
4	1.83	2.19										
4	2.00	2.05	26.6						37.6	57.4	5.0	0.0
ഗ	2.44	2.90	28.8		39	21	18	ರ				
ဖ	3.05	3.51	29.1						41.8	56.7	7.5	0.0
7	3.66	3.99										
7	3.75	3.80	26.6		37	23	4	ፘ				
∞	4.27	4.67										
∞	4.20	4.25	21.5						34.7	63.8	<u>۔</u> رئ	0.0
တ	4.88	5.18										•
တ	4.75	4.80	24.3		36	23	5.	멍				
10	5.49	5.89	28.9						27.3	71.5	1.2	0.0
Ξ	6.10	6.48										
Ξ	00.9	6.05	26.6						48.3	51.4	0.3	0.0
12	6.71	7.01	18.6						20.5	25.6	53.9	0.0
13	7.32	7.75										
13	7.10	7.15	22.6						42.0	47.1	10.9	0.0
14	7.75	7.80	26.9		50	22	7	CL+ML				
14	7.93	8.28										
<del>1</del> .	8.54	8.89	28.6						32.3	57.5	10.2	0.0
16	9.14	9.40	31.7		50	24	26	ರ	48.9	46.9	4.2	0.0
16	9.14	9.40	29.3									
17	9.75	96.6										
18	10.36	10.92	16.4						14.8	20.3	64.9	0.0
18	10.75	10.80	15.9						14.4	16.1	69.5	0.0
9	10.97	11.46	16.1						12.4	21.8	65.8	0.0
			0.00 0.05 1.22 1.83 2.00 2.44 3.05 3.05 3.05 3.75 4.20 6.10 6.00 6.10 6.10 6.10 6.10 6.10 6.1	0.00 0.05 0.05 0.05 1.22 1.22 1.83 2.19 2.00 2.05 2.44 2.90 3.05 3.05 3.99 3.75 4.20 4.25 4.20 4.25 4.20 4.25 4.20 4.25 4.88 5.49 6.10 6.06 6.06 6.06 6.10 6.06 6.10 6.06 6.10 6.10 6.10 6.15 7.75 7.75 7.75 7.75 7.75 7.10 7.15 7.15 7.15 7.16 9.14 9.14 9.14 9.14 9.14 9.14 9.15 10.36 10.36 10.97 11.46	0.00 0.05 0.05 0.05 1.22 1.83 2.00 2.05 2.44 2.00 2.05 2.44 2.90 3.05 3.05 3.05 3.05 3.99 3.75 4.20 4.25 4.20 4.25 4.80 5.49 6.10 6.05 6.10 6.05 6.10 6.05 6.10 6.05 6.10 6.15 7.75 7.75 7.16 9.14 9.14 9.14 9.14 9.17 9.18 9.18 9.18 9.19	0.00       0.51         0.05       0.10       12.0         0.61       1.09       26.5         1.22       1.70       26.6         1.83       2.19       26.6         2.00       2.05       26.6         2.44       2.90       28.8         3.05       3.51       29.1         3.05       3.51       29.1         3.05       3.51       29.1         4.27       4.67       4.25         4.27       4.67       4.80         4.29       4.25       21.5         4.88       5.18       24.3         5.49       5.89       28.9         6.10       6.05       26.6         6.71       7.01       18.6         7.32       7.75       7.80       26.9         7.35       7.75       7.80       26.9         7.75       7.80       26.9         7.39       8.28       8.8         8.54       8.89       28.6         9.14       9.40       29.3         9.14       9.40       29.3         9.17       10.30       15.9         10.35 <td< td=""><td>0.00       0.51         0.05       0.10       12.0         0.61       1.09       26.5         1.22       1.70         1.83       2.19       26.6         2.00       2.05       26.6         2.44       2.90       28.8       39         3.05       3.51       29.1       37         3.05       3.51       29.1       37         4.27       4.67       4.26       21.5         4.20       4.25       21.5       37         4.20       4.25       21.5       37         4.88       5.18       24.3       36         5.49       5.89       28.9       36         6.00       6.05       26.6       6         6.10       6.48       28.9       28.9         6.10       6.48       26.9       29.9         7.75       7.75       7.75       7.80       26.9         7.75       7.80       26.9       29.9         7.75       7.80       26.9       29.3         9.14       9.40       29.3         9.75       9.96       16.4         10.75       11.46</td><td>0.00 0.51 0.05 0.10 12.0 0.61 1.09 26.5 1.22 1.70 1.83 2.19 2.00 2.05 26.6 2.44 2.90 28.8 39 21 11 3.05 3.51 29.1 3.05 3.51 29.1 3.05 3.51 29.1 3.05 3.51 29.1 3.05 3.90 26.6 4.27 4.67 24.3 36 2.3 11 4.75 4.80 24.3 36 2.3 11 6.00 6.05 26.6 6.71 7.01 18.6 7.75 7.80 26.9 29.6 7.75 7.80 26.9 29.8 8.54 8.89 28.6 9.14 9.40 29.3 9.75 9.96 16.4 10.75 10.80 15.9</td><td>0.00 0.51 0.05 0.10 12.0 0.61 1.09 26.5 1.22 1.70 1.83 2.19 2.00 2.05 26.6 2.44 2.90 28.8 3.05 3.51 29.1 3.05 3.51 29.1 3.06 3.99 28.9 6.10 6.48 5.18 36 23 13 4.75 4.80 26.6 6.10 6.48 6.00 6.05 26.6 6.10 7.15 22.6 7.75 7.80 26.9 28.9 8.54 8.89 28.6 6.10 7.15 22.6 7.75 7.80 26.9 29.6 8.74 9.40 29.3 8.75 9.96 10.92 16.4 10.75 10.80 15.9</td><td>0.00 0.51 0.05 0.10 12.0 0.61 1.09 26.5 1.22 1.70 1.83 2.19 26.6 2.00 2.05 26.6 2.04 2.90 28.8 39 21 18 CL 3.05 3.80 26.6 37 23 14 CL 4.27 4.67 21.5 4.20 4.25 21.5 6.10 6.48 5.89 28.9 6.10 6.05 26.6 6.10 6.48 22.6 6.10 7.15 22.6 7.75 7.80 26.9 8.54 8.89 28.6 8.54 8.89 28.6 8.54 8.89 28.6 8.54 8.89 28.6 8.54 8.89 28.6 8.54 8.89 28.6 8.55 9.96 10.92 16.4 10.75 10.80 15.9 10.97 11.46 16.1</td><td>0.00 0.51 0.05 0.10 12.0 0.61 1.09 26.5 1.22 1.70 1.83 2.19 26.6 2.00 2.05 26.6 2.04 2.90 28.8 39 21 18 CL 3.05 3.90 26.6 37 23 14 CL 4.27 4.67 21.5 4.20 4.25 21.5 6.10 6.48 5.89 28.9 6.10 6.48 6.50 26.6 6.10 7.75 7.80 26.9 6.10 7.75 7.80 26.9 8.54 8.89 28.6 8.54 8.89 28.6 8.54 8.89 28.6 8.54 8.89 28.6 8.55 9.96 10.36 10.92 16.4 10.75 10.80 15.9 10.97 11.46 16.1</td><td>0.00 0.51 0.00 0.51 0.00 0.51 0.00 0.51 0.01 12.0 0.01 12.0 0.05 1.10 0.05 1.10 0.05 1.10 0.06 1.10 0.06 1.10 0.07 1.10 0.08 26.5 0.09 26.5 0.09 26.5 0.09 26.5 0.09 26.5 0.09 26.5 0.09 26.5 0.09 26.6 0.09 26.6 0.09 26.6 0.09 26.6 0.00 6.05 26.6 0</td></td<>	0.00       0.51         0.05       0.10       12.0         0.61       1.09       26.5         1.22       1.70         1.83       2.19       26.6         2.00       2.05       26.6         2.44       2.90       28.8       39         3.05       3.51       29.1       37         3.05       3.51       29.1       37         4.27       4.67       4.26       21.5         4.20       4.25       21.5       37         4.20       4.25       21.5       37         4.88       5.18       24.3       36         5.49       5.89       28.9       36         6.00       6.05       26.6       6         6.10       6.48       28.9       28.9         6.10       6.48       26.9       29.9         7.75       7.75       7.75       7.80       26.9         7.75       7.80       26.9       29.9         7.75       7.80       26.9       29.3         9.14       9.40       29.3         9.75       9.96       16.4         10.75       11.46	0.00 0.51 0.05 0.10 12.0 0.61 1.09 26.5 1.22 1.70 1.83 2.19 2.00 2.05 26.6 2.44 2.90 28.8 39 21 11 3.05 3.51 29.1 3.05 3.51 29.1 3.05 3.51 29.1 3.05 3.51 29.1 3.05 3.90 26.6 4.27 4.67 24.3 36 2.3 11 4.75 4.80 24.3 36 2.3 11 6.00 6.05 26.6 6.71 7.01 18.6 7.75 7.80 26.9 29.6 7.75 7.80 26.9 29.8 8.54 8.89 28.6 9.14 9.40 29.3 9.75 9.96 16.4 10.75 10.80 15.9	0.00 0.51 0.05 0.10 12.0 0.61 1.09 26.5 1.22 1.70 1.83 2.19 2.00 2.05 26.6 2.44 2.90 28.8 3.05 3.51 29.1 3.05 3.51 29.1 3.06 3.99 28.9 6.10 6.48 5.18 36 23 13 4.75 4.80 26.6 6.10 6.48 6.00 6.05 26.6 6.10 7.15 22.6 7.75 7.80 26.9 28.9 8.54 8.89 28.6 6.10 7.15 22.6 7.75 7.80 26.9 29.6 8.74 9.40 29.3 8.75 9.96 10.92 16.4 10.75 10.80 15.9	0.00 0.51 0.05 0.10 12.0 0.61 1.09 26.5 1.22 1.70 1.83 2.19 26.6 2.00 2.05 26.6 2.04 2.90 28.8 39 21 18 CL 3.05 3.80 26.6 37 23 14 CL 4.27 4.67 21.5 4.20 4.25 21.5 6.10 6.48 5.89 28.9 6.10 6.05 26.6 6.10 6.48 22.6 6.10 7.15 22.6 7.75 7.80 26.9 8.54 8.89 28.6 8.54 8.89 28.6 8.54 8.89 28.6 8.54 8.89 28.6 8.54 8.89 28.6 8.54 8.89 28.6 8.55 9.96 10.92 16.4 10.75 10.80 15.9 10.97 11.46 16.1	0.00 0.51 0.05 0.10 12.0 0.61 1.09 26.5 1.22 1.70 1.83 2.19 26.6 2.00 2.05 26.6 2.04 2.90 28.8 39 21 18 CL 3.05 3.90 26.6 37 23 14 CL 4.27 4.67 21.5 4.20 4.25 21.5 6.10 6.48 5.89 28.9 6.10 6.48 6.50 26.6 6.10 7.75 7.80 26.9 6.10 7.75 7.80 26.9 8.54 8.89 28.6 8.54 8.89 28.6 8.54 8.89 28.6 8.54 8.89 28.6 8.55 9.96 10.36 10.92 16.4 10.75 10.80 15.9 10.97 11.46 16.1	0.00 0.51 0.00 0.51 0.00 0.51 0.00 0.51 0.01 12.0 0.01 12.0 0.05 1.10 0.05 1.10 0.05 1.10 0.06 1.10 0.06 1.10 0.07 1.10 0.08 26.5 0.09 26.5 0.09 26.5 0.09 26.5 0.09 26.5 0.09 26.5 0.09 26.5 0.09 26.6 0.09 26.6 0.09 26.6 0.09 26.6 0.00 6.05 26.6 0

0101-11413	1413					LABORAT	LABORATORY TEST SUMMARY	UMMARY					Page 5 of 10
Borehole	Sample	Sample Interval	nterval	Moisture	Salinity	Liquid	Plastic	Plasticity	<u>S</u>	Clay	Sit	Sand	Gravel
	Number	from	<b>t</b>	Content		Limit	Limit	Index	Classification				
		(m)	(m)	(%)	(ppt)					(%	(%)	(%)	(%)
11413-05	-	00.0	0.56	NOTE: All sampl		ed from Bo	es obtained from Borehole #11413 -05	13 -05					
11413-05	cų	0.61	1.17	were retained by Geological Survey of Canada, Terrain Sciences Division	by Geologics	al Survey of	Canada, Tel	rrain Science	s Division				
11413-05	ო	1.22	1.78		•	•	,						
11413-05	4	1.83	2.39										
11413-05	9	2.44	2.85										
11413-05	φ	3.05	3.40										
11413-05	7	3.66	4.22										
11413-05	∞	4.27	4.88										
11413-05	თ	4.88	5.26										
11413-05	10	5.49	5.74										
11413-05	11	6.10	6.71										
11413-05	12	6.71	7.24										
11413-05	ე წ	7.32	7.80										
11413-05	14	7.93	8.18										
11413-05	15	8.54	8.84										
11413-05	16	9.14	9.30										
11413-05	17	9.65	10.19										
11413-05	8	10.31	10.82										
11413-05	19	10.97	11.43										
11413-05	20	11.43	12.04										
11413-05	21	12.12	12.65										
11413-05	22	12.65	13.26										
11413-05	23	13.26	13.87										
11413-05	24	13.87	14.48										

Page 6 of 10	Gravei	(%)																				0.4		0.0					0.0	0.0		0.0		0.0				EBA ENGINEERING CONSULTANTS LTD.
	Sand	(%)																				23.8		79.5					74.8	0.5		73.5		69.0				NSULT
	Sil	(%)																				37.7		14.4					20.1	41.1		18.8		23.2				IING CO
	Clay	(%)																				38.1		6.1					5.1	58.4		7.7		7.8				GINEEF
	USC Classification			es Division																				85					&									EBA EN
SUMMARY	Plasticity Index		413 -06	errain Scieno																																		
LABORATORY TEST SUMMARY	Plastic Limit		es obtained from Borehole #11413 -06	f Canada, Te																																		
LABORA	Liquid Limit		ned from B	ai Survey o																																		
	Salinity	(ppt)	All samples obtai	d by Geologic																				27								33						
	Moisture Content		NOTE: All s	were retained by Geological Survey of Canada, Terrain Sciences Division																		24.9	17.5	21.3	18.3	19.8		20.6	16.5	34.6	36.2	14.2	13.6	14.7		21.3		
	Interval to	(E)	0.38	1.04	1.55	2.24	2.85	3.53	3.96	4.60	5.33	5.89	6.50	7.24	7.70	8.46	60.6	9.53	10.31	۲.	11.53	0.31	1.07	1.37	2.13	2.74	3.66	4.06	4.70	0.41	0.91	1.58	2.13	2.90	3.66	3.81	4.88	5.49
	Sample Interval from to	(E)	0.00	0.61	1.22	1.83	2.44	3.05	3.66	4.27	4.88	5.49	6.10	6.71	7.32	7.93	8.54	9.14	9.75	10.36	10.97	0.15	0.91	1.22	1.98	2.59	3.05	3.91	4.55	0.25	97.0	1.42	2.03	2.74	3.05	3.66	4.27	4.88
1413	Sample Number		-	7	ო	4	9	9	7	œ	თ	10	-	12	13	4	15	16	17	18	9	-	2	ო	4	ល	ဖ	7	œ	-	0	ო	4	ស	9	7	Φ	တ
0101-11413	Borehole		11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-06	11413-07	11413-07	11413-07	11413-07	11413-07	11413-07	11413-07	11413-07	11413-08	11413-08	11413-08	11413-08	-	_	11413-08	11413-08	11413-08

0101-11413	1413					LABORAT	LABORATORY TEST SUMMARY	SUMMARY					Page 7 of 10
Borehole	Sample Number	Sample Interval from to	Interval to	Moisture Content	Salinity	Liquid	Plastic Limit	Plasticity Index	USC Classification	Clay	Silt	Sand	Gravel
		(m)	(m)	(%)	(ppt)					(%)	(%)	(%)	(%)
11413-09	-	0.61	0.91	27.8		39	22	- 17	ರ	39.1	55.0	5.9	0.0
11413-09	0	1.37	1.52	12.4					æ	4.6	15.0	75.6	0.0
11413-09	ო	1.83	2.13	15.4	25								
11413-09	4	2.74	2.90	12.7									
11413-09	9	3.20	3.35	11.5									
11413-09	9	3.96	4.12	20.8									
11413-10	-	0.23	0.38	27.6						55.3	43.7	1.0	0.0
11413-10	Ø	92.0	0.97	ഗ									
11413-10	ო	1.37	1.52	21.8	21				SP/SM	1	6.5	93.5	0.0
11413-10	4	2.13	2.29	19.7									
11413-10	တ	2.52	2.67	11.8									
11413-10	9	2.74	2.90	14.0	20					20.1	20.4	59.3	0.2
11413-10	7	3.20	3.35	20.0									
11413-10	89	3.66	4.27										
11413-10	თ	4.57	4.72	22.3									
11413-10	10	4.88	5.33										
11413-11	<del>-</del>	0.76	0.91	21.1					WS/dS	ı	5.6	94.4	0.0
11413-11	8	1.52	1.68	15.8									
11413-11	ო	2.13	2.29	20.4	28				Æ	5.7	11.9	82.4	0.0
11413-11	4	2.74	2.90	22.0									
11413-11	သ	3.43	3.51	14.6									
11413-11	ø	3.96	4.12	20.7	56				₹,	4.1	7.1	88.8	0.0
11413-12	₩.	0.41	0.56	12.3						13.3	17.2	69.5	0.0
11413-12	01	98.0	1.02	11.9						15.6	16.5	67.9	0.0
11413-12	ო	1.63	1.78	15.1	38								
11413-12	4	2.13	2.29	15.6	29								
11413-12	သ	2.44	3.05										
11413-12	ဖ	3.05	3.12	21.0									
413-1	7	3.96	4.12	16.4	24					15.8	16.7	67.5	0.0
11413-12	∞	4.47	4.62	18.3									

0101-11413	1413					LABORAT	LABORATORY TEST SUMMARY	SUMMARY					Page 8 of 10	
Borehole	Sample	Sample Interval	Interval	Moisture	Salinity	Liquid	Plastic	Plasticity	283	Clay	Silt	Sand	Gravel	
	Number	from	ţ	Content		Limit	Limit	Index	Classification					
		(m)	(m)	(%)	(ppt)					(%)	(%)	(%)	(%)	
11413-13	*-	0.23	0.38	32.2						46.6	39.4	14.0	0.0	
11413-13	2	0.97	1.12	21.6										
11413-13	ო	1.37	1.52	23.3					გ	,	2.8	97.2	0.0	
11413-13	4	2.13	2.29	14.0						11.9	19.2	68.9	0.0	
11413-13	5	2.74	2.90	15.3	16									
11413-13	9	3.35	3.51	15.7										
11413-13	7	3.71	3.91	17.2										
11413-14	-	0.15	0.31	20.0						31.0	25.0	44.0	0.0	
11413-14	0	0.91	1.07	18.6	22					10.4	22.9	66.7	0.0	
11413-14	ო	1.52	1.68	20.6					æ	4.7	ල ල	85.1	0.3	
11413-14	4	1.83	2.44											
11413-14	ß	2.44	3.05											
11413-14	9	3.20	3.35	21.7										
11413-14	7	3.96	4.12	19.8	19									
11413-15	-	0.10	0.25	24.4										
11413-15	Ø	0.76	1.07	20.6	27					16.1	29.4	53.4	1.1	
11413-15	ო	1.22	1.83											
11413-15	4	1.83	2.44											
11413-15	လ	2.74	2.90	30.1	24				SP/SM	t	11.2	88.8	0.0	
11413-15	9	3.35	3.51	26.3										
11413-15	7	3.89	4.04	20.2										
11413-15	∞	4.27	4.57	21.8										
11413-15	თ	4.88	5.49											
11413-15	10	5.49	5.94											

Page 9 of 10	Gravel	(%)																									
	Sand	(%)																									
	Silt	(%)																									
	Clay	(%)																									
	OSD (S	Classification		s Division																			s Division				ida,
SUMMARY	Plasticity	Index	113 -16	Geological Survey of Canada, Terrain Sciences Division																		113 -17	were retained by Geological Survey of Canada, Terrain Sciences Division				NOTE: No samples were retained by Geological Survey of Canada, Terrain Sciences Division.
LABORATORY TEST SUMMARY	Plastic	LIMIT	orehole #114	f Canada, Te																		orehole #114	f Canada, Te				Geological S
LABORA	Liquid		es obtained from Borehole #11413 -16	ical Survey o	•																	es obtained from Borehole #11413 -17	ical Survey o				e retained by
	Salinity	(ppt)	All samples obt																			samples obt	d by Geolog				samples wer nces Divisior
	Moisture	(%)	NOTE: All	were retained by																		NOTE: All sample	were retaine				NOTE: No samples were Terrain Sciences Division.
	Interval	2 €	0.20	0.37	0.97	1.50	2.19	2.95	3.48	4.17	4.93	5.36	5.85	6.48	7.06	7.59	8.08	8.97	9.65	10.49	10.97	0.41	98.0	1.78	2.21	3.35	
	Sample Interval	(m)	00.0	0.20	0.37	0.97	1.50	2.19	2.95	3.48	4.17	4.93	5.36	5.85	6.48	7.06	7.59	8.09	8.97	9.65	10.49	0.00	0.41	0.86	1.68	3.20	
1413	Sample	iacilion in action	-	7	ო	4	5	9	7	∞	თ	10	-1	12	13	14	15	16	17	18	6	-	0	က	4	ഹ	-
0101-11413	Borehole		11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-16	11413-17	11413-17	11413-17	11413-17	11413-17	11413-18

0101-11413	1413					LABORAT	LABORATORY TEST SUMMARY	SUMMARY				ď	Page 10 of 10
Borehole	Sample	Sample Interval	Intervai	Moisture	Salinity	Liquíd	Plastic	Plasticity	83	Clay	Silt	Sand	Gravel
	Number	from	ţ	Content		Limit	Limit	Index	Classification	•			
		(E)	(E)	(%)	(ppt)					(%)	(%)	(%)	(%)
11413-19		0.00	0.46	NOTE: All sample	ampies obtai	es obtained from Borehole #11413 -19	rehole #114	13 -19					
11413-19	64	0.61	1.07	were retained by		al Survey of	Canada, Te	Geological Survey of Canada, Terrain Sciences Division	s Division				
11413-19	ო	1.22	1.68										
11413-19	4	1.83	2.34										
11413-19	S	2.44	2.85										
11413-19	မ	3.05	3.66										
11413-19	7	3.66	4.12										
11413-19	ω	4.27	5.03										
11413-19	တ	5.49	5.79										
11413-19	10	6.10	6.55										
11413-19	11	7.62	8.08										
11413-19	12	9.14	9.60										
11413-19	ဗ	10.67	10.82										

PARTICLE SIZE DISTRIBUTION ANALYSIS SUMMARY

Borehole	Del	Depth							_	Percent Pa	Passing								
Number	from	to	20	12.5	9.5	4.75	~	0.85	0.425	0.25	0.15	0.75	0.03	0.02	0.01	600.0	0.006	0.003	0.001
			Æ	E	E	E	E	E	E	E	Ē	E	E	Æ	E	E	æ	E	E
	(m)	(m)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
11413-01	0.00	0.30	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	9.66	99.1	92.4	83.9	68.5	58.5	49.6	34.2	25.7
11413-01	0.30	0.33	100.0	100.0	100.0	100.0	100.0	100.0	9.8	99.4	98.6	98.4	92.1	84.2	0.89	57.2	47.6	33.4	22.2
11413-01	0.34	0.40	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	96.0	87.0	71.5	54.0	32.7	23.8	19.7	14.9	11.1
11413-01	0.40	0.45	100.0	100.0	100.0	100.0	100.0	100.0	8.66	98.8	75.0	37.4	33.4	26.4	16.5	12.7	10.2	8.6	6.4
11413-01	0.50	0.60	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	98.4	93.6	78.1	0.09	37.5	27.6	21.3	12.7	9.5
11413-01	0.72	0.75	100.0	100.0	100.0	100.0	100.0	100.0	100.0	98.3	44.7	10.7	10.6	9.1	6.1	5.5	4.6	3.6	3.0
11413-01	0.78	0.83	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	97.2	79.4	60.4	36.5	28.6	22.9	16.5	12.1
11413-01	1.05	1.10	100.0	100.0	100.0	100.0	100.0	8.66	9.66	99.2	87.0	53.6	46.1	33.4	20.0	16.5	14.3	1.1	9,5
11413-01	1.60	1.65	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	98.0	86.4	68.3	57.2	41.3	31.8	24.8	17.5	12.1
11413-01	1.90	1.95	100.0	100.0	96.3	88.8	86.8	86.4	86.1	84.8	72.7	65.3	56.9	48.6	31.5	24.2	17.7	12.4	8.8
11413-01	2.25	2.30	100.0	100.0	98.1	84.0	71.8	20.3	69.7	56.4	29.6	24.5							
11413-01	2.75	2.80	100.0	100.0	96.0	83.3	77.5	77.3	77.1	7.97	37.4	6.9							
11413-01	3.30	3.35	100.0	100.0	100.0	100.0	100.0	100.0	100.0	6.66	95.3	19.3	11.1	8.7	6.4	5.6	4 8	4.0	3.5
11413-01	3.50	3.55	100.0	100.0	100.0	100.0	100.0	100.0	8'66	9.66	99.2	88.8	6.69	52.4	31.8	22.9	19.1	14.3	1.1
11413-01	4.00	4.05	100.0	100.0	100.0	100.0	100.0	100.0	8.66	99.4	98.0	56.8	41.3	36.5	27.0	20.3	15.9	9.5	6.0
11413-01	4.60	4.65	100.0	100.0	100.0	100.0	100.0	8.66	99.4	0.66	96.4	52.6	34.9	30.2	24.8	21.3	18.1	14.3	1.1
11413-01	5.60	5.65	100.0	100.0	100.0	98.8	98.4	98.2	98.2	97.6	38.0	19.7	16.2	15.0	12.5	10.9	9. 4.	7.8	6.2
11413-01	7.10	7.15	100.0	100.0	100.0	100.0	100.0	100.0	99.6	0.66	84.6	55.8	8.09	46.1	34.3	29.5	24.8	18.4	14.3
11413-01	7.60	7.65	100.0	100.0	100.0	100.0	100.0	100.0	99.8	97.6	43.1	5.2	4.4	4.1	3.8	3.5	3.2	2.9	5.6
11413-01	8.20	8.30	100.0	100.0	100.0	100.0	100.0	100.0	100.0	97.2	78.2	39.8	27.0	24.1	22.6	20.0	18.7	14.0	9.5
11413-01	8.75	8.80	100.0	100.0	100.0	100.0	100.0	8.66	93.6	99.2	72.0	45.6	35.6	34.0	30.2	28.6	25.4	19.7	15.9
11413-01	ന	9.40	100.0	100.0	100.0	100.0	100.0	100.0	8.66	92.6	66.0	40.0	19.1	17.5	14.3	13.3	12.7	12.1	10.2
11413-01	9.55	9.60	100.0	100.0	100.0	100.0	100.0	100.0	8.66	98.0	78.0	58.8	49.2	46.1	41.9	38.1	33.4	26.4	19.7

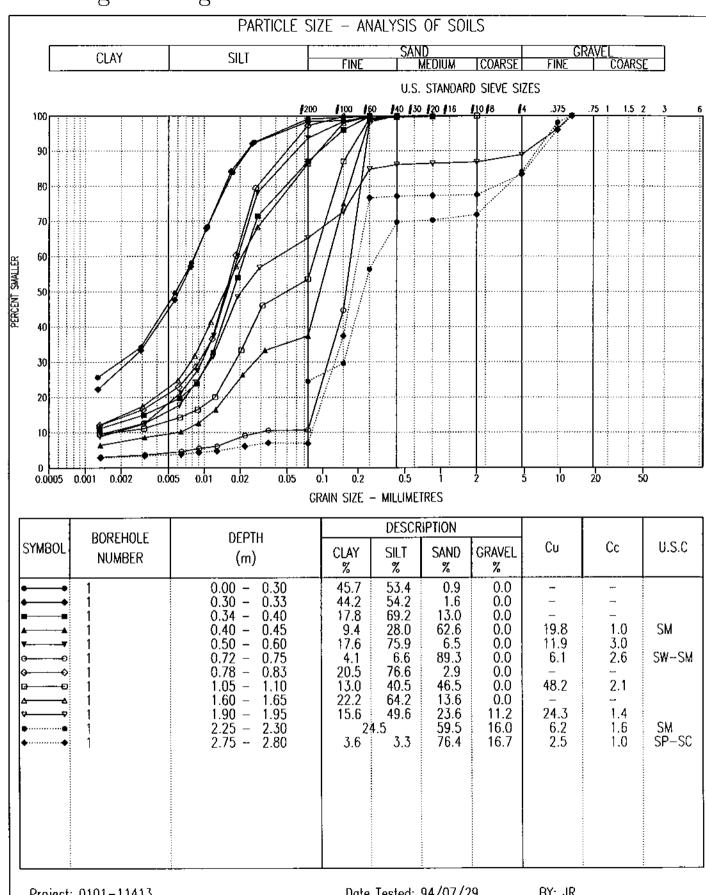
2 0.85 0.425 0.25 0.15 0.75 0.03 0.02 mm mm mm mm mm mm mm mm mm mm (%) (%) (%) (%) (%) (%) (%) (%)	99.7 99.5 98.9 86.5 83.1 66.6 38.7 19.0 14.9 12.1 7.6 6.3 99.8 99.6 99.4 93.8 91.8 68.3 40.3 19.7 15.2 11.8 8.9 6.4 100.0 100.0 99.6 91.8 89.8 82.6 34.9 25.4 10.2 8.9 6.0 3.5	99.3 99.0 51.2 19.8 18.4 15.7 12.5 10.6 8.7 6.2 100.0 99.8 99.3 79.5 67.4 51.7 31.5 21.7 15.7 10.1	99.2 98.8 97.0 81.0 67.3 51.5 41.3 32.4 24.8	77.5 32.7 22.7 19.6 14.8 8.9 6.5 6.1 4.5 99.8 99.2 96.6 85.8 68.3 46.1 39.1 32.4 22.2	99.8 98.8 82.6 69.9 50.8 40.7 33.4 22.9	69.1 14.7 4.6	99.8 78.4	33.0 52.0 53.0 53.0 44.5 41.3 35.6 27.0 50.0 50.0 50.0 50.0 50.0 50.0 50.0 5	41.3 7.4 4.7 3.5 2.8 2.4 2.1 0.7	52.5 8.0 6.6 5.0 4.4 4.0 3.8 3.6	33.0 8.0 5.6 5.4 4.8 4.3 4.0 3.5	31.3 16.8 9.9 8.0 6.5 5.1 3.4 0.9	68.2 35.0 25.4 24.8 22.9 20.6 19.1 15.9	28.6 26.0 22.9 22.2 18.4 13.3
2 0.85 0.425 0.25 0.15 0.75 0.03 0.02 0.01 0.009 0.006 mm mm mm mm mm mm mm mm mm mm mm mm mm	99.5 98.9 86.5 83.1 66.6 38.7 19.0 14.9 12.1 99.6 99.4 93.8 91.8 68.3 40.3 19.7 15.2 11.8 100.0 99.6 91.8 89.8 82.6 34.9 25.4 10.2 8.9	99.3 99.0 51.2 19.8 18.4 15.7 12.5 10.6 8.7 100.0 99.8 99.3 79.5 67.4 51.7 31.5 21.7 15.7	99.2 98.8 97.0 81.0 67.3 51.5 41.3 32.4	77.5 32.7 22.7 19.6 14.8 8.9 6.5 6.1 99.8 99.2 96.6 85.8 68.3 46.1 39.1 32.4	100.0 99.8 98.8 82.6 69.9 50.8 40.7 33.4	69.1 14.7 4.6	99.8 78.4 34.4 28.6 25.4 20.6 18.4 16.5	33.0 52.0 55.6 53.0 44.5 41.3 35.6 40.6 50.0 50.0 50.0 50.0 50.0 50.0 50.0 5	41.3 7.4 4.7 3.5 2.8 2.4 2.1	52.5 8.0 6.6 5.0 4.4 4.0 3.8	33.0 8.0 5.6 5.4 4.8 4.3 4.0	31.3 16.8 9.9 8.0 6.5 5.1 3.4	68.2 35.0 25.4 24.8 22.9 20.6 19.1	.4 41.8 28.6 26.0 22.9 22.2 18.4
2 0.85 0.425 0.25 0.15 0.75 0.03 0.02 0.01 0.009 mm mm mm mm mm mm mm mm mm mm mm mm mm	99.5 98.9 86.5 83.1 66.6 38.7 19.0 14.9 99.6 99.4 93.8 91.8 68.3 40.3 19.7 15.2 100.0 99.6 91.8 89.8 82.6 34.9 25.4 10.2	99.3 99.0 51.2 19.8 18.4 15.7 12.5 10.6 100.0 99.8 99.3 79.5 67.4 51.7 31.5 21.7	99.2 98.8 97.0 81.0 67.3 51.5 41.3	77.5 32.7 22.7 19.6 14.8 8.9 6.5 99.8 99.2 96.6 85.8 68.3 46.1 39.1	100.0 99.8 98.8 82.6 69.9 50.8 40.7	69.1 14.7 4.6	99.8 78.4 34.4 28.6 25.4 20.6 18.4	93.0 52.0 55.6 53.0 44.5 41.3	41.3 7.4 4.7 3.5 2.8 2.4	52.5 8.0 6.6 5.0 4.4 4.0	33.0 8.0 5.6 5.4 4.8 4.3	31.3 16.8 9.9 8.0 6.5 5.1	68.2 35.0 25.4 24.8 22.9 20.6	.4 41.8 28.6 26.0 22.9 22.2
2 0.85 0.425 0.25 0.15 0.75 0.03 0.02 0.01 mm mm mm mm mm mm mm mm mm mm mm mm mm	99.5 98.9 86.5 83.1 66.6 38.7 19.0 99.6 99.4 93.8 91.8 68.3 40.3 19.7 100.0 99.6 91.8 89.8 82.6 34.9 25.4	99.3 99.0 51.2 19.8 18.4 15.7 12.5 100.0 99.8 99.3 79.5 67.4 51.7 31.5	99.2 98.8 97.0 81.0 67.3 51.5	77.5 32.7 22.7 19.6 14.8 8.9 99.8 99.2 96.6 85.8 68.3 46.1	100.0 99.8 98.8 82.6 69.9 50.8	69.1 14.7 4.6	99.8 78.4 34.4 28.6 25.4 20.6	93.0 52.0 55.6 53.0 44.5	41.3 7.4 4.7 3.5 2.8	52.5 8.0 6.6 5.0 4.4	33.0 8.0 5.6 5.4 4.8	31.3 16.8 9.9 8.0 6.5	68.2 35.0 25.4 24.8 22.9	.4 41.8 28.6 26.0 22.9
2 0.85 0.425 0.15 0.15 0.75 0.03 0.02 mm mm mm mm mm mm mm mm mm mm mm mm mm	99.5 98.9 86.5 83.1 66.6 38.7 99.6 99.4 93.8 91.8 68.3 40.3 100.0 99.6 91.8 89.8 82.6 34.9	99.3 99.0 51.2 19.8 18.4 15.7 100.0 99.8 99.3 79.5 67.4 51.7	99.2 98.8 97.0 81.0 67.3	77.5 32.7 22.7 19.6 14.8 99.8 99.2 96.6 85.8 68.3	100.0 99.8 98.8 82.6 69.9	69.1 14.7 4.6	99.8 78.4 34.4 28.6 25.4	33.0 52.0 35.6 53.0 100.0 55.0 55.0	41.3 7.4 4.7 3.5	52.5 8.0 6.6 5.0	33.0 8.0 5.6 5.4	31.3 16.8 9.9 8.0	68.2 35.0 25.4 24.8	.4 41.8 28.6 26.0
2 0.85 0.425 0.25 0.15 0.75 0.03 mm mm mm mm mm mm mm mm mm mm mm mm mm	99.5 98.9 86.5 83.1 66.6 99.6 99.4 93.8 91.8 68.3 100.0 99.6 91.8 89.8 82.6	99.3 99.0 51.2 19.8 18.4 100.0 99.8 99.3 79.5 67.4	99.2 98.8 97.0 81.0	77.5 32.7 22.7 19.6 99.8 99.2 96.6 85.8	100.0 99.8 98.8 82.6	69.1 14.7 4.6	99.8 78.4 34.4 28.6	93.0 62.0 35.6	41.3 7.4 4.7	52.5 8.0 6.6	33.0 8.0 5.6	31.3 16.8 9.9	68.2 35.0 25.4	4 41.8 28.6
Percent Passing 2 0.85 0.425 0.25 0.15 0.75 mm mm mm mm mm mm mm (%) (%) (%) (%) (%) (%)	99.5 98.9 86.5 83.1 99.6 99.4 93.8 91.8 100.0 99.6 91.8 89.8	99.3 99.0 51.2 19.8 100.0 99.8 99.3 79.5	99.2 98.8 97.0	77.5 32.7 22.7 99.8 99.2 96.6	100.0 99.8 98.8	69.1 14.7 4.6	99.8 78.4 34.4	93.0 52.0	41.3 7.4	52.5 8.0	33.0 8.0	31.3 16.8	68.2 35.0	4. 8. 8.
Percent Passing 2 0.85 0.425 0.25 0.15 mm mm mm mm mm mm (%) (%) (%) (%) (%)	99.5 98.9 86.5 99.6 99.4 93.8 100.0 99.6 91.8	99.3 99.0 51.2 100.0 99.8 99.3	99.2 98.8	77.5 32.7 99.8 99.2	100.0 99.8	69.1 14.7	99.8 78.4	0.50	41.3	52.5	33.0	31.3	68.2	4
Percent Pa 2 0.85 0.425 0.25 mm mm mm mm mm (%) (%) (%) (%)	99.5 98.9 99.6 99.4 100.0 99.6	99.3 99.0 100.0 99.8	99.5	77.5 99.8	100.0	69.1	8.66							72.4
2 0.85 0.425 mm mm mm mm (%) (%)	99.5 99.6 100.0	99.3						88.0	91.1	6.99	37.0	Ξ.	ഗ	
2 0.85 0.425 mm mm mm mm (%) (%)			96.6	87.1 100.0	0.00	n					ω	40.1	96.6	97.0
2 mm (%)	99.7 99.8 100.0				7	98.3	100.0	0.00	9.66	0.66	98.0	50.4	8.66	ဆ တ တ
$\vdash$		99.4	100.0	91.6	100.0	0.66	100.0	0000	99.9	99.5	98.6	54.4	100.0	100.0
4.75 mm (%)	99.9 100.0 100.0	99.7	100.0	94.8 100.0	100.0	99.2	100.0	00.0	100.0	2.66	100.0	62.6	100.0	100.0
	99.9 100.0 100.0	99.8	100.0	96.7 100.0	100.0	99.5	100.0	0.00	100.0	100.0	100.0	71.4	100.0	100.0
9.5 mm (%)	100.0 100.0 100.0	100.0	100.0	98.3 100.0	100.0	100.0	100.0	0.00	100.0	100.0	100.0	82.7	100.0	100.0
12.5 mm (%)	100.0	100.0	100.0	100.0 100.0	100.0	100.0	100.0	0.00	100.0	100.0	100.0	92.8	100.0	100.0
20 mm (%)	100.0 100.0 100.0	100.0	100.0	100.0	100.0	100.0	100.0	0.00	100.0	100.0	100.0	100.0	100.0	100.0
(j) to	0.45	1.30	3.10	3.66	5.35	5.82	6.35	07.7	8.30	8.60	9,45	9.87	10.10	10.55
Depth from (m)	0.00	0.70	3.05	3.61 4.80	5.30	5.78	6.30	02.0	8.25	8.55	9.40	9.84	10.05	10.50
Borehole Number	11413-02 11413-02 11413-02	11413-02	11413-02	11413-02	11413-02	11413-02	11413-02	11413-02	11413-02	11413-02	11413-02	11413-02	11413-02	1413-02

	Borehole	Depth	tk th								Percent Passing	assing								
(m)         (m)         (m)         mm	Number	from	t	20	12.5	9.5	4.75	2	0.85	-	0.25	0.15	0.75	0.03	0.02	10.0	0.009	900.0	0.003	0.001
(m) (m) (kg) (kg) (kg) (kg) (kg) (kg) (kg) (kg				E	E	E	E	E	Æ	E	Æ	E	E	E	E	E	æ	E	E	E
0.00         0.15         100.0         1		(m)	(m)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
0.00         1.15         100.0         1																				
1.00 1.05 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 99.5 88.4 78.6 48.1 78.6 48.1 37.0 2.0 2.0 7 100.0	11413-03	0.00	0.15	100.0	100.0	100.0	8.66	99.7	99.5	99.1	87.4	36.8	29.1	25.5	22.6	19.0	16.5	14,4	12.4	7.9
1.56         1.58         100.0         1	11413-03	1.00	1.05	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	9.66	88.4	78.6	49.1	37.0	28.5	17.4	10.5
2.02         2.04         100.0         1	11413-03	1,55	1.58	100.0	100.0	100.0	100.0	99.3	98.9	98.2	87.3	4.1	2.3							
2.70         2.75         100.0         1	11413-03	2.02	2.07	100.0	100.0	100.0	100.0	100.0	100.0	100.0	99.5	26.8	2.4							
3.22         3.27         100.0         1	11413-03	2.70	2.75	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	92.6	82.8	74.6	68.3	54.6	46.7	38.1	25.4	17.5
3.86         3.85         100.0         1	11413-03	3.22	3.27	100.0	100.0	100.0	100.0	100.0	100.0	100.0	93.6	48.4	46.4	41.3	36.5	27.6	22.9	19.1	12.7	9.5
4.84         4.88         (4.8)         (	11413-03	3.80	3.85	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	85.2	84.4	76.2	2.79	52.4	45.1	38.1	26.0	18.4
6.05         6.10         100.0         1	11413-03	4.84	4.88	100.0	100.0	100.0	100.0	100.0	100.0	100.0	99.7	94.3	89.5	81.2	9.77	56.4	45.1	36.1	22.6	13.5
7.15         7.20         100.0         1	11413-03	6.05	6.10	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	0.66	90.5	78.5	60.4	54.0	45.4	31.8	22.9
8.50         8.60         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         99.8         98.4         91.0         82.6         68.2         48.0         35.9         30.5           10.55         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         99.8         98.4         91.0         82.6         69.9         56.5         49.2         10.0         100.0 <t< td=""><td>11413-03</td><td>7.15</td><td>7.20</td><td>100.0</td><td>100.0</td><td>100.0</td><td>100.0</td><td>100.0</td><td>100.0</td><td>100.0</td><td>8.66</td><td>8.86</td><td>98.2</td><td>70.5</td><td>61.0</td><td>50.2</td><td>41.9</td><td>35.6</td><td>24.8</td><td>18.4</td></t<>	11413-03	7.15	7.20	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	8.86	98.2	70.5	61.0	50.2	41.9	35.6	24.8	18.4
9.65         9.70         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         99.8         98.4         91.0         82.6         69.9         56.5         41.9         34.0           10.65         10.70         100.0	11413-03	8.50	8.60	100.0	100.0	100.0	100.0	100.0	100.0	100.0	0.66	73.0	59.6	56.2	48.0	35.9	30.5	26.0	18.7	12.7
10.65         10.70         100.0 <th< td=""><td>11413-03</td><td>9.65</td><td>9.70</td><td>100.0</td><td>100.0</td><td>100.0</td><td>100.0</td><td>100.0</td><td>100.0</td><td>100.0</td><td>8.66</td><td>98.4</td><td>91.0</td><td>82.6</td><td>66.69</td><td>56.5</td><td>49.2</td><td>42.9</td><td>32.4</td><td>23.8</td></th<>	11413-03	9.65	9.70	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	98.4	91.0	82.6	66.69	56.5	49.2	42.9	32.4	23.8
0.05         0.10         100.0         1	11413-03	10.65	10.70	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	98.6	92.0	81.6	63.5	41.9	34.0	27.6	19.7	15.2
0.05         0.10         100.0         1	11413-03	11.95	12.00	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	98.3	94.3	77.2	59.0	52.1	44.9	33.6	21.3
0.05         0.10         100.0         1																				
1.00         1.05         100.0         1	11413-04	0.05	0.10	100.0	100.0	100.0	100.0	100.0	100.0	8.66	9.66	97.2	73.8	64.2	54.6	44.5	38.1	31.8	22.9	16.5
2.00         2.05         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         98.6         96.4         95.0         88.3         76.2         61.9         51.8           3.00         3.05         100.0	11413-04	1.00	1.05	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	98.2	85.6	73.7	66.7	54.6	44.5	36.5	25.4	16.8
3.00         3.05         100.0         1	11413-04	2.00	2.05	100.0	100.0	100.0	100.0	100.0	100.0	100.0	98.6	96,4	95.0	88.3	76.2	6.1.9	51.8	41.3	28.6	20.6
4.20         4.25         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         99.2         98.6         90.1         75.7         57.5         47.3           5.50         5.55         100.0         100.0         100.0         100.0         100.0         100.0         99.8         98.8         93.7         82.6         53.4         40.3           6.00         6.05         100.0         100.0         100.0         100.0         100.0         100.0         99.8         99.8         93.0         79.7         68.7         59.3           7.10         7.15         100.0	11413-04	3.00	3.05	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	98.6	97.6	86.1	65.0	53.3	45.1	31.2	19.8
5.50         5.55         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         99.8         93.7         82.6         53.4         40.3           6.00         6.05         100.0         100.0         100.0         100.0         100.0         100.0         99.8         93.0         79.7         68.7         59.3           6.50         6.55         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         99.8         89.6         98.8         89.2         82.6         71.8         58.8         51.5           8.30         100.0	11413-04	4.20	4.25	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	99.2	98.6	90.1	75.7	57.5	47.3	38.3	26.5	19.2
6.00 6.05 100.0 100.0 100.0 100.0 100.0 100.0 100.0 100.0 99.8 93.0 79.7 68.7 59.3 6.5 0.8 1 10.0 100.	11413-04	5.50	5.55	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	98.8	93.7	82.6	53.4	40.3	31.1	19.1	4.11
6.50 6.55 100.0 100.0 100.0 100.0 100.0 100.0 99.8 80.4 46.2 40.7 36.5 28.6 24.5 7.10 7.15 100.0 100.0 100.0 100.0 100.0 99.8 99.6 98.8 89.2 82.6 71.8 58.8 51.5 8.30 8.35 100.0 100.0 100.0 100.0 100.0 100.0 100.0 99.8 99.6 98.8 89.2 82.6 71.8 58.8 51.5 9.00 9.05 100.0 100.0 100.0 100.0 100.0 100.0 99.8 99.6 99.8 87.4 84.2 67.7 60.4 10.30 10.30 10.00 100.0 100.0 100.0 99.8 99.4 94.0 75.8 35.2 20.6 19.1 16.5 15.9 10.75 10.80 100.0 100.0 100.0 100.0 99.8 99.6 94.2 64.8 30.6 22.2 20.0 18.1 15.9 10.75 11.00 100.0 100.0 100.0 100.0 99.8 99.4 94.2 73.8 34.2 22.2 18.4 17.2 15.6	11413-04	0.00	6.05	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	93.0	79.7	68.7	59.3	51.9	36.6	27.6
7.10 7.15 100.0 100.0 100.0 100.0 100.0 99.8 99.6 98.8 89.2 82.6 71.8 58.8 51.5 8.3 51.5 8.3 0.0 100.0 100.0 100.0 100.0 100.0 99.8 99.6 98.2 89.8 71.5 61.9 50.8 41.3 9.00 9.05 100.0 100.0 100.0 100.0 100.0 100.0 99.8 99.6 95.8 87.4 84.2 67.7 60.4 10.30 10.35 100.0 100.0 100.0 100.0 99.8 99.4 94.0 75.8 35.2 20.6 19.1 16.5 15.9 10.75 10.80 100.0 100.0 100.0 100.0 99.8 99.6 94.2 64.8 30.6 22.2 20.0 18.1 15.9 10.95 11.00 100.0 100.0 100.0 100.0 99.8 99.6 94.2 73.8 34.2 22.2 18.4 17.2 15.6	11413-04	6.50	6.55	100.0	100.0	1,00.0	100.0	100.0	100.0	100.0	8.66	80.4	46.2	40.7	36.5	28.6	24.5	22.2	17.5	13.3
8.30 8.35 100.0 100.0 100.0 100.0 100.0 100.0 100.0 99.8 99.8 71.5 61.9 50.8 41.3 9.00 9.05 100.0 100.0 100.0 100.0 100.0 100.0 99.8 99.6 95.8 87.4 84.2 67.7 60.4 10.30 10.30 100.0 100.0 100.0 100.0 99.8 99.4 94.0 75.8 35.2 20.6 19.1 16.5 15.9 10.75 10.80 100.0 100.0 100.0 100.0 99.8 99.6 94.2 64.8 30.6 22.2 20.0 18.1 15.9 10.35 11.00 100.0 100.0 100.0 100.0 99.8 99.4 94.2 73.8 34.2 22.2 18.4 17.2 15.6	11413-04	7.10	7.15	100.0	100.0	100.0	100.0	100.0	100.0	8.66	9.66	8.86	89.2	82.6	71.8	58.8	51.5	45.1	33.4	24.5
9.00 9.05 100.0 100.0 100.0 100.0 100.0 100.0 100.0 99.8 99.8 95.8 87.4 84.2 67.7 60.4 10.30 10.35 100.0 100.0 100.0 100.0 99.8 99.4 94.0 75.8 35.2 20.6 19.1 16.5 15.9 10.75 10.80 100.0 100.0 100.0 100.0 99.8 99.6 94.2 64.8 30.6 22.2 20.0 18.1 15.9 10.95 11.00 100.0 100.0 100.0 100.0 99.8 99.4 94.2 73.8 34.2 22.2 18.4 17.2 15.6	11413-04	8.30	8.35	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	98.2	89.8	71.5	61.9	50.8	41.3	34.9	26.0	19.1
10.30 10.35 100.0 100.0 100.0 100.0 100.0 99.8 99.4 94.0 75.8 35.2 20.6 19.1 16.5 15.9 10.75 10.80 100.0 100.0 100.0 100.0 99.8 99.6 94.2 64.8 30.6 22.2 20.0 18.1 15.9 10.95 11.00 100.0 100.0 100.0 100.0 99.8 99.4 94.2 73.8 34.2 22.2 18.4 17.2 15.6	11413-04	9.00	9.05	100.0	100.0	100.0	100.0	100.0	100.0	100.0	8.66	9.66	92.8	87.4	84.2	67.7	60.4	51.1	39.1	26.0
10.75	11413-04	10.30	10.35	100.0	100.0	100.0	100.0	100.0	99.8	99.4	94.0	75.8	35.2	20.6	19.1	16.5	15.9	15.2	14.3	1.1
.   10.95 11.00   100.0 100.0 100.0 100.0 100.0 99.8 99.4 94.2 73.8 34.2 22.2 18.4 17.2 15.6 1	11413-04	10.75	10.80	100.0	100.0	100.0	100.0	100.0	8.66	96.6	94.2	64.8	30.6	25.2	20.0	18.1	15.9	15.2	13.3	11.1
	11413-04		11.00	100.0	100.0	100.0	100.0	100.0	8.66	99.4	94.2	73.8	34.2	22.2	18.4	17.2	15.6	13.3	11.1	7.9

from         to         20         12.5         9.5         4.75         2         0.85         0.485         0.485           (m)         (m)         mm	Borehole	Depth	oth								Percent Passing	assing								
(1)         (1) <th>Number</th> <th>from</th> <th></th> <th>20</th> <th>12.5</th> <th>9.5</th> <th>4.75</th> <th>2</th> <th>0.85</th> <th>1-</th> <th>0.25</th> <th>0.15</th> <th>0.75</th> <th>0.03</th> <th>0.02</th> <th>0.01</th> <th>0.009</th> <th>0.006</th> <th>0.003</th> <th>0.001</th>	Number	from		20	12.5	9.5	4.75	2	0.85	1-	0.25	0.15	0.75	0.03	0.02	0.01	0.009	0.006	0.003	0.001
1.50   1.70				E	Ē	E	Æ	E	Ę	E	E	£	E	m m	E	E	E	E	Æ	E
10.15 0.30 100.0 100.0 100.0 99.7 99.5 99.3 99.7 75.8 69.3 61.5 65.3 45.8 411 30.0 44.0 100.0 100.0 100.0 100.0 100.0 100.0 99.9 99.2 54.1 84.2 55.1 11.1 9.1 7.8 7.1 6.7 6.0 4.0 4.0 14.0 100.0		(£)	(m)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)	(%)
1,20         1,40         100.0         1	11413-07	0.15	0.30	100.0	100.0	100.0	2.66	93.6	99.3	98.7	93.5	83.4	75.8	69.5	61.6	55.3	45.8	41.1	30.0	19.0
4.5G         4.7G         100.0         1	11413-07	1.20	1.40	100.0	100.0	100.0	100.0	100.0	100.0	6.66	69.4	44.6	20.5	11.1	9.1	7.8	7.1	6.7	5.6	5.1
0.25         0.41         100.0         1	11413-07	4.50	4.70	100.0	100.0	100.0	100.0	100.0	6.66	99.5	54.1	38.4	25.2	14.3	8. 8.	7.9	6.7	6.0	4.0	3.7
1.40         1.60         100.0         1	11413-08	0.25	0.41	100 0	100.0	0001	100	100 0	100	0.001	100 0	1000	9	93	0	Č	7 27	0	•	7
2.70         2.90         100.0         1		, ,				2 2	9 9	2 2		2 2	2 6	2 6	9 6	- (	9 r	4. 6	/ 5.7	02.5	P	V. 'S
0.60         0.29         100.0         1	00-01-7	4. 6	0 0	0.00	00.0	0.00	0.00	100.0	000.0	0.001	95.7	87.8	26.5	5. S	12.7	10.6	တ က	∞ 4.	80	5.7
0.60         0.90         100.0         100.0         100.0         100.0         100.0         100.0         93.4         94.8         94.2         82.6         76.2         62.3         51.8         43.2         29.5           1.40         1.50         100.0	11413-08	2.70	2.90	100.0	100.0	100.0	100.0	100.0	100.0	100.0	96.4	61.8	31.0	4 6,3	12.7	10.2	9.5	න න	6.4	5.1
1.40         1.50         100.0         1	11413-09	09.0	06.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	99.2	9.96	94.2	82.6	76.2	62.3	51.8	43.2	29.5	19.7
0.20         0.40         100.0         1	11413-09	1.40	1.50	100.0	100.0	100.0	100.0	100.0	100.0	100.0	93.4	49.8	24.4	20.6	16.5	გ.	11.8	10.5	8.3	7.0
1.40         1.50         100.0         1	11413-10	0.20	0.40	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	9.66	0.66	94.7	88.9	75.9	66.7	58.8	42.6	28.6
2.70         2.90         100.0         100.0         100.0         100.0         100.0         100.0         99.9         99.8         89.4         31.5         5.7         23.7         23.1         22.2         20.9         19.0           0.80         0.90         100.0	11413-10	1.40	1.50	100.0	100.0	100.0	100.0	100.0	100.0	100.0	7.07	10.3	6.5					•	!	•
0.80         0.90         100.0         1	11413-10	2.70	2.90	100.0	100.0	100.0	6.66	99.8	93.6	99.2	95.8	79.8	40.5	29.2	24.7	23.1	22.2	20.9	19.0	15.8
2.10         2.30         100.0         1	11413-11	0.80	06.0	100.0	100.0	100.0	100.0	100.0	6.66	99.8	89.4	31.5	5.7							
4.00         4.10         100.0         1	11413-11	2.10	2.30	100.0	100.0	100.0	100.0	100.0	100.0	100.0	96.2	54.9	17.7	12.7	8,0	8.1	7.1	6.4	4.9	4. 6.
0.40         0.60         100.0         1	11413-11	4.00	4.10	100.0	100.0	100.0	100.0	100.0	99.7	99.3	77.2	21.3	11.3	8.7	7.1	6.4	5. T.	8.	3.2	2.9
0.90         1.00         100.0         1	11413-12	0.40	09.0	100.0	100.0	100.0	100.0	7.66	99.5	99.1	91.3	56.6	30.5	23.7	21.5	19.6	18.0	14.9	11.4	9.5
4.00         4.10         100.0         1	11413-12	0.90	1.00	100.0	100.0	100.0	100.0	100.0	100.0	8.66	94.8	8.09	32.2	25.4	22.9	20.6	18.7	17.2	13.7	10.8
0.20         0.40         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         100.0         99.6         96.8         86.0         76.9         74.0         64.8         58.1         50.8         35.3           1.40         1.50         100.0         100.0         100.0         100.0         100.0         99.8         93.2         57.4         31.2         25.4         22.2         18.4         16.2         13.7         9.8           2.10         2.30         100.0         100.0         100.0         100.0         100.0         99.8         95.9         76.9         33.3         20.6         13.2         12.4         11.1         9.5           0.15         0.30         100.0         100.0         100.0         100.0         99.5         92.9         76.9         33.3         20.6         15.9         11.1         9.5           1.50         1.70         100.0         100.0         100.0         100.0         99.7         99.4         99.3         98.5         67.1         33.1         12.6         15.4         17.0         4.4           0.80         0.90	11413-12	4.00	4.10	100.0	100.0	100.0	100.0	100.0	100.0	99.8	93.4	56.2	32.6	25.1	22.9	21.3	19,1	16.8	14.6	9.5
1.40         1.50         100.0         1	11413-13	0.20	0.40	100.0	100.0	100.0	100.0	100.0	100.0	100.0	9.66	96.8	86.0	6.92	74.0	84.8	58.1	50.8	35.3	25.4
2.10         2.30         100.0         1	11413-13	1.40	1.50	100.0	100.0	100.0	100.0	99.5	0.66	98.5	85.0	11.9	5.9							
0.15 0.30 100.0 100.0 100.0 100.0 100.0 100.0 96.4 73.8 56.0 52.7 47.6 43.5 38.8 34.6 24.8 0.90 1.10 100.0 100.0 100.0 100.0 100.0 99.5 92.9 76.9 33.3 20.6 15.9 13.2 12.4 11.1 9.5 1.50 1.70 100.0 100.0 100.0 99.7 99.4 99.3 98.5 67.1 33.1 14.6 11.1 8.2 6.5 5.7 5.1 4.4 0.80 0.90 100.0 100.0 99.0 98.2 96.9 95.7 91.9 70.8 45.6 30.9 23.1 20.4 18.4 17.0 14.5 2.70 2.90 100.0 1	11413-13	2.10	2.30	100.0	100.0	100.0	100.0	100.0	100.0	8.66	93.2	57.4	31.2	25.4	22.2	18.4	16.2	13.7	9.8	9. S
0.90         1.10         100.0         1	11413-14	0.15	0.30	100.0	100.0	100.0	100.0	100.0	100.0	100.0	96.4	73.8	56.0	52.7	47.6	43.5	38.8	34.6	24.8	15.9
1.50         1.70         100.0         1	11413-14	06.0	1.10	100.0	100.0	100.0	100.0	100.0	100.0	99.5	92.9	76.9	33.3	20.6	15.9	13.2	12.4	1.1	9.5	7.9
0.80 0.90 100.0 100.0 100.0 99.0 98.2 96.9 95.7 91.9 70.8 45.6 30.9 23.1 20.4 18.4 17.0 14.5 2.70 2.90 100.0 100.0 100.0 100.0 100.0 100.0 99.9 93.3 35.2 11.3	11413-14	1.50	1.70	100.0	100.0	100.0	2.66	99.4	99.3	98.5	67.1	33.1	14.6	1.	8.2	6.5	5.7	5.1	4.4	3.3
2.70 2.90 100.0 100.0 100.0 100.0 100.0 100.0 99.9 93.3 35.2 11.3	11413-15	0.80	06.0	100.0	100.0	100.0	99.0	98.2	6.96	95.7	91.9	70.8	45.6	30.9	23.1	20.4	18.4	17.0	14.5	4.
	11413-15	2.70	2.90	100.0	100.0	100.0	100.0	100.0	100.0	99.9	93.3	35.2	11.3					į		

# APPENDIX D PARTICLE SIZE ANALYSIS





Project: 0101-11413

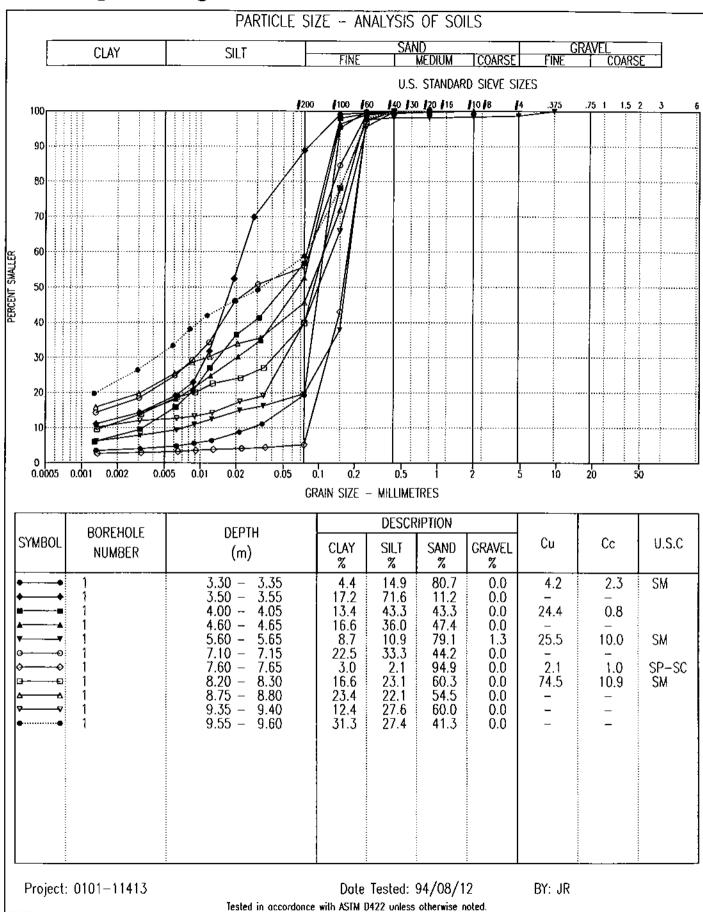
Date Tested: 94/07/29

BY: JR

Tested in accordance with ASTM D422 unless otherwise noted.

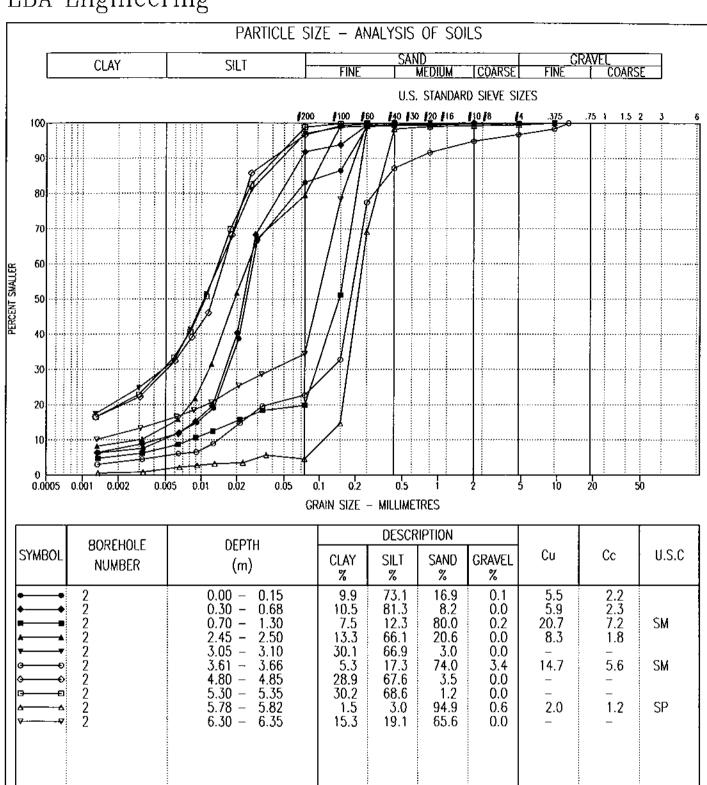
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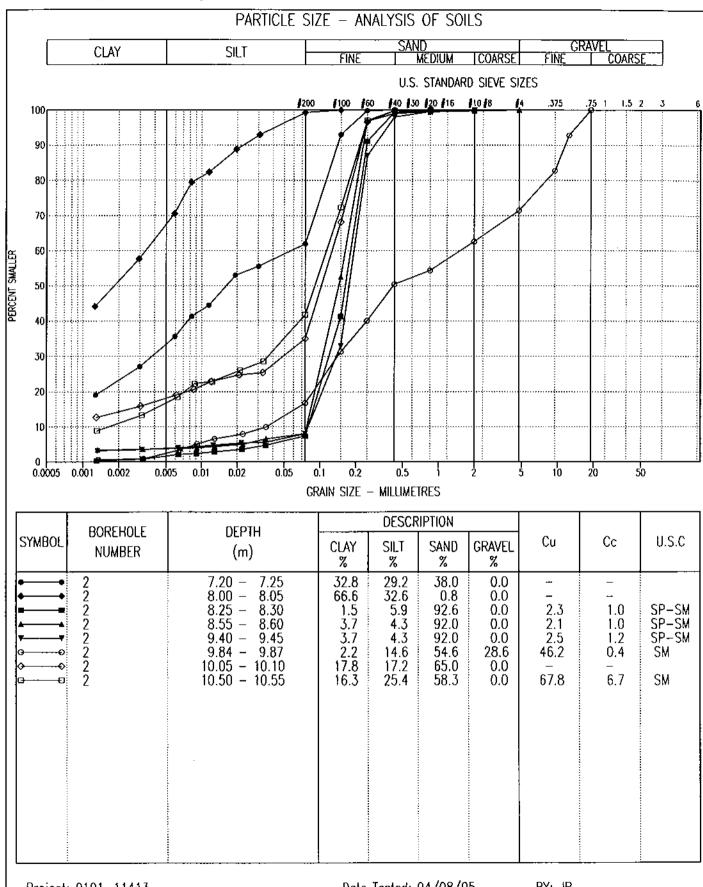
Project: 0101-11413

Date Tested: 94/05/05

BY: IS

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Project: 0101-11413

Date Tested: 94/08/05

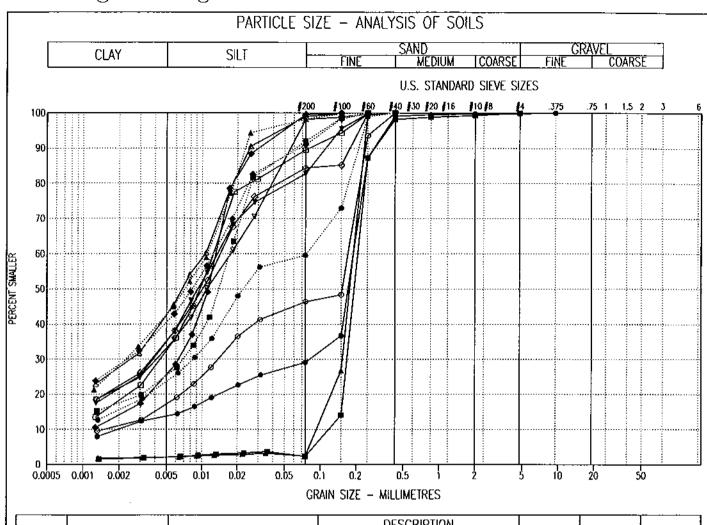
BY: JR

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	BOREHOLE NUMBER	DEPTH (m)	DESCRIPTION						
SYMBOL			CLAY %	SILT %	SAND %	GRAVEL %	Cu	Сс	U.S.C
	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	0.00 - 0.15 1.00 - 1.05 1.55 - 1.58 2.02 - 2.07 2.70 - 2.75 3.22 - 3.27 3.80 - 3.85 4.84 - 4.88 6.05 - 6.10 7.15 - 7.20 8.50 - 8.60 9.65 - 9.70 10.65 - 10.70 11.95 - 12.00	13.6 24.8 1.9 1.9 34.2 16.7 34.4 31.5 41.8 32.5 23.1 39.9 24.7 42.1	15.5 74.7 0.3 0.5 48.6 29.6 50.0 57.9 57.2 65.6 36.4 51.1 67.3 56.1	70.7 0.5 97.8 97.6 17.2 53.7 15.6 10.6 1.0 40.5 9.0 8.0	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	91.4 	16.7 	SM SP SM

Project: 0101-11413

Date Tested: 94/05/05

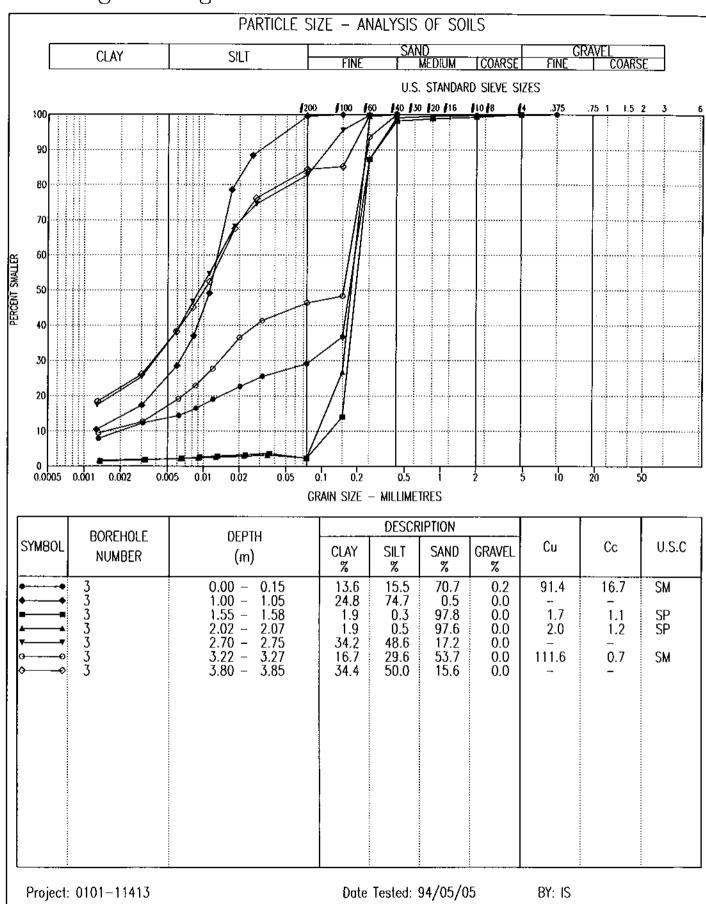
BY: IS

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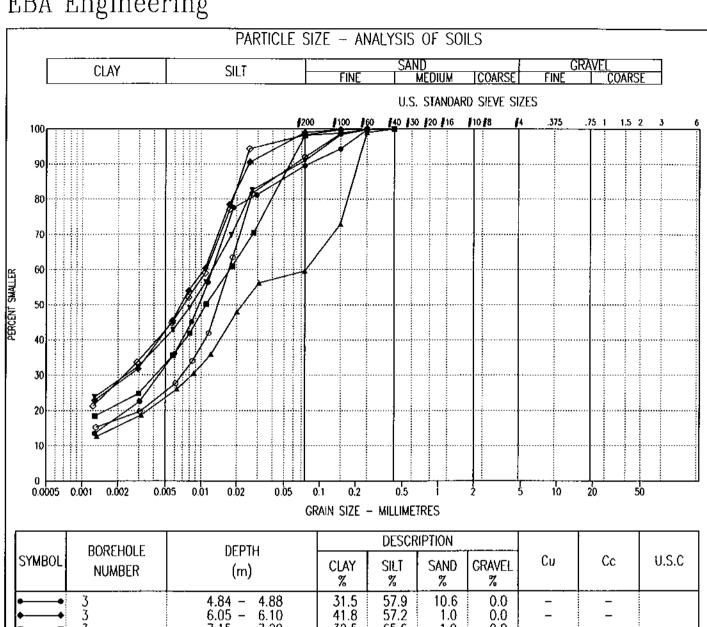
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	BOREHOLE NUMBER	DEPTH (m)	DESCRIPTION						
SYMBOL			CLAY %	SILT %	SAND %	GRAVEL %	Cu	Сс	U.S.C
	3 3 3 3 3 3 3	4.84 - 4.88 6.05 - 6.10 7.15 - 7.20 8.50 - 8.60 9.65 - 9.70 10.65 - 10.70 11.95 - 12.00	31.5 41.8 32.5 23.1 39.9 24.7 42.1	57.9 57.2 65.6 36.4 51.1 67.3 56.1	10.6 1.9 40.5 9.0 8.0 1.8	0.0 0.0 0.0 0.0 0.0	-	- - - - -	

Project: 0101-11413

Date Tested: 94/04/25

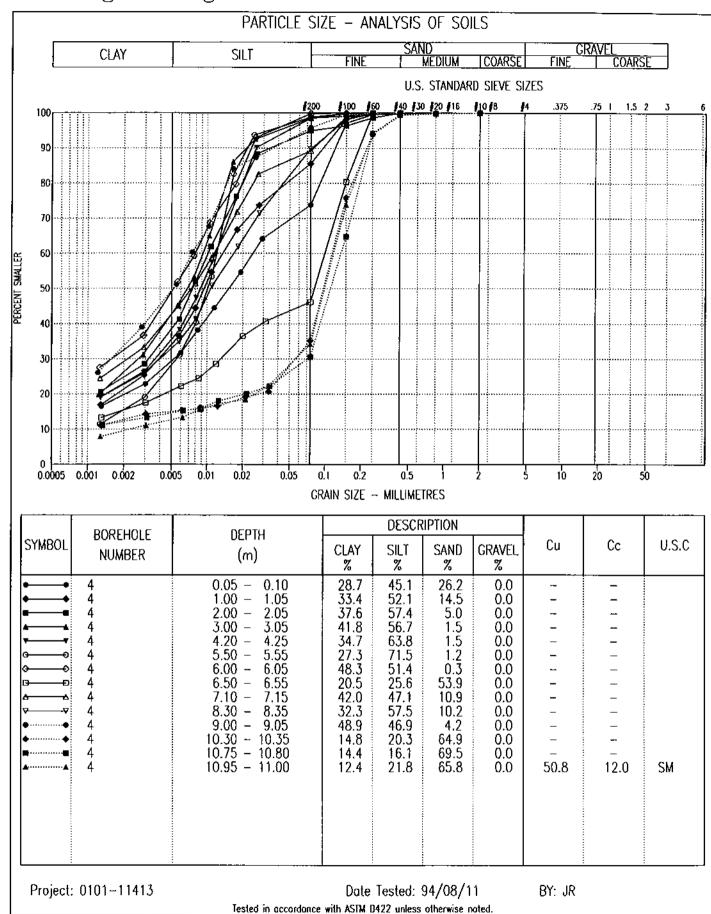
BY: MH

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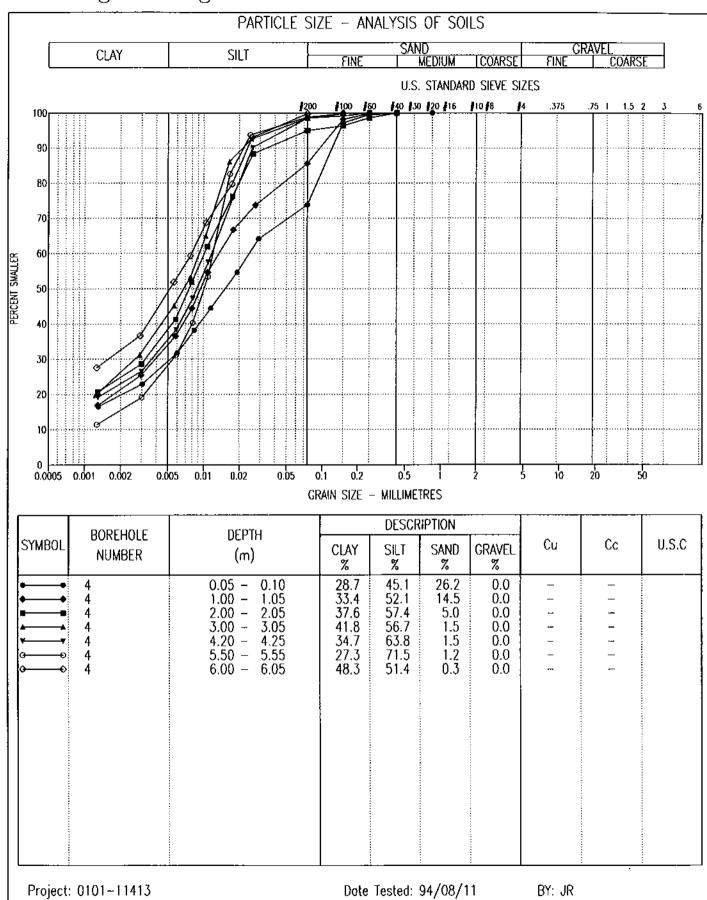
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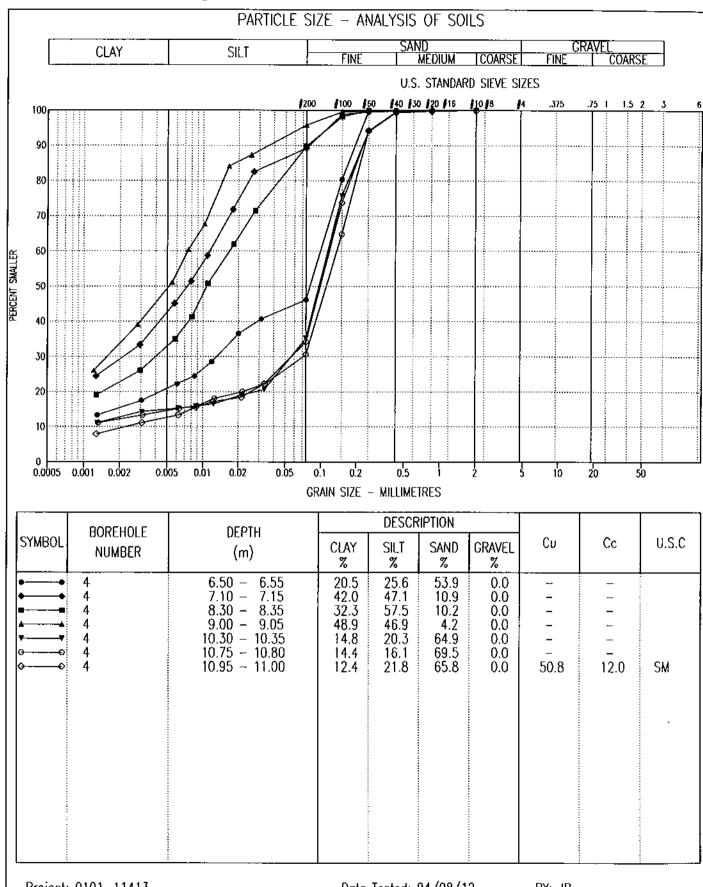
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Project: 0101-11413

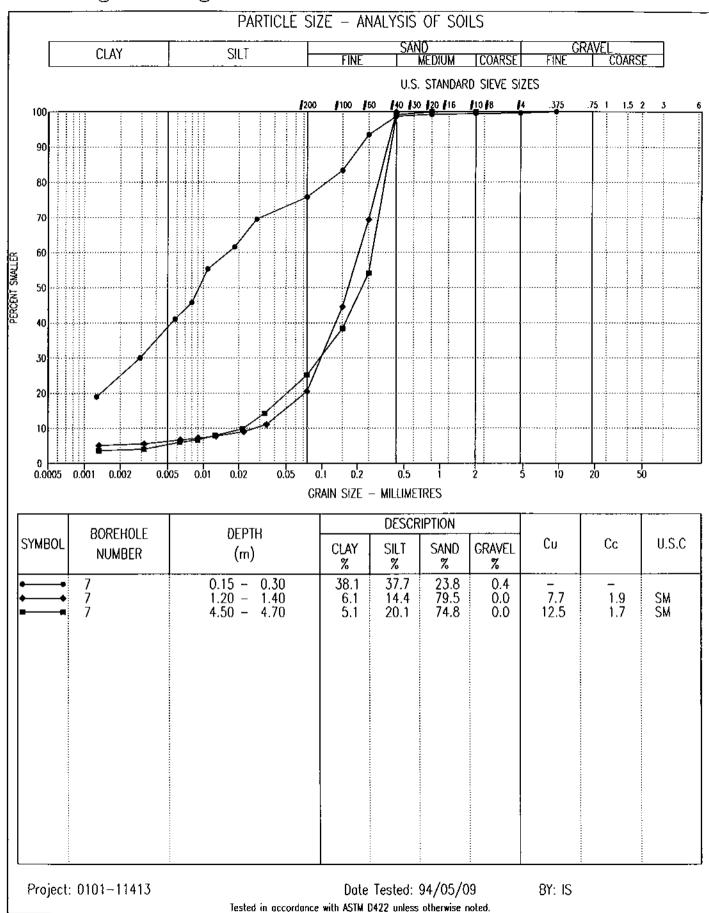
Date Tested: 94/08/12

BY: JR

Tested in accordance with ASTM D422 unless otherwise noted.

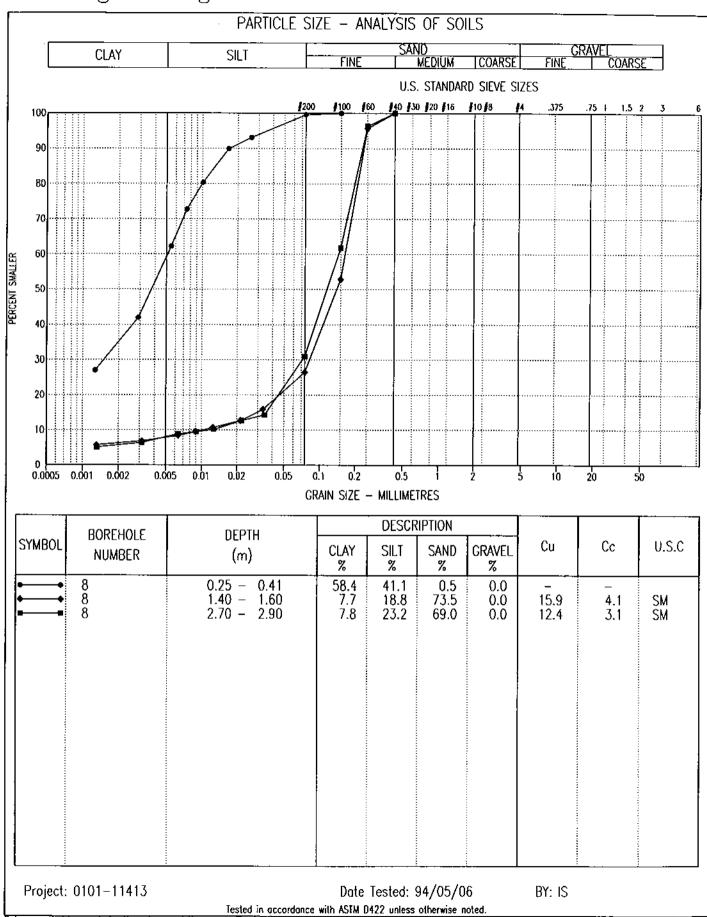
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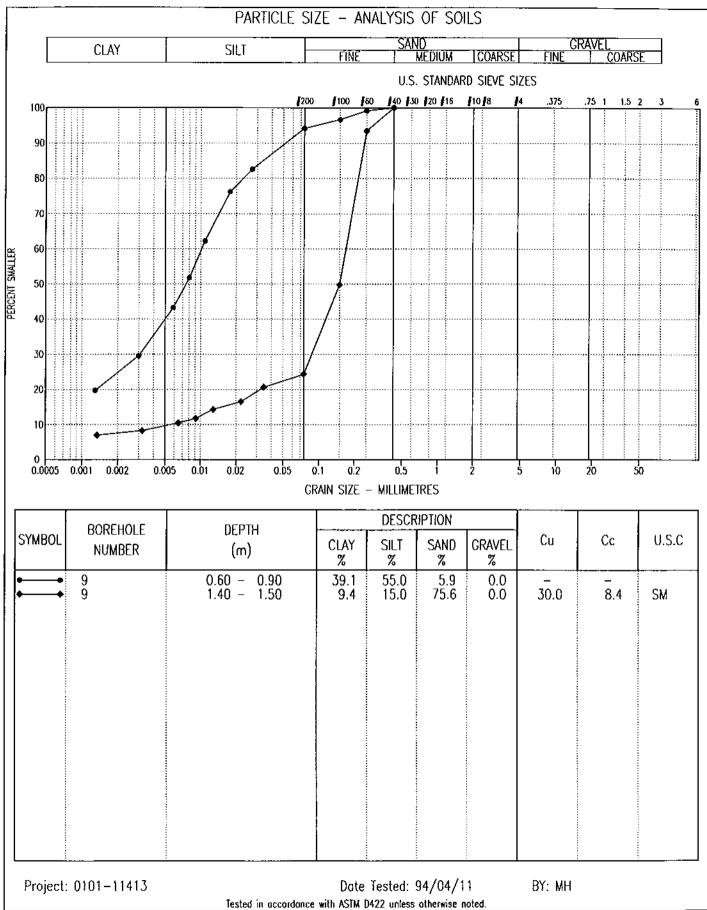
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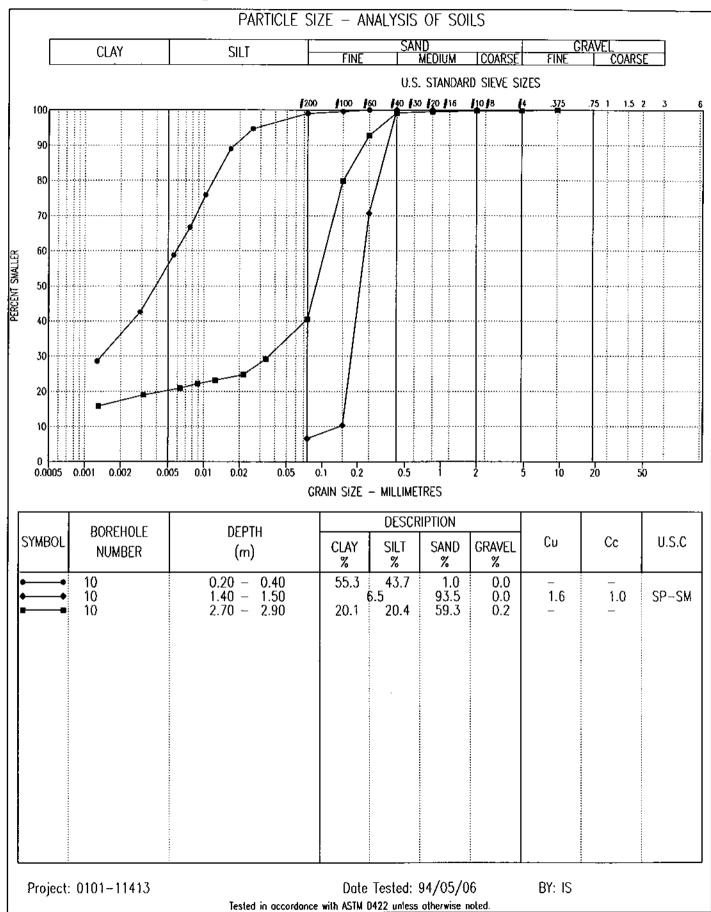
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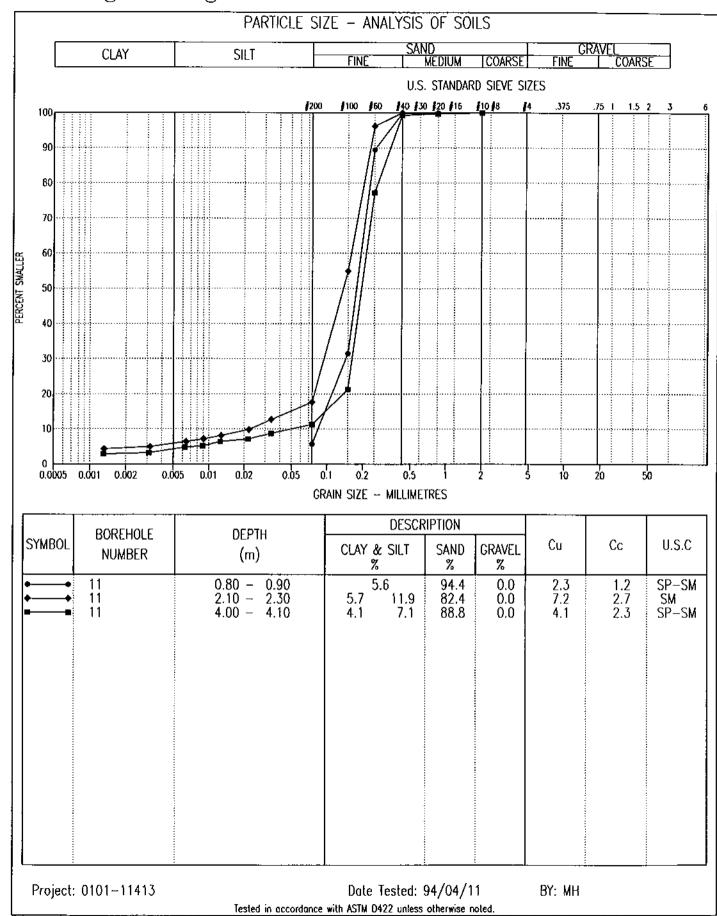
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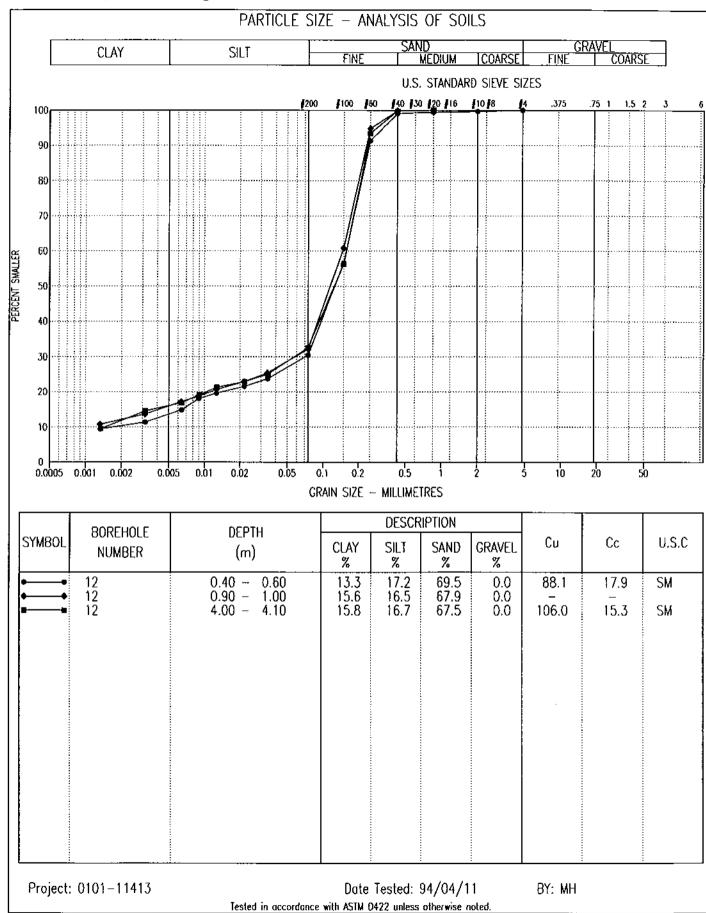
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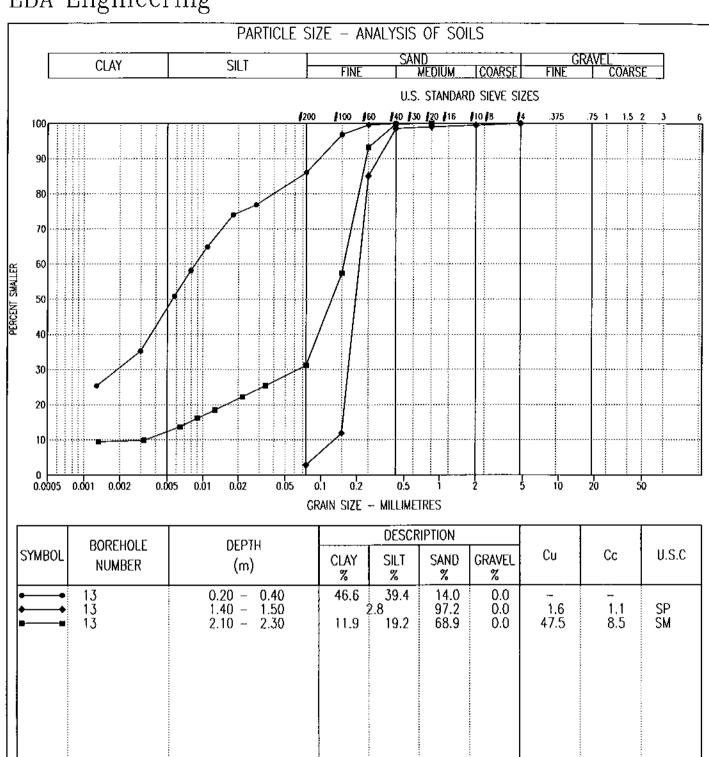
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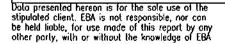


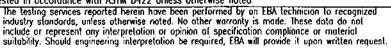
Project: 0101-11413

Date Tested: 94/05/06

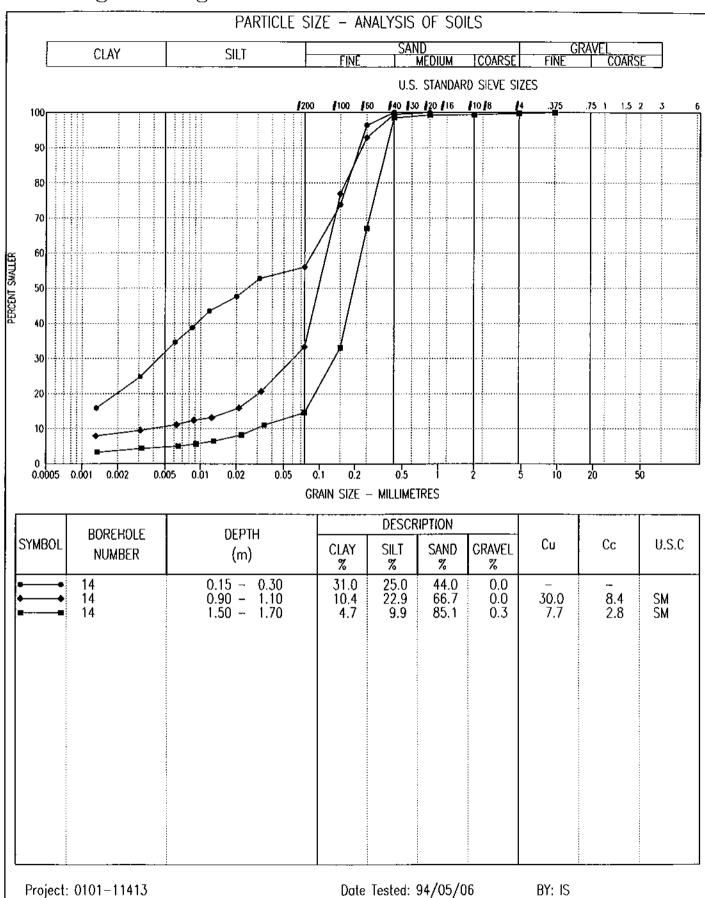
BY: IS

Tested in accordance with ASTM D422 unless otherwise noted



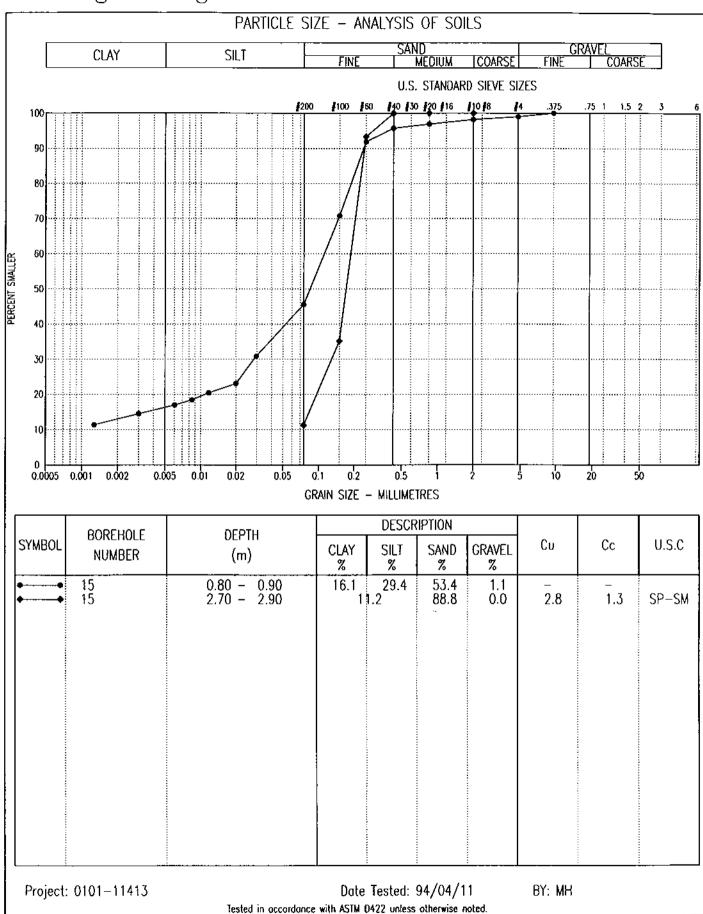






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